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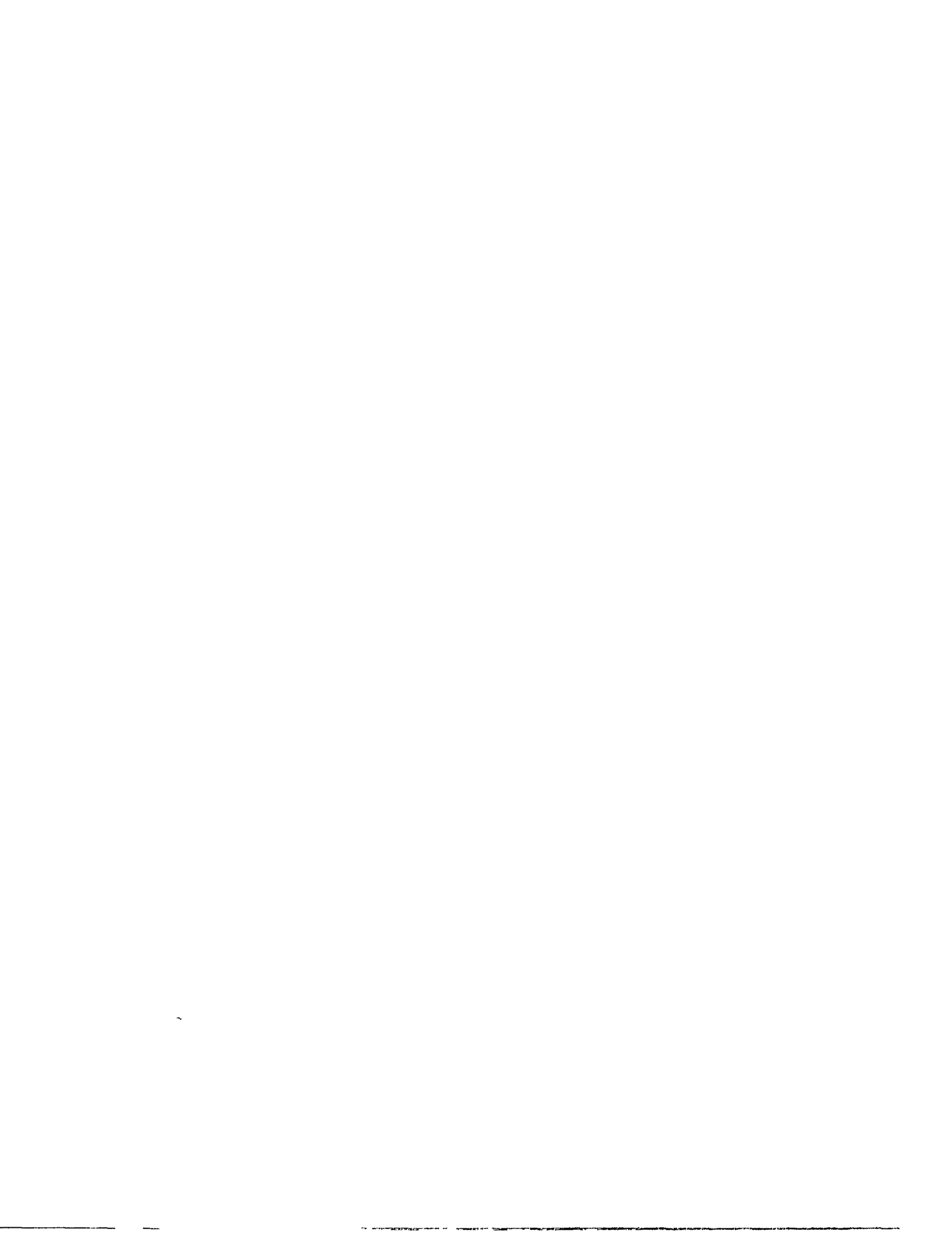
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**Kinetic study on pyrolysis of C_6H_5Cl and $m-C_6H_4Cl_2$ diluted
in H_2 ; detailed reaction kinetics and thermodynamic property
estimation techniques**

Ritter, Edward Robert, D.Eng.Sc.

New Jersey Institute of Technology, 1989

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**KINETIC STUDY on PYROLYSIS of C_6H_5Cl
and $m-C_6H_4Cl_2$ DILUTED IN H_2 ;
DETAILED REACTION KINETICS and
THERMODYNAMIC PROPERTY ESTIMATION TECHNIQUES**

by

Edward R. Ritter

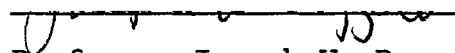
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School of the New Jersey Institute of Technology in partial
fulfilment of the requirements for the degree of
Doctor of Engineering Science
1989

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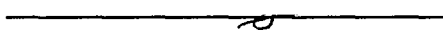
Title of Thesis: Kinetic Study on Pyrolysis of C₆H₅Cl and m-C₆H₄Cl₂ diluted in H₂; Development of Thermodynamic Property Estimation Techniques for use with Detailed Reaction Kinetic Mechanisms

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ABSTRACT

Title of Thesis: Kinetic Study on Pyrolysis of C_6H_5Cl and $m-C_6H_4Cl_2$ Diluted in H_2 ; Detailed Reaction Kinetics and Thermodynamic Property Estimation Techniques

Edward R. Ritter, Doctor of Engineering Science, 1989.

Thesis Directed by: Professor Joseph W. Bozzelli

Thermal reaction studies of dilute mixtures (0.37%) of C_6H_5Cl in hydrogen and $m-C_6H_4Cl_2$ (0.4%) in hydrogen have been performed in tubular flow reactors at various surface to volume ratios, and 1 atm total pressure. Residence times range from 0.02 to 2.5 seconds, with temperatures between 1050 to 1275 K. HCl , C_6H_5Cl , C_6H_6 , and carbon solids ($C(s)$) are observed as the major products; minor products include methane, cyclopentadiene, toluene, naphthalene and biphenyls. Pyrolysis in helium yields significantly less conversion, but more $C(s)$ for similar residence times.

A detailed chemical mechanism is developed to describe this reaction system. Our modeling calculations incorporate Energized Complex QRRK analysis for accurate inclusion of temperature and pressure effects in radical addition reactions. This is a straightforward method to estimate rate constants and branching ratios as a function of both T and P . The detailed mechanism, based upon fundamental thermodynamic and kinetic principles, describes the overall reaction remarkably well. We also propose a plausible

kinetic scheme describing formation of minor products.

The observed reagent loss can be explained in terms of energized adduct formation, followed by unimolecular dissociation to low energy exit channels. Phenyl, chlorophenyl, and Cl radicals produced by the initial unimolecular decay of C_6H_5Cl or $m-C_6H_4Cl_2$ react with H_2 to form C_6H_6 , C_6H_5Cl , and $HCl + H$ respectively. Hydrogen atom addition to C_6H_5Cl and $m-C_6H_4Cl_2$ via ipso attack, with subsequent loss of Cl from the energized complex, is required to explain the faster reaction in H_2 than He.

QRRK Rate constant analysis is presented for the addition of H atom, phenyl and chlorophenyl radicals to C_6H_5Cl and $m-C_6H_4Cl_2$, temperature and pressure ranges of 300 to 1900 K and 10^{-3} to 1.0 atm, respectively. Calculations were performed for both nitrogen and hydrogen dilution gases. Computer simulations show that initial chlorophenyl and phenyl addition reactions cannot, by themselves, explain the rapid formation of solid carbon in these systems.

Computer simulation and QRRK analyses on these reaction systems require accurate thermodynamic property data for all radicals and stable molecules considered. A computer code called THERM was developed to estimate these properties using the group additivity method of Benson. Accurate heat capacity estimates for radicals and molecules are obtained only to 1000 K using Benson's method. Two methods for the accurate extrapolation of this low tempera-

ture heat capacity data ($T < 1000$ K) to higher temperatures were developed in the present study.

The first method uses an exponential function to interpolate and extrapolate heat capacity data, with a typical maximum error of 4%. The second fitting method is based upon the harmonic oscillator model for heat capacity of an ideal gas described by statistical mechanics. A 5 parameter harmonic oscillator equation (HOE) was developed and used to estimate heat capacity data from 300 - 5000 K, with maximum error less than 0.1% for simple polyatomic molecules having no hindered internal rotations. Less than 4% maximum error is obtained for molecules which have hindered internal rotations. The harmonic oscillator equation parameters were determined by a least square regression of heat capacity data using the method of Marquardt. These parameters were used to calculate various molecular properties such as geometric and arithmetic mean frequencies, vibrational partition functions, or the sum and density of vibrational quantum states. Estimates are found to compare favorably to those calculated from actual vibrational frequency data.

A polynomial fitting method was developed to create thermodynamic property functions in the NASA polynomial format which is required by the CHEMKIN reaction simulation computer code. Two polynomials were generated (one for low temperature and one for high temperature) and a point of tangency was determined using the Newton-Raphson method.

This polynomial fitting method differs from those developed at NASA and Sandia National Laboratory, where the point of tangency is fixed at 1000 K.

The heat capacity fitting/extrapolation method, polynomial fitting, and property change for chemical reaction procedures were coupled with the group additivity method of Benson to form the THERM computer package. This code may be used to estimate the required ideal gas thermodynamic properties for radicals and molecules considered in a detailed reaction mechanism used to model kinetic data.

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SECTION I

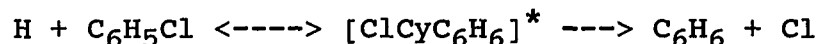
KINETIC STUDY ON THERMAL DECOMPOSITION

OF C_6H_5Cl DILUTED IN H_2

Introduction

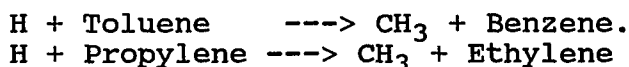
The chemistry and high temperature reactions of chlorinated organic species are currently receiving significant attention due to the consistent observation of known or suspected toxic / carcinogenic chlorocarbons or chloro-oxy carbon species in effluent from waste and resource recovery incinerators^{1,2}

Chuang and Bozzelli³ indicate that thermal reactions of chlorinated hydrocarbons in a hydrogen atmosphere may lead to complete conversion of alkyl chlorocarbon species to HCl and the hydrocarbon products acetylene and ethylene. Louw et.al.⁴ in separate studies have further indicated that thermal reactions of chlorinated biphenyls with hydrogen may lead to detoxification of these species, producing non-chlorinated aromatics and HCl. Louw and his coworkers⁵⁻⁸ have performed thermal studies on a number of chloro-aromatic reactions in the presence of hydrogen, postulating mechanistic pathways and some rate constants. One plausible low activation energy reaction path is the addition of a radical species, e.g. H atoms, to the aromatic ring (adduct formation) with subsequent rapid reaction of the adduct to new products, which serve to propagate a chain reaction e.g.



These reaction paths may be considered displacements, but do not occur on a single bond system where the outer

shell of the central atom is expanded. Instead they follow a scheme suggested in by Benson and Shaw⁹ in a review of hydrogen atom reactions with propylene, benzene, toluene and xylene where the data showed rapid reactions that could be explained within a factor of ten by one rate constant. This rate constant, furthermore, remains nearly constant over order of magnitude variations in pressure and temperature. Benson and Shaw explained this observation in part by indicating that reactions such as:



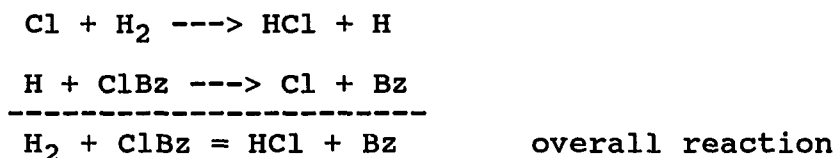
were rapid and pointed out that the reactions could not be explained by abstraction reactions due to the high rate constants observed at lower temperatures. They further indicated, however, that stabilization should occur for any adducts that might be formed. An alternate explanation, which we advocate, when a low energy exit channel such as displacement of methyl by H on an unsaturated hydrocarbon is present, is that unimolecular dissociation of the energized adduct is rapid and often occurs prior to any stabilization. The H atoms in the reviewed data⁹ were initially generated from unimolecular decomposition of the resonantly stabilized parent and the subsequent displacement reaction is exothermic. The ipso attack of H on the toluene carbon bonding the methyl group forms a C - H bond, which is stronger than this $\text{C}_b - \text{CH}_3$ bond and allows facile cleavage of the C - C single bond. Louw⁵ extended

this reaction concept to the carbon chlorine bond system.

W. Tsang¹⁰ has recently reported a rate constant on the displacement reaction of H with chlorobenzene from shock tube studies between 1000 and 1100 K of $2.2 \times 10^{13} \exp(-9000 \text{ cal/mole/RT})$. He further indicates that displacement is the only significant pathway at temperatures included in his study.

Frenklach et. al¹¹ monitored soot formation from chlorobenzene reactions in shock tubes and showed that soot was produced at lower temperatures than occurred with benzene in pyrolysis type reactions strongly suggesting that the Cl on benzene accelerated the reaction to soot. Rao and Skinner¹², on the other hand, studied reactions of chlorobenzene and benzene at low concentrations in shock tubes (1600 to 1900 K) by following atomic hydrogen concentration profiles and observed little difference in overall reaction for the two aromatic species. They concluded that little difference existed in the reaction rates of the two species.

One added complexity in reaction studies of Cl-aromatics and a possible reason for chlorobenzene's acceleration of carbon (soot) formation is the role of Cl, a product in our reaction system. Here the rapid chain carrying or catalytic transfer process can take place:



where abstraction by Cl has lower energies of activation than abstraction by carbon containing radicals.

Earlier studies by Cullis and Manton¹³ on pyrolysis of chlorobenzene between 1043 and 1123 K indicated that aromatic ring rupture did not occur significantly in experiments below 1073 K where principal products were chlorobiphenyls, H₂ and HCl. Loss of aromatic ring structure and production of vinyl chloride was, however, reported as the the major pathway between 1103 and 1123 K while major products of chlorobiphenyls and HCl were again observed above 1123 K. Low concentrations of methane were also observed along with solid carbon or soot formation. Cullis and Manton also added hydrogen to the reaction system and observed significant acceleration of the reaction.

We have elected to study and model the reactions of dilute mixtures of chlorobenzene in hydrogen and helium, at temperatures up to 1275 K in an attempt to understand and characterize the detailed reaction chemistry in these more straightforward 3 element (hydrogen / carbon / chlorine) systems.

Our modeling calculations incorporate the Energized Complex Quantum RRK analysis of Dean¹⁴ for accurate inclusion of temperature and pressure effects on radical addition reactions at our temperatures. Dean demonstrated the

importance of chemical activation in high temperature pyrolysis and oxidation systems and further studies^{15,16} have shown that this approach provides a reliable and straightforward method to estimate rate constants and branching ratios as a function of both T and P.

Experimental

Reaction of chlorobenzene with hydrogen was carried out using the apparatus described in Fig. 1.1. Reactions were studied at 1 atmosphere total pressure with temperatures ranging from 1073-1283 K. Separate experiments were performed using quartz tubular reactors of 4mm, 10.5mm, and 16mm id, residence times 0.02 to 2.5 sec., and with flow conditions determined as in Ref. 17. Varying reactor surface to volume ratio (S/V) allows one to decouple apparent wall and bulk phase decomposition rates using a method based upon the work of Kaufman¹⁸.

Chlorobenzene was reagent grade supplied by Aldrich Co. Hydrogen and helium gases were commercial grade supplied by Airdyne Inc., and were filtered of O₂, H₂O, and hydrocarbon impurities before entering the reactor system.

Reactor tubes were housed within a three zone electric tube furnace. Temperature profiles were obtained using a type K thermocouple probe moved axially within the 0.5 meter length reactor. Thermocouple error caused by furnace wall radiation was minimized by providing a shield for sensor junctions; measurements were made with He (1-2

liter/min) flowing through the reactor. Tight temperature control resulted in temperature profiles isothermal to within ± 5 K over 85-90% of the furnace length throughout the temperature range studied. Steep temperature gradients of 500 K in 5 cm occurred at the inlet and outlet of the reactor (see Fig. 1.2). Uncertainty in absolute temperature measurements is estimated to be $\pm 1\%$ ($\pm 8-12$ K) but relative temperatures are believed to be known to within ± 5 K. Hydrogen (or helium) was bubbled through 273 K liquid chlorobenzene at rates ranging from 50-4000 ml/min (stp). Sufficient contact time was allowed to insure saturation of the gas (initial C_6H_5Cl mole fraction of 0.0037). The flow of the saturated vapor/gas mixture was manipulated to control the residence time within the reactor by adjusting H_2/He flow.

Reactants and stable products were quantified using on-line gas chromatography: Varian 3700, 25m x 0.32mm i.d. fused silica capillary column, methyl silicone stationary phase, automated cryofocussing (concentrator), flame ionization detection, and integration by an SP 4270 integrator / plotter. Initial C_6H_5Cl peak area was obtained using a reactor bypass (473 K) and was verified for each flow rate. All transfer lines were heated to 473 K to prevent condensation and suppress adsorption.

Quantitative analysis of HCl was performed for 1 sec residence time. Reactor effluent was diverted through a bubbler train containing 0.01M $NaOH$ before being exhausted

to a fume hood. The HCl produced was then calculated based upon titration of bubbler solution with 0.01M HCl to its phenolphthalein end point.

Products were identified by GC/Mass Spectrometry (Kratos MS25, 50m x 0.22mm i.d. methyl silicon stationary phase column) on batch samples of reactor gas drawn from the reactor exit into evacuated 25ml stainless steel sample cylinders for later analysis.

EXPERIMENTAL RESULTS: C₆H₅Cl

The reaction of chlorobenzene with hydrogen in excess was observed to follow pseudo-first order kinetics throughout the temperature range studied (1025 - 1283 K). Figure 1.3 illustrates the first order behavior obtained for several temperatures studied in a 10.5mm reactor. Major products were benzene, HCl, and solid carbon.

Decomposition was most rapid within the 4mm i.d. and slowest within the 16mm id reactor. This trend is expected since observed chlorobenzene loss may be the result of two parallel reaction paths, both contributing under our conditions. Clearly the relative importance of the wall reaction is greater when the surface to volume (S/V) ratio or relative extent of the wall surface is greater. The importance of wall reactions was found to drop as S/V was reduced, with 16mm and 10.5mm reactors giving approximately the same results, but 4mm reactors consistently showed higher conversion. Figure 1.4 demonstrates the effect of

reactor diameter upon observed first order rate constants for chlorobenzene loss at several temperatures. Data plotted here have been smoothed by fitting first order rate data to an Arrhenius expression. Wall effects are characterized by the slope of these lines with the intercept estimating the bulk reaction rate. It is apparent that wall effects become very important at temperatures above about 1200 K for 4mm id reactors. These results are in agreement with the trends observed in previous studies at this laboratory.^{3,17}

Decoupling wall and bulk reaction rate constants can be achieved by using a linear relationship which assumes ideal plug flow behavior and is based upon the work of Kaufman,¹⁸ where observed experimental rate constants increase linearly as S/V is increased. Results of decoupling with the plug flow model are global rate constants for reaction in the homogeneous phase (k_b) and the heterogeneous wall reaction (k_w). The Arrhenius expressions for k_b and k_w are as follows:

$$\ln(k_b \text{ \{1/sec\}}) = 23.15 \pm 0.96 - 54 \pm 2.26 \{ \text{Kcal/mol} \} / RT(K)$$

$$\ln(k_w \text{ \{cm/sec\}}) = 25.7 \pm 0.78 - 62 \pm 1.9 \{ \text{Kcal/mol} \} / RT(K)$$

with error bars determined from the scatter in the plot of k_{exp} vs. S/V (2/R).

Figure 1.5 presents the normalized concentration of major products (HCl not included) as a function of residence time, 1.6cm i.d. reactor at 1123 K. The benzene yield rises consistently with time. It reaches an apparent

steady state value near 65% of the initial C_6H_5Cl after approximately 0.4 seconds. At this point, the C_6H_5Cl concentration has fallen to 10% its initial value. The toluene concentration (not shown) rises from zero to an apparent steady state value of 0.5% the initial C_6H_5Cl concentration.

Nearly 30% the C_6H_5Cl initially present is lost to solid carbon (soot) formation. Solid carbon was estimated by difference after taking into account the relative response factors for the stable products which were measured by the GC (FID), and was obvious upon examination of the reactor tube and gas sampling filter. The propensity of chlorobenzene to form soot is well documented¹¹. The C-Cl bond dissociation energy (97 kcal/mol, 298 K) is lower than that of C-H (113.5 kcal/mol), leading to more rapid phenyl radical formation from C_6H_5Cl than C_6H_6 . In our system, C(s) was found in two distinct forms. Graphitic-like deposits covered reactor walls in the high temperature region; and particulate carbon (entrained by gas flow) deposited in post reactor zones and sampling line filters. No carbon deposits were observed at the boundary of the flow tube high temperature (reaction) and low temperature (quenching) zones. This suggests that either particulate growth is occurring during quenching (radical loss and particle agglomeration) or particle settling occurs due to reduced flow velocities outside the reactor.

Minor products ($\leq 0.5\%$) observed in samples of the

reactor gas include cyclopentadiene, toluene, dichlorobenzene, ethylene, methane, naphthalene, 1,1-biphenyl, and chlorobiphenyl. Observations of products are in good agreement with previous studies.⁵⁻⁸

The distribution of major products formed at 1 second average residence time are presented as functions of temperature in Figure 1.6 for the 16mm reactor. Benzene yield increases to approximately 65% the C_6H_5Cl initially present at 1223 K. Nearly 35% of C_6H_5Cl is converted to carbon. HCl yield per mole C_6H_5Cl initially present is also shown. HCl yield rises steadily as temperature is increased. The maximum yield is about 82% and occurs at 1103 K. We do not feel that this incomplete Cl mass balance is a result of systematic error in the HCl measurement. The titration and its calibration are accurate to better than 1.0%. The reactor effluent was bubbled through a two stage sampling train with standard NaOH solution in each stage, until an end point was reached in the 1st stage. The two solutions were then combined and back titrated with standard HCl to phenolphthalein endpoint. Complete mass balance for Cl is obtained, in addition, for almost all other lower temperature pyrolysis and oxidation studies on chlorohydrocarbons completed and ongoing in this lab.

Mass spectral analyses of solids (soot) from the reactor exit show trace levels of high molecular weight chlorinated compounds (chloro and dichlorobiphenyl) are present. It is felt that these accumulated in the carbon

black by adsorption after a period of time. In addition, other compounds in the MW range 228-380 were present. These are believed to be several PAH and chlorinated PAH (such as triphenylene and chlorotriphenylene) which result from phenyl polymerization reactions and are not more highly chlorinated PCB's.

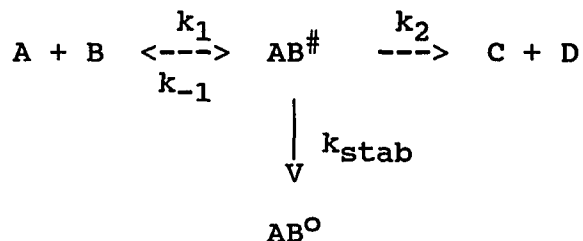
A limited number of experiments were performed to examine C_6H_5Cl decomposition in a helium atmosphere under conditions similar to the hydrodechlorination studies. A comparison of these results is made in Figure 1.7, although we did not collect sufficient data to perform a rigorous kinetic analysis on pyrolysis in He. As shown in Fig. 1.7, the presence of molecular hydrogen was found to greatly accelerate C_6H_5Cl decomposition. This was accompanied by accelerated formation of benzene and, in contrast, polyphe-nyl and soot formation was significantly reduced, although polymerization is not eliminated. If present, hydrogen plays a key role in C_6H_5Cl decomposition.

KINETIC MODELLING RESULTS AND DISCUSSION

Energized Complex/QRRK Theory as presented by Dean¹⁴ was used for modeling of reactions where a chemically activated adduct is formed. Calculations are based upon a geometric mean frequency $\langle v \rangle$. The algorithm presented by Dean was modified, however. Gamma function evaluations have replaced factorials for evaluation of the energy dependent terms. Barriers ($E_a/h\nu$) are not rounded to the nearest integer before summations with respect to energy, so these summations are not forced to stop at integer values of energy ($E_i/h\nu$). This is believed to give better estimates, especially at low temperatures where small changes in barrier height can have a large effect.

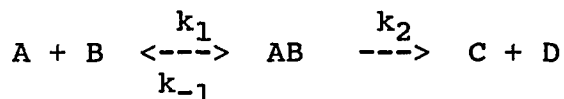
The mechanistic considerations in this paper make use of chemical activation principles for reactions involving atom or radical addition to an unsaturated bond and for atom + radical or radical + radical combination reactions. Consider the addition of two species, A and B to form a chemically activated complex AB^\ddagger , which has energy equal to the sum of the thermal energies of A and B plus the bond energy from adduct formation. This chemically activated adduct AB^\ddagger can now undergo the following reactions:

- i Reaction to new products.
- ii Stabilizing collisions to form AB⁰.
- iii Back reaction to initial reagents A + B.



The Quantum RRK chemical activation treatment provides apparent reaction rate constants k_{rxn} to products C + D and k_{stab} to AB⁰. The unimolecular reaction of AB⁰ to C + D is incorporated into the mechanism separately with consideration for falloff¹⁴. (The channel AB⁰ ---> A + B is included as the reverse of k_{stab}).

This approach can be compared to a more conventional thermal equilibrium analysis of the above system, which would consider the reaction as:



For conditions of steady state:

$$(AB)_{ss} = k_1 [A][B]/(k_{-1} + k_2)$$

$$\frac{d([C]+[D])}{dt} = \frac{k_2 k_1 [A][B]}{(k_{-1} + k_2)} = k_2 K_{eq} [A][B]$$

in the limit that $k_{-1} \gg k_2$ and where K_{eq} is the equilibrium constant.

$$K_{eq} = [AB]/([A][B])$$

We will show that there can be substantial differences in the computed rate of formation of C + D, depending upon whether one uses a thermal or chemical activation approach. The two approaches only become equivalent at the high pressure limit, where all of the AB[#] is stabilized prior to reaction. An important finding is that the pressure required for this complete stabilization varies dramatically with temperature¹⁴. As a result, we find that chemical activation is important in this chlorobenzene / hydrogen system at temperatures 1100 to 1300 K and pressures of 1 atmosphere. Furthermore, the chemical activation approach becomes significantly more important as the temperature is increased.

We feel that the concept of energized complex formation and consideration of its stabilization, forward and reverse reaction channels is a more accurate way to both view and treat the reaction process. We include microreversibility for all reactions in our mechanism so equilibrium can be established for any reaction should the necessary and sufficient conditions exist.

The initial reaction occurring is chlorobenzene dissociation to phenyl radical + Cl. These initial products will both react rapidly with H₂ (if present) to generate benzene and HCl in addition to reactive H atoms. Hydrogen atom addition to the Cl-Carbon in chlorobenzene (ipso position) forms an energized complex and results in rapid dissociation of the adduct to benzene plus Cl, the low energy exit

channel (see Figure 1.8). This addition reaction is believed to be a major pathway for the hydrodechlorination of chlorobenzene to form benzene and HCl under our conditions (H₂ in excess). Virtually every energized complex formed by this addition decomposes to C₆H₆ + Cl, because the exit barrier is so small. This is an example where the rate constant has virtually no pressure dependence even though the process is not an elementary reaction. Parameters used in these calculations appear in Table I.i. The apparent rate constant for reaction to benzene + Cl is therefore, just the rate constant for formation of the adduct, or $1.5 \times 10^{13} \exp(-7,500 \text{ Kcal/mole/RT})$.

Atomic H will add to benzene to form cyclohexadienyl radicals (CHD.)* as shown in Figures 1.9 and 1.10. Also shown are some of the subsequent reactions of this radical. The CHD. complex is initially "hot" since, in addition to the thermal energy, it contains energy resulting from formation of the new chemical bond. Prior to stabilization it may unimolecularly isomerize through a bicyclo intermediate to a cyclopentadiene methyl radical (CpdMe.), which can abstract from H₂, undergo a hydrogen shift to a resonantly stabilized methyl cyclopentadienyl radical (MeCpd.) or beta scission to either fulvene + H or back to CHD radical. The energetics for these isomerizations are significantly less than ring opening reaction to linear C₆H₇ as shown in Fig. 1.9. Calculations for ring opening to linear C₆H₇ show that the energy requirement limits this

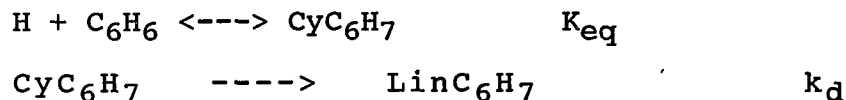
path to less than 0.01% of collisions which form cyclohexadienyl radical complex at our conditions. This channel has been omitted from our reaction mechanism since it was not observed to play a significant role. However at temperatures near 2000 K, this channel may become more significant.

Methane probably arises from further reactions of methyl cyclopentadiene and MeCpd[•] radical. Both unimolecular dissociation of MeCpd and H addition to MeCpd[•], yield methyl + cyclopentadiene radicals, with the methyl reacting with H₂ to form the CH₄. A similar scheme has been proposed by Louw, et. al. to account for the methane observed in their study⁷.

A QRRK analysis of the chemically activated system, using generic or literature values for high pressure rate constants¹² and species thermodynamic properties for the reaction sequence, yields the apparent rate constants shown in Fig. 1.11. Rate parameters used in these calculations are summarized in Table I.ii, with results in Table I.iii. Dissociation of the complex back to reactants (no reaction) clearly dominates and is consistent with work of Skinner.^{12,19} The isomerization channel, however, may result in MeCpd. for slightly more than 0.1% of collisions which create the CHD[•] complex at 1200 K and 1 atm pressure. Analysis predicts that direct production of MeCpd. will be favored at lower pressures. At higher pressures (above 760 torr) the stabilized CHD[•] species are predominant and

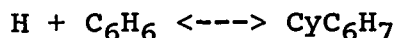
require additional collisions to make MeCpd. or revert to initial reagents. Although our calculations predict that isomerizations will occur to form stabilized MeCypd., the reverse reaction is also rapid due to a low energy barrier so that only a small steady state concentration will exist in equilibrium with the CHD radical and $C_6H_6 + H$.

We can use this reaction to compare the results of the chemical activation QRRK calculations with those where the products are calculated from thermal activation. Consider:



where the $linC_6H_7$ would unimolecularly decompose to acetylene and butadienyl radical. The butadienyl radical would further decompose to acetylene plus vinyl.

For the thermal calculation we assume the equilibrium



or $k_{-1} \gg k_2$ from the earlier discussion.

$$K_{eq} = [CyC_6H_7]/[H][C_6H_6]$$

then $[CyC_6H_7] = K_{eq}[H][C_6H_6]$ and with the rate constant for production of $LinC_6H_7$ from above:

$$d[LinC_6H_7]/dt = k_d K_{eq} [H] [C_6H_6] = k_{therm} [H] [C_6H_6]$$

with k_{therm} the thermal bimolecular rate constant.

We calculate k_d at 1200 K and 1 atm with the energet-

ics and rate constants illustrated in Figure 1.9 and Table I.ii as 4.5×10^3 , 19 percent of the high pressure limit 2.4×10^4 . Other dissociation channels, forward to products and back to reactants, were also considered in the calculation of k_d . Combining this with an equilibrium constant of 2.18×10^4 yields a value for k_{therm} of 9.8×10^7 cc/mole-sec for production of linC_6H_7 . The QRRK analysis at these same conditions yields a chemically activated rate constant of 6.4×10^8 , 6.5 times faster than the thermal calculation result. This demonstrates the importance of these reactions involving energized adducts at high temperatures, prior to their collisional stabilization, even at pressures as high as 1 atm.

Toluene may be formed by methyl addition at the ipso position in chlorobenzene followed by rapid loss of Cl from the complex (figure 1.12b). Methyl addition to benzene would not be as important in this system since the C-H bond in MeCHD. is nearly 10 Kcal/mole stronger than $\text{C}_{\text{benzene}}\text{-CH}_3$ (Fig 1.12a). Methyl cyclohexadienyl radical will dissociate back to $\text{CH}_3 + \text{C}_6\text{H}_6$ reactants at our conditions. We estimate the reaction of methyl radical with chlorobenzene forms toluene 10 times faster than addition of methyl to benzene. The high pressure A factors and barriers are listed in Tables I.iv and I.vi, with results tabulated in Tables I.v and I.vii. While it is clear from Figures 1.12a and 1.12b that enthalpy favors reaction of $\text{CH}_3 + \text{C}_6\text{H}_5\text{Cl}$ to produce Cl + toluene, close analysis shows that entropy

counters this effect to some extent.

The reaction of methyl radicals with benzene to form toluene plus H atoms through the MeCyC₆H₆ (Methylcyclohexadienyl radical) intermediate provides another comparison between chemical and thermal activation.



The equilibrium constant for methyl plus benzene to MeCyC₆H₆ is calculated as 2.5 at 1200 K. The rate constant for dissociation of MeCyC₆H₆ to toluene + H is calculated as 3.2×10^7 , 7 % of the high pressure limit 4.9×10^8 . Initial input data for the unimolecular dissociation of MeCyC₆H₆ are illustrated in Figure 1.12 and Table I.v. These data yield a value of k_{therm} to H + toluene of 7.9×10^7 cc/mole-sec. The chemical activation apparent rate constant from the energized complex calculation at 1200 K and 1 Atm pressure is 1.04×10^9 cc/mole-sec, thirteen times the result obtained assuming equilibrium with the thermally stabilized adduct.

Phenyl radical addition to either chlorobenzene or benzene will yield some biphenyl product, again going through a substituted cyclohexadienyl intermediate, shown in Figures 1.13 and 1.14. Calculations show that more than 90% of the collisions result in biphenyl + Cl for phenyl addition to the chlorobenzene ipso position at 1 atm pressure with H₂ bath gas. This appears to be a primary route to biphenyl production in this system. Phenyl addition at

C-H positions in benzene or chlorobenzene results in nearly equal amounts of stabilized intermediate and the biphenyl or chlorobiphenyl + H products. While dissociation of the complex is again important, the QRRK calculations show 20% of the phenyl + benzene collisions dissociate to biphenyl + H products at 1200 °K and 1 atm. A similar result was obtained for phenyl + chlorobenzene (for all positions except ipso addition). Rate parameters used in the calculations in addition to results are summarized in Tables I.viii - I.xiii. It is noteworthy that our calculation for the reaction of phenyl radical + benzene to give biphenyl + H, 7.7×10^{10} , is in excellent agreement with results recently published by Stein²¹ $6.0 \pm 2 \times 10^{10}$ cc/mole-sec.

Lowering the heat of formation for the phenyl radical to 78.6 Kcal/mole, the value recommended by McMillen and Golden²², versus 81.4 Kcal/mol determined by Tsang²³ (used throughout this study) will lower the entrance barrier relative to the exit barrier for phenyl attack on chlorobenzene (non ipso), cf Figure 1.14. The effect of this change is to lower both the stabilization and the chlorobiphenyl + H product channel formation rates by 30 and 47% respectively at 1200 K and 1 Atm. This effect is much less significant where there is a larger difference in the two exit channels for the energized complex, for example, addition of H or methyl radical to chlorobenzene, Figures 1.8 and 1.12 respectively.

We feel it important to note that improvements in

accuracy of the thermodynamic properties for these molecules are critical to improvements in our thermochemical based reaction mechanisms. A listing of thermochemical data used in this study is included in appendix I-C.

We have developed a detailed reaction mechanism for chlorobenzene pyrolysis in hydrogen which appears in Table I.xiv. Elementary reaction rate parameters for abstraction reactions are based upon literature comparison, thermodynamic estimations and Transition State Theory methods of Benson.²⁰ QRRK calculations, as described above, were used to estimate apparent rate parameters for addition and dissociation reactions (1 atm).

Experimental pyrolysis data are compared with model predictions in Figures 1.15 and 1.16 for chlorobenzene decomposition at 1126 and 1177 K in H₂. Predictions for chlorobenzene loss match experiment well. Prediction of benzene formation, on the other hand, is not quite as good except at low conversions (<50%) where significant soot formation has not yet occurred. Figure 1.17 compares predicted and experimental C₆H₅Cl decay curves as functions of residence time for several temperatures. Our model (Table I.xiv) is a first-principles description of the C₆H₅Cl chain decomposition, and we feel predictions shown are quite acceptable.

Rate parameters for several reactions appearing in Table I.xiv were varied over small intervals to give a better fit of our experimental data on both chlorobenzene

and dichlorobenzene reactions in hydrogen. A discussion of pyrolysis of dichlorobenzene is presented in Section II of this thesis. Optimization was performed primarily on three reactions. The A factor for chlorobenzene dissociation to phenyl radical and chlorine atom ($A_1=3.0E+15$) was estimated to be greater than $7.5E+14$ and less than $3.0E+15$ (A factor for reverse reaction, combination, less than $5E13$) with activation energy ($E_1 = 97.5$ Kcal/mol at 298 K). The high pressure A factor for hydrogen atom addition to chlorobenzene's ipso position ($A_{16}1.5E+13$) was taken as being between $6.0E+12$ and $2.2E+13$, with E_a between 4.5 and 9.0 Kcal/mol) upper limit values are those of W Tsang¹⁰. Abstraction of hydrogen from H_2 by phenyl radical was assumed to have an activation energy E_a between 6.0 and 9.5 kcal/mol²⁹. The A factor for this abstraction was estimated as $2.0E+13$. These reactions along with the H atom combination $H + H + M = H_2 + M$ were found to have the greatest influence (sensitivity) on predictions by the model.

Sensitivity analysis indicates that this H atom combination is the second most important reaction affecting the concentrations of chlorobenzene and benzene in the system. Manion et al.⁸ (and references cited therein) have indicated that the recombination of hydrogen on the walls is efficient and that H recombination above is probably in equilibrium. Changing this recombination rate in our mechanism clearly indicated that we did not have the H in thermal equilibrium with H_2 . To achieve equilibrium in the

system, we needed to increase the H atom recombination rate to greater than $5.0E19$. This slowed the chlorobenzene decomposition dramatically, to a point where we could not match our data with realistic rate constants. Rate constants in the range of 10^{17} - 10^{18} , which are ca. one order of magnitude greater than typical reported homogeneous k's, did permit fitting of our data for both chlorobenzene and dichlorobenzene experiments (rate constants consistent in both mechanisms). We can not fit our results with E_{a-29} larger than 6 kcal/mol for phenyl + H₂ abstraction, if $2H \rightleftharpoons H_2$ is at equilibrium. This is even more dramatically observed in our dichlorobenzene results.

The rate constant with highest sensitivity in the mechanism to chlorobenzene and benzene concentrations is the unimolecular decomposition of chlorobenzene, a chain initiation reaction. We report a best fit of the data with an A factor of $1.0E15$ and an E_a of 95.5 in the temperature range of the experiment. The reaction with third highest sensitivity to the above species is H atom displacement of chlorine atoms. We report a best fit to our data with a rate constant slightly faster than $2.2E13 \exp(-9Kcal/mole/RT)$ reported by W. Tsang¹⁰ with a value of $1.5E13 \exp(-7.5Kcal/mole/RT)$. While we could not fit the experimental data on chlorobenzene and dichlorobenzene with the reported rate constants of W. Tsang, we note that these numbers are very similar in the same temperature range, we have a slightly lower A and E_a , changes which are nearly

offsetting.

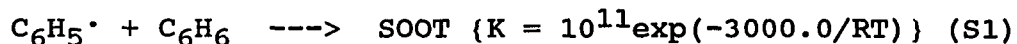
A fourth reaction which is important in this mechanism to the primary stable reactants and products is the abstraction of H from H₂ by phenyl radicals. We use an A factor of 2.0 E13 and an E_a of 9.0 Kcal/mole. The only references to this abstraction reaction are those of Fielding and Prichard²⁴ and Duncan²⁵ who both report an E_a of 6 Kcal/mole, but Stein and Fahr²⁶ indicate that there is some inconsistency in the two reported rate constants, i.e. a factor of 4 difference when referenced to the one common reagent - methane, and indicate that the E_a is probably not well known. Lowering the E_a for this reaction speeds up the reaction slightly.

It is our objective to present a detailed mechanism, which is thermochemically realistic and which models chlorobenzene decay. We do not wish to convey that the rate constants are absolutely correct, but that each k is reasonable in the realm of current thermochemical kinetics.

At the higher conversions, where we overpredict benzene, it should be noted that solid carbon is a significant fraction of product (ca 30%) and that the present mechanism makes no attempt to account for this carbon formation. Since we intuitively expect benzene to be instrumental in the production of carbon in this system, this over-prediction is not surprising.

We have tried several qualitative tests to check this hypothesis. We have evaluated the addition of several

irreversible reactions to our mechanism, attempting to improve agreement between predicted and experimental C_6H_6 production. Irreversible reactions such as:

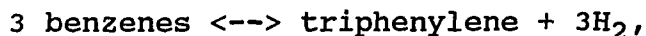


were found to slow the predicted chlorobenzene conversion, and benzene was still over predicted. The decrease in conversion is expected, however, since this is a chain termination reaction and the decomposition occurs via a chain mechanism. It is not unusual in high temperature addition reactions (complex formation) to observe C - H bond cleavage in the complex, so that one might expect an irreversible reaction of the type:



to be a viable path. Inclusion of this reaction did inhibit benzene formation somewhat without significantly decreasing the rate of chlorobenzene disappearance, but was not sufficient to explain the benzene profile.

Use of equilibria²⁶ such as:



does permit accurate modeling of the observed benzene product concentration profile (see figure 1.18). We shall report on this and on a model allowing a fraction of the benzene collisions with soot particles, concentrations estimated from mass balance and size fraction determined

from Harris et. al.²⁷.; to irreversibly stick to soot particles (as Harris did for acetylene) in a more appropriate future publication. These calculations are not, however, based on radical kinetics and do not constitute an elementary mechanism to soot. Our attempts to model soot formation from the gas phase chemistry described here, were unsuccessful. The use of a homogeneous reaction mechanism may not adequately describe the processes which occur when a significant quantity of soot particles have been formed, since heterogeneous effects may become important.

Phenyl dissociation reactions suggested by Frenklach et. al.²⁸ and Kiefer²⁹ have not helped to account for these observations. Their reactions to form soot are not fast enough at our temperatures. Our model does not predict significant phenyl dissociation to linear C₆H₅ at our conditions due to a large excess of H₂ and high energy required for dissociation. Phenyl radical is believed to be reactive toward H₂ and as a result phenyl dissociation would not be an important reaction channel. Predictions shown in Figs. 1.14-1.17 were obtained without the use of irreversible "bleed" reactions.

We have obtained mass spectral evidence on the non-volatile species contained in the carbon residue which are believed to be triphenylene, chlorotriphenylene, and larger PAH and phenyl adducts which support this reaction pathway. In addition, no significant amounts of acetylene, vinyl acetylene, or other ring fragmentation products were ob-

served. In chlorinated aromatic systems, polymerization may be even more favorable due to the relative ease with which chlorine may be eliminated from the PAH/phenyl adducts to promote ring condensation and growth.

Direct phenyl polymerization was suggested by Gordon, Smith, and McNesby³⁰ and more recently by Stein³¹ as a possible mechanism for soot growth in benzene systems where conditions such as temperature and H₂ concentration make ring opening and fragmentation reactions unlikely.

Phenyl radical is believed to add to biphenyl and chlorobiphenyl producing ortho-terphenyl plus hydrogen and chlorine atoms respectively. Ortho-terphenyl is relatively unstable²¹ and would either dissociate or condense to triphenylene. Ring growth may then result from successive additions of phenyl (chlorophenyl) followed by condensation to increasingly larger PAH. Such a mechanism would compete with hydrogen abstraction for phenyl radicals resulting in reduced benzene production. Inclusion of these ring addition pathways improves predictions by the mechanism slightly, similar to irreversible "bleed" reactions mentioned above.

The mechanism predicts essentially complete conversion of chlorine to HCl, while experimentally we observe only ca 82% mass balance for the Cl at 100% loss of chlorobenzene. Trace levels of chlorobiphenyls are observed in the solids by GC/Mass Spec analysis. Most other reaction studies in this laboratory, inclusive of chlorocarbon oxidations,

show complete mass balance for chlorine, with HCl the major product at high conversions. One difference between this and other studies in our lab is that this experiment operated at 100 to 200 K higher temperatures. We do not know if the Cl is in the carbon solids and not extractable, if it reacts with the quartz reactor, which clearly shows vitrification with use or is lost in the heated transfer lines to the titrator. This is an important issue which needs to be resolved.

The experimental results show production of cyclopentadiene, methane, toluene, biphenyl and chlorobiphenyl as trace products or stable intermediates present at levels less than 0.5% of the initial chlorobenzene.

Model predictions for biphenyl indicate a maxima 0.2% of the initial chlorobenzene at 0.24 seconds reaction time (40% parent conversion), 1177 K, with the decrease in concentrations at longer times producing benzene. This is in fair agreement with the experimental levels of 0.05% in vapor, plus GC/Mass Spec on methylene chloride extracts of solids consistently showing significant amounts of biphenyl and chlorobiphenyl. We feel a fair fraction of the biphenyl species were lost by adsorption on particulate in the reactor exit and sample transfer line to the GC. The model predicts chlorobiphenyl levels approximately 0.02% with a maxima at 0.28 seconds corresponding to 45% conversion of the parent chlorobenzene and the experimental levels are 0.05% of the initial chlorobenzene.

Cyclopentadiene levels predicted by the model are ca. 0.01% of CLBZ₀, where the observed concentrations are between 0.1 and 0.5%. The model and the experiment both show cyclopentadiene levels increasing with temperature, reaction time and/or conversion. Experimental observations on toluene show that it is present in concentrations below 0.5% with the model not predicting these levels. Methane is predicted at the 0.01% level, with experimental levels ranging between 0.04 and 0.06%.

While one can describe the reagent and major product concentration profiles with a less detailed reaction mechanism than that used here, we wanted to present a more complete reaction description by trying to model the observed high molecular weight and trace level species. We feel it is worthwhile to include these reactions; they illustrate plausible pathways and product concentrations. The model calculations also indicate that inclusion of ring addition reactions, which terminate at formation of biphenyls and chlorobiphenyls in this mechanism, do not explain the observed benzene loss at high conversions. Work is ongoing to explain formation of the observed PAH's plus multi - phenyl ring systems and especially the benzene loss. The reactions listed form a complete subset in mechanisms which accurately describe our dichlorobenzene results and our separate attempts to predict the observed PAH's (up

to 4 fused rings) plus triphenylene and chloro triphenylene.

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APPENDIX I - A

TABLES FOR SECTION I

TABLE I.i



(see Figure 1.8 for Potential Energy Diagram)

k	A*	Ea**	source
1	1.5 E+13	7.5	a
-1	3.6 E+12	31.0	a
2	1.16 E+13	8.9	b
$\langle v \rangle = 1064/\text{cm}$			c
LJ PARAMETERS :			d
sigma = 5.69 A		e/k = 526.9 cal	

a

This work, Reverse reaction (k-1) from thermodynamics.

b

based upon (ΔS) for $\text{Cl} + \text{C}_6\text{H}_6 = [\text{Cl-CHD}^*]$
 with $A_2 = 2.0\text{E}+13$ cc/mol sec

c

Geometric mean frequency estimated as follows:

$$\langle v \rangle_{\text{Cl-CHD.}} = \langle v \rangle_{\text{C}_6\text{H}_5\text{Cl}} + \langle v \rangle_{\text{C}_6\text{H}_7} - \langle v \rangle_{\text{C}_6\text{H}_6}$$

d

Lennard Jones parameters for radical complexes are estimated by averaging two structurally similar molecules with mixing rules of Prausnitz (Molecular Thermodynamics of Fluid Phase Equilibria, Prentice-Hall, 1969).

$$\text{For example: } (E/K)_{\text{CHD.}} = ((E/K)_{\text{BENZENE}} * (E/K)_{\text{CHD}})^{1/2}$$

$$\text{and } \sigma_{\text{CHD.}} = (\sigma_{\text{BENZENE}} + \sigma_{\text{CHD}}) / 2$$

Molecular L-J parameters are estimated using the correlation of Tee, Gotoh, and Stewart (I. E. & C. Fundamentals, 1966, 5, 363). Required critical property data tabulated in Reid, Prausnitz, and Sherwood (Properties of Gases and Liquids, 3rd ed.) or from Lydersen's group method for critical property estimation (also in Reid, Prausnitz, and Sherwood).

UNITS:

* A_1 (cc/mol sec)* A_2 (sec⁻¹)** E_a (Kcal/mol)

TABLE I.ii



(see Figures 1.9 and 1.10 for Potential Energy Diagrams)

k	A*	E _a **	source
1	4.0 E+13	4.3	a
-1	1.53 E+13	26.0	a
2	2.0 E+13	48.9	b
3	5.0 E+12	38.1	c
-3	8.0E+11	40.0	c
<hr/>			
<v> = 1224/cm			d
LJ PARAMETERS :			e
sigma = 5.40 A		e/k = 464.3 cal	
<hr/>			

a

Tsang, W. J. Phys. Chem. 1986, 90, 1152.
Reverse reaction (k-1) from thermodynamics.

b

E_a = delta H_f : A factor for beta scission
taken as that for C=CCC=C=C = C=C + C=CC=C
Dean, A. M.J. Phys. Chem. 1985, 89, 4600.

c

E₃ = delta H_f + 7.7 kcal/mol. A₃ is estimated from the
reverse reaction: bicyclo-C₆H₇ beta scission to cyclo-
hexadienyl radical (as in Figure 9). A₃=10^{12.75}
estimated from beta scission for primary and secondary
butyl radicals (Dean, A. M.J. Phys. Chem. 1985, 89, 4600).
E₃ is taken as the energy difference between [CHD[·]]°
and methylene cyclopentadienyl radical plus E_a for
1,2-Hydrogen shift to methyl cyclopentadienyl radical
(see Fig. 9).

d

Tsang, W. J. Phys. Chem. 1986, 90, 1152.

e

See note (d) Table I.i

UNITS:

- * A₁ (cc/mol sec)
- A₂ (sec⁻¹)
- A₃ (sec⁻¹)
- ** E_a (Kcal/mol)

TABLE 1.iii

APPARENT REACTION RATE CONSTANTS PREDICTED

USING BIMOLECULAR QRRK ANALYSIS

Bath Gas	P (torr)	Reaction	A factor (cc/mol s)	n	Ea (kcal/mole)	range
H2	7.6	H+C6H6 = [ME-CYPD*] ^o	1.65 E+55	-12.21	41.0	c
	760.0	"	2.39 E+27	-3.92	29.2	"
	7.6	H+C6H6 = [CHD*] ^o	2.79 E+49	-11.55	13.59	"
	760.0	"	4.87 E+56	-12.73	26.8	"
	7.6	H+C6H6 = Lin-C6H7	7.96 E+16	-0.88	28.8	a
	760.0	"	1.67 E+21	-2.01	34.1	"
N2	7.6	H+C6H6 = [ME-CYPD*] ^o	1.05 E+60	-13.66	43.2	c
	760.0	"	5.22 E+28	-4.35	28.8	b
	7.6	H+C6H6 = [CHD*] ^o	4.17 E+46	-10.87	10.87	c
	760.0	"	8.18 E+57	-13.19	26.3	b
	7.6	H+C6H6 = Lin-C6H7	5.04 E+16	-0.82	28.7	a
	760.0	"	9.47 E+19	-1.68	32.5	"

a Valid from 300 - 1900 K

b " " 600 - 1900 K

c " " 900 - 1900 K

TABLE I.iv



(see Figure 1.12a for Potential Energy Diagram)

k	A*	Ea**	source
1	2.9 E+12	11.1	a
-1	2.1 E+14	22.8	a
2	2.7 E+13	26.1	b
$\langle v \rangle = 1200/\text{cm}$			c
LJ PARAMETERS :			d
sigma = 5.74 A		e/k = 494 cal	

a

Tsang, W. J. Phys. Chem. 1986, 90, 4159.
Reverse reaction (k-1) from thermodynamics

b

based upon (ΔS) for $\text{C}_6\text{H}_5\text{CH}_3 + \text{H} = [\text{Me-CHD}^*]$
with $A_{-2} = 1.2\text{E}+13$ (a)

c

Geometric mean frequency estimated as follows:

$$\langle v \rangle_{\text{Me-CHD}} = \langle v \rangle_{\text{C}_6\text{H}_5\text{CH}_3} + \langle v \rangle_{\text{C}_6\text{H}_7} - \langle v \rangle_{\text{C}_6\text{H}_6}$$

d

See note (d) Table I.i

UNITS:

* A_1 (cc/mol sec) A_2 (sec^{-1})** E_a (Kcal/mol)

TABLE I.v

APPARENT REACTION RATE CONSTANTS PREDICTED

USING BIMOLECULAR QRRK ANALYSIS

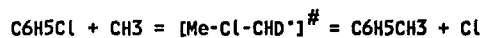
Bath Gas	P (torr)	Reaction	A factor (cc/mol s)	n	Ea (kcal/mole)	range
H2	7.6	CH3+C6H6 = [ME-CHD*] ⁰	6.64 E+29	-6.93	-4.8	c
	760.0	"	1.49 E+57	-13.84	28.3	b
	7.6	CH3+C6H6 = C6H5CH3+H	6.22 E+15	-1.20	17.1	a
	760.0	"	3.41 E+26	-4.15	26.4	b
N2	7.6	CH3+C6H6 = [ME-CHD*] ⁰	1.59 E+27	-6.29	2.8	c
	760.0	"	5.30 E+48	-11.60	21.2	c
	7.6	CH3+C6H6 = C6H5CH3+H	4.56 E+14	-0.88	16.3	a
	760.0	"	8.65 E+23	-3.44	24.1	b

a Valid from 300 - 1900 K

b " " 600 - 1900 K

c " " 900 - 1900 K

TABLE I.vi



(see Figure 1.12b for Potential Energy Diagram)

k	A*	Ea**	source
1	1.45 E+12	11.1	a
-1	8.54 E+12	26.5	a
2	5.6 E+13	11.1	b
<hr/>			
<v> = 1070/cm			c
LJ PARAMETERS :			d
sigma = 5.99 A			
e/k = 548 cal			

a

A factor taken as 1/2 that for CH₃+C₆H₆ (Table I.iiia)

Reverse reaction (k-1) from thermodynamics.

b

based upon (del S) for C₆H₅CH₃+Cl = [Me-Cl-CHD[†]]
with A₋₂=1.0E+12(a)

c

Geometric mean frequency estimated as follows:

$$\langle v \rangle_{\text{Me-Cl-CHD.}} = \langle v \rangle_{\text{Me-CHD.}} + \langle v \rangle_{\text{C}_6\text{H}_5\text{Cl}} - \langle v \rangle_{\text{C}_6\text{H}_6}$$

d

See note (d) Table I.i

UNITS:

* A₁ (cc/mol sec)A₂ (sec⁻¹)** E_a (Kcal/mol)

TABLE I.vii

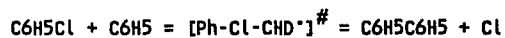
APPARENT REACTION RATE CONSTANTS PREDICTED

USING BIMOLECULAR QRRK ANALYSIS

Bath Gas	P (torr)	Reaction	A factor (cc/mol s)	n	Ea (kcal/mole)	range
H2	7.6	CH3+C6H5Cl=[ME-Cl-CHD*] ^o	5.91 E+25	-5.78	13.5	a
	760.0	"	1.98 E+28	-5.93	13.9	"
	7.6	CH3+C6H5Cl = C6H5CH3+Cl	5.15 E+13	-0.49	11.6	"
	760.0	"	1.96 E+14	-0.65	12.0	"
N2	7.6	CH3+C6H5Cl=[ME-Cl-CHD*] ^o	2.31 E+25	-5.76	13.5	"
	760.0	"	4.17 E+27	-5.83	13.7	"
	7.6	CH3+C6H5Cl = C6H5CH3+Cl	5.11 E+13	-0.49	11.6	"
	760.0	"	9.80 E+13	-0.53	11.8	"

^aValid from 300 - 1900 K

TABLE I.viii



(see Figure 1.13 for Potential Energy Diagram)

k	A*	E _a **	source
1	1.0 E+12	4.3	a
-1	1.6 E+15	33.2	a
2	1.9 E+14	10.0	b
<v> = 975/cm			c
LJ PARAMETERS :			d
sigma = 6.66 A		e/k = 694 cal	

a

Louw, R.; Dijks, J. H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635.

Reverse reaction (k-1) from thermodynamics.

b

A factor based upon entropy change for reverse.
 $\text{Cl} + \text{Ph-Ph} = [\text{Ph-Cl-CHD}^*]$ (ipso attack)
 with $A_{-2} = 1.2 \text{ E}+13$ and $E_{-2} = 2.0 \text{ kcal/mol}$.

c

Geometric mean frequency estimated as follows:
 $\langle v \rangle_{\text{Ph-Cl-CHD}} = \langle v \rangle_{\text{Ph-Ph}} + \langle v \rangle_{\text{Cl-CHD}} - \langle v \rangle_{\text{C}_6\text{H}_6}$

d

See note (d) Table I.i

UNITS:

* A_1 (cc/mol sec)
 A_2 (sec⁻¹)

** E_a (Kcal/mol)

TABLE I.ix

APPARENT REACTION RATE CONSTANTS PREDICTED

USING BIMOLECULAR QRRK ANALYSIS

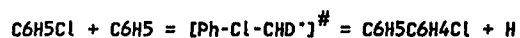
Bath Gas	P (torr)	Reaction	A factor (cc/mol s)	n	Ea (kcal/mole)	range
H2	7.6	C6H5+C6H5Cl=[Ph-Cl-CHD*] ^o	4.45 E+22	-5.06	5.7	a
	760.0	"	7.97 E+24	-5.13	5.87	"
	7.6	C6H5+C6H5Cl = C6H5C6H5+Cl	9.85 E+11	0.0	4.29	"
	760.0	"	2.59 E+12	-0.12	4.53	"
N2	7.6	C6H5+C6H5Cl=[Ph-Cl-CHD*] ^o	1.68 E+22	-5.03	5.7	"
	760.0	"	2.17 E+24	-5.06	5.79	"
	7.6	C6H5+C6H5Cl = C6H5C6H5+Cl	9.85 E+11	0.0	4.29	"
	760.0	"	1.0 E+12	0.0	4.32	"

^a Valid from 300 - 1900 K

^b " " 600 - 1900 K

^c " " 900 - 1900 K

TABLE I.x



(see Figure 1.14 for Potential Energy Diagram)

k	A*	Ea**	source
1	2.0 E+12	4.3	a
-1	2.2 E+15	32.74	a
2	6.7 E+13	24.5	b
<v> = 975/cm			c
LJ PARAMETERS :			d
sigma = 6.66 A		e/k = 694 cal	

a

Louw, R.; Dijks, J. H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635.

Reverse reaction (k-1) from thermodynamics.

b

A factor based upon entropy change for reverse.
 $\text{H} + \text{Cl-Ph-Ph} = [\text{Cl-Ph-CHD}^*]$
 with $A_{-2} = 1.3 \text{ E}+13$ and $E_{-2} = 4.0 \text{ kcal/mol}$.

c

Geometric mean frequency estimated as follows:
 $\langle v \rangle_{\text{Ph-Cl-CHD}} = \langle v \rangle_{\text{Ph-Ph}} + \langle v \rangle_{\text{Cl-CHD}} - \langle v \rangle_{\text{C}_6\text{H}_6}$

d

See note (d) Table I.i

UNITS:

* A_1 (cc/mol sec) A_2 (sec⁻¹)** E_a (Kcal/mol)

TABLE I.xi

APPARENT REACTION RATE CONSTANTS PREDICTED

USING BIMOLECULAR QRRK ANALYSIS

Bath Gas	P (torr)	Reaction	A factor (cc/mol s)	n	Ea (kcal/mole)	range
H2	7.6	$C_6H_5 + C_6H_5Cl = [Ph-Cl-CHD^*]^{\circ}$	6.82 E+47	-12.12	6.62	c
	760.0	"	2.80 E+69	-17.31	29.2	b
	7.6	$C_6H_5 + C_6H_5Cl = C_6H_5C_6H_4Cl + H$	9.52 E+19	-2.51	7.08	c
	760.0	"	4.50 E+49	-10.65	33.3	b
N2	7.6	$C_6H_5 + C_6H_5Cl = [Ph-Cl-CHD^*]^{\circ}$	3.34 E+42	-10.76	2.36	c
	760.0	"	5.42 E+72	-18.39	29.94	b
	7.6	$C_6H_5 + C_6H_5Cl = C_6H_5C_6H_4Cl + H$	3.43 E+32	-6.04	15.97	"
	760.0	"	4.50 E+49	-10.65	31.95	"

^a Valid from 300 - 1900 K

^b " " 600 - 1900 K

^c " " 900 - 1900 K

TABLE I.xii



k	A*	Ea**	source
1	2.0 E+12	4.3	a
-1	3.9 E+14	29.4	a
2	1.1 E+13	23.55	b
<v> = 1050/cm			c
LJ PARAMETERS :			d
sigma = 6.45 A		e/k = 662 cal	

a

Louw, R.; Dijks, J. H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635.

Reverse reaction (k-1) from thermodynamics.

b

A factor based upon entropy change for reverse.
 $\text{H} + \text{Ph-Ph} = [\text{Ph-CHD}^*]$
 with $A_{-2} = 2.0 \text{ E}+13$ and $E_{-2} = 4.0 \text{ kcal/mol}$.

c

Geometric mean frequency estimated as follows:
 $\langle v \rangle_{\text{Ph-CHD}} = \langle v \rangle_{\text{Ph-Ph}} + \langle v \rangle_{\text{CHD}} - \langle v \rangle_{\text{C}_6\text{H}_6}$

d

See note (d) Table I.i

UNITS:

* A_1 (cc/mol sec) A_2 (sec^{-1})** E_a (Kcal/mol)

TABLE I.xiii

APPARENT REACTION RATE CONSTANTS PREDICTED

USING BIMOLECULAR QRRK ANALYSIS

Bath Gas	P (torr)	Reaction	A factor (cc/mol s)	n	Ea (kcal/mole)	range
H2	7.6	$C_6H_5 + C_6H_6 = [Ph-CHD^*]^{\circ}$	1.92 E+45	-11.24	6.61	c
	760.0	"	3.30 E+60	-15.18	26.43	"
	7.6	$C_6H_5 + C_6H_6 = C_6H_5C_6H_6 + H$	1.21 E+20	-2.56	7.29	b
	760.0	"	1.61 E+45	-9.39	31.0	"
N2	7.6	$C_6H_5 + C_6H_6 = [Ph-CHD^*]^{\circ}$	1.09 E+40	-9.89	2.38	c
	760.0	"	4.11 E+56	-14.15	16.42	"
	7.6	$C_6H_5 + C_6H_6 = C_6H_5C_6H_6 + H$	1.91 E+30	-5.42	14.64	"
	760.0	"	7.31 E+26	-4.42	13.11	"

^a Valid from 300 - 1900 K

^b " " 600 - 1900 K

^c " " 900 - 1900 K

TABLE I.xiv
REACTION MECHANISM#

REACTION	A	n	Ea(kcal/mol)	source
1. C6H5CL=CYC6H5+CL	3.0 E+15	0.0	95.5	a
2. CYC6H6=CYC6H5+H	1.67E+16	0.0	111.5	b
3. CYC6H7=MECY24PD1	5.0 E+12	0.0	38.1	c
4. MECY24PD=CY13PD5+CH3	1.0 E+16	0.0	67.5	d
5. CY13PD=CY13PD5+H	6.0 E+14	0.0	75.1	e
6. C6H5C6H5= CYC6H5+CYC6H5	5.0 E+16	0.0	117.0	g
7. PPHCL=CYC6H5+C6H4CL	1.9 E+16	0.0	117.0	h
8. CYC6H5=LINC6H5	3.16E+13	0.0	55.2	i
9. LINC6H5=C*CC*C.+C2H2	6.09E+14	0.0	47.6	j
10. LINC6H7=C*CC*C.+C2H2	5.50E+14	0.0	41.0	j
11. H+CL+M=HCL+M	1.0 E+17	0.0	0.0	k
12. CL2=CL+CL	7.69E+08	0.0	55.6	k
13. H+H+M=H2+M	1.0 E+18	0.0	0.0	m
14. C6H5CL=C6H4CL+H	1.3 E+16	0.0	110.5	f
15. CYC6H6+H=MECY24PD1	2.39E+27*	-3.92	29.2	l
16. C6H5CL+H=CYC6H6+CL	1.5 E+13*	0.0	7.5	l
17. CYC6H6+H=CYC6H7	4.87E+56*	-12.73	26.8	l
18. CYC6H6+H=LINC6H7	1.22E+22*	-1.87	31.2	l
19. CH3+C6H5CL=C6H5CH3+CL	1.96E+14*	-0.65	12.0	l
20. CH3+CYC6H6=C6H5CH3+H	3.4 E+26*	-4.15	26.4	l
21. CH3+H=CH4	8.09E+36*	-7.19	9.2	l
22. CYC6H5+C6H5CL=PPHCL+H	4.5 E+49*	-10.65	33.3	l
23. CYC6H5+C6H5CL=C6H5C6H5+CL	2.6 E+12*	-0.12	4.5	l
24. CYC6H5+CYC6H6=C6H5C6H5+H	1.6 E+45*	-9.39	31.0	l
25. C6H4CL+C6H4CL=PHCLPHCL	1.8 E+13*	0.0	0.0	l
26. C6H4CL+C6H5CL=PPHCL+CL	2.6 E+12*	-0.13	4.43	l
27. C6H4CL+C6H5CL=PHCLPHCL+H	5.43E+15*	-1.39	3.85	l
28. C6H4CL+CYC6H6=PPHCL+H	9.92E+37*	-5.48	19.97	l
29. CYC6H6+H=CYC6H5+H2	2.0 E+13	0.0	18.6	m
30. CH3+H2=CH4+H	5.0 E+12	0.0	11.0	n
31. C6H5CL+H=CYC6H5+HCL	1.0 E+13	0.0	11.3	m
32. H+C6H5CL=H2+C6H4CL	2.0 E+13	0.0	18.6	m
33. CL+H2=HCL+H	4.8 E+13	0.0	5.0	p
34. CL+C6H5CL=HCL+C6H4CL	1.0 E+13	0.0	12.5	m
35. CL+CYC6H6=HCL+CYC6H5	1.1 E+13	0.0	12.5	m
36. H+CL2=CL+HCL	7.94E+13	0.0	1.2	p
37. MECY24PD1+H=CY13PD+CH3	8.0 E+13	0.0	0.0	q
38. CYC6H7=ME.CY24PD	5.5 E+10	0.0	23.5	r
39. ME.CY24PD+H2=MECY24PD+H	3.98E+12	0.0	14.0	s

* Pressure dependent : rate expression given for 760 torr

Temperature ranges given in Tables I.ii-I.xiv.

See Figures 1.15 - 1.17 for comparison of experimental data with model results.

References for Mechanism (Table I.xiv)

- a A factor from reverse with $A_{-1} = 9 \text{ E}+12$: this work.
- b A factor based upon reverse with $A_{-2} = 1 \text{ E}+14$. H addition to secondary C_4 radicals (Allara, D. L. and Shaw, R. J. Phys. Chem. Ref. Data, 1980, 9, 523).
- c see Table II : Qrrk/Energized complex analysis of $\text{H} + \text{C}_6\text{H}_6$.
- d A factor from reverse with $A_{-4} = 1 \text{ E}+13$. CH_3 addition to C_4 radicals (Allara, D. L. and Shaw, R. J. Phys. Chem. Ref. Data, 1980, 9, 523).
- e A factor from reverse with $A_{-5} = 1 \text{ E}+14$: see ref. b.
- f A factor from reverse with $A_{-14} = 7.5\text{E}+13$: see ref. b.
- g A factor from reverse with $A_{-6} = 1 \text{ E}+12$ (Louw, R; Dijks, J. H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1984, 103, 271).
- h see ref. g.
- i taken as linear $\text{C}_6\text{H}_7 = \text{C}_4\text{H}_7 + \text{C}_2\text{H}_2$ (Dean, A. M. J. Phys. Chem. 1985, 89, 4600).
- j A factor and E_a from $\text{C}=\text{CC}=\text{C} + \text{C}_2\text{H}_2$ (see ref. i).
- k Kerr, J. A. and Moss, S. J. eds Handbook of Bimolecular and Termolecular Gas Reactions V I and II CRC Press, Inc. 1981.
- l QRRK/ Energized complex analysis presented in this work (Tables I.i - I.xiii) or by analogy to those in tables.
- m optimized reaction : this work
- n $\text{CH}_3 + \text{H}_2$ from Allara and Shaw (see ref. d).
- o $\text{C}_3\text{H}_5 + \text{H}_2$ from Allara and Shaw (see ref. d).
- p (Kerr, J. A. and Moss, S. J. eds Handbook of Bimolecular and Termolecular Gas Reactions Vol. I and II CRC Press, Inc. 1981).
- q see ref. b.
- r Pressure dependence accounted for with QRRK analysis of Dean (see ref. j).
- s A factor taken as $\text{CCC} + \text{H}_2$ (Allara, D. L. and Shaw, R. J. Phys. Chem. Ref. Data, 1980, 9, 523).

APPENDIX I - B

FIGURES FOR SECTION I

Figure 1.1

SCHEMATIC DIAGRAM OF EXPERIMENTAL APPARATUS

- Tubular Flow Reactors
- Temp Constant to ± 5 Degrees
- Chlorobenzene:H₂ 270:1
- GC AND GC/Mass Spec Analysis

VARIABLES

- Reaction Time (0.02 to 2.5 sec)
- Temperature (1100 to 1300 K)
- Surface to Volume Ratio (10 to 2.5/cm)

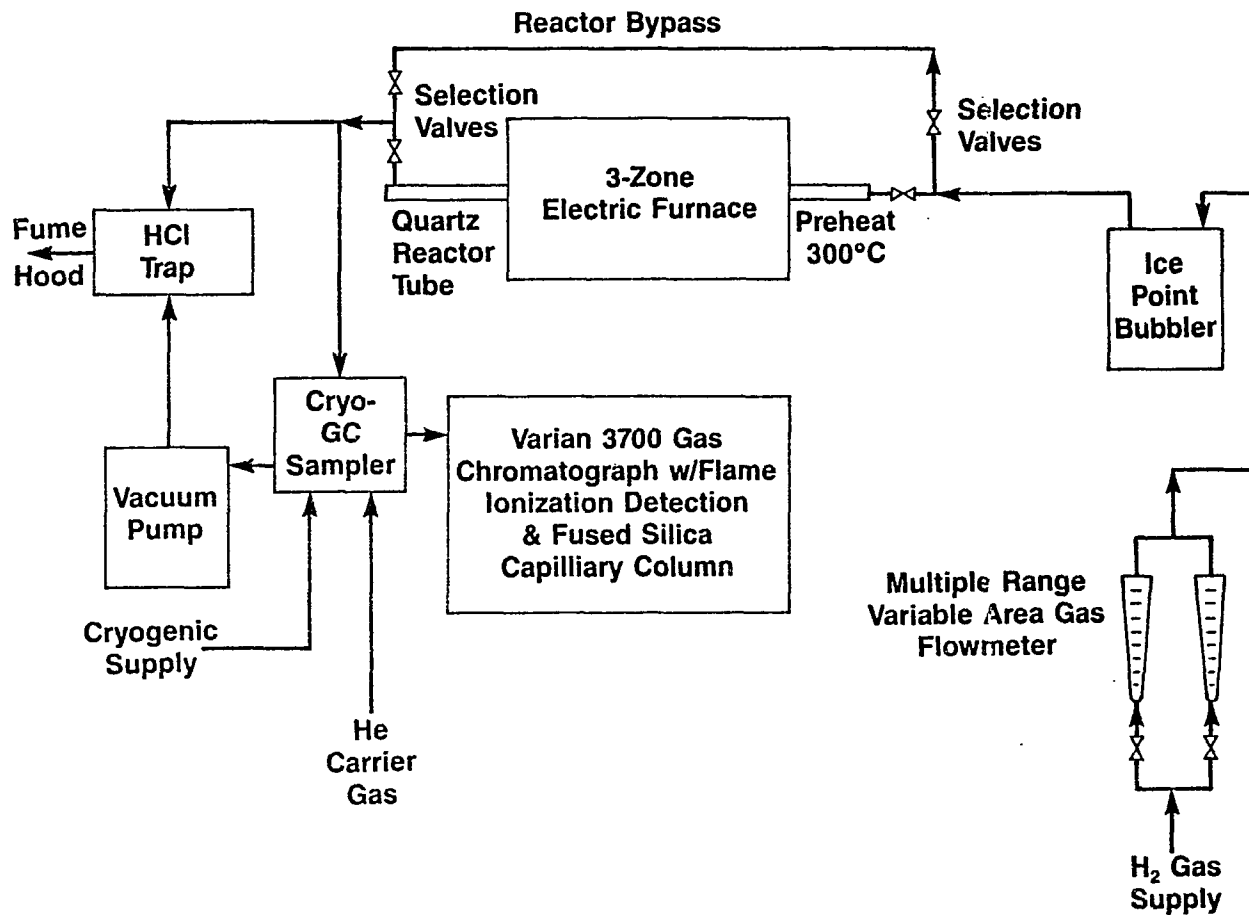


Figure 1.2

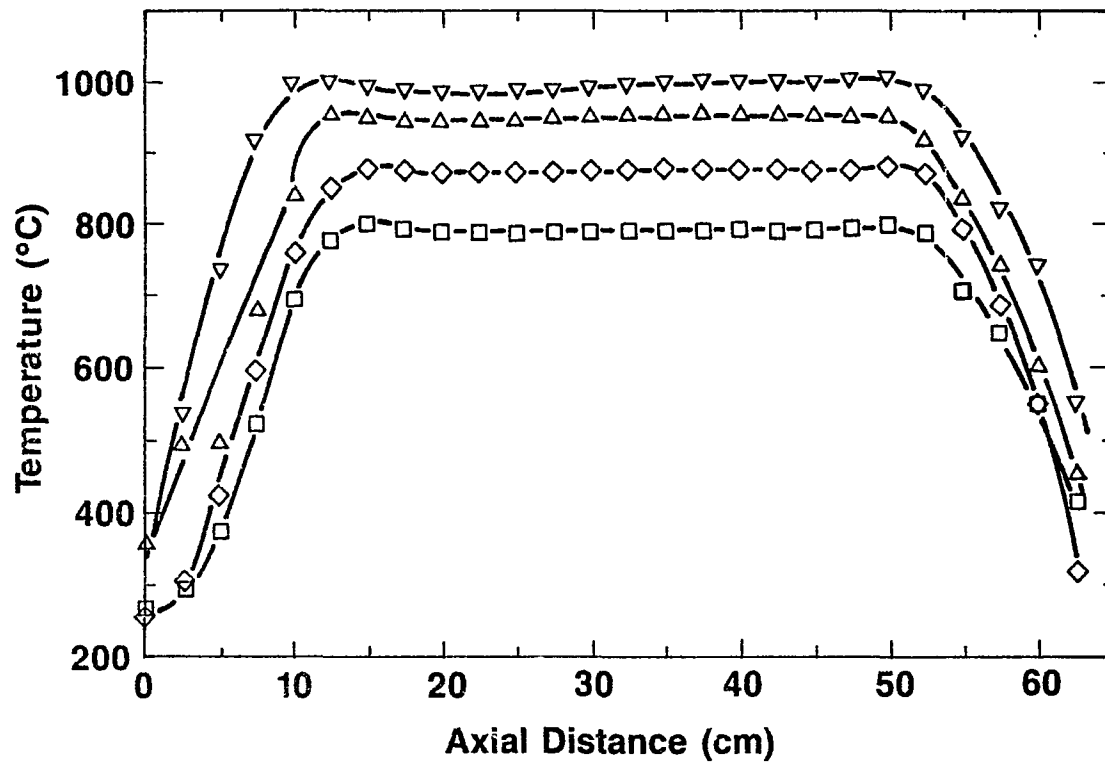
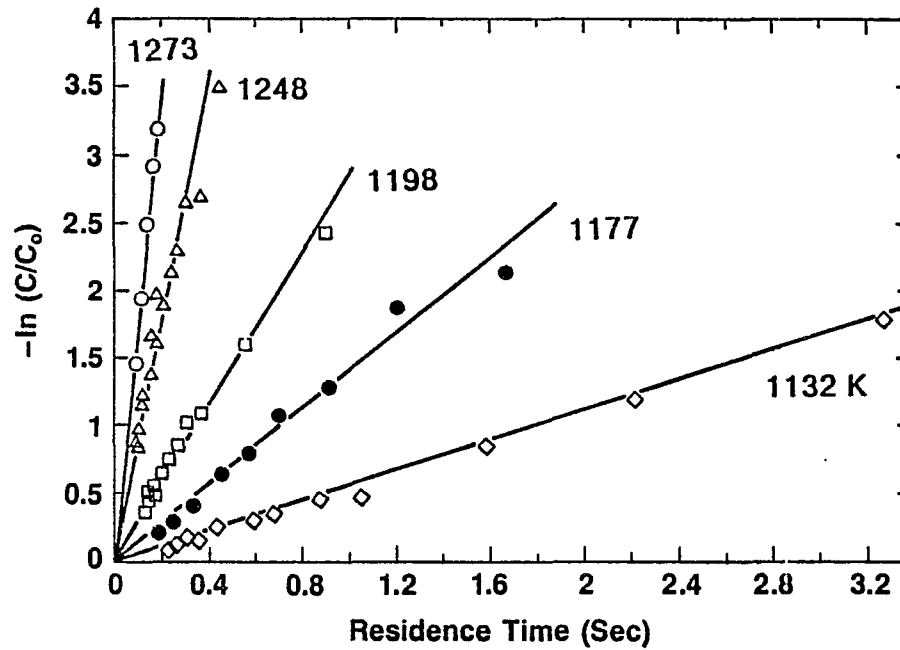


Figure 1.3

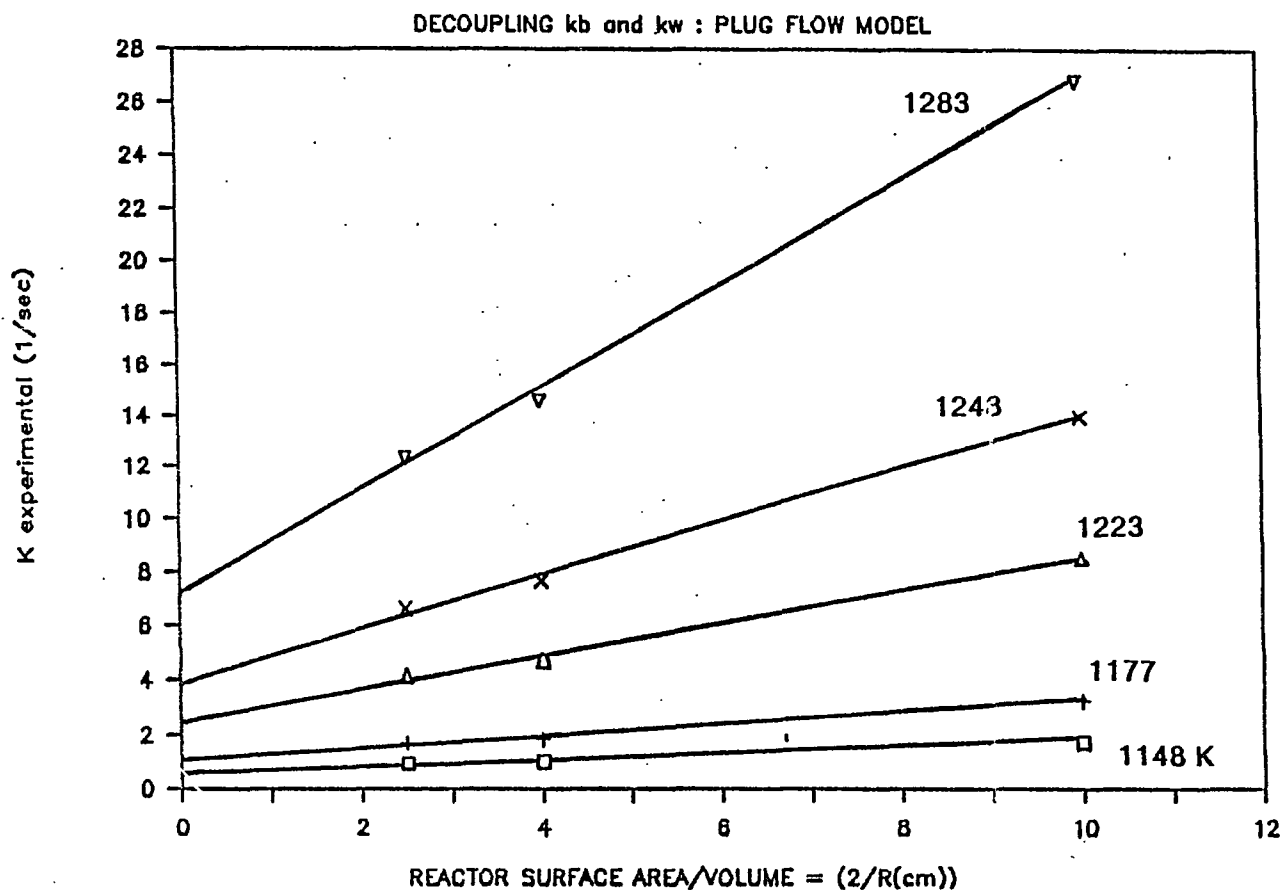
PSEUDO FIRST ORDER REACTION H₂ EXCESS



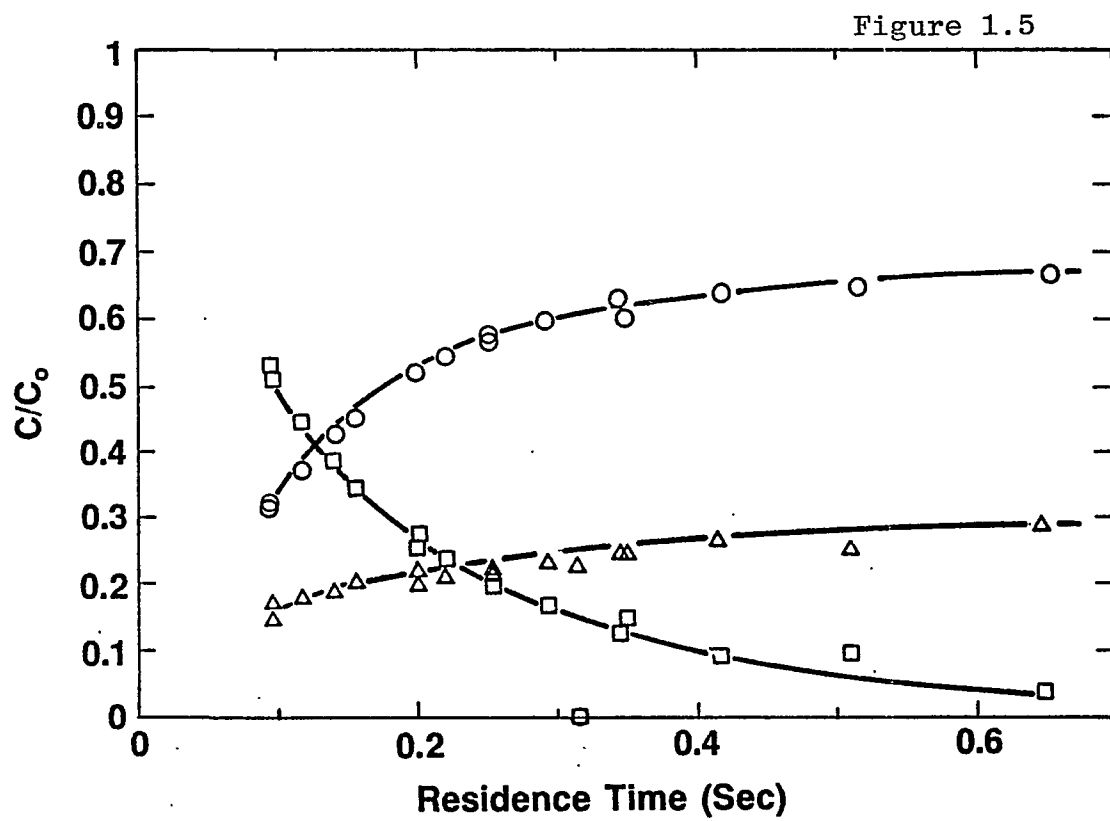
OVERALL REACTION EXHIBITS FIRST ORDER DECAY FOR CHLOROBENZENE LOSS

VARIATION IN OBSERVED RATE CONSTANT WITH REACTOR SURFACE TO VOLUME RATIO ($2/r$)

Figure 1.4



- Global Rate Constant is Function of S/V for Small Diameter Reactors
- Data Allows Separation of BULK Rate Constants from Wall Effects



CHLOROBENZENE + H₂ ---> PRODUCTS

1 Second Reaction Time

Figure 1.6

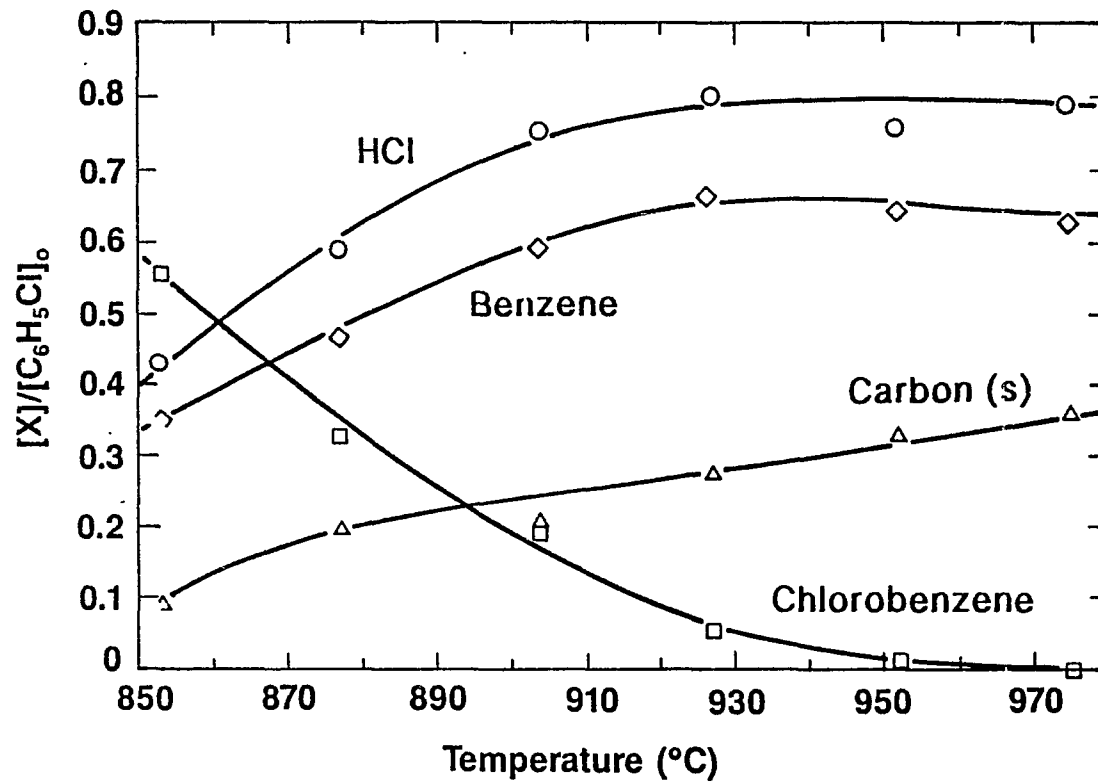
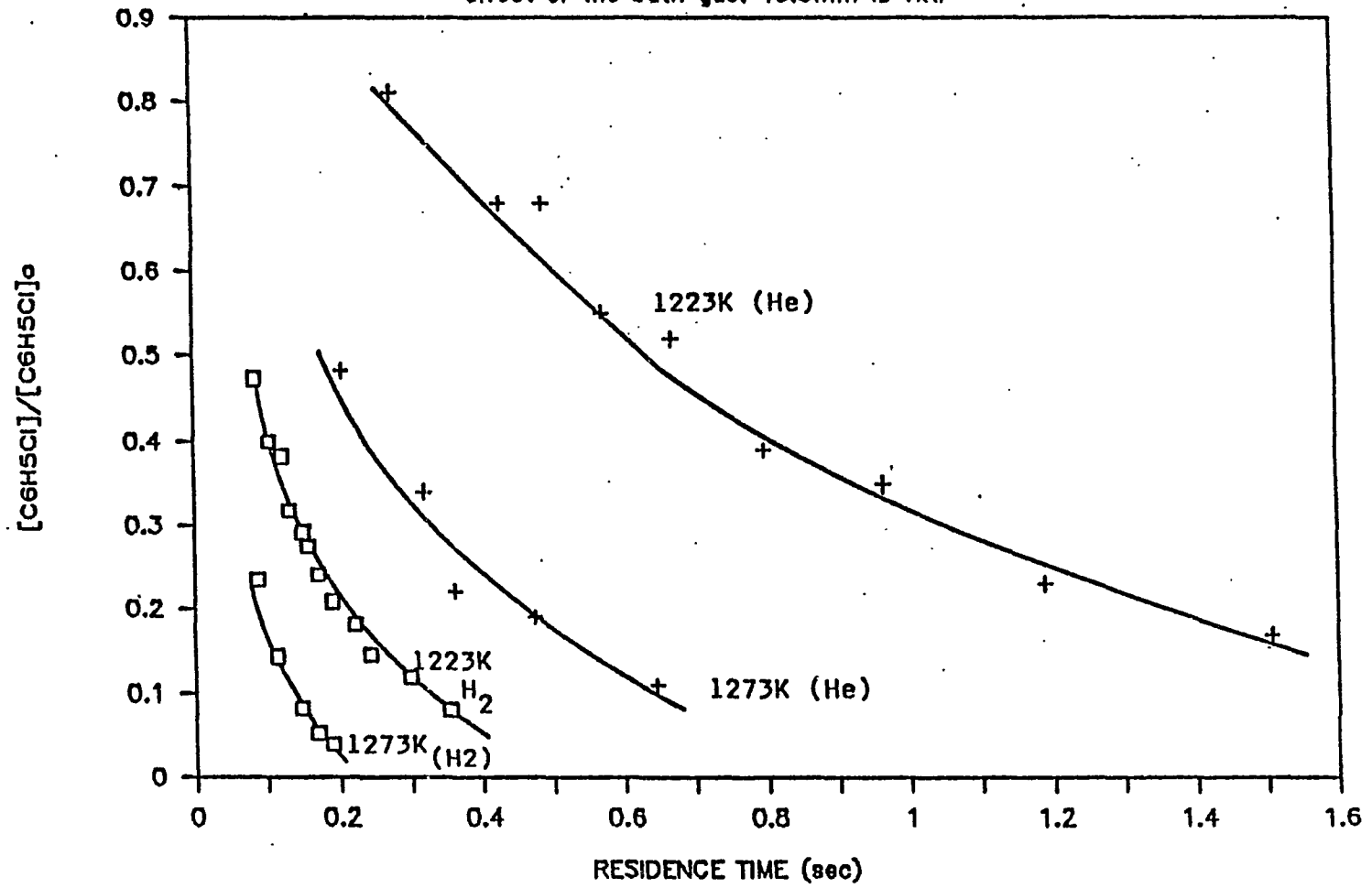


Figure 1.7

effect of the bath gas: 10.5mm ID rxtr



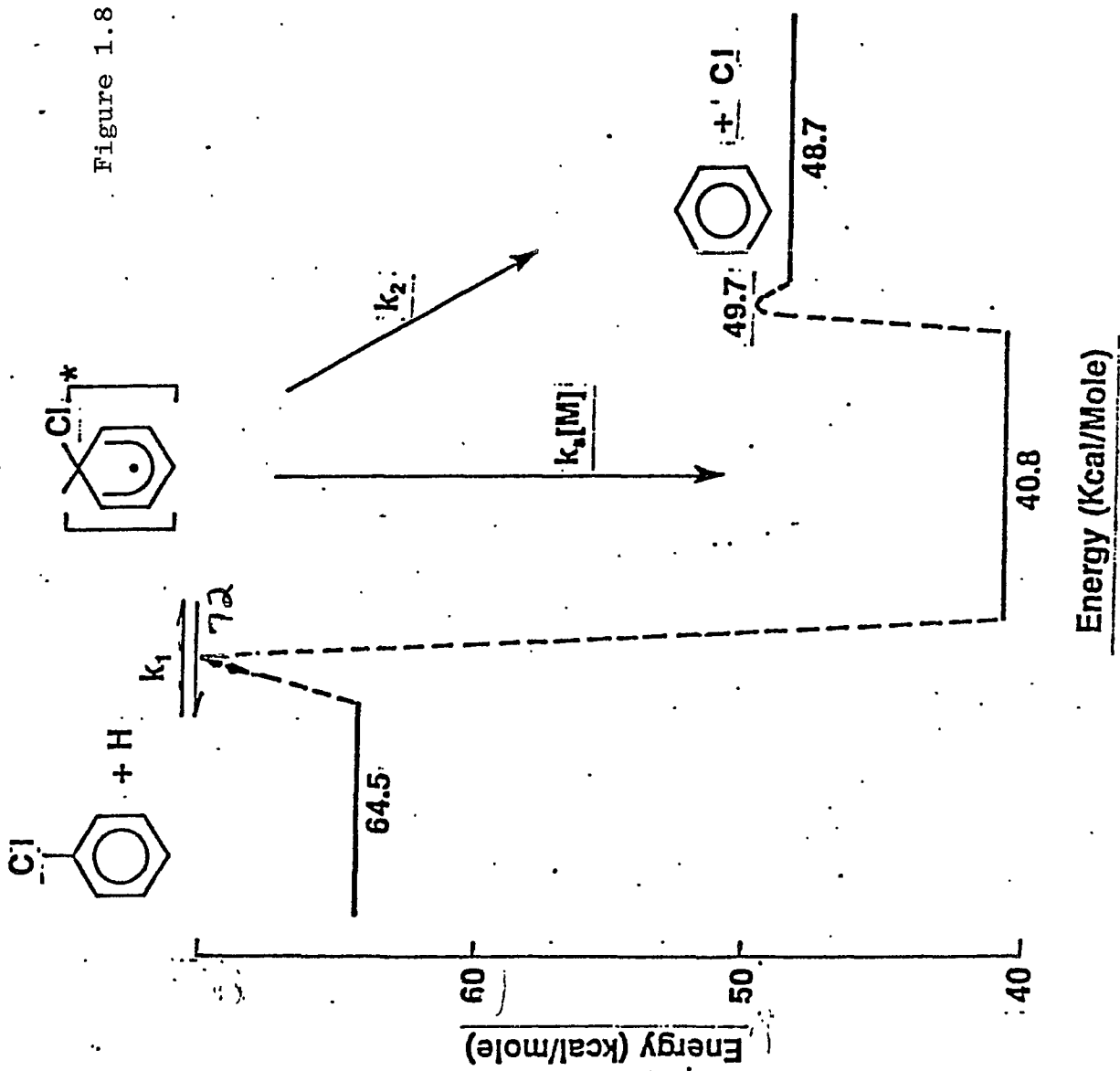


Figure 1.9

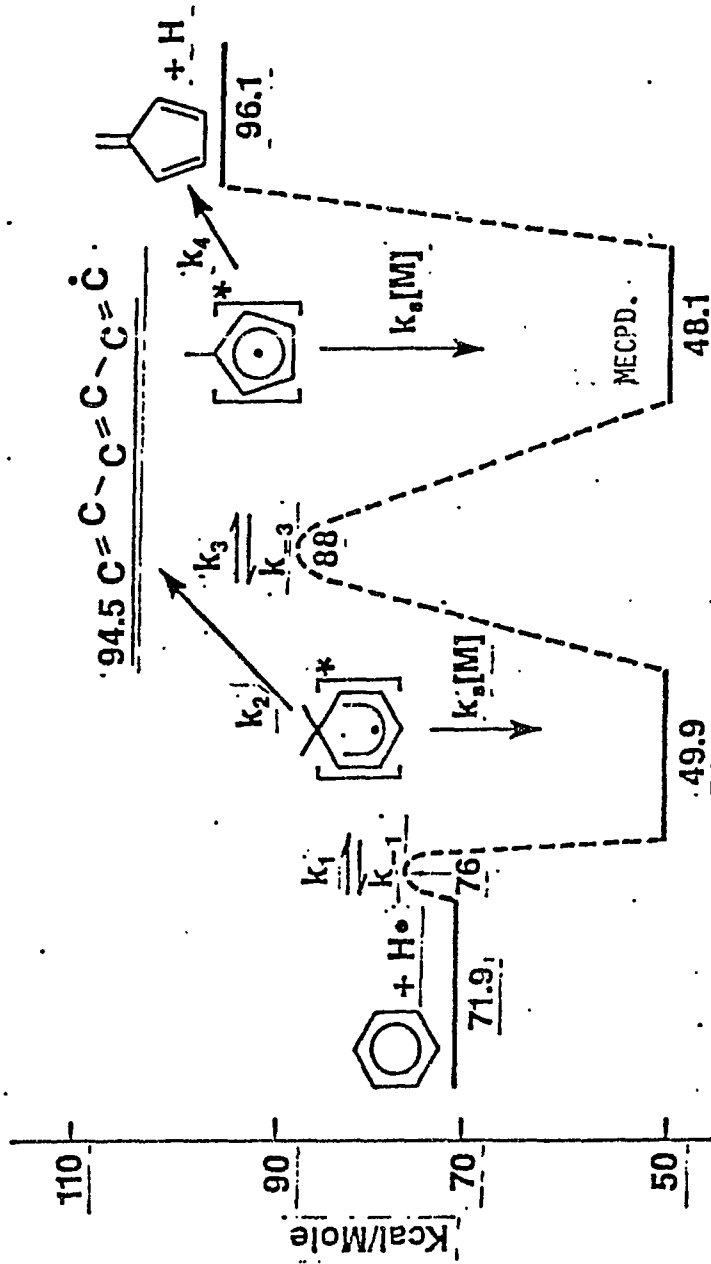
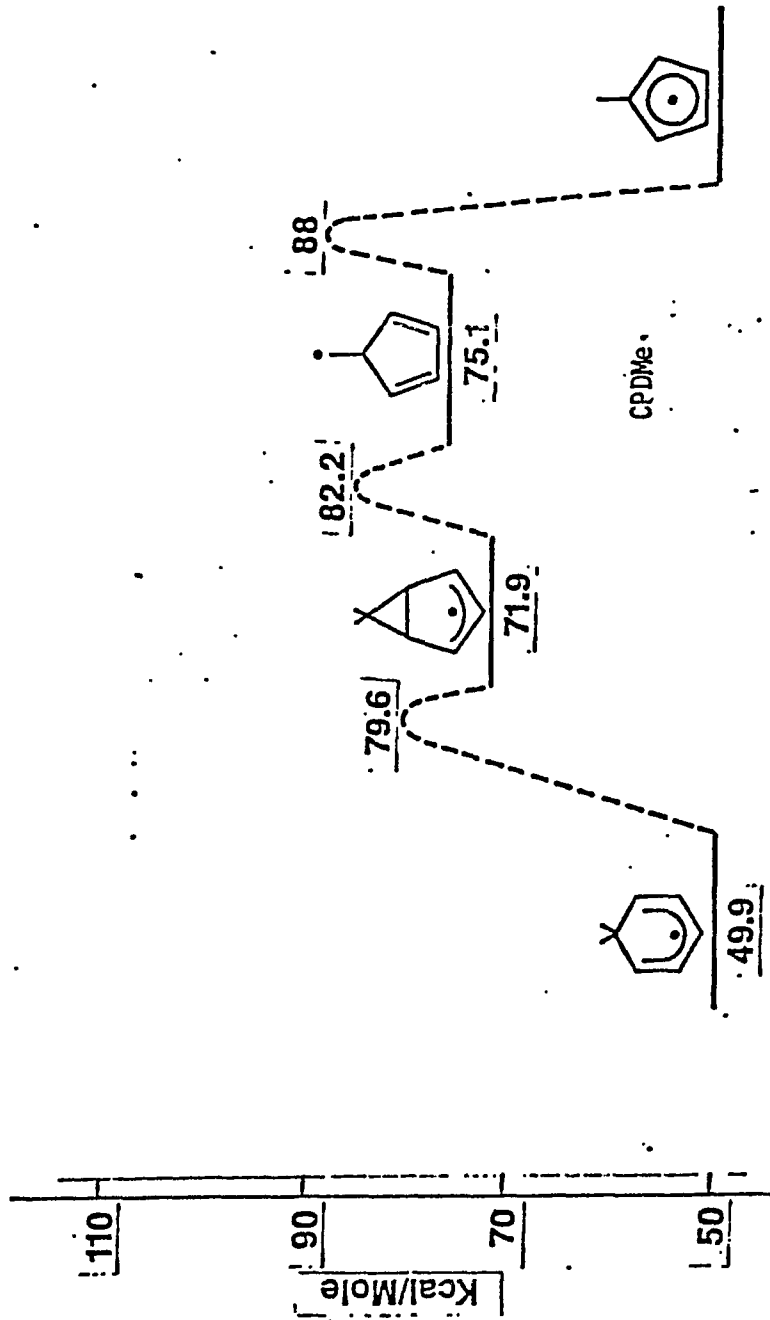


Figure 1.10



H + C6H6 ADDITION PRODUCTS vs PRESSURE APPARENT RATE CONSTANTS at 1200 K

Figure 1.11

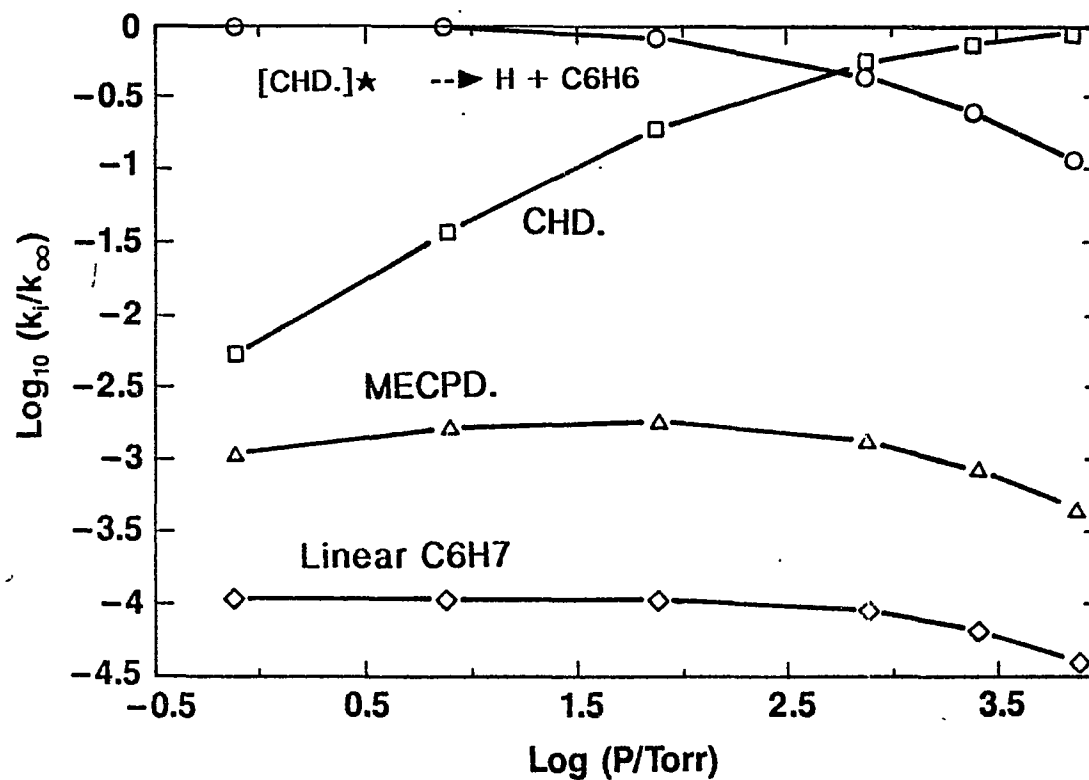


Figure 1.12a

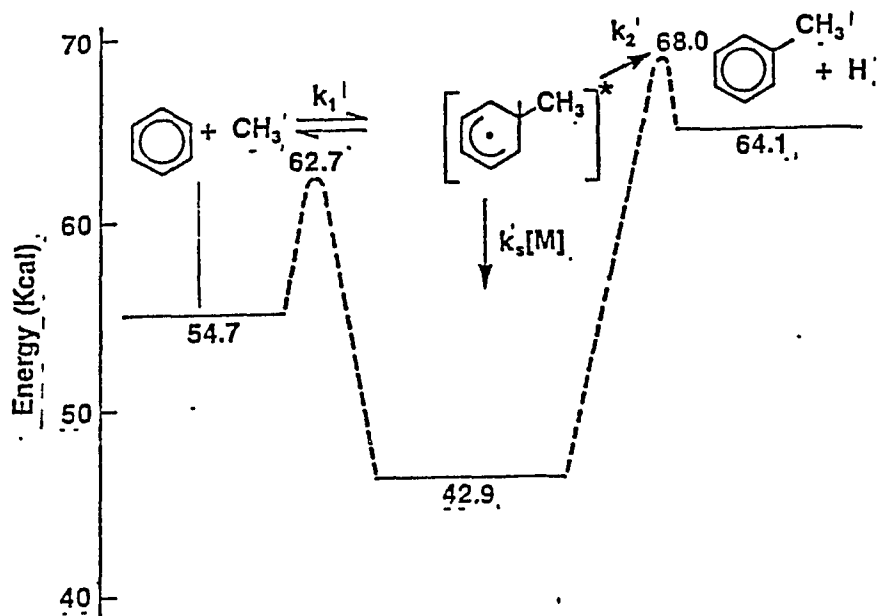


Figure 1.12b

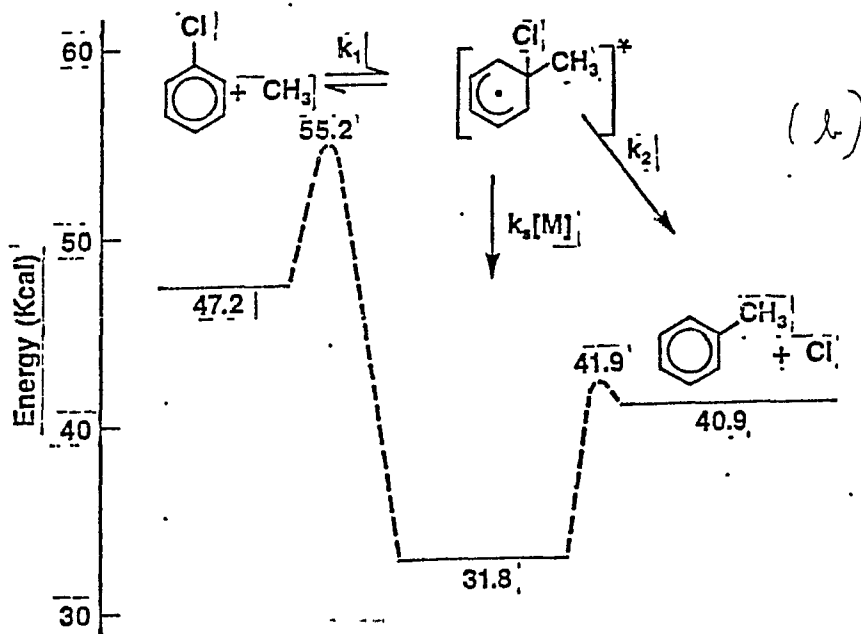


Figure 1.13

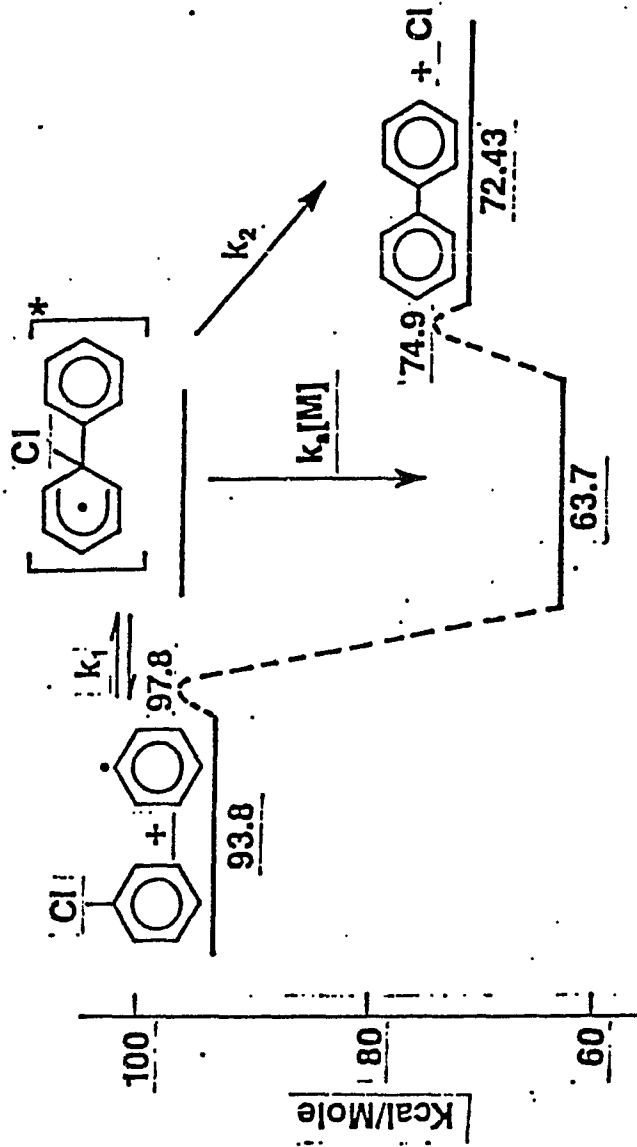
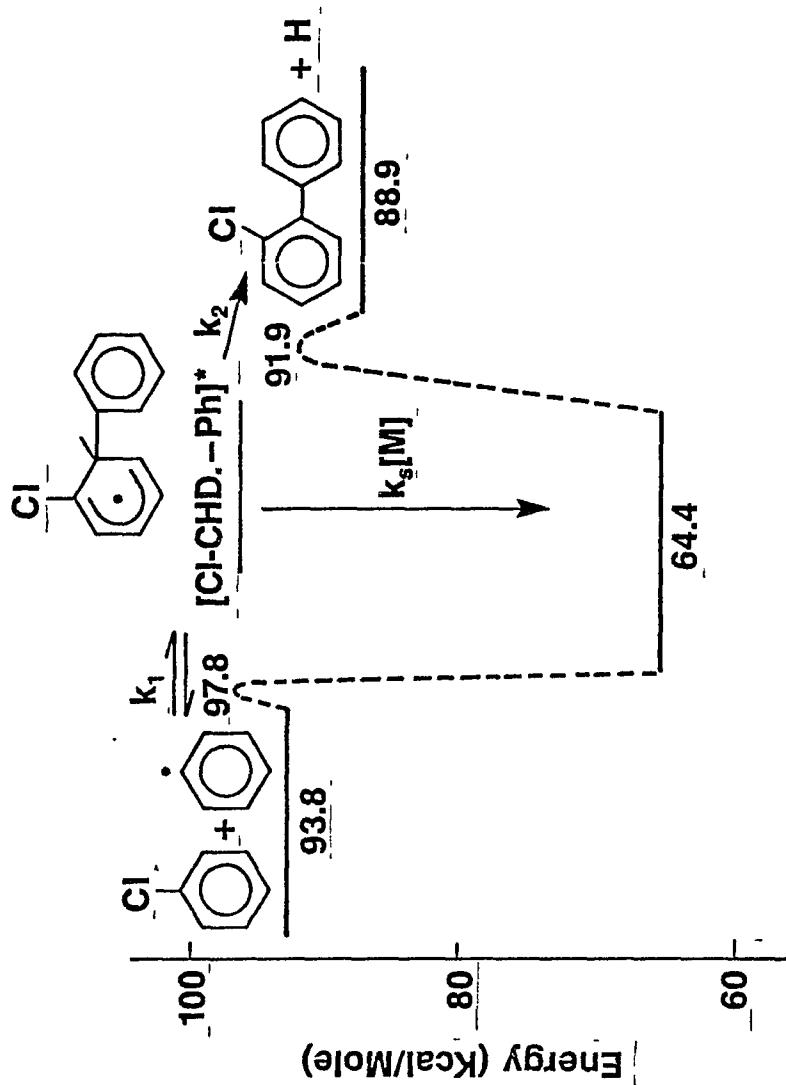
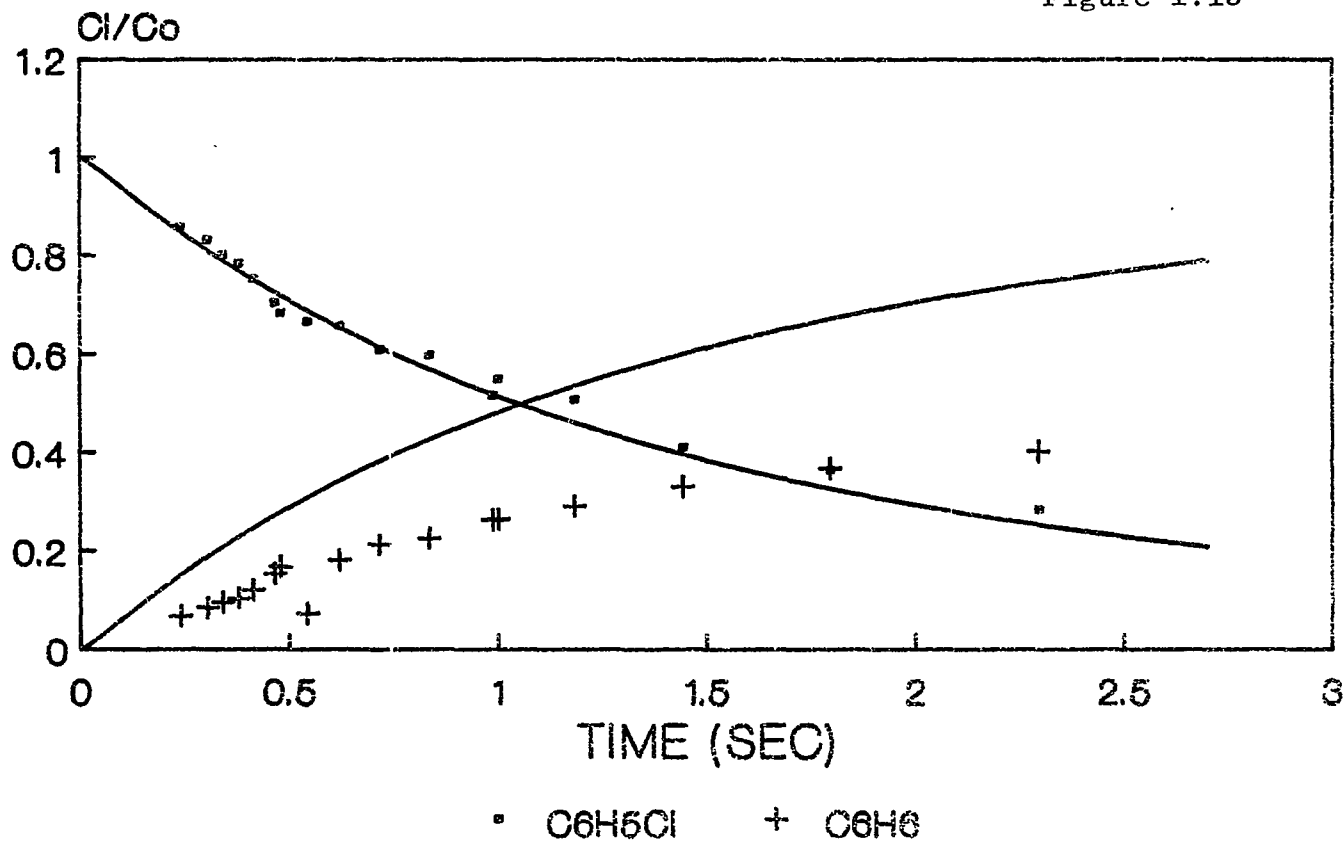


Figure 1.14



PREDICTED VS. OBSERVED BEHAVIOR 1126 K C6H5Cl DECOMPOSITION IN H2

Figure 1.15



PREDICTED VS. OBSERVED BEHAVIOR 1177 K C6H5Cl DECOMPOSITION IN H2

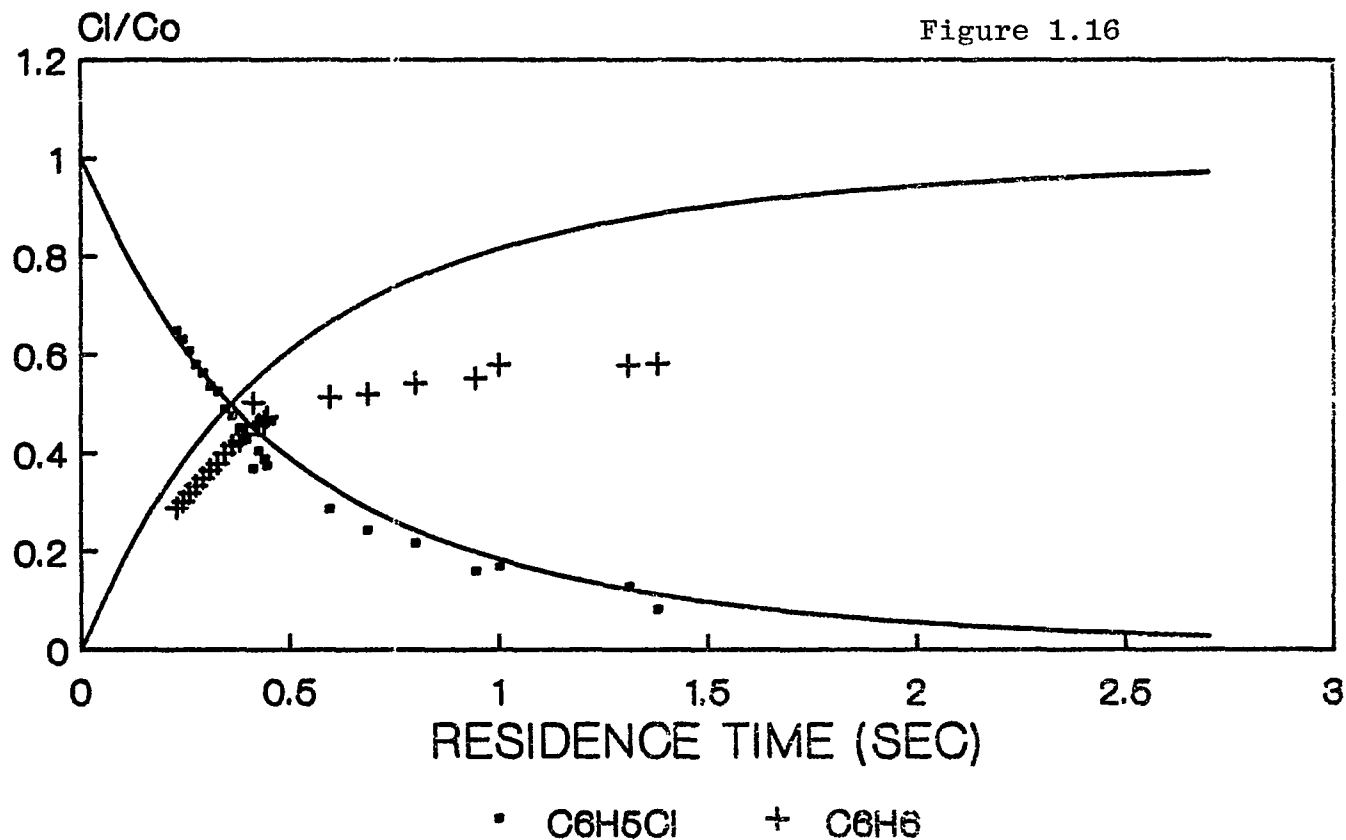


Figure 1.17

DETAILED KINETIC MODEL ACCOUNTS FOR OBSERVED DECAY OF OF CHLOROBENZENE

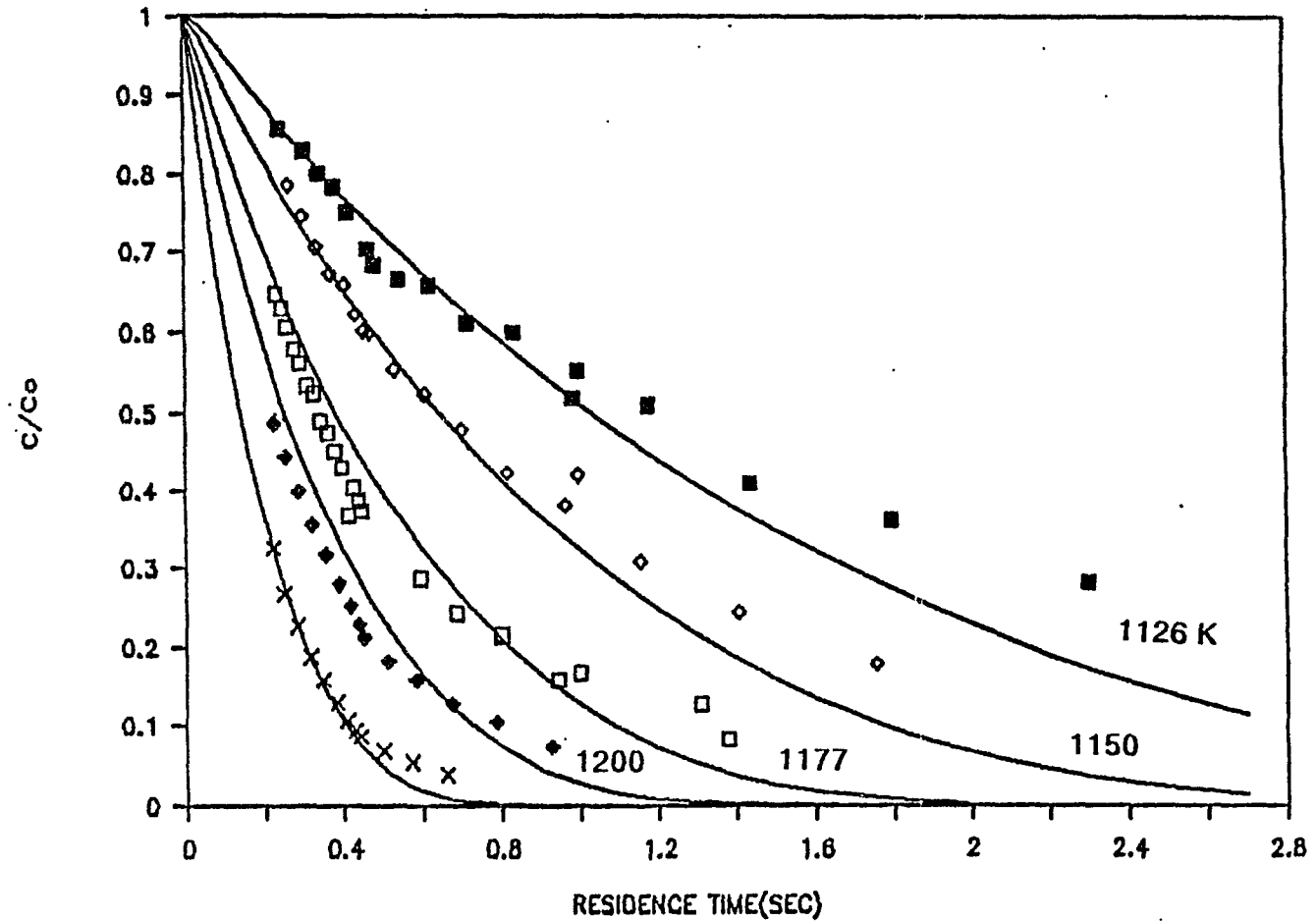
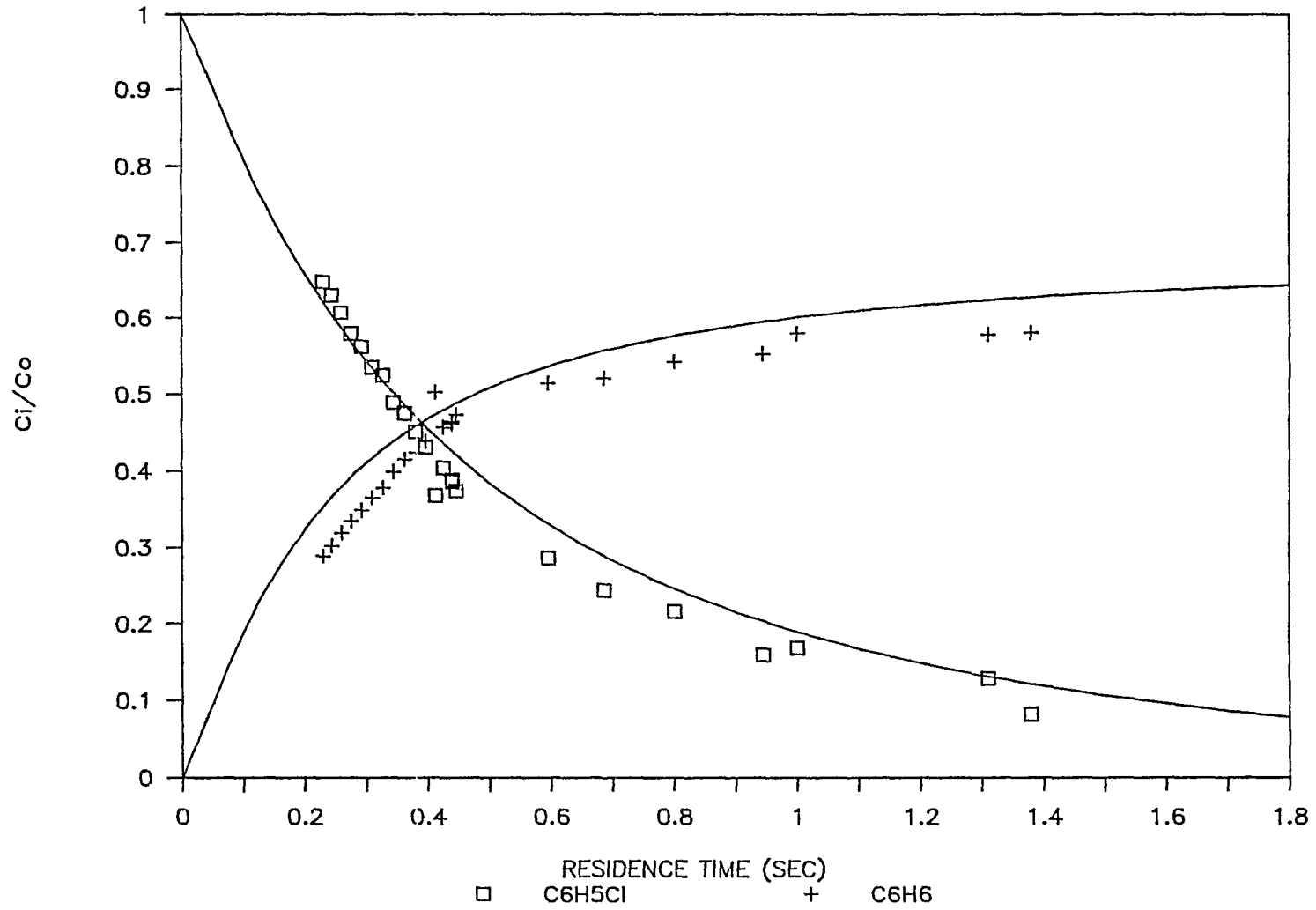


Figure 1.18

PREDICTED VS. OBSERVED BEHAVIOR 1177 K

C6H5Cl DECOMPOSITION IN H2



APPENDIX I - C

THERMO DATA FOR MECHANISM

SPECIES	HF(298)	S(298)	CP300	CP500	CP800	CP1000	CP1500	CP2000	FORMULA
CH3	34.82	46.38	9.26	10.81	12.90	14.09	16.26	17.56	CH3
CH4	-17.90	44.49	8.49	11.15	14.98	17.13	20.57	22.61	CH4
C2H2	54.19	48.00	10.60	13.03	15.29	16.30	18.34	19.57	C2H2
MECY24PD1	48.10	75.50	23.11	36.37	49.85	55.84	64.70	68.39	C6H7
BICYC6H7	71.86	71.52	27.62	34.98	48.20	55.52	63.32	67.20	C6H7
H	52.11	27.39	4.97	4.97	4.97	4.97	4.97	4.97	H
CYC6H5	81.37	69.20	18.79	30.52	41.70	46.37	53.18	56.21	C6H5
CYC6H6	19.82	64.34	19.55	33.07	48.14	54.77	62.27	67.35	C6H6
CYC6H7	49.86	72.01	20.79	35.11	48.74	54.33	62.34	67.34	C6H7
CHD14	26.16	70.80	22.63	37.47	52.04	58.27	67.47	72.45	C6H8
CHD	25.40	72.49	22.67	37.73	52.30	58.45	67.56	72.55	C6H8
CY13PD5	54.30	62.40	17.24	29.40	39.46	43.13	49.10	53.20	C5H5
CY13PD	32.40	64.20	17.64	30.01	41.29	45.81	52.80	57.30	C5H6
MECY14PD3	48.06	75.36	23.11	36.37	49.85	55.84	64.70	68.39	C6H7
MECY24PD	28.30	73.00	23.03	36.74	51.51	58.23	67.83	73.50	C6H8
NAPTH	36.10	80.21	31.89	52.13	70.77	78.43	90.21	94.66	C10H8
C*CC*C	26.33	66.62	19.22	28.36	36.95	40.57	46.34	49.44	C4H6
C#CC*C.	126.27	69.60	17.50	22.98	27.91	29.93	33.27	34.91	C4H3
ME.CY24PD	75.10	76.42	23.11	36.36	49.64	55.53	64.71	69.20	C6H7
C6H5CH3	11.95	76.41	24.88	40.53	55.73	62.22	71.78	75.20	C7H8
H2	0.00	31.21	6.90	6.99	7.10	7.21	7.72	8.17	H2
CL	28.90	39.47	5.20	5.40	5.35	5.30	5.20	3.14	CL
CL2	-0.01	53.29	8.10	8.59	8.91	8.99	9.10	9.16	CL2
C6H5CL	12.35	74.79	23.27	36.47	47.96	52.41	59.17	61.16	C6H5CL
PHCLPHCL	28.72	112.76	44.07	66.94	86.58	93.99	104.92	108.68	C12H8CL2
C6H5C6H5	43.50	93.85	35.74	59.44	81.20	90.05	103.37	108.73	C12H10
PHPHCL	35.82	105.39	39.90	63.17	83.88	92.03	104.14	108.25	C12H9CL
HCL	-22.06	44.64	6.96	6.99	7.29	7.56	8.10	8.40	HCL
C6H4CL	72.45	77.78	22.92	34.33	45.16	49.86	57.75	61.39	C6H4CL
LINC6H5	136.55	80.70	25.50	36.41	45.21	48.39	53.56	55.10	C6H5
PHCYC6H4	104.47	98.02	38.20	62.11	83.59	92.10	104.90	110.93	C12H9
NAPTH	36.00	79.49	31.92	52.07	70.74	78.27	89.14	94.37	C10H8
BICYC6H7.	68.95	76.97	21.04	35.51	48.62	54.14	63.67	67.32	C6H7
CLCHD.	40.83	82.80	23.45	38.43	51.35	56.29	63.90	67.48	C6H6CL
MECHD.	42.92	79.32	25.76	43.62	59.87	66.44	76.69	82.15	C7H9
ICLMECHD.	31.78	85.62	29.42	47.45	63.00	68.98	78.48	83.27	C7H8CL
PHCHD.	76.05	100.40	38.79	65.90	89.97	99.33	113.26	120.62	C12H11
ICLPHCHD.	64.91	106.70	42.45	69.74	93.11	101.87	115.04	121.75	C12H10CL
CLIPHCHD.	65.36	107.43	42.39	69.22	92.56	101.39	114.35	121.31	C12H10CL

SECTION II

KINETIC STUDY ON THERMAL DECOMPOSITION
OF $m\text{-C}_6\text{H}_4\text{Cl}_2$ DILUTED IN H_2

EXPERIMENTAL RESULTS: m-C₆H₄Cl₂

The decomposition of m-dichlorobenzene (m-C₆H₄Cl₂) in hydrogen at 1 atm. total pressure was observed to follow pseudo-first order kinetics throughout the temperature range studied (1095 - 1225 K). The first order behavior obtained for decomposition at several temperatures is shown in figure 2.1 for reaction in a 4 mm id reactor. Major products were chlorobenzene (C₆H₅Cl), HCl, carbon solids, and benzene (C₆H₆).

Decomposition was found to be most rapid within the 16mm id reactor and slowest within the 4mm id reactor. This trend is the opposite to results obtained for reactions of C₆H₅Cl in H₂ studied at this laboratory under similar conditions (see SECTION I : Results for C₆H₅Cl).^{<1>} It is believed that hydrogen atom loss by surface reaction is responsible for this trend. The production rate of H atoms by reaction of Cl atom with H₂ is believed to be more rapid in this system than in the C₆H₅Cl system for two reasons. There is a higher concentration of Cl atom since m-C₆H₄Cl₂ dissociates to chlorophenyl radical and Cl atom more rapidly and there are more sites of chlorine substitution for the rapid displacement of Cl atom by addition of H atom to occur. The bond dissociation energy for loss of Cl from m-C₆H₄Cl₂ is lower by about 1.5 Kcal/mol ^{<2>} than that for loss of Cl from C₆H₅Cl. It is expected that H atom concentration is higher in this system; and therefore loss of H atom at the reactor wall will

have a more pronounced effect. This H atom loss mechanism is believed to be the same for $m\text{-C}_6\text{H}_4\text{Cl}_2$ and $\text{C}_6\text{H}_5\text{Cl}$ systems, but H atoms are believed to be much more important in the dichlorinated system. The importance of this recombination increases to the point where it dominates over other wall processes (activation) and reverses the direction of the experimentally observed wall effect. It is felt that we are observing chain termination at the wall instead of initiation. H atom concentration will be discussed further with kinetic modeling results later in this paper.

This inhibition by the wall was found to become more important as the surface to volume (S/V) ratio was increased, even though the opposite trend was observed with $\text{C}_6\text{H}_5\text{Cl}$ studies (large S/V accelerating decomposition). The conclusions one arrives at are, however, completely consistent in both data sets regarding the magnitude of this wall effect in larger id reactors. The importance of wall reactions is found to drop as S/V is decreased, with 16mm and 10.5 mm id reactors giving approximately the same results, but 4mm id reactors consistently giving different conversion.

Figure 2.2 illustrates the effect of reactor diameter upon the observed decomposition of $m\text{-C}_6\text{H}_4\text{Cl}_2$ at 1148 K. Reactors of 10.5mm and 16mm id are shown to give virtually identical conversion while reaction is significantly slower in the 4mm id reactor.

Figure 2.3 demonstrates the influence S/V has on the

observed first order decomposition rate constants. It is apparent that wall effects become very important at temperatures above 1200 K for 4mm id reactors. Although large S/V is found to inhibit $m\text{-C}_6\text{H}_4\text{Cl}_2$ decomposition instead of accelerate it, we feel these results are in agreement with trends observed in other studies at this laboratory.^{<3>}

Figure 2.4 presents the normalized concentration of major products (HCl not included) as a function of average residence time, 16 mm id reactor at 1123 K. Reactant concentration decreases steadily reaching 80% conversion by 1.2 sec average residence time. Chlorobenzene concentration increases to a maximum near 35 % after 1 sec and then begins to decrease as it is converted to benzene and solid carbon. Benzene production only rises to 28 % of the $m\text{-C}_6\text{H}_4\text{Cl}_2$ initially present. Nearly 35% of $m\text{-C}_6\text{H}_4\text{Cl}_2$ reagent is converted to solids which accumulated on the reactor tube wall and in exit lines. Carbon solid was estimated from material balance after taking into account the relative response factors of $m\text{-C}_6\text{H}_4\text{Cl}_2$, $\text{C}_6\text{H}_5\text{Cl}$, and C_6H_6 to detection by flame ionization detector (FID).

Several minor products were detected in samples of reactor gas. Minor products present at less than 0.5 mole percent the initial $m\text{-C}_6\text{H}_4\text{Cl}_2$ consistently include cyclopentadiene, toluene, ethylene, methane, naphthalene, biphenyl, chlorobiphenyl isomers, and isomers of dichlorobiphenyl. These observations are in good agreement with

other studies performed at this laboratory ^{<5>} and elsewhere^{<6>}.

The distribution of major products formed at 1 second average residence time are presented as functions of temperature in figure 2.5. 98% decomposition of $m\text{-C}_6\text{H}_4\text{Cl}_2$ occurs by about 900°C. Chlorobenzene production rises to a maximum near 30% the initial $m\text{-C}_6\text{H}_4\text{Cl}_2$ near 850°C and then decreases to near 10% by about 900°C. Benzene yield increases steadily as temperature is increased, rising to nearly 45% the initial $m\text{-C}_6\text{H}_4\text{Cl}_2$ near 900°C. Solid carbon accounts for a minimum of 25% and maximum near 40% the initial $m\text{-C}_6\text{H}_4\text{Cl}_2$. Between 850°C and 900°C carbon solid is the major organic product observed for 1 second average residence time.

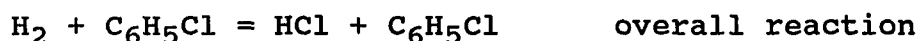
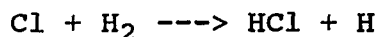
Methylene chloride extracts were obtained from portions of solid carbon deposits and analyzed by GC/Mass Spectrometry. Spectra were obtained for several compounds in the molecular weight range 154 - 380 (see figure 2.6). These compounds are believed to include biphenyl, isomers of chlorobiphenyl and dichlorobiphenyl, in addition to chlorinated terphenyls and triphenylenes.

KINETIC MODELING RESULTS and DISCUSSION:

Bimolecular activated complex/QRRK analysis of Dean^{<7>} is used to account for temperature and pressure effects on apparent rate constants for radical and atom addition reactions to unsaturated bonds. Addition reactions presented here and elsewhere^{<1,8,9>} focus on likely pathways to biphenyls, chlorinated biphenyls, and other species observed in the soot extracts. Required input parameters come from literature or are estimated as noted in the tables that follow. Required geometric mean vibrational frequencies are estimated using the method described in SECTION IV of this thesis and are tabulated in Table II.i along with Lennard-Jones parameters estimated using Lydersen's group method. Due to the large uncertainties in these estimates, L-J parameters for stable molecules were used for the radical adducts. For example, the L-J parameters for chlorophenyl cyclohexadienyl radical were taken to be those estimated for chlorobiphenyl, which differs by only an H atom. This is not expected to cause serious error since QRRK calculations are not sensitive to small changes in L-J parameters.

The initial reaction occurring when $m\text{-C}_6\text{H}_4\text{Cl}_2$ is pyrolyzed is dissociation to m -chlorophenyl radical ($m\text{-C}_6\text{H}_4\text{Cl}$) and Cl atom. These radicals produced by initial unimolecular decay react rapidly with H_2 (if present) to generate $\text{C}_6\text{H}_5\text{Cl}$ and HCl in addition to reactive H atoms. H atom addition to the Cl-Carbon bond in $m\text{-C}_6\text{H}_4\text{Cl}_2$ (attack at

ipso positions) forms an energized complex and results in rapid decomposition of the adduct to $C_6H_5Cl + Cl$, the low energy exit channel. An energy diagram for this reaction appears in figure 2.7. This reaction is believed to be a major pathway in the hydrodechlorination of chlorinated benzenes and all chlorinated unsaturates under our conditions (H_2 in excess). Virtually every dichloro-cyclohexadienyl radical complex which is formed dissociates by loss of Cl atom before stabilization of the complex can occur at these temperatures. This occurs because the exit barrier is small compared with that for dissociation back to reactants. QRRK calculations show that the rate constant for displacement of Cl by H atom essentially has no pressure dependence even though it is not an elementary reaction. Parameters used in these calculations appear in Table II.ii. The apparent rate constant for reaction to $C_6H_5Cl + Cl$ is simply the rate constant for formation of the adduct, $2.0 \times 10^{13} \exp(-7,500 \text{ Kcal/mol}/RT)$. H atom addition to C_6H_5Cl will produce $C_6H_6 + Cl$ atom passing through an analogous chloro-cyclohexadienyl intermediate.^{<1>}



Phenyl addition to C_6H_6 will yield some biphenyl product, while addition to C_6H_5Cl will produce both biphenyl and chlorobiphenyl products, passing through a substi-

tuted cyclohexadienyl intermediate. These systems have been discussed elsewhere (see SECTION I).

Phenyl and chlorophenyl radical addition to chlorinated benzenes can be divided into two groups; ipso addition (at a position of chlorine substitution) and addition at a Carbon-H bond. Addition at an ipso position will result in rapid reaction to a biphenyl (chlorobiphenyl) + Cl. Fahr and Stein^{<11>} have shown that phenyl migration is much slower than complex dissociation. Therefore, phenyl must add to the site of chlorine substitution for a displacement reaction to occur.

As an example we shall consider $m\text{-C}_6\text{H}_4\text{Cl}$ radical addition to the ipso position of $\text{C}_6\text{H}_5\text{Cl}$. Dissociation of the chlorophenyl-chloro-cyclohexadienyl radical complex back to $m\text{-C}_6\text{H}_4\text{Cl} + \text{C}_6\text{H}_5\text{Cl}$ is nearly 25 Kcal/mol more endothermic than dissociation to chlorobiphenyl + Cl products. An energy diagram for this reaction is presented in figure 2.8. Despite the size of this adduct (MW 223), stabilization is of little importance even at 1 atm and low temperature (300 K) see figure 2.9. This reaction is analogous to that of H addition to a position of chlorine substitution in that the reaction to products essentially proceeds at the rate of formation of the complex. Figure 2.9 shows the pressure dependence for apparent rate constants in this system at 300 and 2000 K. Reaction to products is found to dominate at all pressures with dissociation to reactants of little importance even at temperatures near

2000 K. Table II.iii summarizes parameters used in these QRRK calculations in addition to the apparent rate constants calculated as functions of temperature for reaction at 1 atm in H₂ bath gas.

Addition of m-C₆H₄Cl to a site of chlorine substitution results in rapid reaction since the energetics of this system favor the displacement reaction products over dissociation back to reactants. This is not the case, however, for addition to a carbon-H bond. As an example we shall examine m-C₆H₄Cl radical addition to C₆H₅Cl (non ipso). In this case, dissociation to products is only about 6 Kcal/mol less endothermic than that for dissociation to reactants (see figure 2.10). As one might expect, stabilization and dissociation to reactants (no reaction) are significantly more important in this case. Such a system is expected to have unusual pressure and temperature dependence for apparent rate constants. Figure 2.11 shows the non-Arrhenius behavior of apparent rate constants for this system at 1 atm pressure. Reaction to products is shown to drop sharply at low temperatures. This is due in part to the increase in stabilization of the adduct. The rate constant for stabilization is found to dominate at low temperatures, pass through a maximum near 800 K, and then to decrease at higher temperatures as reaction to products and dissociation back to reactants begin to dominate.

The Arrhenius like behavior for the displacement reaction of m-C₆H₄Cl plus C₆H₅Cl (discussed earlier) is

also shown for comparison. The relative barrier height for inlet and exit channels is shown to have dramatic effect upon the temperature dependence for these addition reactions to aromatics. In a system where the barrier for dissociation to products is significantly lower than for dissociation back to reactants, such as with ipso attack, Arrhenius like behavior is expected. On the other hand, when the barrier for dissociation to products is similar to that for dissociation back to reactants, such as addition at a carbon-H bond, unusual pressure and temperature (non-Arrhenius) effects are observed. Input parameters used in these QRRK calculations in addition to apparent rate constants calculated for H₂ bath gas are presented in Tables II.iii and II.iv.

Another important route to dichlorobiphenyl formation during dichlorobenzene pyrolysis is ipso m-C₆H₄Cl addition to m-C₆H₄Cl₂. An energy diagram is presented for this reaction in figure 2.12. This system is analogous to the cases discussed above where a low energy exit channel is available. Reaction to products is found to dominate with stabilization and dissociation of the adduct back to reactants of little or no importance. Temperature dependence for reaction to dichlorobiphenyl + Cl at 1 atm total pressure follows:

$$k = 4.1 \times 10^{13} T^{-0.4} \exp(-4.82 \text{ Kcal/mol/RT}).$$

Phenyl radical (C₆H₅) may also add to m-C₆H₄Cl₂ to form either chlorobiphenyl or dichlorobiphenyl depending

upon the position of addition. These reactions are analogous to those discussed above. Rate parameters determined for these addition reactions are presented in tables II.v and II.vi along with input data used for these QRRK calculations. The behavior of these additions are similar to the chlorophenyl additions to C_6H_5Cl discussed previously, with ipso addition resulting in reaction to products for nearly every complex formed while addition at a non-ipso position produces a more complex temperature and pressure dependence.

Terphenyls result from subsequent phenyl and chlorophenyl additions to biphenyl species. These additions are complicated by differing thermodynamic properties for the different positional isomers. Formation of ortho and meta terphenyls, which doubles the number of combinations which need to be examined, will be considered separately.

Figure 2.13 is an energy diagram for $m-C_6H_4Cl$ radical addition to dichlorobiphenyl at a position of chlorine substitution. The energetics of this system favor loss of Cl (the low energy exit channel). Activated complex/QRRK calculations suggest that nearly 100% of collisions which form the energized complex, dissociate by loss of Cl.

Figure 2.14 shows the pressure dependence for apparent rate constants obtained for this system at 1000 K. Reaction to products proceeds at the rate of formation of the complex. At 1 atm (760 torr), stabilization accounts for only about 1% of collisions, while at 10 atm it accounts

for only 10%. Dissociation of the adduct back to reactants is unimportant.

Figure 2.15 is an energy diagram for $m\text{-C}_6\text{H}_4\text{Cl}$ addition at a position ortho to the phenyl-phenyl bond in chlorobiphenyl. The carbon/carbon bond formed is stronger by about 5 Kcal/mol than the carbon/hydrogen bond in the complex. As a result, some of this complex will dissociate by loss of H atom. The primary route of dissociation, however, is back to reactants as a result of the unfavorable entropy change for the displacement of H atom. Calculations show that greater than 47.5% of collisions forming the complex dissociate back to reactants, 52% are stabilized, and only 0.5% dissociate by loss of H atom to form dichlorinated terphenyl at 1000 K and 1 atm. Addition of $m\text{-C}_6\text{H}_4\text{Cl}$ to a carbon/hydrogen position meta to the phenyl/phenyl bond is slightly more favorable due to the fact that meta-terphenyls are less sterically hindered and therefore more stable than are ortho-terphenyls. The carbon/carbon bond formed from addition to a meta hydrogen is stronger by nearly 7.5 kcal/mol than the carbon/hydrogen bond which must break for reaction to terphenyl + H to occur. This phenylation at a meta hydrogen is expected to be about 2.4 Kcal/mol more exothermic than phenylation at an ortho position due to the hindered internal rotation in an ortho-terphenyl. The entropy change for this reaction is also slightly more favorable (also due to the hindered internal rotation in the ortho-terphenyl).

Twelve of the various combinations for phenyl/chlorophenyl additions to biphenyls have been examined with input parameters and apparent rate constants tabulated in tables II.xv - II.xix. For additions where stabilization is important at our conditions we must also consider the thermal dissociation of the complex to both products and reactants. This is done using unimolecular QRRK theory of Dean et al.^{<7>}

Triphenylenes may result from reaction of the o-terphenyl radical with itself (condensation). The o-terphenyl radicals may be produced by abstraction of an ortho hydrogen by Cl, H, or aryl radical. Figure 2.16 is an energy diagram showing conversion of o-terphenyl radical to triphenylene + H atom. In this case the carbon/carbon bond which is formed from this isomerization is stronger by nearly 15 Kcal/mol than the carbon/hydrogen bond in the complex. Calculations show reaction to triphenylene + H to be the dominant reaction channel with stabilization of little importance above 800 K. The pressure dependence for these rate constants are compared in figure 2.17 demonstrating again that addition rate constants for reactions which have low energy exit channels available (ie, those which are more than 10 kcal/mol exothermic) exhibit little pressure dependence. Two additional examples for chlorinated triphenylene formation have been examined and input parameters and results for these systems are presented in tables II.xx - II.xxii.

We have developed a detailed reaction mechanism for $m\text{-C}_6\text{H}_4\text{Cl}_2$ pyrolysis in hydrogen which appears in Table II.xxiii. Elementary reaction rate parameters for abstraction reactions are based upon literature comparison, thermodynamic estimations and Transition State Theory methods of Benson.^{<12>} Qrrk calculations, as described above and elsewhere^{<1>}, were used to estimate apparent rate parameters for addition and dissociation reactions (1 atm).

Experimental pyrolysis data are compared with model predictions for $m\text{-C}_6\text{H}_4\text{Cl}_2$ reactions at 1095 and 1198 K in figures 2.18 and 2.19. Predictions for $m\text{-C}_6\text{H}_4\text{Cl}_2$ loss match experiment well. Predictions for $\text{C}_6\text{H}_5\text{Cl}$ formation and loss show slightly less agreement, but still match observed trends well. Prediction of benzene formation, on the other hand, is not quite as good except at low conversion. Modeling suggests that the phenyl/chlorophenyl addition reactions discussed earlier cannot explain the rapid solid carbon formation which is observed in this system by themselves.

Figure 2.20 compares predicted and experimental decomposition curves as function of residence time for several temperatures. Table II.xxiii contains only those reactions which are specific to $m\text{-C}_6\text{H}_4\text{Cl}_2$ pyrolysis, but our model contains the subset of reactions used in our separate study of $\text{C}_6\text{H}_5\text{Cl}$ decomposition. These reactions have been discussed elsewhere (see SECTION I : Results for $\text{C}_6\text{H}_5\text{Cl}$). Our model is a first principles description of the

m-C₆H₄Cl₂ chain decomposition, and we feel predictions shown are quite acceptable.

Rate parameters for reactions appearing in Table II.xxiii were varied over small intervals to obtain a better fit of our experimental data. Rate constants were required to be consistent with all reactions of the C₆H₅Cl mechanism. The A factor for m-C₆H₄Cl₂ dissociation to m-C₆H₄Cl radical and chlorine atom (6.0E+15) was set equal to that for C₆H₅Cl decomposition on a per Cl basis.

The high pressure A factor for hydrogen atom addition to m-C₆H₄Cl₂ (ipso position) was taken as being between 1.5E+13 and 3.0E+13, with an Ea the same as that determined for H atom addition to C₆H₅Cl^{<1>}. Abstraction of hydrogen from H₂ by chlorophenyl radical was assumed to have an activation energy (Ea) of 9.0 kcal/mol; the same as that used in our C₆H₅Cl study. These reactions along with the H atom recombination H + H + M = H₂ + M were found to have the greatest influence on concentrations predicted by our model.

Attempts to model carbon formation using an equilibrium approach and irreversible bleed reactions are discussed in SECTION I.

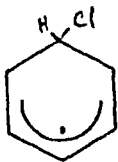
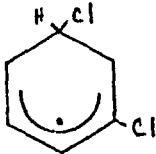
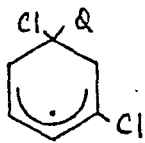
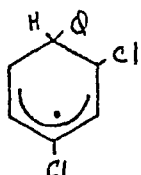

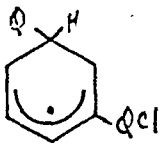
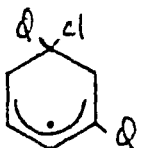
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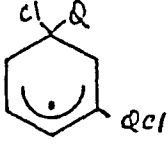
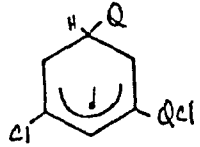
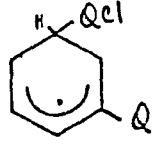
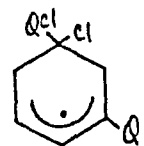
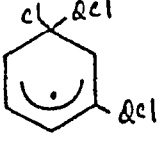
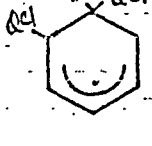
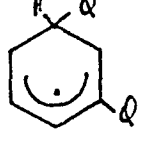
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APPENDIX II-A

TABLES for SECTION II

TABLE II.i
 PROPERTIES FOR RADICAL ADDUCTS CONSIDERED FOR QRRK ANALYSIS

NAME	STRUCTURE	FORMULA MW	ω_{gm} (cm^{-1})	σ (A)	e/k (K)
CLCHD.		C_6H_5Cl (113)	1110	5.69	526.9
CL2CHD.		$C_6H_4Cl_2$ (147)	1000	6.10	571.5
BPH1R		$C_{12}H_9Cl_2$ (223)	975	7.01	658.9
BPH2R		$C_{12}H_9Cl_2$ (223)	977	"	"
BPH3R		$C_{12}H_9Cl_2$ (223)	956	"	"
TPH1R		$C_{18}H_{14}Cl$ (265)	925	7.73	760.2
TPH2R		$C_{18}H_{14}Cl$ (265)	980	"	"

NAME	STRUCTURE	FORMULA MW	w _{gm} (cm ⁻¹)	σ (Å)	e/k (K)
TPH3R		C ₁₈ H ₁₃ Cl ₂ (299)	936	7.91	781.2
TPH4R		C ₁₈ H ₁₃ Cl ₂ (299)	950	"	"
TPH5R		C ₁₈ H ₁₄ Cl (265)	925	7.73	760.2
TPH6R		C ₁₈ H ₁₃ Cl ₂ (299)	936	7.91	781.2
TPH7R		C ₁₈ H ₁₂ Cl ₃ (333)	893	8.10	803.4
TPH8R		C ₁₈ H ₁₃ Cl ₂ (299)	866	7.91	781.2
TPH9R		C ₁₈ H ₁₅ (231)	985	7.53	731.7

NAME	STRUCTURE	FORMULA MW	w _{gm} (cm ⁻¹)	σ (Å)	e/k (K)
TPH10R		C ₁₈ H ₁₅ (231)	985	7.53	731.7
TPH11R		C ₁₈ H ₁₃ Cl ₂ (299)	866	7.91	781.2
TPH12R		C ₁₈ H ₁₄ Cl (265)	925	7.73	760.2
TPHF1R		C ₁₈ H ₁₃ (229)	1040	7.68	738.8
TPHF2R		C ₁₈ H ₁₁ Cl ₂ (297)	930	8.37	748.3

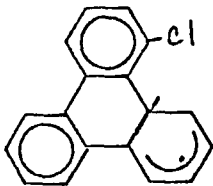
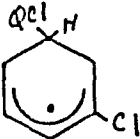
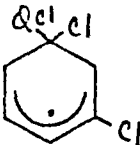
NAME	STRUCTURE	FORMULA	w_{CD}^1 (cm^{-1})	σ (\AA)	e/k (K)
TPHF3R		$\text{C}_{18}\text{H}_{12}\text{Cl}$ (262)	985	7.86	744.6
CLIPCLCD.		$\text{C}_{12}\text{H}_9\text{Cl}_2$ (223)	967	7.01	658.9
R46CLIPCL		$\text{C}_{12}\text{H}_8\text{Cl}_3$ (257)	901	7.23	698.4

TABLE II.ii



k	A*	E _a **	source
1	2.0 E+13	7.5	a
-1	1.19E+13	34.86	a
2	7.9 E+13	12.2	b

^a This work, reverse reaction (k-1) from thermodynamics.

^b Based upon entropy change for $\text{Cl} + \text{C}_6\text{H}_5\text{Cl} \rightleftharpoons [\text{CL}_2\text{CHDR}]$
with $A_{-2} = 1.2\text{E}+13$ cc/mol sec. $E_{-2} = 2\text{kcal/mol}$.

UNITS:

* A_1 (cc/mol sec)

A_2 (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H_2 BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	H+PHCL ₂ = C ₆ H ₅ CL + CL	2.0E+13	0.0	7.5	i
760.0	"	2.96E+13	-0.05	7.63	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.iii



k	A*	E _a **	source
1	1.0 E+12	4.3	a
-1	2.33E+15	33.14	a
2	2.9 E+14	8.87	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics.

^b Based upon entropy change for Cl + PhPhCl = [BPH₃R] with A₋₂ = 6.0E+12 cc/mol sec per site of attack. E₋₂ = 2 kcal/mol

UNITS:

* A₁ (cc/mol sec)
A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₄ Cl+C ₆ H ₅ Cl=PhPhCl+Cl	1.5E+12	-0.06	4.36	i
760.0	"	1.78E+12	-0.08	4.41	"

i valid from 300 - 2000 K
ii " " 800 - 1500 K
iii " " 800 - 2000 K

TABLE II.iv



k	A*	E _a **	source
1	2.0 E+12	4.3	a
-1	3.68E+15	31.78	a
2	7.09E+13	25.60	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 5 sites for attack at H.

^b Based upon entropy change for H + PhClPhCl = [CLIPCLCD] with A₋₂ = 1.0E+13 cc/mol sec per site of attack and 2 sites for attack. E₋₂ = 4.3 kcal/mol.

UNITS:

* A₁ (cc/mol sec)
A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₄ Cl + C ₆ H ₅ Cl = PhClPhCl + H	4.4E+20	-2.76	7.47	i
760.0	"	6.79E+60	-14.00	38.67	ii
7.6	C ₆ H ₄ Cl + C ₆ H ₅ Cl = [CLIPCLCD.] ^o	2.5E+71	-18.99	21.01	"
760.0	"	6.97E+86	-22.39	39.37	"

i valid from 300 - 2000 K
ii " " 800 - 1500 K
iii " " 800 - 2000 K

TABLE II.v



k	A*	E _a **	source
1	2.0 E+12	4.3	a
-1	4.9 E+15	37.42	a
2	5.75E+14	12.15	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics.

^b Based upon entropy change for Cl + PhPhCl = [BPH1R] with A₋₂ = 6.0E+12 cc/mol sec per site of attack. E₋₂ = 2 kcal/mol.

UNITS:

* A₁ (cc/mol sec)
A₂ (1/sec)

** Ea (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	Ea (kcal/mol)	range
7.6	C ₆ H ₅ +PHCL ₂ = PhPhCl+Cl	2.85+12	-0.05	4.35	i
760.0	"	4.87E+12	-0.11	4.52	"

i valid from 300 - 2000 K
ii " " 800 - 1500 K
iii " " 800 - 2000 K

TABLE II.vi



k	A*	E _a **	source
1	1.3 E+12	4.3	a
-1	3.06E+15	38.22	a
2	1.11E+14	30.77	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 4 sites for attack at H.

^b Based upon entropy change for $\text{H} + \text{PhClPhCl} = [\text{BPH}_2\text{R}]$ with $A_2 = 1.3\text{E}+13$ cc/mol sec per site of attack and 1 sites for attack. $E_{-2} = 4.3$ kcal/mol.

UNITS:

* A_1 (cc/mol sec)
 A_2 (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H_2 BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	$\text{C}_6\text{H}_5 + \text{PHCL}_2 = \text{PhClPhCl} + \text{H}$	2.7E+32	-5.95	17.36	iii
760.0	"	2.62E+57	-12.69	42.38	"
7.6	$\text{C}_6\text{H}_5 + \text{PHCL}_2 = [\text{BPH}_2\text{R}]^\circ$	7.21+86	-23.08	33.49	ii
760.0	"	1.12E+80	-20.10	39.45	iii

i valid from 300 - 2000 K
 ii " " 800 - 1500 K
 iii " " 800 - 2000 K

TABLE II.vii



k	A*	E _a **	source
1	2.0 E+12	4.3	a
-1	4.6 E+16	37.84	a
2	5.91E+14	11.90	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 2 sites for attack.

^b Based upon entropy change for Cl + PhClPhCl = [R₄6ClIPCl] with A₂ = 6.0E+12 cc/mol sec per site of attack and 2 sites for attack. E₂ = 2 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

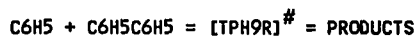
P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₄ Cl+PhCl ₂ =PhClPhCl+Cl	2.25+13	-0.33	4.64	i
760.0	"	4.06E+13	-0.40	4.82	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.viii



k	A*	E _a **	source
1	1.3 E+12	4.3	a
-1	2.10E+15	30.90	a
2	6.42E+13	24.20	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 4 sites for attack at H.

^b Based upon entropy change for $\text{H} + \text{MPH}_3 = [\text{TPH}_9\text{R}]$ with $A_{-2} = 2.7\text{E}+13$ cc/mol sec and 4 sites for attack. $E_{-2} = 4.3$ kcal/mol.

UNITS:

* A_1 (cc/mol sec)
 A_2 (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H_2 BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	$\text{C}_6\text{H}_5 + \text{C}_6\text{H}_5\text{C}_6\text{H}_5 = \text{MPH}_3 + \text{H}$	9.34E+23	-3.66	10.16	iii
760.0	"	2.57E+71	-16.91	47.26	ii
7.6	$\text{C}_6\text{H}_5 + \text{C}_6\text{H}_5\text{C}_6\text{H}_5 = [\text{TPH}_9\text{R}]^\circ$	7.80+65	-17.43	17.69	ii
760.0	"	7.22E+86	-22.37	40.19	iii

i valid from 300 - 2000 K
 ii " " 800 - 1500 K
 iii " " 800 - 2000 K

TABLE II.ix



k	A*	E _a **	source
1	1.3 E+12	4.3	a
-1	2.10E+15	30.90	a
2	2.80E+13	26.33	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 4 sites for attack at H.

^b Based upon entropy change for H + OPH₃ = [TPH10R] with A₂ = 2.0E+13 cc/mol sec and 2 sites for attack. E₋₂ = 4.3 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₅ +C ₆ H ₅ C ₆ H ₅ =OPH ₃ + H	1.38E+24	-3.84	11.31	iii
760.0	"	3.91E+74	-17.91	51.36	ii
7.6	C ₆ H ₅ +C ₆ H ₅ C ₆ H ₅ =[TPH10R] ^o	2.07E+80	-21.55	26.09	ii
760.0	"	7.19E+86	-22.31	40.81	iii

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.x



k	A*	E _a **	source
1	6.7 E+11	4.3	a
-1	7.87E+15	30.70	a
2	3.69E+13	26.33	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 1 site for attack at H.

^b Based upon entropy change for $\text{H} + \text{OPH3Cl} = [\text{TPH12R}]$ with $A_2 = 1.3\text{E}+13$ cc/mol sec and 1 sites for attack. $E_{-2} = 4.3$ kcal/mol.

UNITS:

* A_1 (cc/mol sec)

A_2 (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H_2 BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	$\text{C}_6\text{H}_5 + \text{PhPhCl} = \text{OPH3Cl} + \text{H}$	7.60E+18	-2.56	7.84	i
760.0	"	4.26E+71	-17.34	47.85	ii
7.6	$\text{C}_6\text{H}_5 + \text{PhPhCl} = [\text{TPH12R}]^0$	1.55E+70	-18.93	18.45	ii
760.0	"	7.20E+86	-22.61	38.63	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xi



k	A*	E _a **	source
1	6.7 E+11	4.3	a
-1	5.28E+15	31.26	a
2	6.27E+13	24.82	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 1 site for attack at H.

^b Based upon entropy change for H + MPH3CL = [TPH1R] with A₂ = 1.3E+13 cc/mol sec and 1 sites for attack. E₂ = 4.3 kcal/mol.

UNITS:

* A₁ (cc/mol sec)
A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₅ +PhPhCl=MPH3Cl + H	6.48E+21	-3.28	8.24	iii
760.0	"	5.26E+73	-17.82	47.83	ii
7.6	C ₆ H ₅ + PHCL2 = [TPH1R] ^o	2.68E+68	-18.39	17.88	i
760.0	"	7.23E+86	-22.59	38.89	"

i valid from 300 - 2000 K
ii " " 800 - 1500 K
iii " " 800 - 2000 K

TABLE II.xii



k	A*	E _a **	source
1	1.0 E+12	4.3	a
-1	2.25E+16	33.69	a
2	4.93E+14	9.45	b

^a Louw, R.; Dijks, J.H.; Mulder, P. *J. Chem. Soc. Perkin Trans. II*, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 1 site for attack.

^b Based upon entropy change for Cl + MPH3 = [TPH2R] with A₂ = 6.0E+12 cc/mol sec per site of attack and 2 sites for attack. E₂ = 2 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

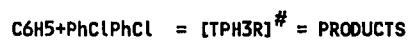
P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₅ + PhPhCl = MPH ₃ + Cl	5.65+12	-0.23	4.54	i
760.0	"	8.78E+12	-0.29	4.68	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xiii



k	A*	E _a **	source
1	1.5 E+12	4.3	a
-1	2.0 E+16	33.7	a
2	1.77E+15	8.86	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 2 sites for attack.

^b Based upon entropy change for Cl + MPH₃Cl = [TPH₃R] with A₂ = 6.0E+12 cc/mol sec per site of attack and 1 site for attack. E₂ = 2 kcal/mol.

UNITS:

* A₁ (cc/mol sec)
A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₅ + PhClPhCl=MPH ₃ Cl+Cl	5.89+12	-0.18	4.49	i
760.0	"	8.21E+12	-0.22	4.60	"

i valid from 300 - 2000 K
ii " " 800 - 1500 K
iii " " 800 - 2000 K

TABLE II.xiv



k	A [*]	E _a ^{**}	source
1	6.7 E+11	4.3	a
-1	8.5 E+15	33.9	a
2	8.47E+13	25.20	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 1 site for attack.

^b Based upon entropy change for H + MPH₃Cl₂ = [TPH₄R] with A₋₂ = 1.3E+13 cc/mol sec per site of attack and 1 site for attack. E₋₂ = 4.3 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

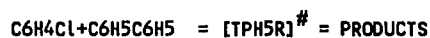
P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₅ + PhClPhCl=MPH ₃ Cl ₂ +H	2.17+27	-4.79	11.52	iii
760.0	"	8.35E+77	-18.94	50.81	ii
7.6	C ₆ H ₅ +PhClPhCl = [TPH ₄ R] ^o	7.59E+74	-20.16	22.48	"
760.0	"	7.22E+86	-22.51	39.73	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xv



k	A*	E _a **	source
1	1.3 E+12	4.3	a
-1	2.3 E+15	31.32	a
2	6.26E+13	23.90	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. 11, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 4 sites for attack.

^b Based upon entropy change for H + MPH₃CL = [TPH₅R] with A₂ = 1.3E+13 cc/mol sec per site of attack and 1 site for attack. E₂ = 4.3 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

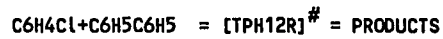
P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₄ Cl+C ₆ H ₅ C ₆ H ₅ =MPH ₃ Cl+H	1.48+25	-3.99	10.83	iii
760.0	"	2.35E+72	-17.17	47.87	ii
7.6	C ₆ H ₄ Cl+C ₆ H ₅ C ₆ H ₅ =[TPH ₅ R] ^o	1.54E+65	-17.21	17.43	"
760.0	"	7.20E+86	-22.36	40.33	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xvi



k	A*	E _a **	source
1	1.3 E+12	4.3	a
-1	2.3 E+15	31.32	a
2	3.73E+13	26.33	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 4 sites for attack.

^b Based upon entropy change for H + OPH3Cl = [TPH12R] with A₂ = 1.3E+13 cc/mol sec per site of attack and 1 site for attack. E₂ = 4.3 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₄ Cl + C ₆ H ₅ C ₆ H ₅ = OPH ₃ Cl + H	4.51E+36	-7.42	18.91	ii
760.0	"	1.18E+76	-18.29	52.61	"
7.6	C ₆ H ₄ Cl + C ₆ H ₅ C ₆ H ₅ = [TPH12R] ^o	1.29E+82	-22.06	27.19	"
760.0	"	7.18E+86	-22.30	40.94	"

i valid from 300 - 2000 K
 ii " " 800 - 1500 K
 iii " " 800 - 2000 K

TABLE II.xvii



k	A*	E _a **	source
1	6.7 E+11	4.3	a
-1	5.77E+15	31.05	a
2	2.84E+13	26.60	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 2 sites for attack.

^b Based upon entropy change for $\text{H} + \text{OPH}_3\text{Cl}_2 = [\text{TPH}_8\text{R}]$ with $A_{-2} = 2.0\text{E}+13$ cc/mol sec per site of attack and 2 site for attack. $E_{-2} = 4.3$ kcal/mol.

UNITS:

* A_1 (cc/mol sec)
 A_2 (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H_2 BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	$\text{C}_6\text{H}_4\text{Cl} + \text{PhPhCl} = \text{OPH}_3\text{Cl}_2 + \text{H}$	6.42E+19	-2.84	8.30	ii
760.0	"	1.06E+74	-18.04	49.54	"
7.6	$\text{C}_6\text{H}_4\text{Cl} + \text{PhPhCl} = [\text{TPH}_8\text{R}]^\circ$	3.17E+72	-19.58	19.84	"
760.0	"	7.17E+86	-22.59	38.81	"

i valid from 300 - 2000 K
 ii " " 800 - 1500 K
 iii " " 800 - 2000 K

TABLE II.xviii



k	A*	E _a **	source
1	1.0 E+12	4.3	a
-1	3.2 E+16	33.8	a
2	5.3 E+14	8.86	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 1 site for attack.

^b Based upon entropy change for $\text{Cl} + \text{MPH}_3\text{Cl} = [\text{TPH}_6\text{R}]$ with $A_{-2} = 6.0\text{E}+12$ cc/mol sec per site of attack and 1 site for attack. $E_{-2} = 2$ kcal/mol.

UNITS:

* A_1 (cc/mol sec)

A_2 (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H_2 BATH GAS)

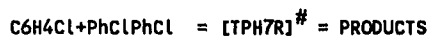
P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	$\text{C}_6\text{H}_4\text{Cl} + \text{PhPhCl} = \text{MPH}_3\text{Cl} + \text{Cl}$	5.12+12	-0.22	4.53	i
760.0	"	7.12E+12	-0.26	4.63	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xix



k	A*	E _a **	source
1	1.5 E+12	4.3	a
-1	2.2 E+16	34.1	a
2	5.3 E+14	8.86	b

^a Louw, R.; Dijks, J.H.; Mulder, P. J. Chem. Soc. Perkin Trans. II, 1973, 40, 1635. Reverse reaction (k-1) from thermodynamics. 2 sites for attack.

^b Based upon entropy change for Cl + MPH3Cl2 = [TPH7R] with A₂ = 6.0E+12 cc/mol sec per site of attack and 2 sites for attack. E₋₂ = 2 kcal/mol.

UNITS:

* A₁ (cc/mol sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (cc/mol sec)	n	E _a (kcal/mol)	range
7.6	C ₆ H ₄ Cl+PhClPhCl=MPH3Cl2+Cl	5.97+12	-0.19	4.49	i
760.0	"	8.85E+12	-0.23	4.62	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE 11.xx

o-TERPHENYL RADICAL = [TPHF1R][#] = PRODUCTS

k	A*	E _a **	source
1	1.43E+11	4.3	a
-1	6.0 E+13	23.90	a
2	2.81E+12	8.78	b

^a Transition State Theory (est at 1000 K).

A₁ = 6E+10 * T * exp(ΔS/R) ; reverse from thermo

^b Based upon entropy change for H + TRIPHENYLENE= [TPHF1R]

with A₋₂ = 4.0E+13 cc/mol sec and

6 sites for attack. E₋₂ = 4.3 kcal/mol.

UNITS:

* A₁ (1/sec)

A₂ (1/sec)

** Ea (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (1/sec)	n	Ea (kcal/mol)	range
7.6	OPH3R = TRIPHENYLENE +H	1.14E+14	-0.90	5.36	i
760.0	"	1.89E+18	-2.06	8.86	"
7.6	OPH3R = [TPHF1R] ^o	3.64E+24	-5.38	5.48	"
760.0	"	3.58E+30	-6.48	8.94	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xxi

o-PH3CL2 RADICAL = [TPHF2R][#] = PRODUCTS

k	A [*]	E _a ^{**}	source
1	1.80E+11	4.3	a
-1	6.0 E+13	23.90	a
2	4.20E+12	8.78	b

^a Transition State Theory (est at 1000 K).

A₁ = 6E+10 * T * exp(ΔS/R) ; reverse from thermo

^b Based upon entropy change for H + TRIPHCL2 = [TPHF2R]
with A₋₂ = 2 E+13 cc/mol sec and
2sites for attack. E₋₂ = 4.3 kcal/mol.

UNITS:

* A₁ (1/sec)A₂ (1/sec)

** Ea (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (1/sec)	n	Ea (kcal/mol)	range
7.6	OPH3CL2R = TRIPHCL2 +H	3.12E+13	-0.69	5.16	i
760.0	"	1.64E+18	-2.00	8.88	"
7.6	OPH3CL2R = [TPHF2R] ^o	1.45E+23	-4.98	4.72	"
760.0	"	6.20E+29	-6.27	8.46	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xxii

o-PH3CL RADICAL = [TPHF3R][#] = PRODUCTS

k	A [*]	E _a ^{**}	source
1	1.43E+11	4.3	a
-1	6.0 E+13	23.90	a
2	5.48E+12	8.78	b

^a Transition State Theory (est at 1000 K).

A₁ = 6E+10 * T * exp(ΔS/R) ; reverse from thermo

^b Based upon entropy change for H + TRIPHCL = [TPHF3R]

with A₋₂ = 1.3E+13 cc/mol sec and

1 site for attack. E₋₂ = 4.3 kcal/mol.

UNITS:

* A₁ (1/sec)

A₂ (1/sec)

** E_a (kcal/mol)

APPARENT REACTION RATE CONSTANT PREDICTED

USING BIMOLECULAR QRRK ANALYSIS (H₂ BATH GAS)

P (torr)	REACTION	A factor (1/sec)	n	E _a (kcal/mol)	range
7.6	OPH3CLR = TRIPHCL + H	7.70E+12	-0.53	4.96	i
760.0	"	1.47E+17	-1.73	8.30	"
7.6	OPH3CLR = [TPHF3R] ^o	7.32E+22	-4.94	4.81	"
760.0	"	1.15E+29	-6.10	8.17	"

i valid from 300 - 2000 K

ii " " 800 - 1500 K

iii " " 800 - 2000 K

TABLE II.xxiii

REACTION	A	n	E _a (kcal/mol)	source
1 - 39.	see TABLE I.xiv (SECTION I)			
40. PHCL ₂ =C ₆ H ₄ CL+CL	6.0E+15	0.0	93500.0	a
41. PHCL ₂ =C ₆ H ₃ CL ₂ +H	1.0E+16	0.0	108500.0	b
42. PHCL ₂ +H=C ₆ H ₅ CL+CL	2.96E+13	-0.05	7630.0	c
43. CYC ₆ H ₅ +PHCL ₂ =PHCLPHCL+H	1.92E+12	0.0	6740.0	"
44. CYC ₆ H ₅ +PHCL ₂ =PHPHCL+CL	4.87E+12	-0.11	4520.0	"
45. C ₆ H ₄ CL+PHCL ₂ =PHCLPHCL+CL	2.62E+57	-12.69	42380.0	"
46. C ₆ H ₄ CL+C ₆ H ₅ CL=PHPHCL+CL	1.50E+12	-0.06	4360.0	"
47. C ₆ H ₄ CL+C ₆ H ₅ CL=PHCLPHCL+H	6.79E+60	-14.00	38670.0	"
48. C ₆ H ₄ CL+PHCL ₂ =PHCLPHCL+CL	4.06E+13	-0.40	4820.0	"
49. CYC ₆ H ₅ +C ₆ H ₅ C ₆ H ₅ =MPH ₃ +H	2.57E+71	-16.91	47260.0	"
50. CYC ₆ H ₅ +C ₆ H ₅ C ₆ H ₅ =OPH ₃ +H	3.91E+74	-17.91	51360.0	"
51. CYC ₆ H ₅ +PHPHCL=OPH ₃ CL+H	4.26E+71	-17.34	47850.0	"
52. CYC ₆ H ₅ +PHPHCL=MPH ₃ CL+H	5.26E+73	-17.82	47830.0	"
53. CYC ₆ H ₅ +PHPHCL=MPH ₃ +CL	8.78E+12	-0.29	4680.0	"
54. CYC ₆ H ₅ +PHCLPHCL=MPH ₃ CL+CL	8.21E+12	-0.22	4600.0	"
55. CYC ₆ H ₅ +PHCLPHCL=MPH ₃ CL ₂ +H	8.35E+77	-18.94	50810.0	"
56. C ₆ H ₄ CL+C ₆ H ₅ C ₆ H ₅ =MPH ₃ CL+H	2.35E+72	-17.17	47870.0	"
57. C ₆ H ₄ CL+C ₆ H ₅ C ₆ H ₅ =OPH ₃ CL+H	1.18E+76	-18.29	52610.0	"
58. C ₆ H ₄ CL+PHPHCL=OPH ₃ CL ₂ +H	1.06E+74	-18.04	49540.0	"
59. C ₆ H ₄ CL+PHPHCL=MPH ₃ CL+CL	7.12E+12	-0.26	4630.0	"
60. C ₆ H ₄ CL+PHCLPHCL=MPH ₃ CL ₂ +CL	8.85E+12	-0.23	4620.0	"
61. OPH ₃ R=TRIPHENE+H	1.89E+18	-2.06	8860.0	"
62. OPH ₃ CL ₂ R=TRIPHCL ₂ +H	1.64E+18	-2.00	8880.0	"
63. OPH ₃ CLR=TRIPHCL+H	1.47E+17	-1.73	8300.0	"
64. PHCL ₂ +H=C ₆ H ₃ CL ₂ +H ₂	2.0E+13	0.0	18600.0	d
65. PHCL ₂ +H=C ₆ H ₄ CL+HCL	2.0E+13	0.0	11300.0	"
66. CL+PHCL ₂ =HCL+C ₆ H ₃ CL ₂	1.0E+13	0.0	12500.0	"

References for Mechanism

- a.
Twice rate for C₆H₅Cl dissociation by loss of Cl. See Chlorobenzene mechanism: SECTION I (Table I.xiv.)
- b.
A factor 2/3 that for C₆H₆ dissociation (see section I).
- c.
Pressure and temperature dependence accounted for with the CHEMACT computer program (see Tables II.ii-II.xxii). This work.
- d.
Optimized reaction. This work.

APPENDIX II-B

FIGURES for SECTION II

FIRST ORDER BEHAVIOR

Figure 2.1

0.4 cm ID, In H2 Atmosphere

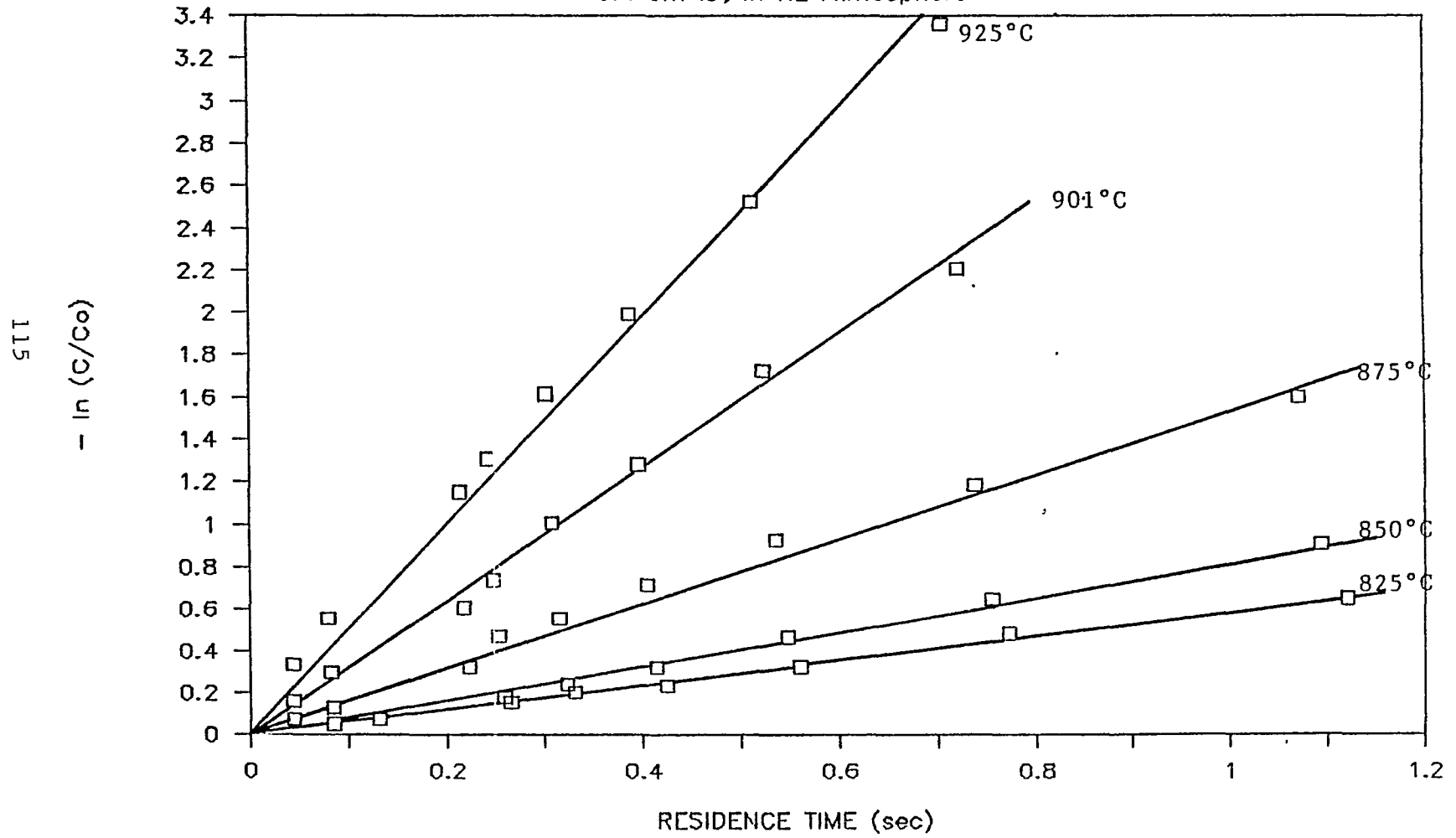


Figure 2.2

C6H4CL2+H2 EFFECT OF REACTOR DIAMETER

DECOMPOSITION OF C6H4CL2 IN H2 AT 1148K

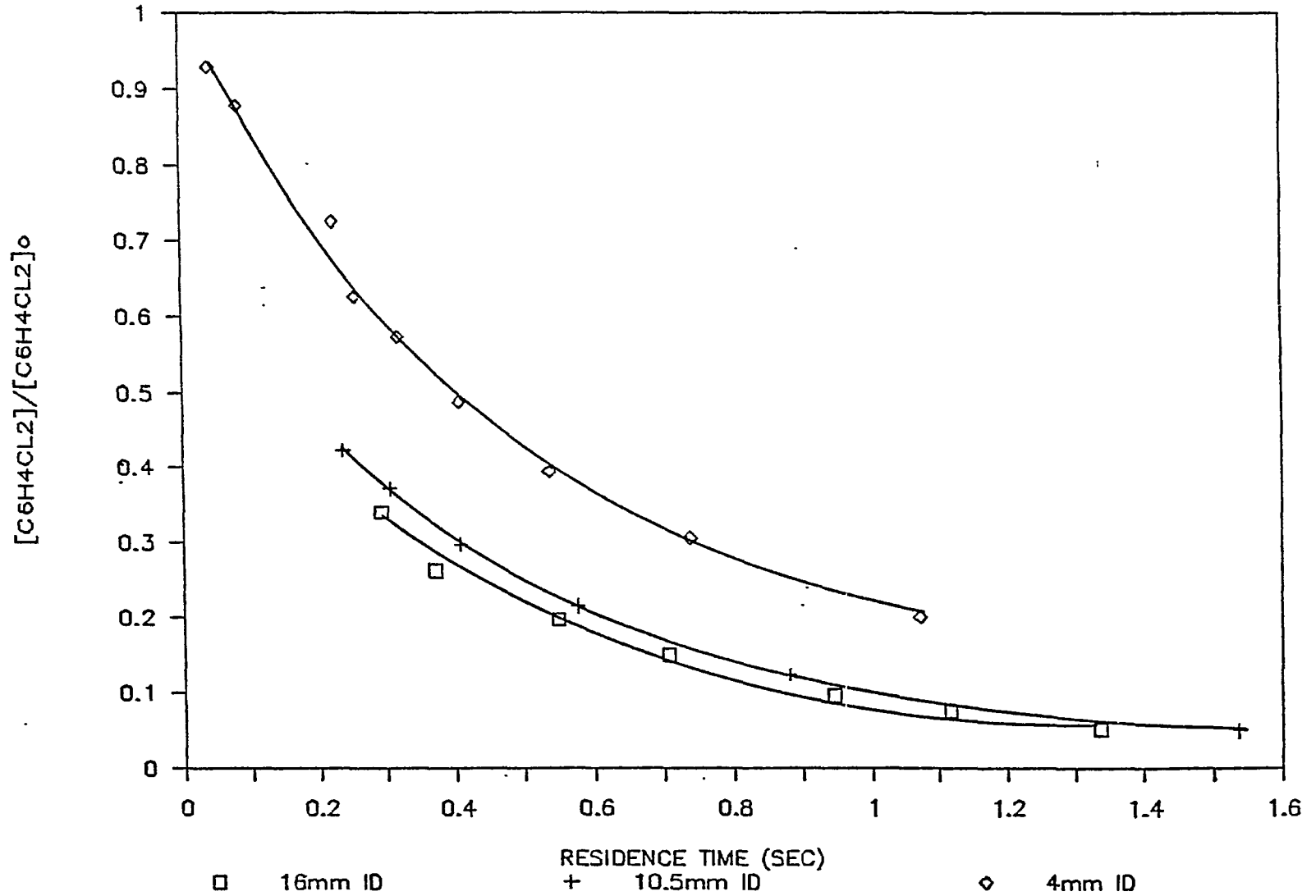
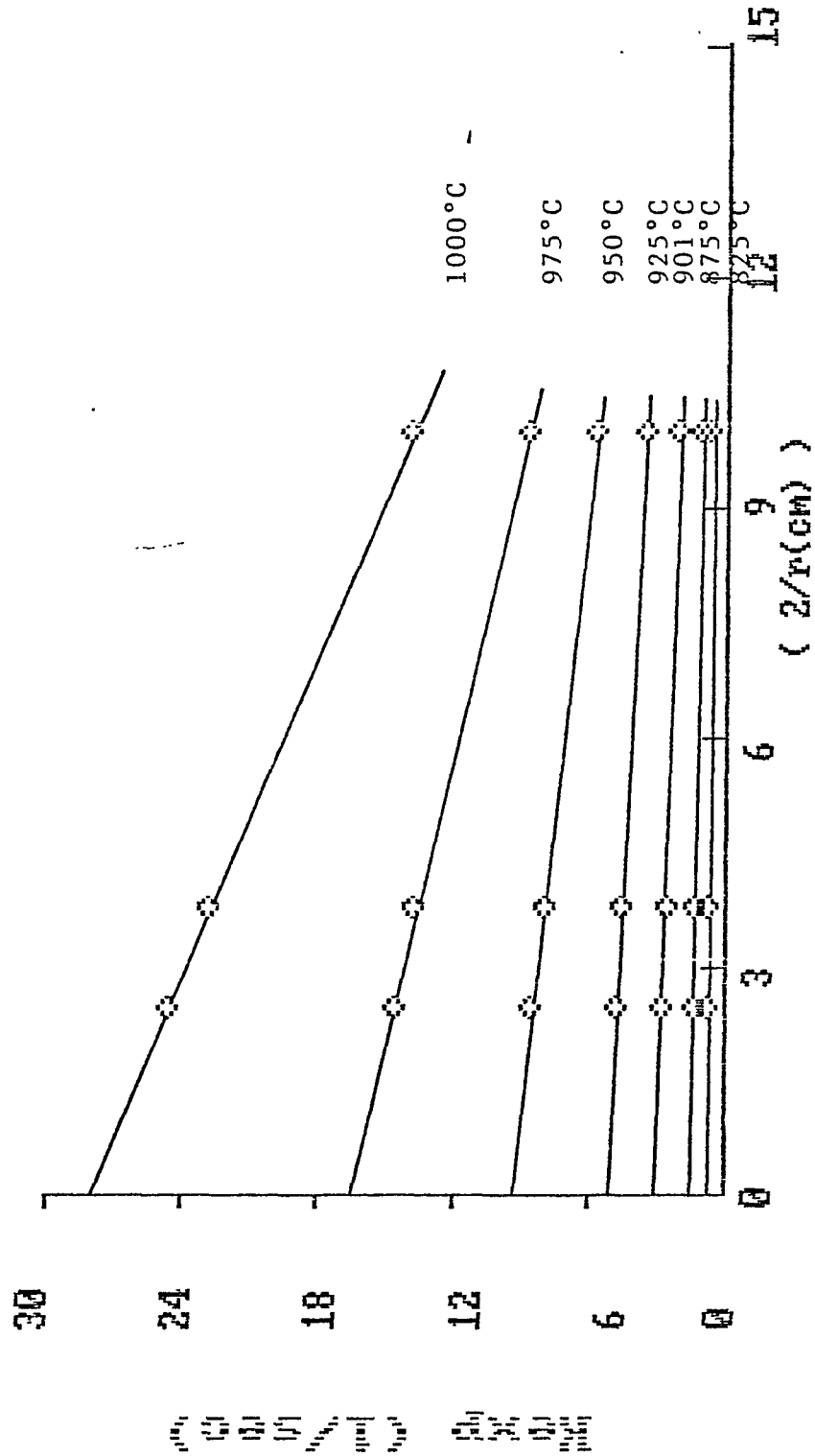


Figure 2.3
 DECOUPLING OF M_b and M_w with the Plug Flow Model



m-C₆H₄Cl₂ Pyrolysis in H₂ : 1123 K Experimental Product Distribution

Figure 2.4

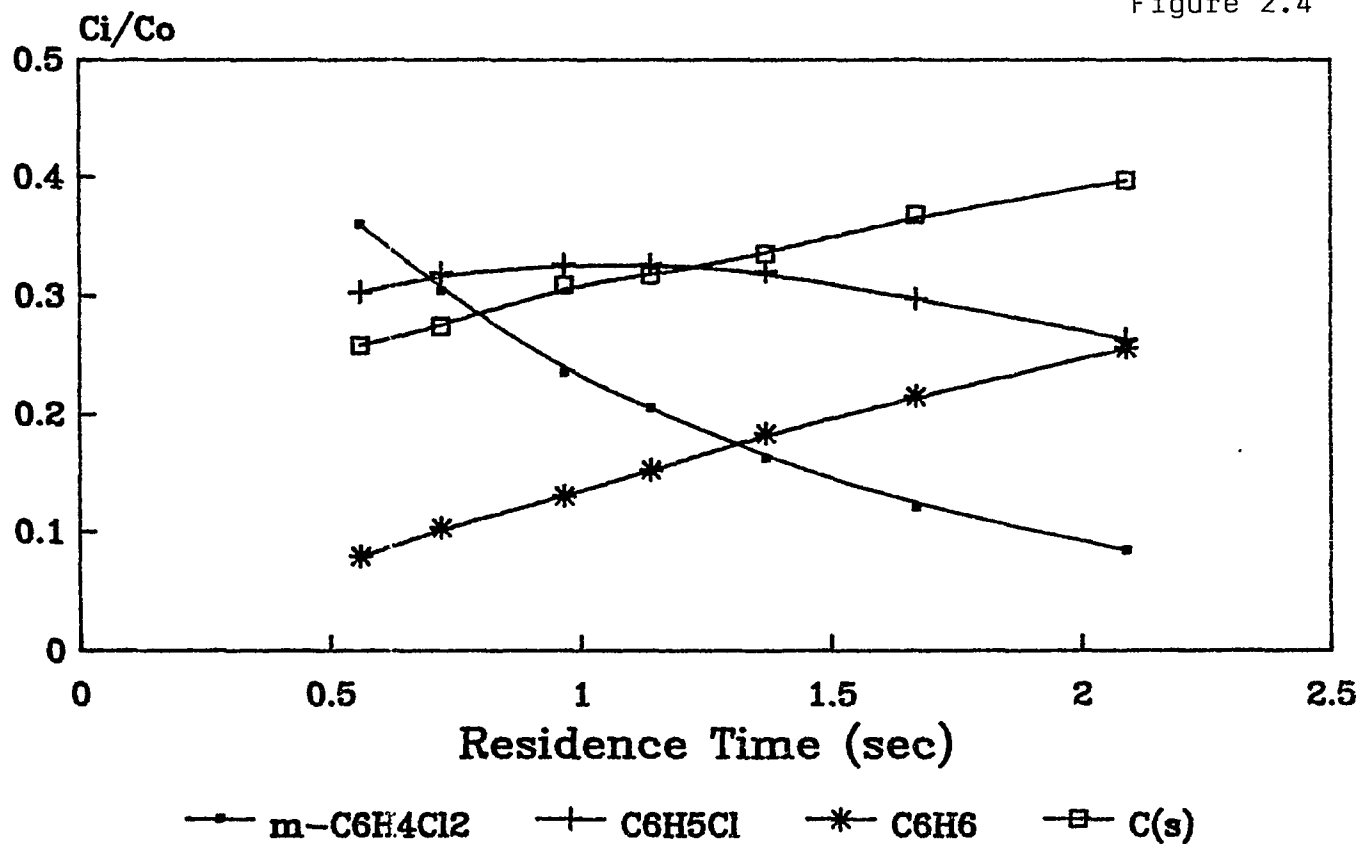


Figure 2.5

1.6 cm ID rxtr : 1 sec residence time

PRODUCT DIST vs. T(C) : C6H4CL2 + H2

611

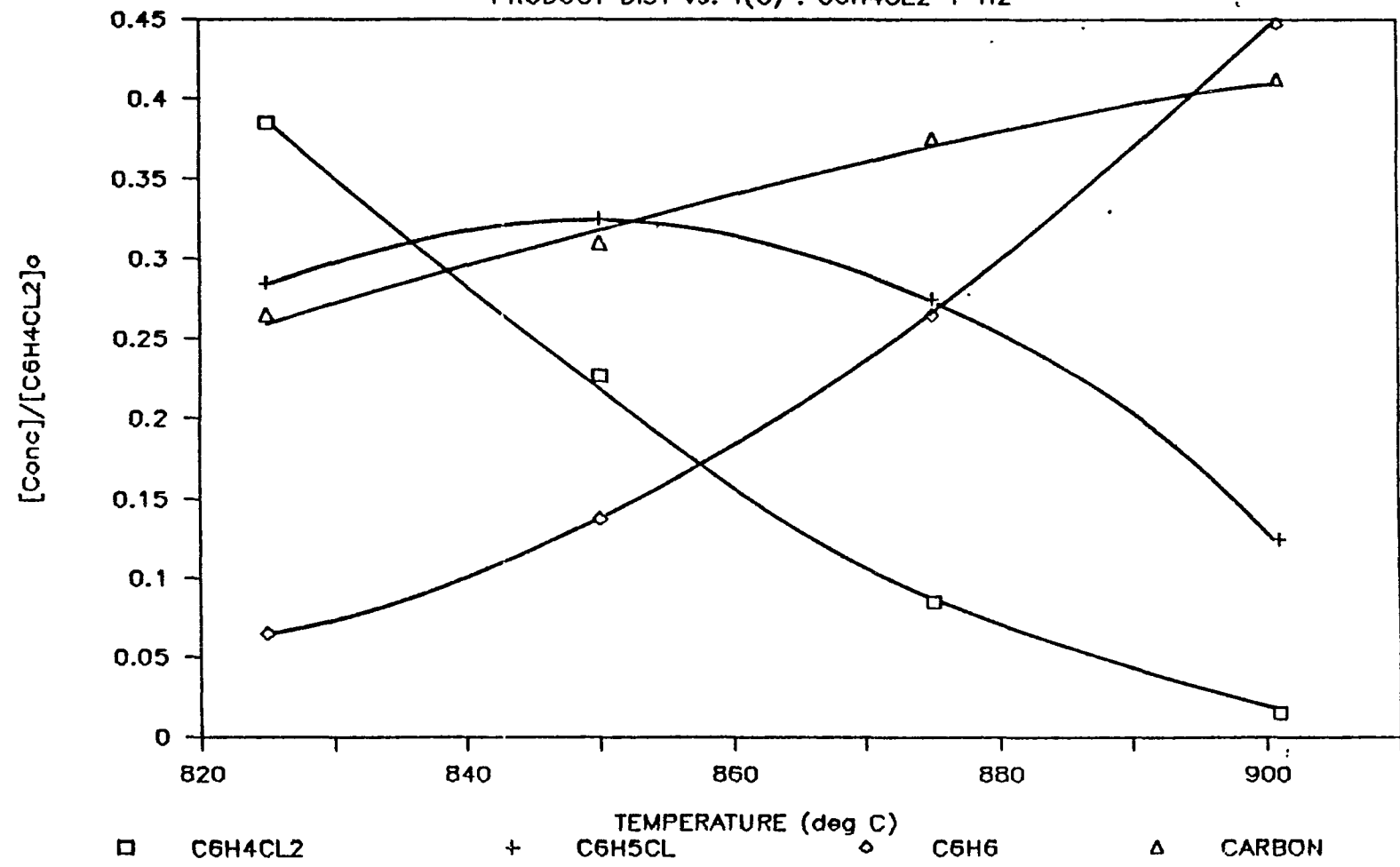


Figure 2.6

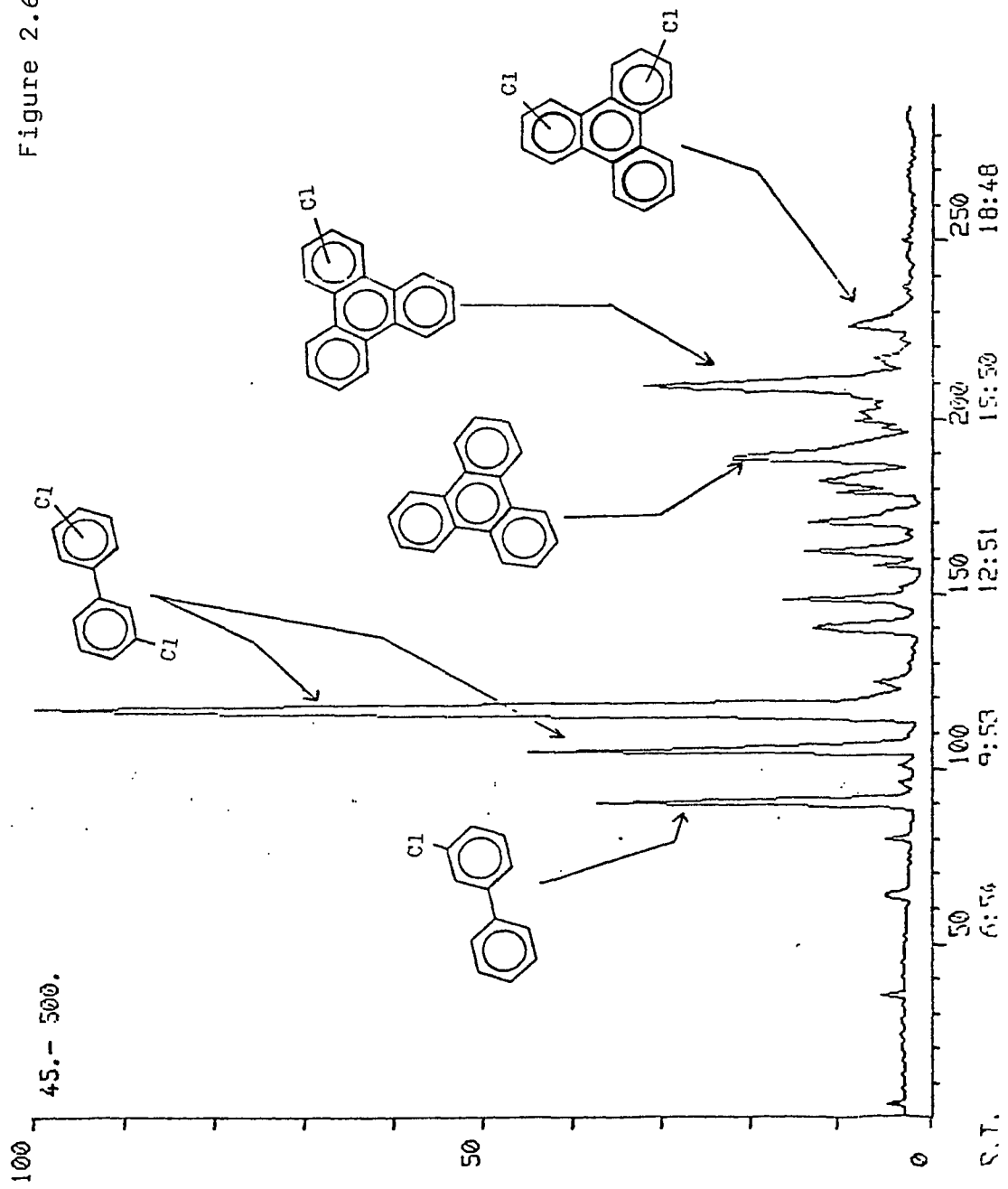


Figure 2.7

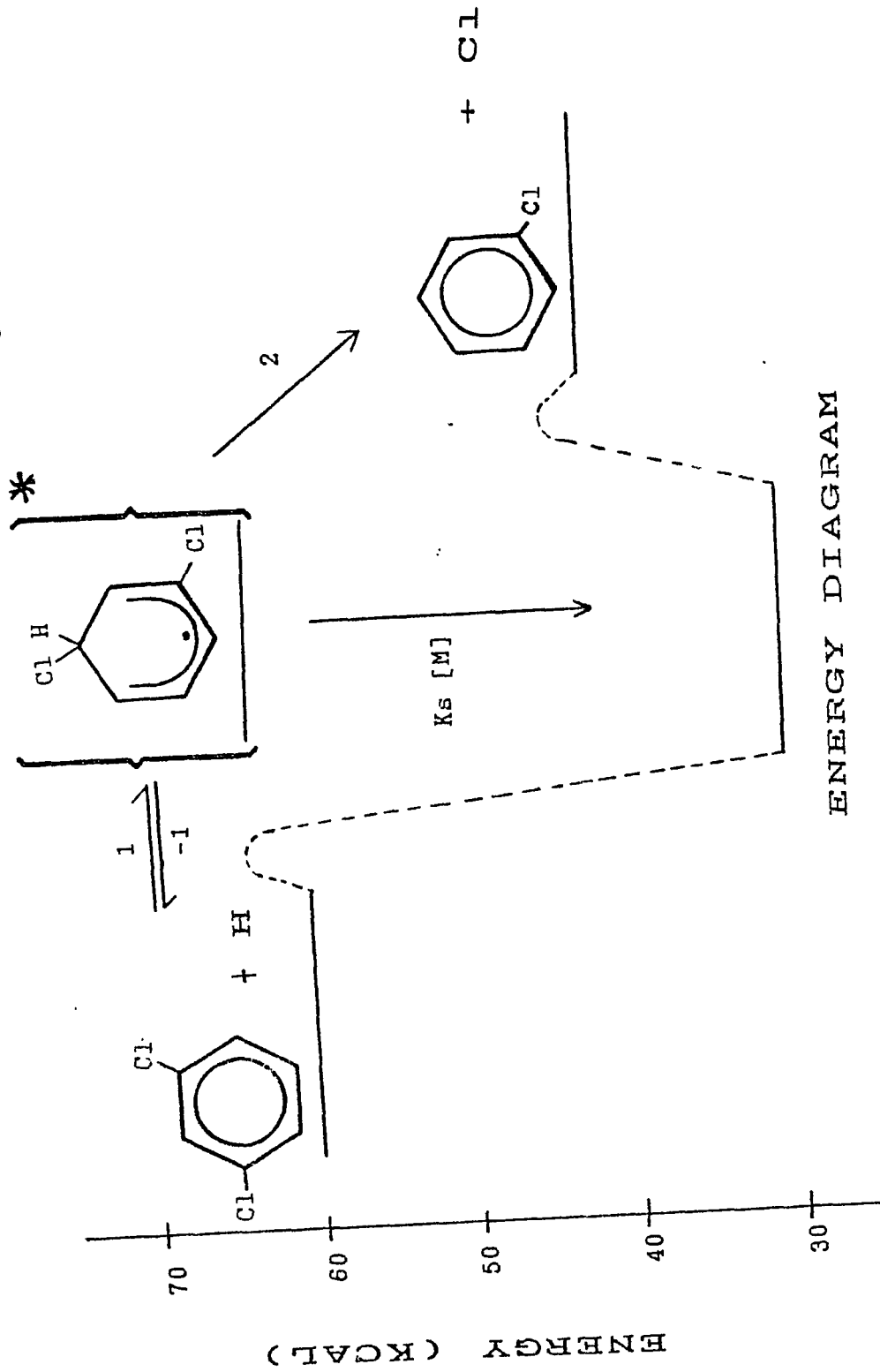


Figure 2.8

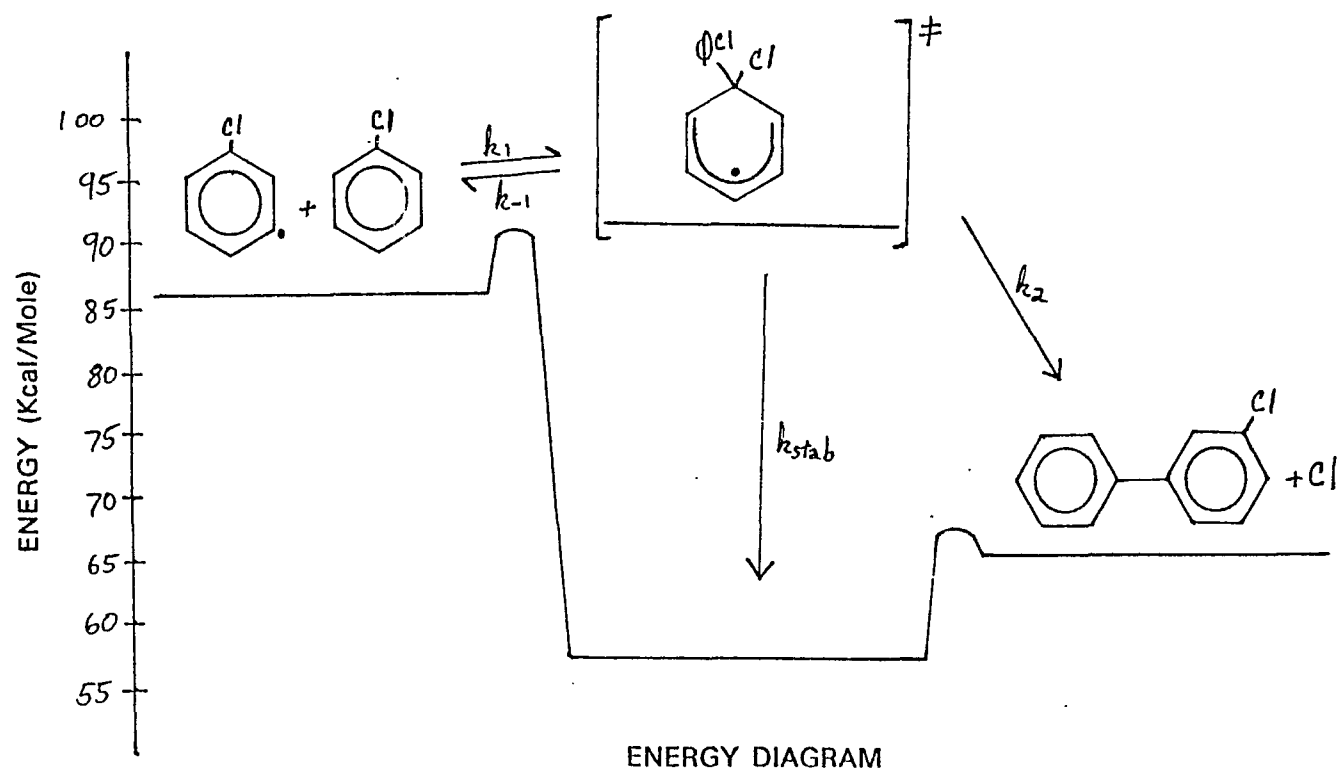


Figure 2.9

C6H4Cl+C6H5Cl \rightarrow PRODUCTS PRESSURE DEPENDENCE @ 300 & 2000 K

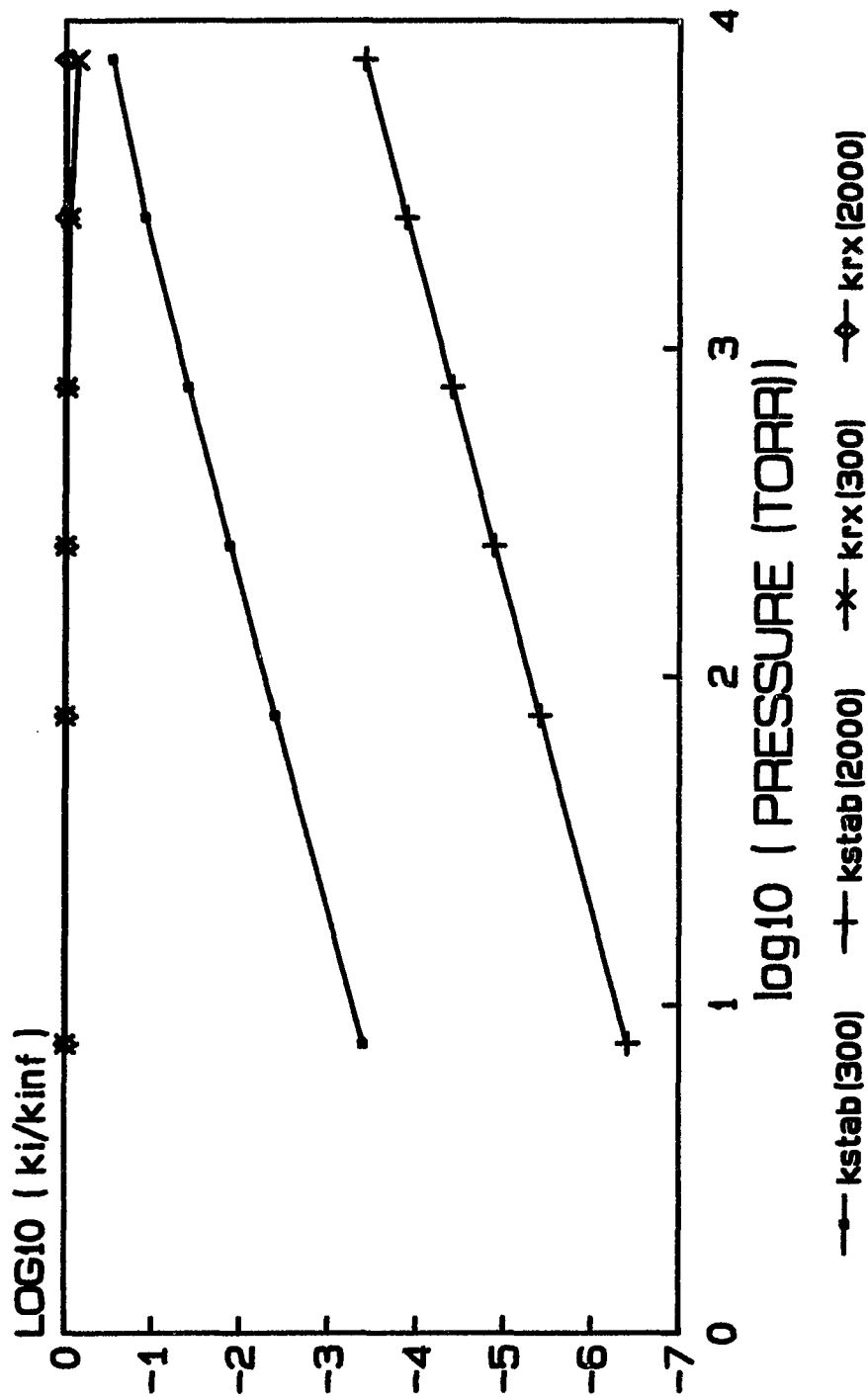


Figure 2.10

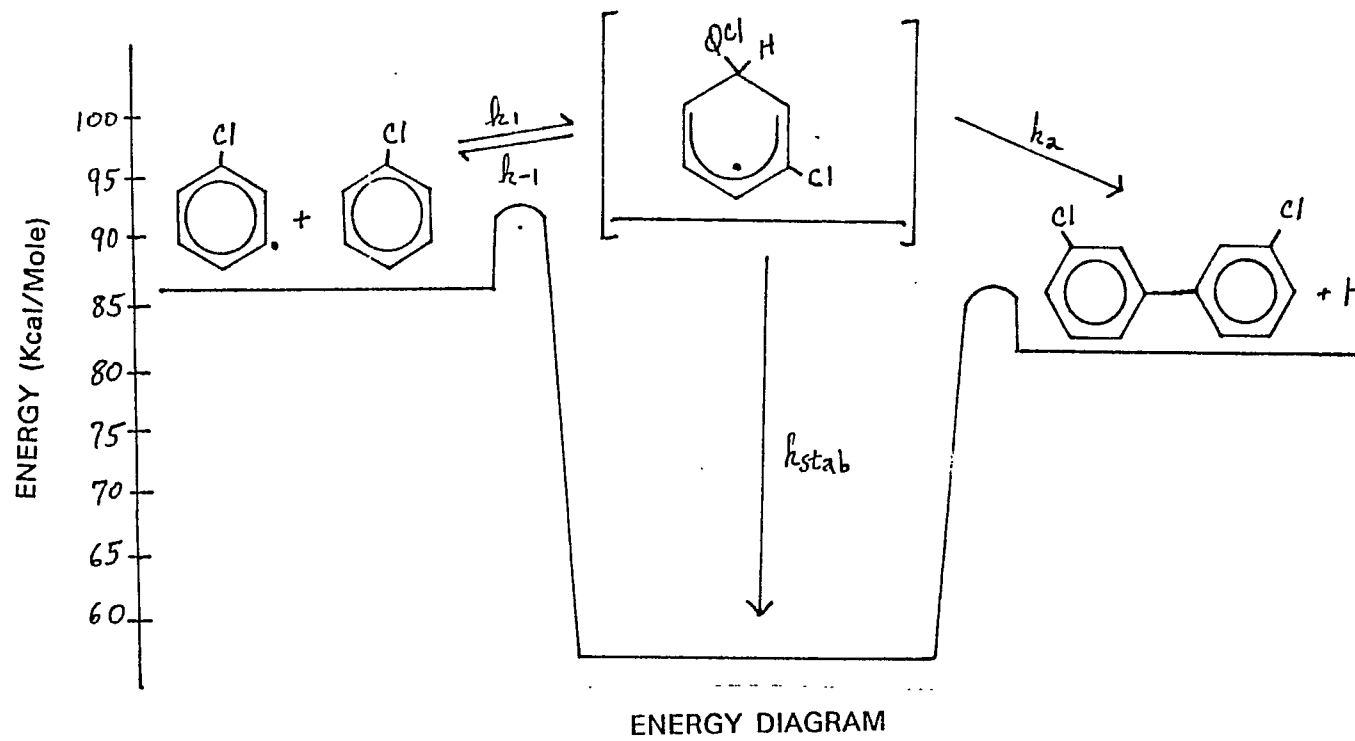


Figure 2.11

C6H4Cl + C6H5Cl --> PRODUCTS
APPARENT RATE CONSTANTS vs. 1/T

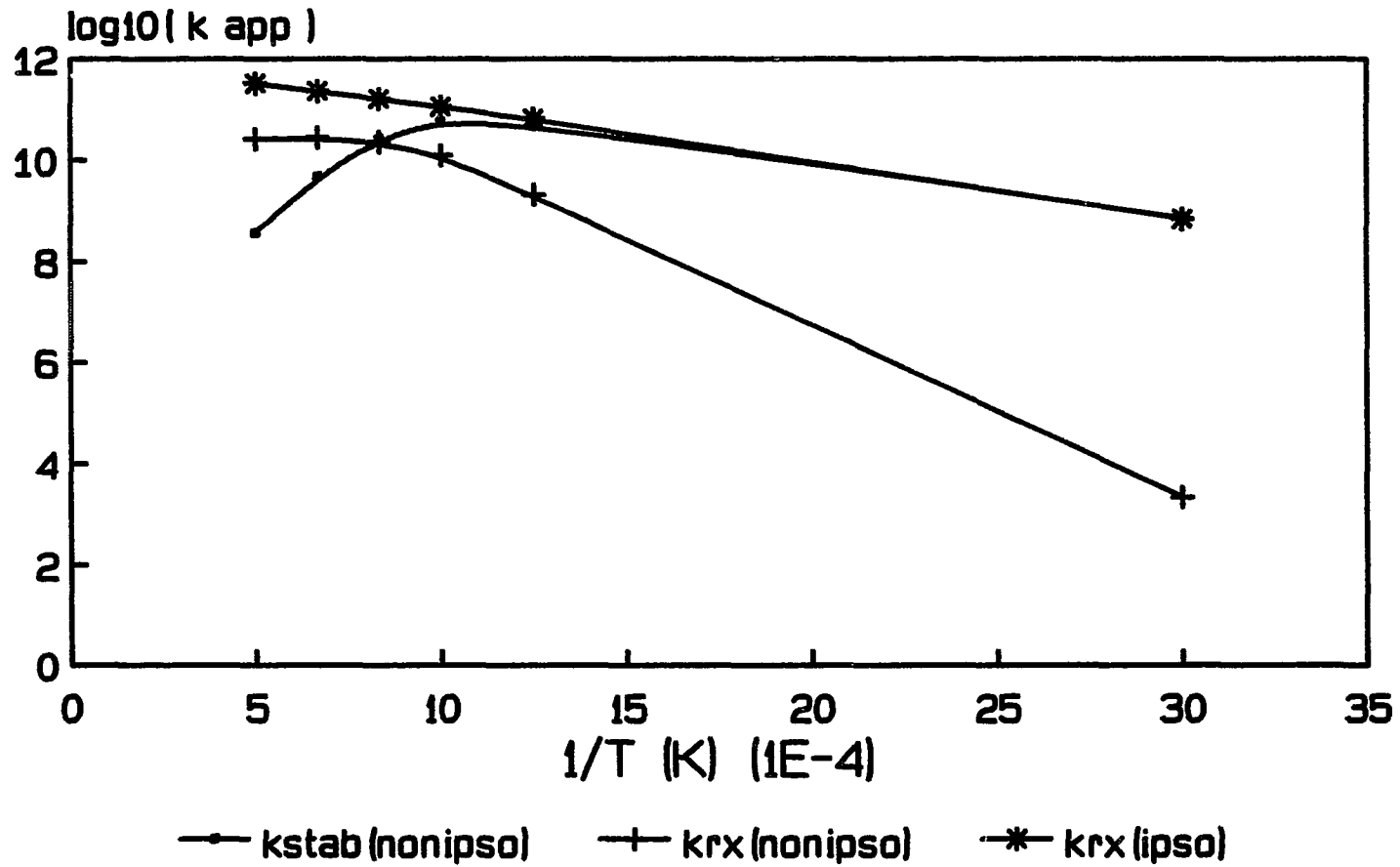


Figure 2.12

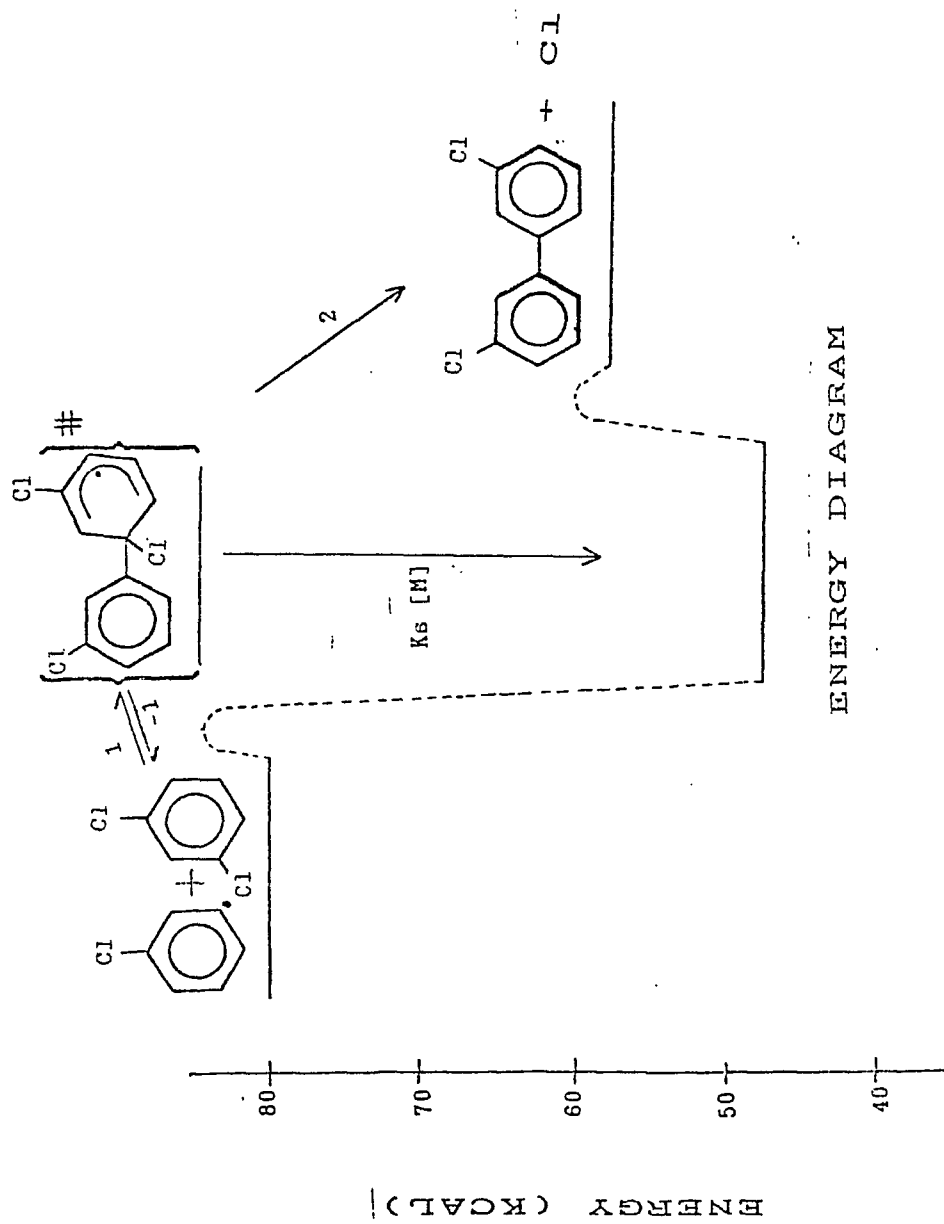


Figure 2.13

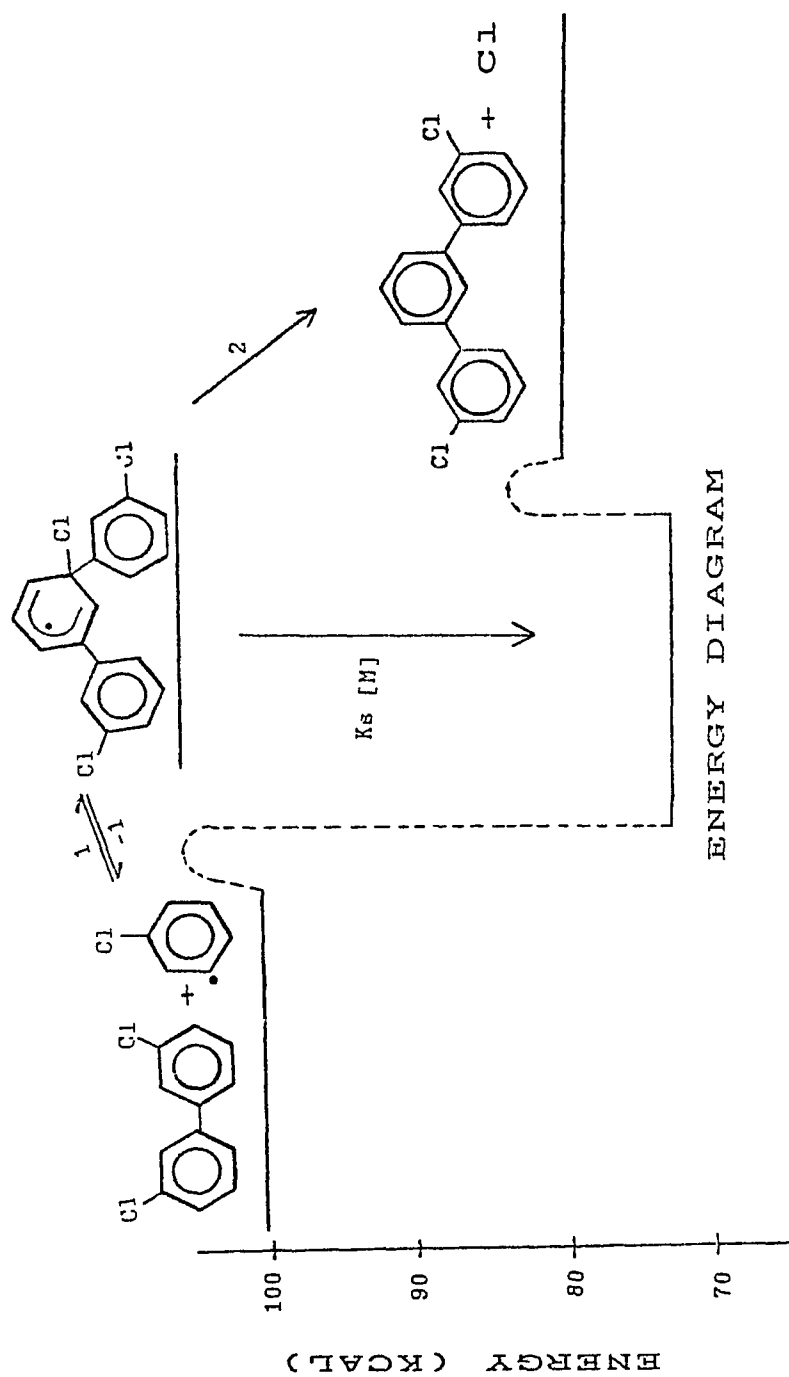
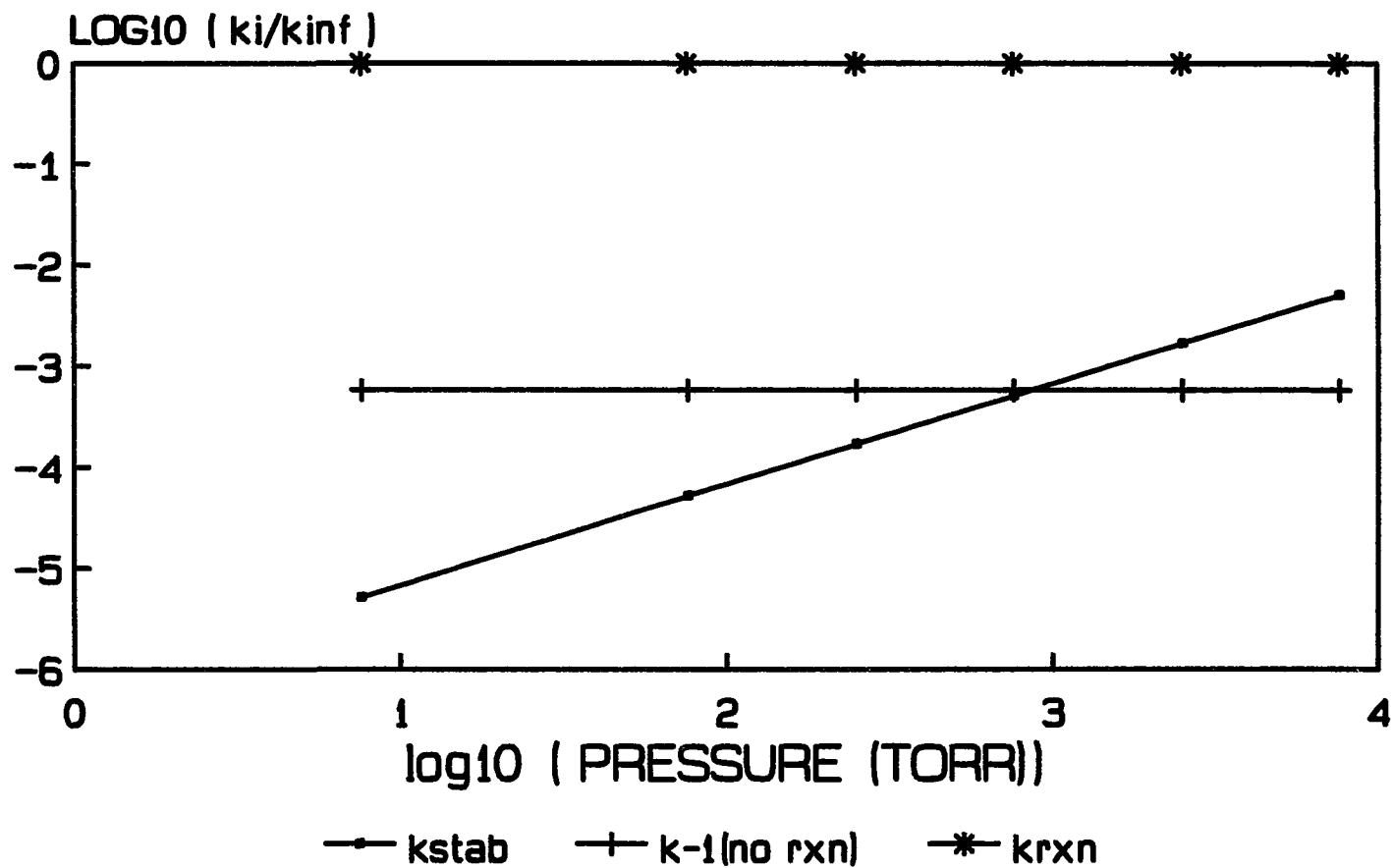


Figure 2.14

$C_6H_4Cl + PhCl \rightleftharpoons PRODUCTS$
PRESSURE DEPENDENCE @ 1000 K



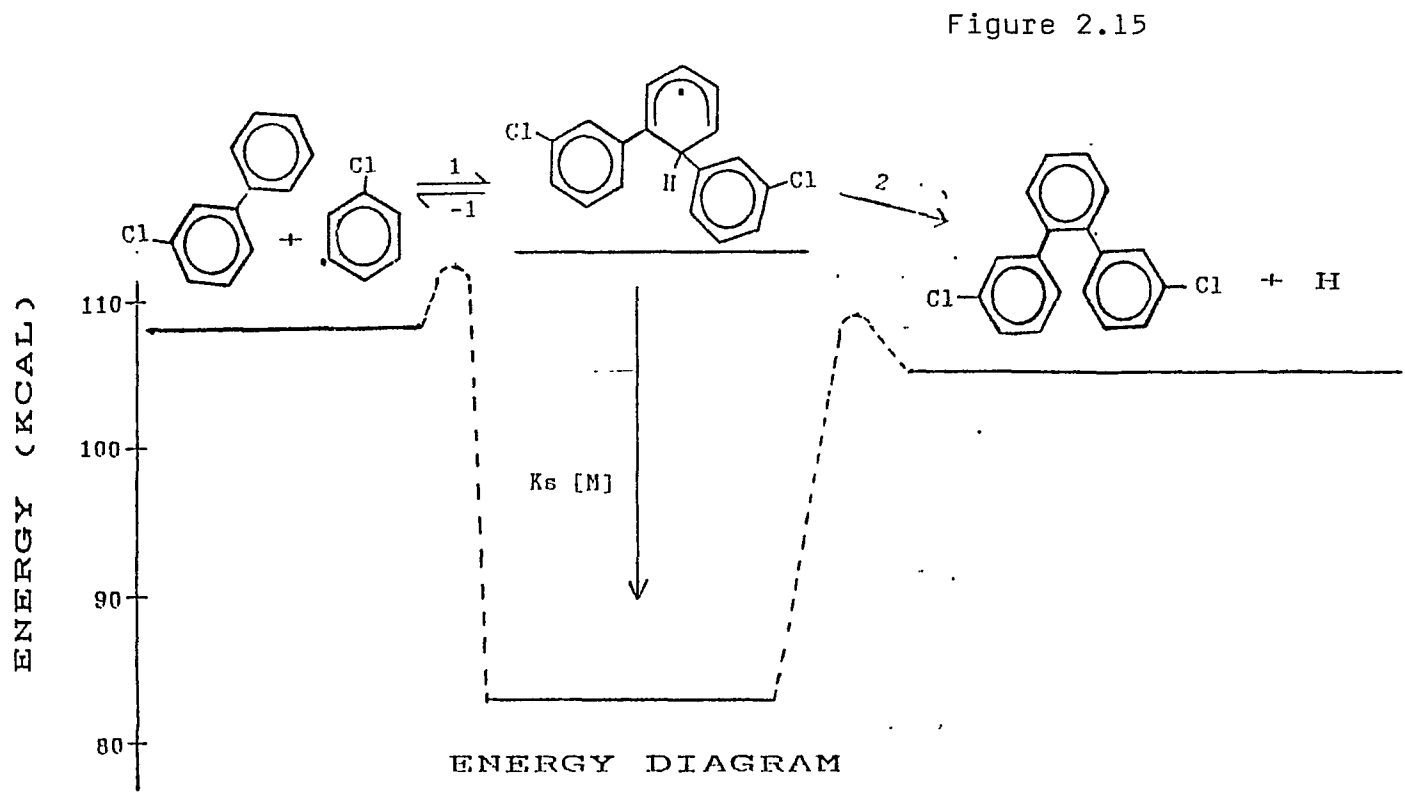
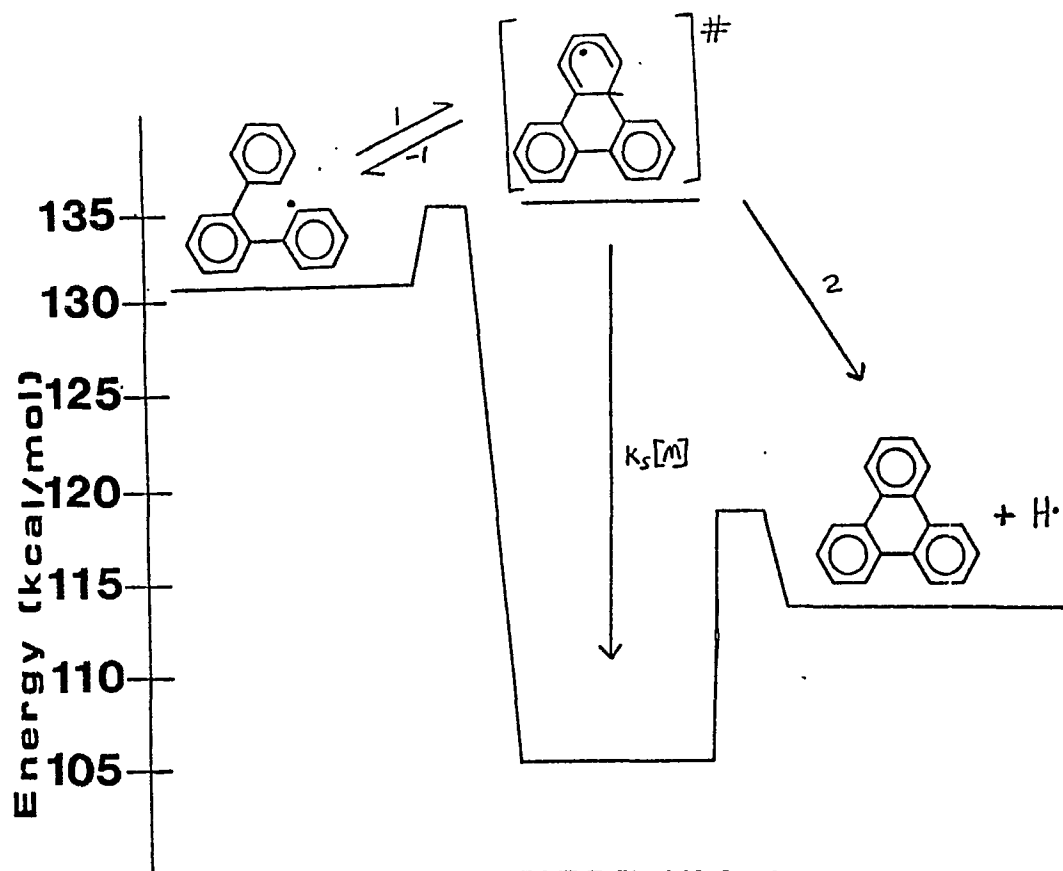


Figure 2.16



ENERGY DIAGRAM

Figure 2.17

O-TERPHENYL RADICAL \Rightarrow TRIPHENYLENE + H
PRESSURE DEPENDENCE @ 1000 K

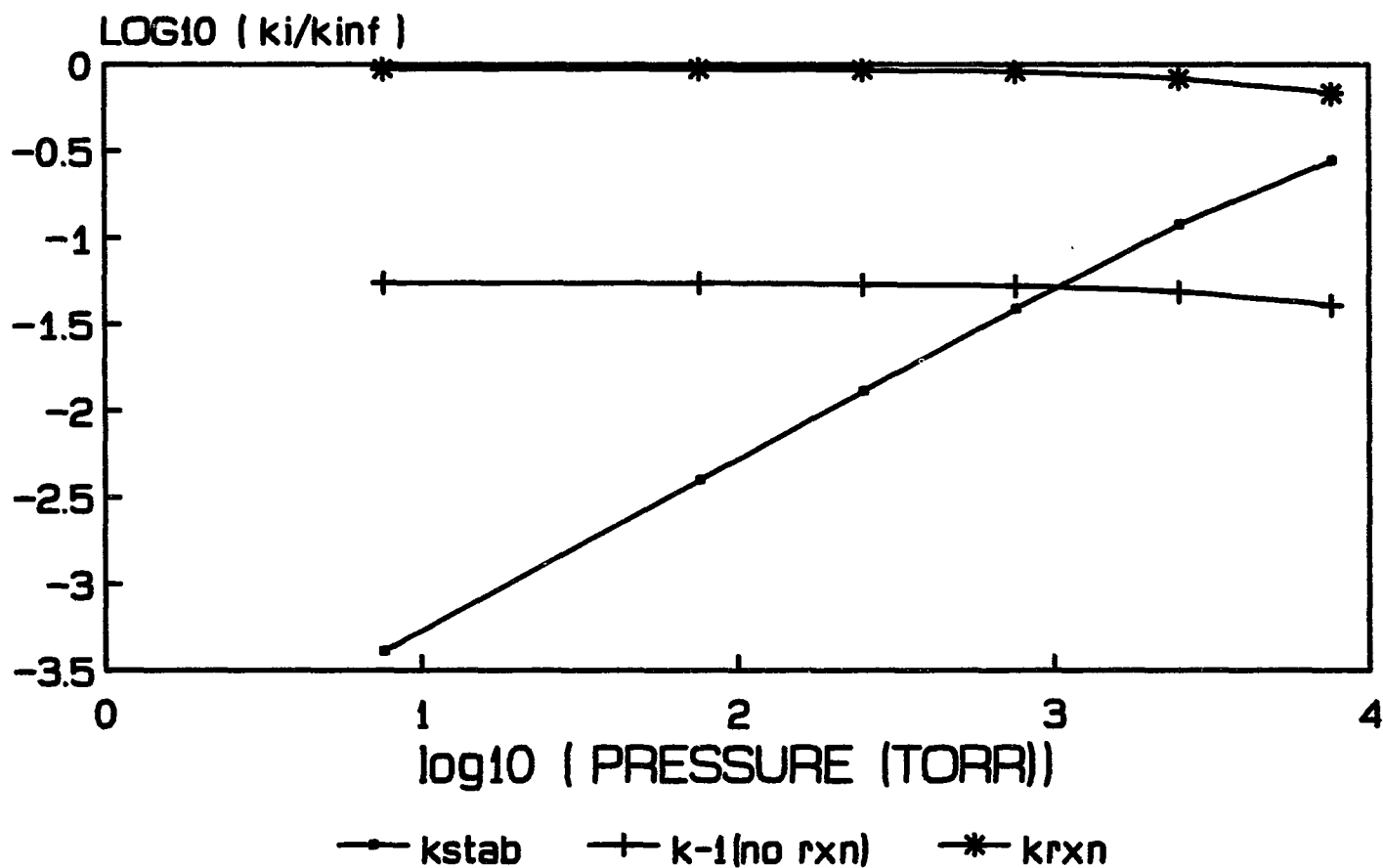


Figure 2.18

C6H4Cl2 PYROLYSIS IN H2 : 1096 deg K EXPERIMENTAL vs. PREDICTED RESULTS

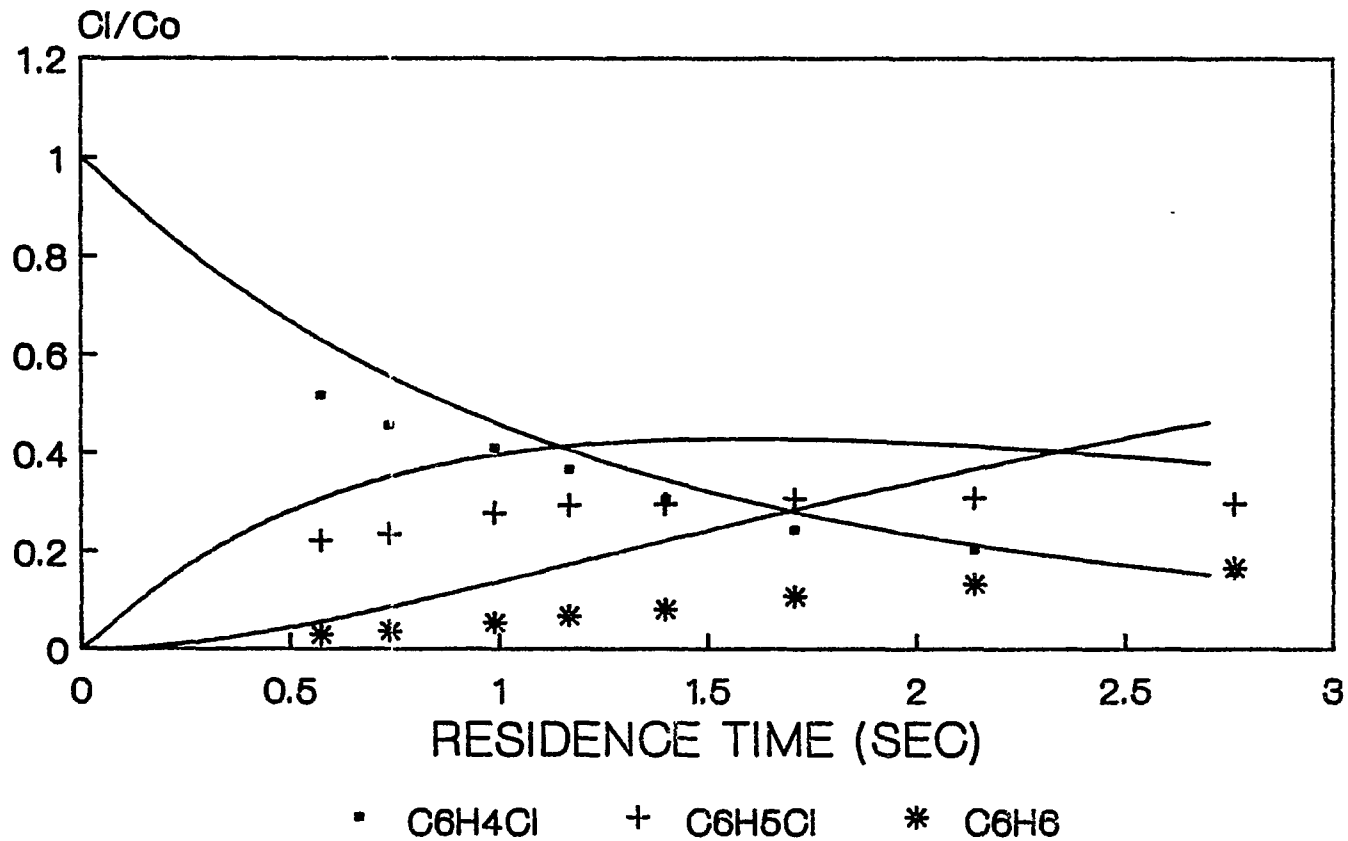


Figure 2.19

C6H4Cl2 PYROLYSIS IN H2 : 1200 deg K EXPERIMENTAL vs. PREDICTED RESULTS

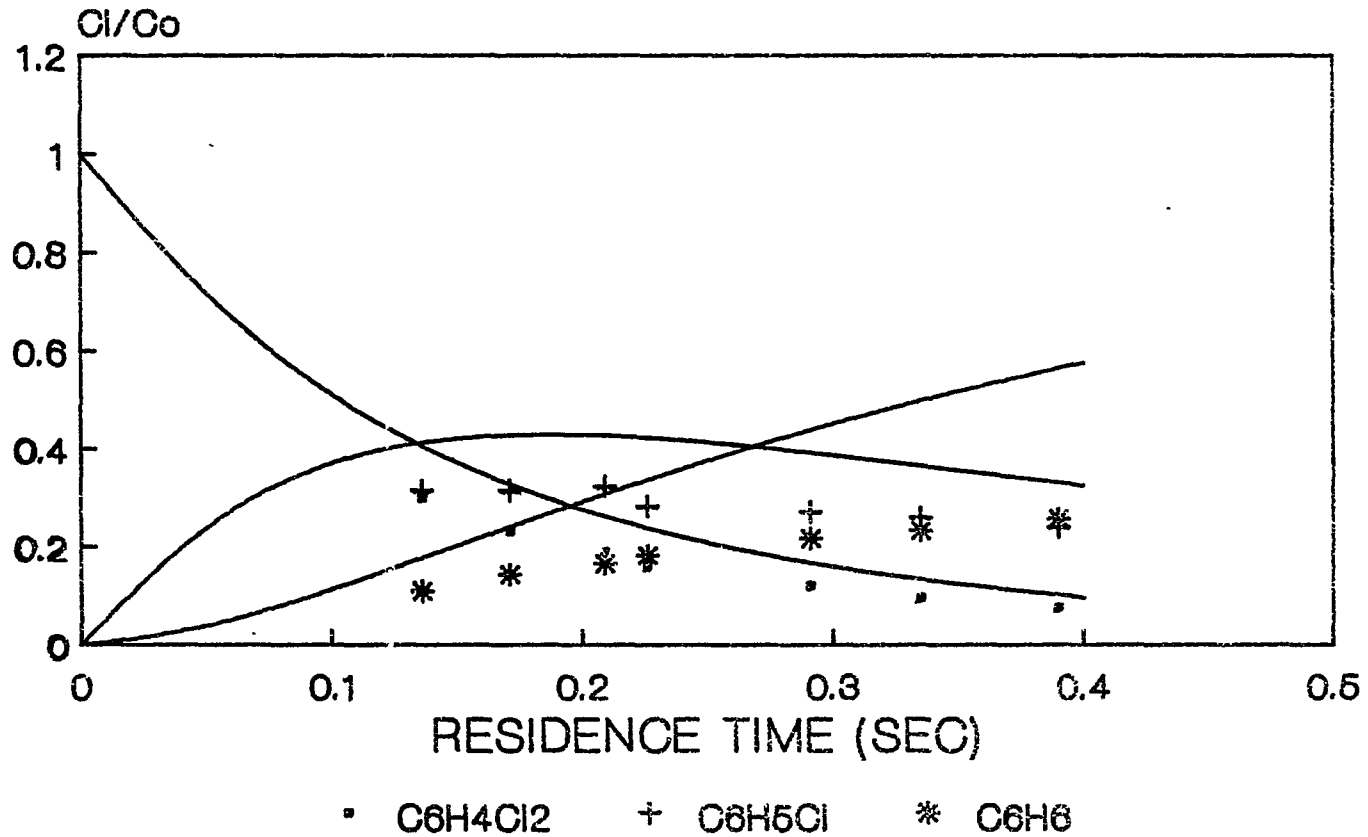
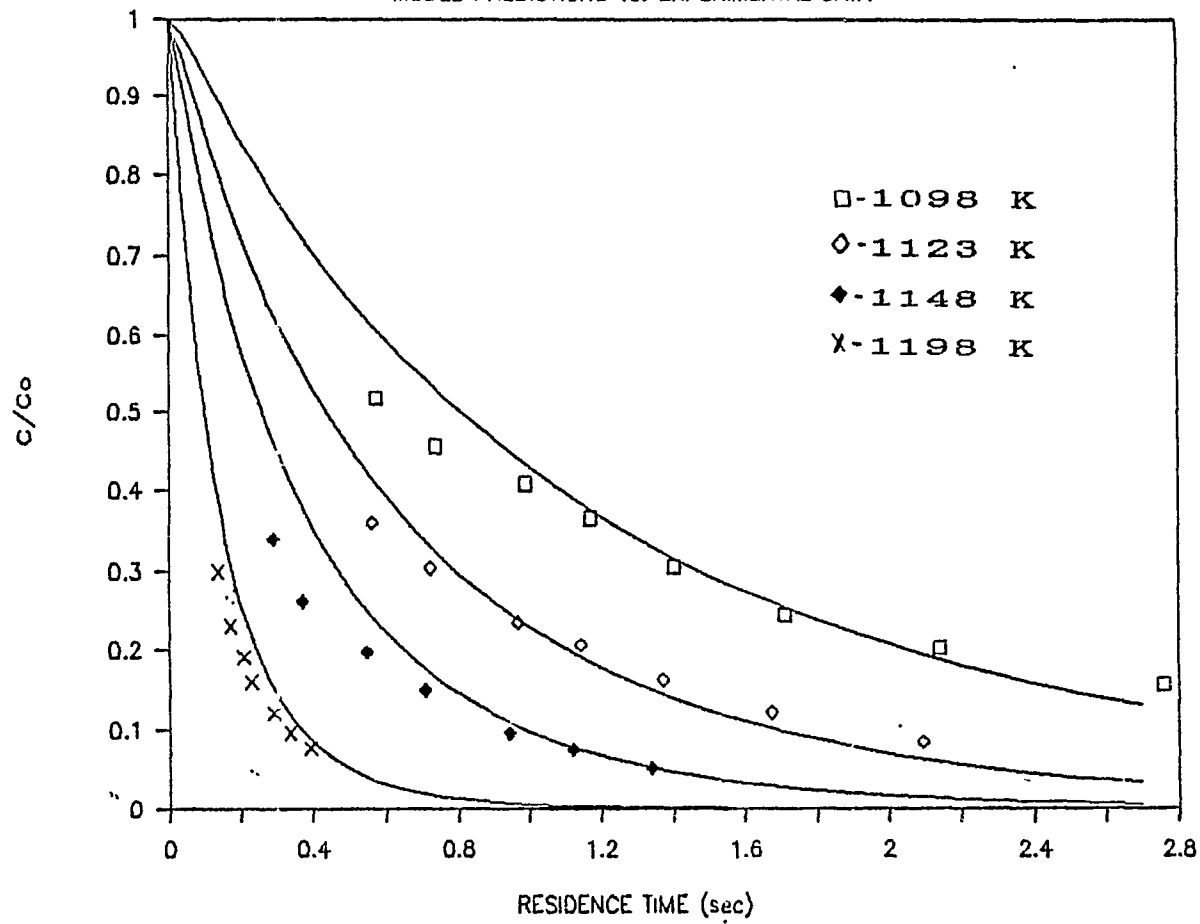


Figure 2.20

C6H4Cl2 DECOMPOSITION vs. REACTION TIME

MODEL PREDICTIONS vs. EXPERIMENTAL DATA



APPENDIX II-C

THERMO PROPERTY LIST
for SPECIES CONSIDERED IN DETAILED
KINETIC MECHANISM

APPENDIX II-C: THERMO PROPERTY LIST

UNITS (KCAL/MOL; CAL/MOL K)

SPECIES	Hf	S	Cp 300	400	500	600	800	1000	1500	FORMULA
CH3	34.82	46.38	9.26	10.05	10.81	11.54	12.90	14.09	16.26	CH3
CH4	-17.90	44.49	8.49	9.81	11.15	12.48	14.98	17.13	20.57	CH4
C2H2	54.19	48.00	10.60	11.94	13.03	13.93	15.29	16.30	18.34	C2H2
C2H4	12.54	52.39	10.28	12.74	14.92	16.85	20.03	22.45	26.21	C2H4
C2H6	-20.24	54.85	12.58	15.77	18.68	21.31	25.80	29.33	34.91	C2H6
CYC6H10	-1.28	74.27	25.24	34.78	42.74	49.37	59.51	66.65	77.29	C6H10
CYC6H9	45.61	80.05	25.10	34.07	41.50	47.65	56.95	63.42	73.01	C6H9
MECY24PD1	48.10	75.50	23.11	30.25	36.37	41.60	49.85	55.84	64.70	C6H7
BICYC6H7	71.86	71.52	27.62	30.93	34.98	39.40	48.20	55.52	63.32	C6H7
BICYC6H8	39.54	69.19	18.61	27.92	35.67	42.07	51.65	58.09	67.71	C6H8
H	52.11	27.39	4.97	4.97	4.97	4.97	4.97	4.97	4.97	H
CYC6H5	81.37	69.20	18.79	25.18	30.52	34.96	41.70	46.37	53.18	C6H5
CYC6H6	19.82	64.34	19.70	26.93	33.09	38.05	45.35	50.40	57.80	C6H6
CYC6H7	49.86	72.01	20.79	28.59	35.11	40.54	48.74	54.33	62.34	C6H7
LINC6H7	93.05	84.80	27.27	34.43	40.09	44.55	50.85	55.00	62.12	C6H7
CHD14	26.16	70.80	22.63	30.67	37.47	43.20	52.04	58.27	67.47	C6H8
CHD	25.40	72.49	22.67	30.85	37.73	43.49	52.30	58.45	67.56	C6H8
CY13PD5	54.30	62.40	17.24	24.03	29.40	33.61	39.46	43.13	49.10	C5H5
CY13PD	32.40	64.20	17.64	24.43	30.01	34.56	41.29	45.81	52.80	C5H6
MECY24PD3	81.76	75.80	22.91	29.99	36.09	41.31	49.58	55.57	64.44	C6H7
MECY14PD4	79.66	75.40	22.95	30.01	36.09	41.31	49.58	55.57	64.44	C6H7
MECY14PD3	48.06	75.36	23.11	30.25	36.37	41.60	49.85	55.84	64.70	C6H7
MECY24PD	28.30	73.00	23.03	30.31	36.74	42.37	51.51	58.23	67.83	C6H8
NAPTH	36.10	80.21	31.89	43.00	52.13	59.61	70.77	78.43	90.21	C10H8
C*CC*C	26.33	66.62	19.22	24.22	28.36	31.78	36.95	40.57	46.34	C4H6
C*CC*C.	79.82	70.70	18.40	22.71	26.28	29.24	33.75	36.95	42.09	C4H5
C*CC*CC*C	39.60	80.70	28.09	35.79	41.91	46.76	53.70	58.33	66.33	C6H8
C#CC.*C	115.57	68.20	17.50	20.52	22.98	24.97	27.91	29.93	33.27	C4H3
C#CC*C.	126.27	69.60	17.50	20.52	22.98	24.97	27.91	29.93	33.27	C4H3
C#CC#C	112.30	59.86	17.19	19.77	21.77	23.30	25.33	26.55	28.72	C4H2
C#CC#C.	192.20	62.72	14.98	17.00	18.59	19.82	21.50	22.53	24.21	C4H
C#CC#CC#C	170.66	73.74	20.65	24.21	27.51	30.49	35.35	38.60	40.79	C6H2
ME.CY24PD	75.10	76.42	23.11	30.27	36.36	41.53	49.64	55.53	64.71	C6H7
C6H5CH3	11.95	76.41	24.88	33.38	40.53	46.52	55.73	62.22	71.78	C7H8
CYC6H4	112.52	68.88	16.38	22.95	28.22	32.42	38.45	42.42	48.70	C6H4
H2	.00	31.21	6.90	6.95	6.99	7.02	7.10	7.21	7.72	H2
CL	28.90	39.47	5.22	5.37	5.44	5.45	5.39	5.31	5.17	CL
CL2	-.01	53.29	8.10	8.38	8.59	8.74	8.91	8.99	9.10	CL2
C2H	131.98	49.55	8.92	9.61	10.21	10.72	11.55	12.18	13.31	C2H
C6H5CL	12.35	74.79	23.27	30.58	36.47	41.18	47.96	52.41	59.17	C6H5CL
PHCLPHCL	28.72	112.76	44.07	56.76	66.94	75.04	86.58	93.99	104.92	C12H8CL2
PHCL2	6.32	82.09	27.35	34.19	39.70	44.10	50.37	54.36	59.96	C6H4CL2
C6H5C6H5	43.50	93.85	35.74	48.75	59.44	68.19	81.20	90.05	103.37	C12H10
TERPHEN	66.04	123.30	58.70	79.26	95.92	109.33	128.74	141.44	160.44	C18H14
PHPHCL	35.82	105.39	39.90	52.74	63.17	71.60	83.88	92.03	104.14	C12H9CL
HCL	-22.06	44.64	6.96	6.95	6.99	7.07	7.29	7.56	8.10	HCL
C6H4CL	74.34	77.78	22.92	29.16	34.33	38.62	45.16	49.86	57.75	C6H4CL

LINC6H6	82.73	77.88	26.31	32.66	37.79	41.91	47.86	51.75	57.77	C6H6
LINC6H5	136.55	80.70	25.50	31.62	36.41	40.12	45.21	48.39	53.56	C6H5
CY13HD	25.40	72.90	22.44	30.74	37.70	43.51	52.35	58.47	67.44	C6H8
NAPTH.H	127.32	33.89	41.77	46.37	52.56	59.60	73.82	85.40	95.91	C10H9
CHD.C4H3	135.33	89.24	42.06	49.46	57.08	64.36	76.42	84.12	95.22	C10H9
BICYC10H9	115.33	82.47	41.50	53.03	62.44	70.07	81.11	88.15	97.07	C10H9
BICYPD	79.15	90.58	33.71	51.29	64.12	73.26	84.08	89.66	101.32	C10H10
C6H3CL2	66.01	82.84	26.90	34.25	38.96	42.01	46.21	51.46	76.84	C6H3CL2
CYC6H5CL2	28.16	76.24	28.70	35.98	41.70	46.23	52.98	58.28	71.60	C6H5CL2
NAPTHC#C	94.51	94.04	40.07	51.52	61.11	69.08	81.06	89.09	99.78	C12H8
NAPH.C#C	156.06	95.42	39.20	49.90	58.88	66.36	77.66	85.25	95.29	C12H7
PHPH	42.92	92.51	39.07	52.99	64.34	73.54	87.00	95.95	109.41	C12H10
NAPTH	36.00	79.49	31.92	42.95	52.07	59.57	70.74	78.27	89.14	C10H8
NAPH.	97.55	83.62	31.05	41.34	49.85	56.86	67.33	74.42	84.64	C10H7
PHC#C	78.31	79.62	27.59	35.29	41.79	47.24	55.57	61.28	69.02	C8H6
PH.C#C	139.86	82.36	26.72	33.67	39.57	44.54	52.17	57.43	64.52	C8H5
ACENAPTH	66.36	48.35	38.39	49.15	58.07	65.39	76.17	83.14	92.47	C12H8
PHC#C.	156.10	80.98	25.90	32.95	38.95	44.02	51.81	57.13	64.00	C8H5
BICYC6H8	36.88	71.46	21.42	29.39	36.10	41.74	50.52	56.94	67.52	C6H8
BICYC6H7.	68.95	76.97	21.04	29.02	35.51	40.78	48.62	54.14	63.67	C6H7
DHNAPH	60.50	85.79	34.40	46.79	57.02	65.43	78.03	86.69	99.90	C10H10
H.NAPH	82.90	86.69	32.52	44.54	54.41	62.48	74.44	82.53	94.68	C10H9
DHNAPH.	113.94	90.98	34.24	46.12	55.85	63.78	75.48	83.38	95.40	C10H9
CHDC4H3	100.58	98.24	37.50	49.73	59.64	67.63	79.24	86.91	98.68	C10H10
CHD.C4H3	125.04	97.76	35.63	47.46	57.01	64.67	75.68	82.80	93.46	C10H9
ICLPHCHD	40.45	107.18	44.32	59.87	72.37	82.36	96.67	105.98	120.26	C12H11CL
ICLPHCHD.	64.91	106.70	42.45	57.60	69.74	79.40	93.11	101.87	115.04	C12H10CL
CLIPHCHD	40.90	107.91	44.26	59.51	71.85	81.78	96.12	105.50	119.57	C12H11CL
CLIPHCHD.	65.36	107.43	42.39	57.24	69.22	78.82	92.56	101.39	114.35	C12H10CL
PHCLCHD	44.49	109.63	44.82	60.01	72.26	82.08	96.21	105.41	119.35	C12H11CL
PHCLCHD.	68.95	109.15	42.95	57.74	69.63	79.12	92.65	101.30	114.13	C12H10CL
ICLC4H3CD	89.44	104.54	41.21	53.50	63.31	71.09	82.13	89.25	100.50	C10H9CL
CLC4H3CD.	113.90	105.44	39.34	51.23	60.68	68.13	78.56	85.14	95.28	C10H8CL
4CLICLCD	5.68	88.93	28.92	37.51	44.36	49.80	57.50	62.46	70.22	C6H6CL2
4CLICLCD.	30.14	88.45	27.05	35.25	41.74	46.84	53.94	58.36	65.00	C6H5CL2
CLHNAPH	56.54	90.84	35.60	49.87	61.03	69.69	81.62	89.17	101.99	C10H9CL
CLHNAPH.	109.98	94.65	35.44	49.20	59.86	68.04	79.07	85.86	97.49	C10H8CL
CL.NAPH	78.94	90.36	33.73	47.60	58.40	66.73	78.06	85.06	96.77	C10H8CL
CLICLPH	29.76	114.21	47.91	63.35	75.68	85.46	99.26	108.04	121.36	C12H10CL2
CLICLPH.	54.22	113.70	46.04	61.09	73.06	82.50	95.70	103.93	116.14	C12H9CL2
R46CLIPCL	22.66	122.96	52.08	67.34	79.41	88.86	101.94	110.02	122.23	C12H9CL3
R46CLIPCL.	47.12	122.42	50.21	65.08	76.79	85.91	98.38	105.91	117.01	C12H8CL3
ICLPCLCD	33.35	115.93	48.48	63.86	76.10	85.77	99.35	107.95	121.14	C12H10CL2
ICLPCLCD.	57.81	115.45	46.61	61.59	73.47	82.81	95.79	103.85	115.92	C12H9CL2
CLIPCLCD	34.15	116.05	48.41	63.51	75.59	85.18	98.78	107.49	120.91	C12H10CL2
CLIPCLCD.	58.61	115.57	46.54	61.25	72.96	82.22	95.21	103.39	115.69	C12H9CL2
TRIPHENE	61.80	104.80	56.89	75.42	90.70	103.22	121.71	133.90	150.66	C18H12
TERPHEN	66.04	123.30	58.70	79.26	95.92	109.33	128.74	141.44	160.44	C18H14
TERPHEN.	127.59	126.86	57.84	77.65	93.70	106.63	125.34	137.59	155.94	C18H13
CL2CHDR	30.48	88.45	27.55	34.75	40.06	44.91	53.01	57.69	.00	C6H5CL2
CL2CHD	5.96	88.93	29.42	37.04	42.70	47.91	56.57	61.72	.00	C6H6CL2
CLCHD.	41.17	81.42	23.71	31.38	37.37	42.41	51.46	56.74	.00	C6H6CL
BZ	19.80	64.24	19.44	26.64	32.76	37.80	45.24	50.46	58.38	C6H6
CLCHD	16.65	81.90	25.58	33.67	40.01	45.41	55.02	60.77	.00	C6H7CL

CYC6H7	49.93	72.01	20.79	28.43	35.12	40.56	48.71	54.41	.00	C6H7
CHD13	25.41	72.49	22.66	30.72	37.76	43.56	52.27	58.44	67.52	C6H8
CLMECHD.	32.31	86.43	29.67	39.82	47.40	53.30	63.07	69.46	.00	C7H8CL
CLMECHD	7.79	86.91	31.54	42.11	50.04	56.30	66.63	73.49	.00	C7H9CL
MECHD.	43.45	80.13	26.02	35.32	43.54	50.05	59.97	66.89	.00	C7H9
MECHD	18.93	80.61	27.89	37.61	46.18	53.05	63.53	70.92	82.02	C7H10
CPICL2CD.	47.15	122.13	50.46	65.26	76.10	84.77	97.48	105.60	.00	C12H8CL3
BP3R	57.84	115.10	46.62	61.89	73.41	82.27	95.93	104.65	.00	C12H9CL2
BP1R	54.56	113.73	46.53	61.35	72.40	81.36	94.68	103.33	.00	C12H9CL2
BP2R	54.36	113.85	46.72	60.26	71.19	80.59	93.13	101.55	.00	C12H9CL2
CPICL2CD	22.63	122.61	52.33	67.55	78.74	87.77	101.04	109.63	.00	C12H9CL3
BP2	29.84	114.33	48.59	62.55	73.83	83.59	96.69	105.58	.00	C12H10CL2
BP1	30.04	114.21	48.40	63.64	75.04	84.36	98.24	107.36	.00	C12H10CL2
BP3	33.32	115.58	48.49	64.18	76.05	85.27	99.49	108.68	.00	C12H10CL2
PHICLCHD.	65.05	106.82	42.88	56.89	68.50	78.09	91.58	100.60	.00	C12H10CL
PHICLCHD	40.53	107.30	44.75	59.18	71.14	81.09	95.14	104.63	.00	C12H11CL
PHCHD.	75.39	100.40	39.04	53.48	65.85	75.61	90.03	99.81	.00	C12H11
PHCHD	50.87	100.88	40.91	55.77	68.49	78.61	93.59	103.84	118.58	C12H12
TRIPHCL2	46.98	121.02	68.82	83.18	98.12	110.08	127.28	139.66	.00	C18H10CL2
OPH3CL2R	162.17	143.27	66.71	84.76	99.47	110.64	126.26	136.31	.00	C18H11CL2
TRIPHCL	54.39	115.38	64.89	79.27	94.42	106.67	124.48	137.39	.00	C18H11CL1
TPHF2R	94.04	129.44	60.51	81.27	98.84	112.16	131.22	143.19	.00	C18H11CL2
TRIPHENE	61.80	104.80	60.96	75.36	90.72	103.26	121.68	135.12	153.96	C18H12
TPHF3R	101.45	122.42	56.58	77.36	95.14	108.75	128.42	140.92	.00	C18H12CL1
TPHF2	69.52	129.92	62.38	83.56	101.48	115.16	134.78	147.22	.00	C18H12CL2
PHPHPHCL2	51.22	139.52	66.54	86.86	103.40	116.10	134.20	146.08	.00	C18H12CL2
TPH7R	72.67	149.40	70.58	92.31	108.91	121.58	140.56	152.75	.00	C18H12CL3
OPH3CLR	121.04	132.57	63.56	82.04	97.39	109.32	126.47	137.84	.00	C18H12CL1
MPH3CL	51.22	139.52	66.54	86.86	103.40	116.10	134.20	146.08	.00	C18H12CL2
OPH3CL2	53.61	138.47	68.36	87.56	103.31	115.43	132.68	143.95	.00	C18H12CL2
OPH3CL2	53.61	138.47	68.36	87.56	103.31	115.43	132.68	143.95	.00	C18H12CL2
TPHF1R	108.86	115.40	52.65	73.45	91.44	105.34	125.62	138.65	.00	C18H13
PHPHPHCL	58.63	132.50	62.61	82.95	99.70	112.69	131.40	143.81	.00	C18H13CL
TPH4R	79.88	141.12	66.84	87.31	104.00	117.40	136.21	148.70	.00	C18H13CL2
TPHF3	76.93	121.52	58.45	79.65	97.78	111.75	131.98	144.95	.00	C18H13CL
TPH3R	80.08	141.00	66.65	88.40	105.21	118.17	137.76	150.48	.00	C18H13CL2
TPH7	48.15	149.88	72.45	94.60	111.55	124.58	144.12	156.78	.00	C18H13CL3
TPH8R	82.81	143.10	66.93	87.81	105.05	118.33	137.46	150.18	.00	C18H13CL2
TPH6R	80.08	141.00	66.65	88.40	105.21	118.17	137.76	150.48	.00	C18H13CL2
OTERPHENR	129.98	125.55	59.63	78.13	93.69	105.90	123.67	135.57	156.07	C18H13
TPH11R	82.81	143.10	66.93	87.81	105.05	118.33	137.46	150.18	.00	C18H13CL2
OPH3CL	61.02	131.45	64.43	83.65	99.61	112.02	129.88	141.68	.00	C18H13CL
OTERPHEN	68.43	121.68	60.50	79.74	95.91	108.61	127.08	139.41	160.57	C18H14
MPH3	66.04	122.73	58.68	79.04	96.00	109.28	128.60	141.54	160.42	C18H14
MPH3PH	66.04	122.73	58.68	79.04	96.00	109.28	128.60	141.54	160.42	C18H14
TPH4	55.36	141.60	68.71	89.60	106.64	120.40	139.77	152.73	.00	C18H14CL2
TPH3	55.56	141.48	68.52	90.69	107.85	121.17	141.32	154.51	.00	C18H14CL2
TPH2R	87.49	132.61	62.72	84.49	101.51	114.76	134.96	148.21	.00	C18H14CL
TPH12R	90.22	134.70	63.00	83.90	101.35	114.92	134.66	147.91	.00	C18H14CL
TPH1R	90.22	134.70	63.00	83.90	101.35	114.92	134.66	147.91	.00	C18H14CL
TPH11	58.29	142.20	68.80	90.10	107.69	121.33	141.02	154.21	.00	C18H14CL2
MTERPH	66.04	122.73	58.68	79.04	96.00	109.28	128.60	141.54	160.42	C18H14
TPHF1	84.34	114.50	54.52	75.74	94.08	108.34	129.18	142.68	161.66	C18H14
TPH8	58.29	143.58	68.80	90.10	107.69	121.33	141.02	154.21	.00	C18H14CL2

TPH6	55.56	141.48	68.52	90.69	107.85	121.17	141.32	154.51	.00	C18H14CL2
TPH5R	90.22	134.70	63.00	83.90	101.35	114.92	134.66	147.91	.00	C18H14CL
TPH2	62.97	133.09	64.59	86.78	104.15	117.76	138.52	152.24	.00	C18H15CL
TPH1	65.70	135.18	64.87	86.19	103.99	117.92	138.22	151.94	.00	C18H15CL
TPH12	65.70	135.18	64.87	86.19	103.99	117.92	138.22	151.94	.00	C18H15CL
TPH9R	97.63	126.31	59.07	79.99	97.65	111.51	131.86	145.64	.00	C18H15
TPH10R	97.63	126.31	59.07	79.99	97.65	111.51	131.86	145.64	.00	C18H15
TPH5	65.70	135.18	64.87	86.19	103.99	117.92	138.22	151.94	.00	C18H15CL
TPH10	73.11	126.79	60.94	82.28	100.29	114.51	135.42	149.67	170.08	C18H16
TPH9	73.11	126.79	60.94	82.28	100.29	114.51	135.42	149.67	170.08	C18H16
OPH3CL2R	113.63	140.97	67.49	85.95	101.09	112.73	129.27	140.11	.00	C18H12CL2

SECTION III

THERM: THERMODYNAMIC PROPERTY ESTIMATION
COMPUTER CODE FOR USE WITH
DETAILED REACTION KINETIC MECHANISMS

**THERM: THERMODYNAMIC PROPERTY ESTIMATION COMPUTER CODE FOR
USE WITH DETAILED REACTION KINETIC MECHANISMS**

ABSTRACT

Detailed reaction kinetic models using mechanisms, based upon fundamental thermodynamic and kinetic principles, are currently being developed by researchers attempting to emulate reaction systems in combustion, CVD, and other related fields. A major requirement for these simulations is accurate thermodynamic property data (estimated or experimental) for all molecular and radical species considered in a mechanism.

We have developed a computer code for an IBM PC/XT/AT or compatible which can be used to estimate, edit, or enter thermodynamic property data for gas phase radicals and molecules using Benson's group additivity method.^{<1,2,3,4>} The computer code is called **THERM** (Thermo Estimation for Radicals and Molecules). All group contributions considered for a species are recorded and thermodynamic properties are generated in NASA polynomial format (for compatibility with CHEMKIN^{<5>}) in addition to listings more convenient for thermodynamic, kinetic and equilibrium calculations. Polynomial coefficients are valid from 300-5000 K. In addition, THERM contains a chemical reaction interpreter which can be used to calculate thermodynamic property changes for chemical reactions as functions of temperature. This interpreter can process CHEMKIN input files.

INTRODUCTION

Benson's group estimation technique is an accurate method for the estimation of ideal gas phase heat capacities, heats of formation, and entropies of molecules. This technique is thoroughly discussed in Benson's text **Thermochemical Kinetics**^{<1>} as well as other sources.^{<2,3,4,6>} This method assumes that the properties for a chemical substance are the sum of the contributions from each group or polyvalent atom (central atom) in that molecule. It is referred to as a second order estimation technique since next-nearest-neighbor corrections, and to some extent, chemical structure are accounted for. Estimation based upon chemical bond contributions alone are known as first order estimation techniques, while those based upon atomic contributions alone are referred to as zero order techniques.^{<7>} The second order estimates are naturally more accurate than lower order techniques, however, more information about the molecule is required. Several other estimation techniques based upon group contribution principles are presented in Reid, Prausnitz, and Sherwood.^{<4>} This method, however, has become the most widely accepted due, in part, to its ease of use and relative accuracy when compared with other techniques.

Group contributions were derived by Benson and co-workers^{<2>} and various other researchers^{<6,8,9,10,11,12,13,14,15>} by breaking similar groups of

molecules with known thermodynamic properties into their constituent groups and then performing multivariable linear regression to find group contributions which gave the best fit to available experimental property data.

To use Benson's method, one must become familiar with the notation used to describe the groups. For example if we consider chlorobenzene (C_6H_5Cl) we say that it has one $C_B-(Cl)$ group and five $C_B-(H)$ groups. $C_B-(Cl)$ refers to a carbon atom in a benzene ring which is attached to a Cl atom, while $C_B-(H)$ refers to a carbon atom in a benzene ring which is attached to an H atom. THERM identifies $C_B-(Cl)$ as CB/CL and $C_B-(H)$ as CB/H. For a second example consider propane (C_3H_8). This molecule contains two $C-(H_3)(C)$ groups for the two terminal methyls, and one $C-(H_2)(C_2)$ for the center CH_2 group. THERM identifies $C-(H_3)(C)$ as C/C/H3, with $C-(H_2)(C_2)$ identified as C/C2/H2. In addition, various corrections for symmetry, optical isomers, ring structure, steric effects must be included where necessary. More examples are presented in the THERM Users Manual which appears in appendix III - C.

OTHER COMPUTER IMPLEMENTATIONS OF BENSON'S METHOD:

Benson's method has been programmed by others.^{<16,17,18>} The most notable implementation of this estimation technique on computer is the code called CHETAH^{<16,17>} which is distributed by ASTM. This program has been in use since 1974. Its primary purpose is to

predict chemical reactivity hazards. Many publications are available which demonstrate its usefulness.^{<7>}

THERM was not designed to compete with or replace this code. It was written to automate several tasks which are routine to high temperature reaction modeling studies. There are several important differences between THERM and CHETAH. THERM estimates properties between 300 and 5000 K while CHETAH estimates are valid from 300 - 1500 K, a range less suitable for combustion studies. THERM generates thermodynamic property functions in the NASA format but does not address hazard assessment. Properties for both radicals and molecules can be estimated using THERM, while CHETAH is used for stable molecules only. The user interface for THERM is a little more friendly; CHETAH requires the user to look up a reference number for each group in a molecule and then enter the reference numbers to build a species (reference numbers consist of the table and line number for a particular group). THERM, on the other hand, identifies the group name directly. Other codes have been developed, however, which break a molecule down into its constituent groups automatically after the user enters a structural representation of the species;^{<18>} THERM makes no attempt to determine groups from a graphical representation such as this.

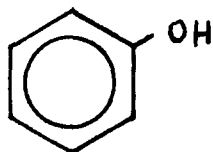
The method for calculation of radical species is similar to that implemented by Muller, Scacchi, and Come^{<18>}, but was developed independently.

SOURCE OF GROUP CONTRIBUTION DATA:

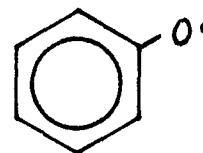
Group data for molecules containing C, O, N, S, and halogen atoms were obtained from Benson^{<1,2,3>}; Reid, et al.^{<4>}; Stein and Fahr^{<12>}; Cohen^{<6>}; and Patel, Ritter, and Bozzelli.^{<13>} Radical group contributions were derived from Benson^{<1>}, McMillen and Golden^{<19>}, Griller^{<20>} and Lossing.^{<21,22>} Bond dissociation increments^{<14>} were derived from Tsang^{<23>}, Slagle and Gutman^{<24,25>}, McMillian and Golden.^{<19>} Ring corrections for C, O, N, and S containing rings were obtained by Patel, Ritter, and Bozzelli.^{<13>}

SOME EXAMPLES OF THE USE OF THIS PROGRAM:

In Table III.i, ΔH_f° for 27 assorted species are compared with literature values obtained from various sources as noted. In most cases, estimates agree within 1 Kcal/mol. Deviations range from 0.0 Kcal/mol for chloroethane (C₂H₅Cl) to 3.61 Kcal/mol for pyrene (C₁₆H₁₀).



PHENOL



PHENOXY

The structures for phenol and phenoxy radical are shown above. ΔH_f° (298 K) for phenol (C₆H₆O) is estimated as -22.30 Kcal/mol; while Burcat^{<26>} gives -23.03 Kcal/mol. Seven group contributions are considered for phenol (see

Fig. 3.1). Phenol is comprised of 5 CB/H groups [CB-(H)], one CB/O group [CB-(O)], and one O/CB/H group [O-(H)(C)]. Groups in brackets refer to names appearing in Benson^{<1>}; while those with slashes are the equivalent group name identified by THERM (see Fig. 3.1). Figure 3.1 is a sample of the documentation generated when estimating a species. Elemental formula (C₆H₅OH), Cp infinity (limiting high temperature heat capacity), symmetry number used to correct entropy, and the number of rotors in the molecule (if any) are also recorded (see table III.ii for examples).

Properties for radicals may be estimated two different ways. One may estimate thermodynamic properties directly with radical group contributions as described in Benson.^{<1>} A second method applies a bond dissociation (BD) increment to stable molecules reflecting loss of an H atom from that species. We prefer this method, especially when estimating resonantly stabilized radicals. Documentation for phenoxy radical, which was estimated in this way, is shown in figure 3.1. Additional notes which are recorded for radicals include bond dissociation energy (298 K) for loss of hydrogen atom from the parent molecule, entropy correction for a free electron, and the name of the parent molecule. $\Delta H_f(298)$ for phenoxy is estimated as 12.10 Kcal/mol while Burcat^{<26>} gives ΔH_f equal to 11.40 Kcal/mol a difference of only 0.70 Kcal/mol as shown in Table III.i.

Figure 3.2 shows NASA format polynomial coefficients generated by THERM for phenol and phenoxy radical (this format is required by CHEMKIN). Polynomial coefficients are valid over the temperature range from 300 - 5000 K. The first line of figure 3.2 includes the species name, creation date/reference, elemental composition, phase, lower and upper temperature limits for the polynomial, and the break point temperature (T_{bk}). Fourteen coefficients follow. The first seven coefficients are used to calculate properties at temperatures above T_{bk} , while the second seven coefficients apply to temperatures below T_{bk} (as described by Kee^{<31>} and Burcat^{<26>}). The break point temperature (T_{bk}) is located at a point of tangency between the two polynomials. T_{bk} is determined by matching C_p , H_f° , and S° to 0.005 % ; while dC_p/dT , dH_f/dT , and dS/dT are matched within an absolute tolerance of 0.005. Solving for a point of tangency between two polynomials differs from the method cited by Kee, et.at.^{<31>} It should be noted that midpoint temperatures for our polynomials determined by this matching criteria are usually not the more common 1000 K calculated with other fitting methods.^{<27,28,29>}

In Fig. 3.3, a portion of a thermo table lists data for several substituted aromatics. The list contains species name, $\Delta H_f(298)$, $\Delta S(298)$, and C_p at 300 - 1500 K. In addition, creation date, elemental composition, and phase (g) are recorded. An extended table to 5000 K can

also be generated. Units for this table are Kcal/mol for ΔH_f and cal/mol K for ΔS and C_p , however tables can also be created with units of KJ/mol (J/mol K).

Note that figure 3.1 lists C_p (1500K) as 0.0 since no contribution was available at this temperature for one of the groups in phenol. However, the temperature range for C_p data can be extended with THERM to 5000 K by using available low temperature C_p data (300 - 1000 K). This is done by projecting an asymptote to the high temperature limiting heat capacity (C_p infinity). To do this we use an harmonic oscillator equation (HOE) derived from statistical mechanics to describe vibrational contributions to C_p . Two polynomials which overlap by 500 K are then determined by linear regression of data approximated with this equation. A point of tangency (T_{pk}) is determined between the polynomials using the Newton/Raphson method.

Heat capacity estimates determined in this fashion are compared with literature data in figure 3.4 for dimethyl ether, phenol, and biphenyl. It should be emphasized that the solid lines are generated from group additivity values alone, while symbols (literature values) result from rigorous calculations requiring frequency data for all vibrational modes in addition to contributions from all restricted rotors in the particular species. We obtain excellent agreement with typical maximum errors less than two percent. Literature data for this comparison are obtained from Stull^{<30>} for dimethyl ether and from

Burcat^{<26>} for biphenyl and phenol. Heat capacity estimates for other species agree similarly when compared to available literature data.

Once one records an estimate with THERM (figure 3.1), polynomials and tables (figures 3.2 and 3.3) can be recalculated automatically to reflect changes or improvements made to the group contribution database.

One may enter data from the literature directly into the data files. Automatic recalculation does not effect literature data, or any species where auto-recalculation has been disabled.

Reaction analysis is another useful function incorporated into this code. One may calculate thermodynamic property changes for a desired reaction or an entire CHEMKIN input file. The thermodynamic properties which are calculated are ΔU_r (ΔE_r), ΔH_r , ΔS_r , ΔG_r , and Af/Ar: ratio forward to reverse Arrhenius A factors. All species appearing in a reaction must be defined in a database similar to Figure 3.2. Property changes are estimated as a function of temperature over a range specified by the user. This is useful for kineticists wishing to check thermodynamic and kinetic consistency of reaction mechanisms being developed.

Some important aspects of this program are heat capacity extrapolation to 5000 K, thermo property polynomial determination, and calculation of thermodynamic property changes for reaction.

More examples of the use of THERM appear in appendix III-C, the THERM Users Manual. Extensive source code listings are given in appendices V-A to V-F for all fortran programs and subroutines which constitute the THERM package.

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APPENDIX III-A

TABLES for SECTION III

TABLE III.i
Hfo(g) [kcal/mol]

formula	species	calc	exp	deviation	ref
C5H6	cyclopentadiene	32.4	31.94	0.46	32
C7H8	toluene	11.81	11.99	-0.18	"
C8H8	styrene	35.22	35.30	-0.08	"
C8H10	ethyl benzene	6.95	7.15	-0.2	"
C9H8	indene	40.42	39.08	1.34	"
C9H10	indane	14.74	14.42	0.32	"
C9H12	n-propyl benzene	2.09	1.89	0.2	"
C9H12	i-propyl benzene	0.63	0.96	-0.33	"
C10H8	azulene	74.92	73.5	1.42	"
C10H8	naphthalene	36.0	36.05	-0.05	"
C12H10	acenaphthene	36.65	37.4	-0.75	"
C14H10	anthracene	52.2	55.2	-3.0	"
C14H10	phenanthrene	50.0	49.52	0.48	"
C16H10	fluoranthene	68.39	69.78	-1.39	"
C16H10	pyrene	55.20	51.59	3.61	"
C18H12	triphenylene	61.80	63.4	-1.6	"
C2H6O	dimethyl ether	-43.40	-43.99	0.59	30
C6H7N	aniline	20.80	20.76	0.04	"
C2H5Cl	chloroethane	-26.70	-26.70	0.0	"
C6H5Cl	chlorobenzene	12.70	12.39	0.31	"
C6H5F	fluorobenzene	-26.30	-27.86	1.56	"
C6H5I	iodobenzene	39.00	38.85	0.15	"
C7H8	toluene	11.81	11.95	-0.14	"
C6H6O	phenol	-22.30	-23.03	0.73	26
C6H5O	phenoxy radical	12.10	11.40	0.70	"
C12H10	biphenyl	42.92	43.53	-0.61	"

TABLE III.ii

<u>SPECIES</u>	<u># ROTORS</u>	<u>SYMMETRY NUMBER</u>
CH ₄	0	12
CH ₃ Cl	0	3
C ₂ H ₆	1	18
C ₃ H ₈	2	18
C ₂ H ₅ Cl	1	3
biphenyl	1	8
o,m-chlorobiphenyl	1	2
benzene	0	12
chlorobenzene	0	2
toluene	1	6
m-terphenyl	2	6
p-terphenyl	2	16

APPENDIX III-B

FIGURES for SECTION III

SPECIES
 PHENOL
 Thermo estimation for molecule
 PHENOL C6H5OH
 UNITS:KJ
 GROUPS 3
 Gr # - GROUP ID - Quantity
 1 - O/CB/H - 1
 2 - CB/O - 1
 3 - CB/H - 5
 Hf S Cp 300 400 500 600 800 1000 1500
 -93.30 314.52 102.09 133.47 160.33 181.29 211.79 232.46 .00
 CPINF = 307.60
 NROTORS: 1
 SYMMETRY 2
 CREATION DATE: 1/23/89
 ENDSPECIES
 SPECIES
 PHENOXY
 Thermo estimation for radical
 PHENOXY C6H5O
 RADICAL BASED UPON PARENT PHENOL
 PARENT FORMULA C6H5OH
 PARENT SYMMETRY 2
 UNITS:KJ
 GROUPS 4
 Gr # - GROUP ID - Quantity
 1 - O/CB/H - 1
 2 - CB/O - 1
 3 - CB/H - 5
 4 - PHENOXY - 1
 Hf S Cp 300 400 500 600 800 1000 1500
 50.63 303.64 96.32 125.02 149.75 169.12 197.40 216.52 .00
 CPINF = 282.66
 SYMMETRY 2
 R ln(2) has been added to S to account
 for unpaired electron
 BOND 361.92
 CREATION DATE: 1/23/89
 ENDSPECIES

Figure 3.1.

PHENOL	1/23/89	C	6H	60	1	OG	300.000	5000.000	1409.000	11
	1.63648312E+01	1.70449252E-02	5.78030903E-06	8.92493813E-10	5.15898598E-14					2
	-1.90753231E+04	-6.50928503E+01	-4.55522360E+00	7.29677980E-02	-6.36049836E-05					3
	2.81167771E-08	-4.93074225E-12	-1.25992897E+04	4.46177541E+01						4
PHENOXY	1/23/89	C	6H	50	1	OG	300.000	5000.000	1406.000	01
	1.56466637E+01	1.53982771E-02	-5.27582225E-06	8.20290758E-10	-4.76482873E-14					2
	-1.39961846E+03	-6.16489564E+01	-3.72846136E+00	6.60173510E-02	-5.64043045E-05					3
	2.43749961E-08	-4.19086680E-12	4.71909590E+03	4.03825155E+01						4

Figure 3.2.

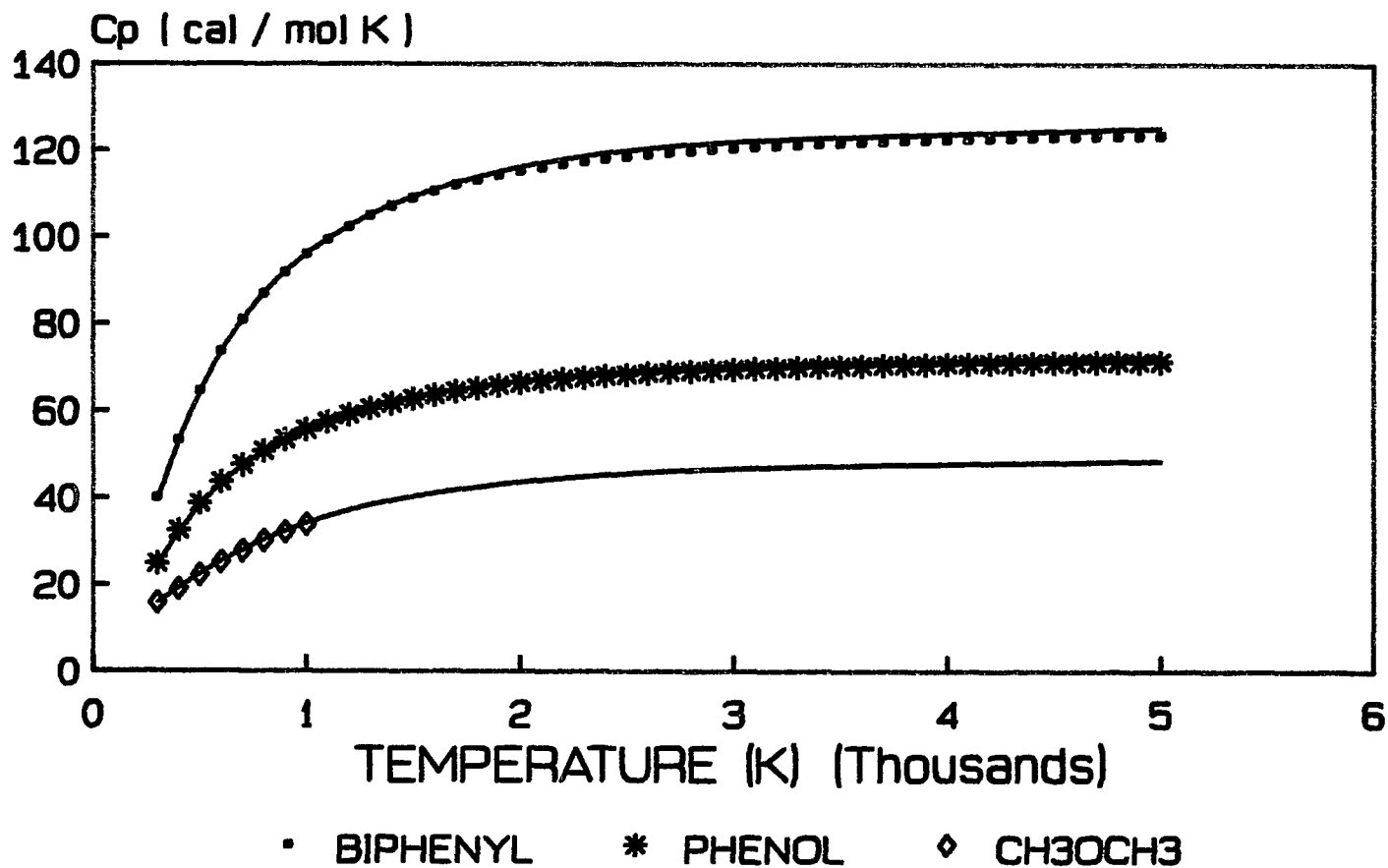
UNITS:KCAL

EXAMPLE THERMODYNAMIC PROPERTY TABLE (SHORT FORMAT)

SPECIES	HF(298)	S(298)	CP300	CP400	CP500	CP600	CP800	CP1000	CP1500	DATE	SOURCE	ELEMENTS	PH
C6H5F	-26.30	72.38	22.60	29.83	35.73	40.53	47.57	52.27	58.95	1/23/89	THERM	C 6 H 5 F	1 0 G 0
C6H6	19.80	64.25	19.54	26.69	32.68	37.68	45.30	50.60	58.17	1/23/89	THERM	C 6 H 6	0 0 G 0
C6H5CL	12.70	75.18	25.39	30.94	35.87	40.20	47.19	52.23	58.97	1/23/89	THERM	CL 1 C 6 H 5	0 0 G 0
C6H5I	39.00	79.98	24.26	31.13	36.74	41.31	48.04	52.56	59.05	1/23/89	THERM	C 6 H 5 I	1 0 G 0
PHENOL	-22.30	75.18	24.50	32.05	38.22	43.24	50.64	55.62	62.94	1/23/89	THERM	C 6 H 6 O	1 0 G 1
PHENOXY	12.10	72.58	23.10	30.02	35.69	40.33	47.19	51.80	58.42	1/23/89	THERM	C 6 H 5 O	1 0 G 0
C6H5	81.19	66.51	18.86	25.35	30.76	35.26	42.08	46.79	53.43	1/28/89	THERM	C 6 H 5	0 0 G 0
BIPHENYL	42.92	93.90	39.22	52.98	64.24	73.42	86.97	96.09	109.28	1/23/89	THERM	C 12 H 10	0 0 G 1

Figure 3.3.

Figure 3.4 : Cp (T)
COMPARISON OF ESTIMATES with LITERATURE



APPENDIX III-D

THERM USERS MANUAL

THERM

Thermodynamic property

Estimation

for

Radicals and Molecules

USER'S MANUAL

March 16, 1987

by

Edward R. Ritter and Joseph W. Bozzelli

**Department of Chemical Engineering, Chemistry,
and Environmental Science**

**New Jersey Institute of Technology
Newark, NJ. 07102**

Questions or requests for copies of this program should be addressed to:

Joseph W. Bozzelli
Chemical Engineering Dept.
New Jersey Inst. of Tech.
323 King Blvd.
Newark, NJ. 07102

Copies of this program and documentation are available on disk free of charge. To obtain a copy of this software and documentation, send one of the following to the above address:

- A. 1 - 1.2 Mb floppy disk (5.25")
- B. 1 - 720 kb floppy disk (3.5")
- C. 2 - 360 kb floppy disks (5.25")

Make sure the disk (s) is formatted and contains the MS-DOS system (*command.com*, etc.). Your disk (s) will be returned with THERM and this manual installed.

Contact the authors at the above address for further details.

This program may be copied freely, however, we request that users notify us so that we may keep them informed of any improvements or problems with this program.

Please contact us if you have any questions, comments, or problems with this program package.

E. R.

THERM

Thermo Estimation for Radicals and Molecules

System Requirements:

- * IBM PC / AT or COMPATIBLE
- * 512 K available memory
- * 1 - 1.2 Mb (5.25 in.), or 720 kb (3.5 in.), or
2 - 360 K floppy drives (hard disk may be used
if all files are copied into a subdirectory)
- * 8087 or 80287 "math processor"
NOTE: the program will not run if the computer
does not have a math processor.

Programs included in this package:

EXE files:

- * THERM.EXE - therm main program.
group estimation procedure.
- * THERMFIT.EXE - thermo fitting procedure:
fit Cp data to polynomials and
output in NASA format.
input file : list file "*.LST"
output file: polynomial file "*.DAT"
- * THERMLST.EXE - thermo listing procedure:
create a thermo table from
polynomials.
input file : polynomial file "*.DAT"
output file: list file "*.LST"
- * THERMRXN.EXE - reaction analysis procedure:
calculate ΔH_r , ΔS_r , ΔU , (ΔE),
 ΔG_r , and ratio Arrhenius A factors
forward to reverse (Af/Ar).
CHEMKIN input files can be processed
(only gas phase molecules and radi-
cals are supported:
no ions, liquids, or solids !)
- * STOD.EXE - sequential to direct file conversion
utility. THERM requires polynomial
files "*.DAT" and documentation files
 "*.DOC" to be formatted to specific
record lengths (DIRECT ACCESS FORMATTED).
DAT files require 80 character records
while DOC files require 70 character
records. In sequential files, record
length varies from line to line, therefore
if one edits a file using a word processor
this utility may be used to pad each record
to the required length. All editing must be
done as ASCII files w/ no formatting.

EXAMPLE SPECIES DATABASE FILES:

* THERMO.DOC - sample documentation file "*.DOC".
* THERMO.LST - sample database listing file "*.LST".
* THERMO.DAT - sample nasa format database
listing "*.DAT".

GROUP DATABASE FILES:

* HC. - hydrocarbon groups.
* HCO. - oxygen containing groups.
* CDOT. - radical groups.
* BD. - bond dissociation increment
groups.
* CLC. - Chlorinated hydrocarbon groups.
* CYCH. - ring corrections.
* HCN. - nitrogen containing groups.

BOOTING UP the THERM program:

To boot up THERM place the disk marked "THERM PROGRAM DISK:
DRIVE A:" in drive A and then reboot your computer ("Ctrl-Alt-
Delete"). At the prompt for drive A:, type "THERM" and hit
return. The program title page should appear with the message:

```
***Loading Configuration File***  
***LOADING GROUP DATABASE FILES***
```

When all files are loaded, the number of groups in the database
is displayed. Hit return and you advance to the main menu:

THERM MAIN MENU.

SAMPLE SESSION: Calculate and file thermodynamic properties
of PHENOL and PHENOXY RADICAL.

note: Help is available for most input if "?" is entered instead
of the requested input. The letter "Q" (upper or lower case) is a
reserved character used to "QUIT" back to a previous menu or point in
the program. As a result the first character of a species ID

should not begin with either of these characters (Q or ?).

SHORT SAMPLE SESSION:

In the following paragraphs, quote marks are used for emphasis only. You should only enter what is inside the quote marks.

1. At the main menu prompt hit return to accept the default option "1 - ENTER/ESTIMATE SPECIES".

2. You are now asked to "enter species name (ID)". Enter "phenol" followed by a return (upper or lower case are accepted; but THERM converts all strings to capital letters).

3. At this point you are asked to enter the "elemental formula" for the species. Enter "C6H5OH" or "C6H6O" whichever you prefer.

4. You are now asked to verify that the formula was interpreted correctly. Hit return if correct or enter "Q" if it was not.

5. After a brief description of how THERM calculates radicals, you are asked to enter the number of groups in this species. Phenol is comprised of 5 - CB/H groups, 1 - CB/O group, and 1 - O/CB/H group. This is a total of 7 groups. Enter "7" at this prompt.

If one wants to enter literature data instead of estimating thermo properties using Benson's method, they should simply enter "0" when prompted for the number of groups in the species. THERM will then prompt for literature data to be input.

6. You are now asked to enter the number of different groups which are present in this species. Above we see that PHENOL only has 3 different groups. Enter "3" at this prompt.

7. Enter the number of rotors (tops) in the species. Default is no rotors. The number of rotors is used to adjust the high temperature limiting heat capacity. Phenol has 1 rotor (-OH), enter 1 and press return.

8. It is now time to enter the groups which are present in phenol. Enter the following:

"CB/H,5"	(note 1: a blank or comma are the same. "CB/H 5" is equivalent.)
"CB/O"	(note 2: if no quantity is entered quantity "1" is understood)
"O/CB/H"	

In group names, slashes delimit atoms or functional groups. The letters appearing before the first slash represent the central atom or next nearest neighbor (or other) correction (ex: C/, O/, or /N (central atom) or CIS/, ORT/, /MET, GAUCHE/, or OI/ (corrections)).

The atoms or functional groups that follow are each delimited with slashes "/" and appear in alphabetic order (ex: Bensons

O-(H)(C) would be O/C/H, C-(Cd)(C)2(H) would be C/C2/CD/H2,
AND C-(Cd)(CB)(H)2 would be C/CB/CD/H2).

9. The symmetry number for phenol is 2. Enter "2" at this prompt.

The SPECIES SCREEN appears showing all data entered in addition to the thermodynamic properties which have been calculated. An EDIT option is available; enter "?" for more details (we will not edit at this point).

10. Hit return to advance to the SPECIES ESTIMATION OPTIONS MENU.

11. Choose option "F" to add this species to a file.

12. You are asked for a filename. Enter "B:THERMO".

13. Since "B:THERMO.LST" already exists, the following message appears:

THERMO.LST already exists:

- 1 - DELETE (OVERWRITE)
- 2 - APPEND (ADD TO THE END OF THE FILE)
- 3 - ENTER A DIFFERENT FILENAME

ENTER OPTION:

We want to add Phenol to the end of this file so enter "2".

14. Similarly "B:THERMO.DOC" already exists. Again enter "2" and the data for phenol will be added to the end of these files.

You now have returned to the SPECIES ESTIMATION OPTIONS MENU. Note that you are notified that PHENOL is the last species that you have filed. Now that these files are connected you will not be asked to input the filename when filing. To close or change output files "Q" quit back to the MAIN menu and choose option "*".

15. One can now calculate the properties of PHENOXY radical. To do this choose option "R". The RADICAL ESTIMATION MENU appears listing all bond dissociation "BD" increments which are defined. For a description of these increments enter "?" and then the increment group name (not the group number) when prompted. We are interested in the "PHENOXY" bond dissociation increment. Enter "PHENOXY" when you are done looking at the help on these groups.

16. You must now enter the symmetry number for PHENOXY radical. Enter "2" at this prompt. Had the symmetry number been 1 you could have just hit return since if no symmetry number is entered "1" is assumed.

17. Now enter the name for your radical (9 characters maximum). Enter "PHENOXY" or "C6H5O." whichever you prefer.

18. The formula for phenoxy is C6H5O; so enter "C6H5O".

19. Hit return to confirm that the elemental composition is correct.

20. The species screen now displays the data for PHENOXY radical. Hit return to advance to the SPECIES ESTIMATION OPTIONS MENU.

21. Choose option "F" and PHENOXY's data is added to the current file (since the file is already initialized you are not asked for any additional input). You return to the SPECIES ESTIMATION OPTIONS MENU automatically and are notified that PHENOXY is the last species which you filed.

22. At this point you can review the help which is available on the other options. Entering "M" will return you to PHENOL where you could use the edit option to change/add groups to estimate a substituted phenol for example meta-ChloroPhenol.

Note: Phenoxy radical could have been calculated directly (without calculating PHENOL first) if you had used the RADICAL GROUP "O/CB/." when first entering groups. Both methods of radical calculation are supported, however, use of RADICAL GROUPS in the case of resonantly stabilized allylic species may result in a significant error. These groups do not address the resonance stabilization energy accounted by BD BOND INCREMENT GROUPS.

For a more detailed example see SAMPLE SESSION.

THERM CONFIGURATION: The "THERM.CFG" file

#FILES 7 the number of group files
BD.
HC.
CYCH.
CLC. GROUP FILE NAMES
HCO.
HCN.
CDOT.
#ELEMENTS 11 the number of elements defined
C
H
O
CL ELEMENTS
S
N
F
P
I
BR
B
#HELP 8 the number of help files
THM1P1.HLP
THM1P2.HLP
THS1.HLP
THM2P1.HLP HELP FILE NAMES
THM2P2.HLP
THM3.HLP
THE1.HLP
THE2.HLP
OPTIONS: other values allowed:
THERMFIT.EXE THERMFIT.EXE D: where D: is the disk
THERMRXN.EXE THERMRXN.EXE D: drive where this
THERMLST.EXE THERMLST.EXE D: EXE file resides
#KEYS 3 The number of keys used in sorting
UNITS:KCAL **UNITS:KJ** (default to KJ units)
ERRORCK=ON **ERRORCK=OFF** (defeat error checking)
TRANGE=5000 could also be **TRANGE=2000**

MAIN MENU - options and explanations:

THERM MAIN MENU

Units: Kcal/mol (cal/mol K)

3/ 5/89

-
- 1 - ENTER/ESTIMATE SPECIES
 - 2 - VIEW GROUPS
 - 3 - SELECT SHORT MENU
 - 4 - SELECT LIST FILE (*.LST)
 - 5 - REVIEW (LST FORMAT FILE)
 - 6 - GET SPECIES FROM FILE (*.DOC)
 - 7 - ReWrite THERMO FILES (*.DOC, *.LST)
 - 8 - RUN THERMFIT create NASA (*.DAT)
 - 9 - RUN THERMRXN (calculate dU, dH, dS, dG for reaction)
 - 10 - Sort & ReWrite THERMO FILES { *.DOC, *.LST }
 - 11 - Sort/Write *.LST file { no *.DOC is needed }
 - 12 - RUN THERMLST (LIST NASA FORMAT FILE) /create *.LST
 - 13 - DOS utilities
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)
 - * - CLOSE ALL OPENED FILES
 - X - EXIT PROGRAM
 - ? - HELP

enter option : { 1 }

The following pages describe each option listed above.

OPTION 1:

1 - ENTER/ESTIMATE SPECIES

This option invokes THERM'S code to calculate thermodynamic properties using Benson's group additivity method.

To estimate molecular or radical species you will be asked for specific information about the species, such as:

- * Species ID { limited to 9 characters so as to fit CHEMKIN format}
 - * # of groups in the species
 - * # of different groups to be entered (DO NOT INCLUDE BD GROUPS)
 - * Elemental formula { limited to 70 characters }
 - * Groups contained in the species
 - * species symmetry number
-

OPTION 2:

2 - VIEW GROUPS

This option allows you to review the group database currently in memory. This is useful if you are looking for a group, but have forgotten its name.

OPTION 3:

3 - SELECT SHORT/LONG MENU

This option toggles the amount of information displayed when a menu is on the screen.

The MAIN menu is not affected by this option.

LONG menu shows all information

SHORT menu only lists available options with no description

In both cases this help information is available.

OPTION 4:

4 - CHANGE SPECIES LIST FILE (*.LST)

THIS OPTION IS USED TO CHANGE THE "LST" FILE CURRENTLY IN MEMORY.

THERE ARE A MAXIMUM OF 300 SPECIES ALLOWED AT ANY TIME.

THIS DATA IS NOT PASSED TO THE REACTION ANALYSIS PROCEDURE BUT IS USED FOR SORTING AND REWRITING THE DATABASE.

THE "LST" FILE CONTAINS THE SPECIES ID (9 CHARACTERS MAX); Hf, S, Cp 300, Cp 400, Cp 500, Cp600, Cp 800, Cp 1000, Cp 1500; ELEMENTAL COMPOSITION; PHASE (G = gas), AND CAN HAVE SOME ABBREVIATED REFERENCE INFORMATION. THE "LST" FILE IS THE INPUT FOR THE NASA FORMAT DATABASE GENERATION PROCEDURE "THERMFIT".

OPTION 5:

5 - LIST THERMO D BASE FILE (*.LST)

THIS OPTION ALLOWS ONE TO REVIEW THE CURRENT "LST" FILE.

YOU CAN NOT ONLY REVIEW SPECIES NAMES BUT CAN REQUEST EXTENDED OUTPUT SUCH AS:

Hf, S, Cp 300, Cp400, Cp 500, Cp600, Cp 800, Cp 1000, Cp 1500

A DELETE/UNDELETE OPTION IS AVAILABLE IN CASE YOU HAVE DUPLICATE OR INCORRECT RECORDS.

THE "LST" FILE MUST BE REWRITTEN USING OPTION " 10 or 11" IN ORDER TO DELETE SPECIES FROM THE FILE.

OPTION 6:

6 - GET SPECIES FROM DOCUMENTATION FILE (*.DOC)

THIS OPTION REQUIRES YOU TO HAVE A DOCUMENTATION FILE WHICH CONTAINS ALL PERTINENT INFORMATION ABOUT THE SPECIES.

THE DOCUMENTATION FILE CONTAINS:

- * SPECIES ID & ELEMENTAL FORMULA
- * ALL GROUPS
- * THERMO DATA
- * BOND DISSOCIATION INCREMENT (IF A RADICAL)
- * SYMMETRY CORRECTION
- * ANY TEXT ADDED FOR REFERENCE
- * ANY ALTERATIONS MADE TO A CALCULATED VALUE (EDIT OPTION) ETC.

The user is required to enter a species name. THERM then reads into memory all data from a DOC file. The species can be edited or modified at this point just as if the user had typed in the data.

OPTION 7:

7 - ReWrite THERMO FILES (*.DOC, *.LST)

THIS OPTION RECALCULATES THERMO PROPERTIES. IT IS USEFUL IF ANY CHANGES HAVE BEEN MADE TO GROUP VALUES. THE DOCUMENTATION FILE IS READ FOR GROUPS AND THE THERMO PROPERTIES ARE RECALCULATED USING THE CURRENT GROUP VALUES.

BE WARNED: ON AN "AT" CLASS MACHINE (10 MHZ) 100 SPECIES WILL REQUIRE ABOUT 5 MINUTES FOR REGENERATION OF THE DATABASE.

A "PC" CLASS MACHINE W/ ONLY FLOPPY DRIVES WILL TAKE ~15 MINUTES.

OPTION 8:

8 - RUN THERMFIT: CREATE NASA FORMAT FILE (*.DAT)

This option spawns THERM'S heat capacity extrapolation/polynomial fitting program : THERMFIT.

"LST" file format is used as input to the program "THERMFIT.EXE".

This program converts thermo data to polynomials in NASA format for use with CHEMKIN or other codes which require this format and allow one to specify a common temperature other than 1000 K.

Two sets of polynomials are generated with a common (breakpoint) temperature determined so as to match Cp and dCp/dT. This break point is typically not the more common 1000 K as with SANDIA'S fitting code.

OPTION 9:

9 - RUN THERMRXN: REACTION ANALYSIS (del H, del U, del S, del G)

This program allows one to enter reaction expressions such as:

C6H5CL=CYC6H5. + CL

and have property change of reaction calculated from NASA format polynomials in addition to the ratio of forward/reverse A factors.

Data are taken from "DAT" files and one is prompted for a *.DAT filename. (OBVIOUSLY ALL SPECIES ID'S ENTERED IN THE REACTION EXPRESSION MUST APPEAR IN THE SPECIFIED "DAT" FILE).

Entire CHEMKIN input files can also be processed automatically.

OPTION 10:

10 - Sort, Recalculate, & ReWrite THERMO FILES (*.DOC, *.LST)

This option is essentially the same as OPTION 7 except the "DOC" file is first sorted in order of elemental composition.

Sorting is performed on the # of levels defined in the configuration file "THERM.CFG". The key word "#KEYS" is followed by the number of sort keys (or levels). The priority for sorting is determined by the order elements appear in "THERM.CFG" (configuration file).

For example: if the configuration file contains the following elements in the following order (each element actually appears on a separate line):

C H O CL N BR (and #KEYS 2)

Data is first sorted in order of increasing carbon number; then each sub group is sorted by increasing hydrogen number. If #KEYS 3 appears in the file "THERM.CFG" then sorting would continue by oxygen number. If the order elements appear in "THERM.CFG" is changed, so is the order of sorting.

Literature data are not recalculated.

OPTION 11:

11 - SORT/REWRITE *.LST FILE

Same sorting procedure as OPTION 10; but DATABASE RECALCULATION is not performed.

This option is useful if one wants to sort a "LST" file but has no documentation file to recalculate the database.

OPTION 12:

12 - RUN THERMLST: Uses NASA format "DAT" file to create "LST" format

This option spawns THERM'S listing program : THERMLST.EXE

A *.LST FORMAT FILE IS CREATED FROM A NASA FORMAT *.DAT FILE.
COEFFICIENTS ARE READ AND HEAT CAPACITY VALUES ARE GENERATED AT
300, 400, 500, 600, 800, 1000, 1500 deg K. (An extended listing
to 5000 K may also be created.)

OPTION 13:

13 - DOS UTILITIES

ALLOWS ONE TO INVOKE THE DOS INTERPRETER FROM WITHIN THE PROGRAM.
SEVERAL OPTIONS ARE AVAILABLE. CHOOSE THIS OPTION (13) FOR MORE
DETAILS.

OPTION U:

U - CHANGE UNITS

This option toggles the units which results are displayed on screen
and saved in documentation files. Units can either be Kcal/mol (Hf)
and cal/mol K (S and Cp) or KJ/mol (Hf) and J/mol K (S and Cp).

This has no effect on units saved in a "LST" file. If one adds data
to a "LST" file, units remain the same as those already in use in
that file. If one starts a new "LST" file they will be prompted for
units.

Units may be changed at various other parts of the program.

OPTION *:

* - CLOSE ALL OPENED FILES

This option is necessary to change the output or other files that are
connected.

All files are closed automatically when exiting THERM as below.

OPTION X:

**X - EXIT PROGRAM
ENDS THERM SESSION , CLOSSES ALL FILES, AND RETURNS TO DOS.**

EDIT OPTIONS ARE AVAILABLE: for both MOLECULES and RADICALS

EDITING A MOLECULE

Thermo estimation for molecule

BZ

C6H6

Gr # - GROUP ID - Quantity
1 - CB/H - 6

UNITS: Hf(Kcal/mol) S & Cp (cal/mol K)

Hf	S	Cp 300	400	500	600	800	1000	1500
19.80	64.24	19.44	26.64	32.76	37.80	45.24	50.46	58.38
CPINF	67.56							

Symmetry number used to correct S value is 12

EDIT THESE RESULTS? "Y" OR ("N")

Y <----- to edit enter "Y" at this prompt.

===== next screen =====

EDIT SPECIES MENU

(this menu for
molecules only)

-
- 1 - CHANGE SYMMETRY NUMBER
 - 2 - CHANGE/MODIFY THERMO
 - 3 - CHANGE SPECIES ID / FORMULA
 - 4 - ADD TEXT TO SPECIES SCREEN
 - 5 - RETURN TO SPECIES SCREEN
 - 6 - ADD A GROUP TO THE CURRENT SPECIES
 - 7 - DELETE A GROUP
 - 8 - CHANGE A GROUP
 - 9 - CHANGE NUMBER OF ROTORS
 - ? - HELP

enter option : { Q }

EDITING A RADICAL:

Thermo estimation for radical
PHENYL
RADICAL BASED UPON PARENT BZ

C6H5

C6H6

PARENT SYMMETRY 12

Gr # - GROUP ID - Quantity
1 - CB/H - 6
2 - BZ - 1

UNITS: Hf(Kcal/mol) S & Cp (cal/mol K)

Hf	S	Cp 300	400	500	600	800	1000	1500
81.35	68.92	18.57	25.03	30.54	35.09	41.83	46.62	53.88
CPINF	61.60							

Symmetry number used to correct S value is 2

R ln(2) has been added to S to account for unpaired electron

bond dissociation energy used= 113.650000

EDIT THESE RESULTS? "Y" OR {"N"}

Y <----- to edit enter "Y" at this prompt.

===== next screen =====

EDIT SPECIES MENU

(this menu for
radicals only)

-
- 1 - CHANGE SYMMETRY NUMBER
 - 2 - CHANGE/MODIFY THERMO
 - 3 - CHANGE SPECIES ID / FORMULA
 - 4 - ADD TEXT TO SPECIES SCREEN
 - 5 - RETURN TO SPECIES SCREEN
 - 6 - CHANGE BOND DISSOCIATION ENERGY
 - 7 - RETURN TO PREVIOUS PARENT MOLECULE
 - 8 - CHANGE NUMBER OF ROTORS
 - ? - HELP

enter option : { Q }

THE FOLLOWING PAGES GIVE BRIEF DESCRIPTIONS OF EACH OPTION

EDIT OPTIONS EXPLAINED:

OPTION 1:

1 - CHANGE SYMMETRY NUMBER

THIS OPTION ALLOWS YOU TO CORRECT/MODIFY THE SYMMETRY NUMBER WHICH YOU PREVIOUSLY ENTERED. UNLIKE IN THE ESTIMATION PROCEDURE A BLANK IS INTERPRETED AS NO CHANGE.

OPTION 2:

2 - CHANGE/MODIFY THERMO

THIS OPTION ENABLES YOU TO MAKE ANY SMALL ADJUSTMENTS TO THE CALCULATED THERMO VALUES. YOU CAN EITHER ADD A CORRECTION ((-)FOR NEGATIVE CORRECTIONS) OR REPLACE THE VALUE.

YOU CAN CHANGE Hf,S, OR A Cp VALUE (ONE AT A TIME).

ANY CHANGES YOU MAKE WILL BE RECORDED IN THE DOCUMENTATION FILE UNDER THE NAME "DELTA EDIT". THIS INSURES THAT LATER USE OF AUTOMATIC UPDATING PROCEDURES WILL CONSIDER THESE SMALL ADJUSTMENTS. IF AFTER CHANGING AND SAVING YOUR RESULTS, YOU DECIDE TO REMOVE THE "DELTA EDIT" YOU MUST DO SO OFF-LINE USING ANY CONVENIENT WORD PROCESSOR. YOU MUST EDIT THE DOCUMENTATION FILE AS AN ASCII FILE (no formatting) AND DELETE THE "DELTA EDIT" REFERENCE AND GROUP.

OPTION 3:

3 - CHANGE SPECIES FORMULA / ID

THIS OPTION ALLOWS YOU TO CHANGE THE FORMULA AND/OR SPECIES ID.

THIS IS USEFUL IF YOU CHANGE A GROUP TO FORM A NEW SPECIES RATHER THAN RE-ENTERING ALL GROUPS IN THAT SPECIES. IT IS ALSO USEFUL IF YOU MADE AN ERROR IN THE SPECIES NAME OR FORMULA. IF YOU WANT TO CHANGE THE SPECIES ID WITHOUT CHANGING THE FORMULA, ENTER A BLANK WHEN ASKED FOR THE NEW FORMULA (THE FORMULA WILL REMAIN UNCHANGED AND YOU WILL ADVANCE TO THE CHANGE SPECIES NAME PROMPT).

CHANGING A GROUP IS NOT ALLOWED FOR RADICALS ESTIMATED USING BOND INCREMENTS (8D groups). FOR MORE INFORMATION ON THIS OPTION REQUEST HELP ON OPTIONS 6, 7, OR 8.

OPTION 4:

4 - ADD TEXT TO SPECIES SCREEN

THIS OPTION ALLOWS YOU TO ENTER UP TO 50 LINES OF TEXT TO THE SPECIES SCREEN (DATA WILL SCROLL OFF THE SCREEN UNLESS YOU USE "Ctrl S" TO STOP SCROLL).

Text is stored in a DOC file.

TEXT IS USEFUL FOR ADDING ANY DOCUMENTATION YOU LIKE TO THE DOCUMENTATION FILE (EX: COMMON NAME).

OPTION 5: DEFAULT OPTION !

5 - RETURN TO THE SPECIES SCREEN:

"QUIT" RETURN TO THE PREVIOUS MENU

This is the default option.

OPTION 6:

6 - ADD A GROUP TO THE CURRENT SPECIES

THIS OPTION IS USEFUL IF YOU FORGOT A GROUP OR IF YOU ARE CREATING A NEW SPECIES BY EDITING THE GROUPS OF THE CURRENT SPECIES. THIS OPTION IS ONLY ENABLED FOR STABLE MOLECULES AND RADICALS WHICH WERE CALCULATED USING RADICAL GROUPS FROM "CDOT".

OPTION 7:

7 - DELETE A GROUP FROM THE CURRENT SPECIES

THIS OPTION IS USEFUL IF YOU ARE CREATING A NEW SPECIES BY EDITING THE CURRENT GROUPS. THIS OPTION IS ONLY ENABLED FOR STABLE MOLECULES AND RADICALS WHICH WERE CALCULATED USING RADICAL GROUPS "CDOT"; not enabled for any BD increments.

OPTION 8:

8 - CHANGE A GROUP

THIS OPTION ALLOWS YOU TO CREATE A NEW SPECIES BY EDITING THE GROUPS FROM THE PREVIOUS SPECIES. THIS IS THE MOST USEFUL OPTION OF THE THREE (6, 7, 8). YOU CAN CHANGE THE GROUP ID AND/OR QUANTITY.

EXAMPLE:

STARTING WITH BENZENE: "CB/H,6"; EDIT/ESTIMATE CHLOROBENZENE. YOU CAN CHANGE THIS FROM "CB/H,6" TO "CB/H,5" THEN YOU CAN SELECT OPTION "6" ADD A GROUP; AND ADD "CB/CL". NOW YOU HAVE THE GROUPS FOR CHLOROBENZENE. ALL YOU HAVE TO DO IS CHANGE THE SYMMETRY NUMBER, FORMULA, AND SPECIES ID.

THIS MIGHT NOT SEEM LIKE IT SAVES WORK; BUT IF YOU HAVE A SPECIES WITH 10 OR 15 DIFFERENT GROUPS, AND ALL YOU NEED TO CHANGE IS ONE TO CREATE YOUR NEW SPECIES, THERE IS A SIGNIFICANT SAVINGS IN TIME OVER ENTERING ALL 10 - 15 GROUPS.

OPTION 9:

9 - Change the number of rotors in the species

This allows one to change the number of rotors which are considered to be free rotors at high temperature (5000 K).

Molecules with attached tops that have large barriers to internal rotation ($V > 10$ kcal/mol) cannot be considered free rotations even at high temperature.

The number of free rotors changes the limiting heat capacity C_p infinity, since each vibrational mode contributes 1 heat capacity unit while a free rotation only contributes 1/2 a heat capacity unit and a vibrational mode is lost when a free rotor exists.

OPTIONS FOR RADICAL SPECIES

OPTION 6 - RADICAL SPECIES:

6 - CHANGE BOND DISSOCIATION ENERGY FOR A RADICAL

THIS OPTION ALLOWS YOU TO ALTER THE BOND ENERGY FROM ONE OF THE BD GROUPS TO MEET YOUR NEEDS. A NEW GROUP CALLED "DELTA BOND ENERGY" IS CREATED AND ADDED TO THE DOCUMENTATION FILE.

AN EXAMPLE IS THE ESTIMATION OF THE CHLOROPHENYL RADICAL.

THE BOND ENERGY USED FOR LOSS OF H ATOM FROM BENZENE IS 113.5 Kcal. THAT FOR LOSS OF H ATOM FROM CHLOROBENZENE IS LOWER BY ABOUT 1 Kcal.

TO CREATE CHLOROPHENYL RADICAL YOU CAN APPLY THE "BZ" BOND INCREMENT GROUP TO CHLOROBENZENE AND THEN USE THIS OPTION TO CORRECT THE BOND ENERGY USED IN THE CALCULATION OF CHLOROPHENYL TO 112.5 Kcal.

OPTION 7 - RADICAL SPECIES:

7 - RETURN TO PREVIOUS PARENT MOLECULE

THIS OPTION IS THE SAME AS OPTION "M" FROM THE SPECIES ESTIMATION OPTIONS MENU. IT IS INCLUDED HERE FOR CONVENIENCE ONLY.

WHEN THIS OPTION IS CHOSEN ALL DATA ON THE RADICAL IS DISCARDED.

OPTION 8:

8 - Change the number of rotors in the species

This allows one to change the number of rotors which are considered to be free rotors at high temperature (5000 K).

Molecules with attached tops that have large barriers to internal rotation ($V > 10$ kcal/mol) cannot be considered free rotations even at high temperature.

The number of free rotors changes the limiting heat capacity C_p infinity, since each vibrational mode contributes 1 heat capacity unit while a free rotation only contributes 1/2 a heat capacity unit and a vibrational mode is lost when a free rotor exists.

SPECIES ESTIMATION OPTIONS MENU

Units: Kcal/mol (cal/mol K)

- R - CALCULATE RADICAL BASED UPON PREVIOUS SPECIES
- F - ADD CURRENT SPECIES TO OUTPUT FILE
- H - TOGGLE (SHORT/LONG) MENU
- P - RETURN TO PREVIOUS SPECIES SCREEN
- RETURN - ENTER A NEW SPECIES
- L - LIST GROUPS
- Q - RETURN TO MAIN MENU {choose "F"
first; current species is discarded
when you return to MAIN menu}
- X - EXIT PROGRAM
- S - GET SPECIES FROM { *.DOC } FILE
- ? - HELP
- U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)

enter option : { ENTER NEW SPECIES }

OPTION R:

R - CALCULATE RADICAL

THIS OPTION ENABLES YOU TO ESTIMATE PROPERTIES OF A RADICAL SPECIES BY ADDING AN APPROPRIATE BOND DISSOCIATION INCREMENT TO THE CURRENT SPECIES.

BOND DISSOCIATION INCREMENTS ASSUME LOSS OF A HYDROGEN ATOM FROM THE PARENT SPECIES. TO ESTIMATE PHENYL RADICAL WE FIRST ESTIMATE BENZENE AND THEN APPLY THE "BZ" BOND INCREMENT TO THIS SPECIES.

$R \cdot \ln(2)$ IS ADDED TO THE SPECIES ENTROPY TO ACCOUNT FOR THE FREE ELECTRON. BOND INCREMENT GROUPS ALSO INCLUDE ANY INTERNAL ENTROPY CHANGE. THE USER MUST SUPPLY THE SYMMETRY NUMBER FOR THE RADICAL, IN ADDITION TO IT'S NAME(ID) AND ELEMENTAL FORMULA.

OPTION F:

F - ADD THE CURRENT SPECIES TO A FILE

THIS OPTION SAVES THE CURRENT SPECIES IN THE "LST" FORMAT. IN ADDITION, THE DEFAULT IS TO CREATE A DOCUMENTATION FILE WHICH IS NECESSARY FOR AUTOMATIC UPDATE/RECALCULATION PROCEDURES AVAILABLE FROM THE MAIN MENU.

OPTION H:

H - TOGGLE SHORT/LONG MENU

TRY THIS OPTION TO SEE WHAT HAPPENS. CHOOSING "H" A SECOND TIME WILL RESTORE THE CURRENT MENU FORMAT.

OPTION P:

P - RETURN TO THE LAST SPECIES SCREEN

This option returns the user to the previous species screen.

OPTION M:

M - RETURN TO THE PREVIOUS PARENT MOLECULE

THIS OPTION IS ONLY ACTIVE IF THE LAST SPECIES SCREEN CONTAINED A RADICAL SPECIES. CHOOSING THIS OPTION RESTORES THE PARENT IF AND ONLY IF BOND INCREMENT GROUPS WERE USED TO CALCULATE THE RADICAL.

NOTE: CURRENT RADICAL SPECIES DATA IS DISCARDED WHEN THIS OPTION IS CHOSEN. THEREFORE, YOU SHOULD FILE "F" THIS SPECIES BEFORE CHOOSING OPTION "M".

END

OPTION L:

L - LIST GROUPS:

THIS OPTION ENABLES YOU TO REVIEW THE CURRENT GROUP FILE DATABASE.

OPTION Q:

Q - RETURN TO THE MAIN MENU

WHEN RETURNING TO THE MAIN MENU, ALL CURRENT SPECIES DATA ARE LOST. THEREFORE, ONE SHOULD FILE "F" THE CURRENT SPECIES BEFORE MAKING THIS CHOICE.

OPTION S:

S - GET SPECIES FROM { *.DOC } FILE

SAME FUNCTION AS OPTION "6" FROM THE MAIN MENU.

THIS OPTION ENABLES YOU TO RECALL/RECALCULATE A SPECIES BASED UPON INFORMATION CONTAINED IN THE DOCUMENTATION FILE.

THIS OPTION DISCARDS CURRENT SPECIES DATA. FILE "F" SHOULD BE CHOSEN FIRST TO SAVE THE CURRENT DATA.

END

RADICAL CALCULATION MENU
(radical by loss of H from parent)

Q - RETURN TO PREVIOUS MENU
? - HELP

THE FOLLOWING BOND INCREMENT GROUPS ARE DEFINED:

GR#	GROUP ID	GR#	GROUP ID	GR#	GROUP ID
199	- VIN	200	- CHD	201	- CHD14
202	- CYPD	203	- CYPENE	204	- CLBZ
205	- CHENE	206	- CHENEA	207	- BZ
208	- P	209	- S	210	- T
211	- ALPEROX	212	- ALKOXY	213	- PHENOXY
214	- ALLYLP	215	- ALLYLS	216	- ALLYLT

ENTER BOND INCREMENT NAME ONLY

enter option : (Q)

NOTE: These are the bond increments included with this package. If desired, more can be added to the file BD.

All bond increments must be included in this file.

Bond increments consist of a bond energy (assuming loss of H atom from the parent molecule), S and Cp increments to account for respective changes due to loss of H atom from the parent. These include loss of vibrational modes as well as adjustments for changes in barriers to internal rotation.

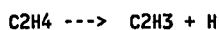
BOND DISSOCIATION "BD" INCREMENTS EXPLAINED:

OPTION VIN:

VIN - VINYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 105.5 Kcal/mol

based upon loss of H atom from ethylene:



OPTION CHD:

CHD - CYCLOHEXA-1,3-DIENYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 76.6 Kcal/mol

based upon loss of H atom from CY13HD ---> CYC6H7 + H

OPTION CHD14:

CHD - CYCLOHEXA-1,4-DIENYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 75.8 Kcal/mol

based upon loss of H atom from CY14HD ---> CYC6H7 + H

OPTION BZ:

BZ - PHENYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 113.65 Kcal/mol

based upon loss of H atom from CYC6H6 ---> CYC6H5 + H

OPTION CYPD:

CYPD - CYCLOPENTADIENYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 74.0 Kcal/mol

based upon loss of H atom from CYPD ---> CYPD. + H

OPTION CYPENE:

CYPENE - ALLYLIC CYCOLOPENTENYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 84.2 Kcal/mol

based upon loss of H atom from $CYC5H8 \rightarrow CYC5H7 + H$

OPTION CLBZ:

CLBZ - CHLOROPHENYL RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 112.5 Kcal/mol

based upon loss of H atom from $C6H5Cl \rightarrow C6H4Cl + H$

OPTION CHENE:

CHENE - CYCOLHEXENENYL RADICAL { NON-ALLYLIC }

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 98.98 Kcal/mol

based upon loss of H atom from $CYC6H9 \rightarrow CYC6H9 + H$

OPTION CHENEA:

CHENEA - CYCOLHEXENENYL RADICAL { ALLYLIC }

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 83.8 Kcal/mol

based upon loss of H atom from $CYC6H9 \rightarrow CYC6H9A + H$

OPTION P:

P - PRIMARY RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 100.6 Kcal/mol

based upon loss of H atom from $C2H6 \rightarrow C2H5 + H$

Barrier to internal rotation is lower for the CH₂ rotor in the product than it is for the CH₃ rotor in the parent.

OPTION S:

S - SECONDARY RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 98.2 Kcal/mol

based upon loss of H atom from CCC ---> CC.C + H (GUTMAN)

OPTION T:

T - Tertiary Radical

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 95.2 Kcal/mol

based upon loss of H atom from C3C ---> C3C. + H (W. Tsang)

OPTION ALPEROX:

ALPEROX - ALKYL PEROXY RADICAL:

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 88.0 Kcal/mol

based upon loss of H atom from ROOH ---> ROO. + H

OPTION ALKOXY:

ALKOXY - ALKOXY RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 104.1 Kcal/mol

based upon loss of H atom from CH3OH ---> CH3O. + H

Entropy loss an average of 2.6 for loss of rotor.

OPTION PHENOXY:

PHENOXY - PHENOXY RADICAL

BOND DISSOCIATION ENERGY (assuming loss of H atom) = 86.5 Kcal/mol

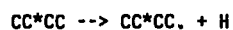
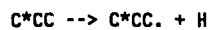
based upon loss of H atom from C6H5OH ---> CYC6H5O. + H

OPTION ALLYLP:

ALLYLP - primary allylic

Bond dissociation energy (assuming loss of H atom) = 88.2 Kcal/mol

average for delta H for following two reactions:



OPTION ALLYLS:

ALLYLS - secondary allylic

Bond dissociation energy (assuming loss of H atom) = 84.4 Kcal/mol

based upon loss of H atom from $\text{C}^*\text{CCC} \rightarrow \text{C}^*\text{CC}\cdot\text{C} + \text{H}$

OPTION ALLYLT:

ALLYLT - tertiary allylic

Bond dissociation energy estimated as 81.8 Kcal/mol

Bozzelli : estimate

EXAMPLES: SAMPLE SESSION

THERM

Thermo Estimation for Radicals & Molecules

written by

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revision 4.0 : 2/11/89

****** Loading Configuration File ******

******* LOADING GROUP DATAFILES *******

336 Groups in the dataBase.

{ hit return to continue }

===== next screen =====

THERM MAIN MENU

Units: Kcal/mol (cal/mol K)

3/ 5/89

-
- 1 - ENTER/ESTIMATE SPECIES
 - 2 - VIEW GROUPS
 - 3 - SELECT SHORT MENU
 - 4 - SELECT LIST FILE (*.LST)
 - 5 - REVIEW (LST FORMAT FILE)
 - 6 - GET SPECIES FROM FILE (*.DOC)
 - 7 - ReWrite THERMO FILES (*.DOC, *.LST)
 - 8 - RUN THERMFIT create NASA (*.DAT)
 - 9 - RUN THERMRXN (calculate dU, dH, dS, dG for reaction)
 - 10 - Sort & ReWrite THERMO FILES (*.DOC, *.LST)
 - 11 - Sort/Write *.LST file (no *.DOC is needed)
 - 12 - RUN THERMLST (LIST NASA FORMAT FILE) /create *.LST
 - 13 - DOS utilities
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)
 - * - CLOSE ALL OPENED FILES
 - X - EXIT PROGRAM
 - ? - HELP

enter option : { 1 } <----- default option
(press return)

===== next screen =====

Enter species name (ID)
9 characters maximum
{ "Q" return to opening menu }
BIPHENYL <----- enter the species name and
press return.

===== next screen =====

enter the elemental formula for this species
{ example: for PHENOL enter " C6H5OH " }
{ for TOLUENE enter " C6H5CH3 " }
{ for CHLOROPHENOL enter " C6H4CLOH " }

4 ELEMENTS MAXIMUM : 70 CHARACTERS MAX

THE FOLLOWING ELEMENTS ARE DEFINED:
C H O CL S N F P I BR
B

ALL OTHER ELEMENTS OR NON-NUMERIC CHARACTERS
WILL BE IGNORED !

enter formula here: {Q=QUIT}
C6H5C6H5 <----- enter elemental formula
C6H5C6H5 or C12H10

===== next screen =====

FORMULA ENTERED :
C6H5C6H5

ELEMENTAL COMPOSITION:

C	12	
H	10	<----- this message is disabled if
	0	"ERRORCK=OFF" appears
	0	in the config file
		(see THERM.CFG)

number of Atoms for This Species = 22

IF THIS IS INCORRECT ENTER " Q "
TO BEGIN AGAIN
OTHERWISE HIT RETURN TO CONTINUE <----- press return

===== next screen =====

Radicals are estimated either by entering a radical (CDOT) group such as " CB/. " on this screen; or by first estimating the properties for the stable molecule here (ex: benzene) and then applying a bond increment (BD) group to account for loss of H atom from the molecule.

Bond increments cannot be entered here. They are entered at the RADICAL menu (available after the molecule's properties are estimated).

You must be sure that groups you enter adequately define a molecule (no unbonded electrons). THERM makes no attempt to check the context of the groups entered (only whether they are defined).

This message can be disabled if "ERRORCK=OFF" is set in THERM.CFG.

Enter the Number of Groups in this species
(each Central Atom or Ring Correction counts as 1 group)

12 <----- enter 12

How many different groups are to be entered?

1 <----- enter 1

NOTE: To enter literature data one would answer "0" to the prompt "Enter the number of Groups in this species". If one chooses to enter literature data, they are prompted for different information than that which follows. Literature data remains unchanged when automatic recalculation is performed.

===== next screen =====

how many rotors in this species {0} enter the number of rotors in
1 <----- this species and press return

===== next screen =====

336 groups in the database

You must enter a total of 2 different groups | one may review the group
(enter " D " to re-enter the last group) | database "L", start a new
(enter " Q " to start a new species) | species "Q", or correct/
(enter " L " to list group database) | re-enter the last group
| "D" by entering one of
| these options instead of
| a group id.

ENTER: "GROUP ID,QUANTITY" <----- a group ID and quantity are separated
by either a space or a comma. If no
quantity is entered, "1" is assumed.

ENTER GROUP # 1
CB/H 10 <----- enter the group id : CB/H,10
ENTER GROUP # 2
CB/CB 2 <----- enter the group id : CB/CB,2
Enter symmetry # for molecule
8 <----- enter symmetry number for
biphenyl : 8
IF no symmetry number is entered,
"1" is assumed.

===== next screen =====

Thermo estimation for molecule
BIPHENYL

C6H5C6H5

Gr # - GROUP ID - Quantity
1 - CB/H - 10
2 - CB/CB - 2

UNITS: Hf{Kcal/mol} S & Cp {cal/mol K}

Hf	S	Cp 300	400	500	600	800	1000	1500
42.92	93.89	39.06	52.84	64.38	73.54	86.92	96.00	109.40
CPINF	127.17							

Symmetry number used to correct S value is 8

EDIT THESE RESULTS? "Y" OR {"N"} <----- press return
to accept no

===== next screen =====

SPECIES ESTIMATION OPTIONS MENU

Units: Kcal/mol (cal/mol K)

-
- R - CALCULATE RADICAL BASED UPON PREVIOUS SPECIES
 - F - ADD CURRENT SPECIES TO OUTPUT FILE
 - H - TOGGLE (SHORT/LONG) MENU
 - P - RETURN TO PREVIOUS SPECIES SCREEN
 - RETURN - ENTER A NEW SPECIES
 - L - LIST GROUPS
 - Q - RETURN TO MAIN MENU {choose "F"
first; current species is discarded
when you return to MAIN menu}
 - X - EXIT PROGRAM
 - S - GET SPECIES FROM (*.DOC) FILE
 - ? - HELP
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)

enter option : { ENTER NEW SPECIES }

F <----- choose "F" to file
(press return)

===== next screen =====

Enter output filename:

{ no file extension is needed }:

THERMO <----- enter a filename for output

CREATE DOCUMENT FILE [Y or N]

enter choice: { Y } <----- press return

choose output units for LST file

1- Kcal/mol (cal/mol K) 2- KJ/mol (J/mol K)

enter option { 1 }

2 <----- enter "2" for output in KJ

enter title for *.LST file output { blank or Q= no title }

EXAMPLE USE OF THERM <----- enter a file heading if desired

NOTE: If the file which is specified already exists, the user is asked if it should be overwritten, appended, or if a different filename is desired.

===== next screen =====

SPECIES ESTIMATION OPTIONS MENU

Units: Kcal/mol (cal/mol K)

-
- R - CALCULATE RADICAL BASED UPON PREVIOUS SPECIES
 - F - ADD CURRENT SPECIES TO OUTPUT FILE
 - H - TOGGLE (SHORT/LONG) MENU
 - P - RETURN TO PREVIOUS SPECIES SCREEN
 - RETURN - ENTER A NEW SPECIES
 - L - LIST GROUPS
 - Q - RETURN TO MAIN MENU {choose "F"
first; current species is discarded
when you return to MAIN menu}
 - X - EXIT PROGRAM
 - S - GET SPECIES FROM (*.DOC) FILE
 - ? - HELP
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)

LAST SPECIES FILED: BIPHENYL <----- biphenyl has been
filed

enter option : (ENTER NEW SPECIES)

R <----- enter "R" to calculate
a radical

===== next screen =====

RADICAL CALCULATION MENU
{radical by loss of H from parent}

- Q - RETURN TO PREVIOUS MENU
- ? - HELP

THE FOLLOWING BOND INCREMENT GROUPS ARE DEFINED:

GR#	GROUP ID	GR#	GROUP ID	GR#	GROUP ID
199	- VIN	200	- CHD	201	- CHD14
202	- CYPD	203	- CYPENE	204	- CLBZ
205	- CHENE	206	- CHENEA	207	- BZ
208	- P	209	- S	210	- T
211	- ALPEROX	212	- ALKOXY	213	- PHENOXY
214	- ALLYLP	215	- ALLYLS	216	- ALLYLT

ENTER BOND INCREMENT NAME ONLY
enter option : { Q }

BZ <----- choose the "BZ" bond increment or "?" to review
bond increment (BD) definitions. The BD group
name is required here. DO NOT enter the number.

===== next screen =====

PARENT = C6H5C6H5

BOND TYPE = BZ

enter the symmetry number for the radical

2 <----- symmetry number for ortho or
meta - biphenyl radical is "2"

Enter radical name(ID)

C6H5C6H4. <----- give the radical a name (9 char max)

enter the elemental formula for this radical

{ example: for PHENYL enter " C6H5 " }

{ for BENZYL enter " C6H5CH2 " }

{ FOR VINYL enter " C2H3 " }

4 ELEMENTS MAXIMUM

C6H5C6H4 <----- enter elemental formula for the radical

FORMULA ENTERED :

C6H5C6H4

ELEMENTAL COMPOSITION:

C 12

H 9

0 <----- this message can be disabled

0 see ERRORCK in configuration

file

number of Atoms for This Species = 21

IF THIS IS INCORRECT ENTER " Q "

TO BEGIN AGAIN

OTHERWISE HIT RETURN TO CONTINUE <----- hit return to continue

===== next screen =====

how many rotors in this species {0} enter the number of rotors in

1 <----- this species and press return

===== next screen =====

Thermo estimation for radical
C6H5C6H4.

C6H5C6H4

RADICAL BASED UPON PARENT BIPHENYL

C6H5C6H5

PARENT SYMMETRY 8

Gr # - GROUP ID - Quantity
1 - CB/H - 10
2 - CB/CB - 2
3 - BZ - 1

UNITS: Hf(Kcal/mol) S & Cp (cal/mol K)

Hf	S	Cp	300	400	500	600	800	1000	1500
104.47	97.76	38.19	51.23	62.16	70.83	83.51	92.16	104.90	
CPINF	121.21								

Symmetry number used to correct S value is 2

R ln(2) has been added to S to account for unpaired electron

bond dissociation energy used= 113.65

EDIT THESE RESULTS? "Y" OR {"N"} <----- press return

===== next screen =====

SPECIES ESTIMATION OPTIONS MENU

Units: Kcal/mol (cal/mol K)

-
- R - CALCULATE RADICAL BASED UPON PREVIOUS SPECIES
 - F - ADD CURRENT SPECIES TO OUTPUT FILE
 - H - TOGGLE (SHORT/LONG) MENU
 - P - RETURN TO PREVIOUS SPECIES SCREEN
 - M - RETURN TO PREVIOUS PARENT MOLECULE
 - RETURN - ENTER A NEW SPECIES
 - L - LIST GROUPS
 - Q - RETURN TO MAIN MENU (choose "F"
first; current species is discarded
when you return to MAIN menu)
 - X - EXIT PROGRAM
 - S - GET SPECIES FROM (*.DOC) FILE
 - ? - HELP
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)

LAST SPECIES FILED: BIPHENYL

enter option : { ENTER NEW SPECIES }

F <----- file this entry.
enter "F" and press
return

NOTE: Since an output file has already been connected, the user is not prompted for any file information. To change the file, one must return to the MAIN menu and choose option "*" to close all opened files. Then the next time option "F" is chosen, the user will again be prompted for filename, etc.

===== next screen =====

SPECIES ESTIMATION OPTIONS MENU

Units: Kcal/mol (cal/mol K)

-
- R - CALCULATE RADICAL BASED UPON PREVIOUS SPECIES
 - F - ADD CURRENT SPECIES TO OUTPUT FILE
 - H - TOGGLE (SHORT/LONG) MENU
 - P - RETURN TO PREVIOUS SPECIES SCREEN
 - M - RETURN TO PREVIOUS PARENT MOLECULE
 - RETURN - ENTER A NEW SPECIES
 - L - LIST GROUPS
 - Q - RETURN TO MAIN MENU {choose "F"
first; current species is discarded
when you return to MAIN menu}
 - X - EXIT PROGRAM
 - S - GET SPECIES FROM { *.DOC } FILE
 - ? - HELP
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)

LAST SPECIES FILED: C6H5C6H4.

enter option : (ENTER NEW SPECIES)

L <----- enter "L" to list groups

LIST GROUPS MENU

- 1 - HC
- 2 - CYCH
- 3 - CDOT
- 4 - BD
- 5 - CLC
- 6 - HCO
- 7 - HCN
- A - All Groups in DataBase
- Q - QUIT (return to previous menu)

enter option : { Q }

4 <----- choose option "4" to review bond increment (BD) groups

===== next screen =====

GR#	GROUP ID	GR#	GROUP ID	GR#	GROUP ID
199	VIN	200	CHD	201	CHD14
202	CYPD	203	CYPENE	204	CLBZ
205	CHENE	206	CHENEA	207	BZ
208	P	209	S	210	T
211	ALPEROX	212	ALKOXY	213	PHENOXY
214	ALLYLP	215	ALLYLS	216	ALLYLT

HIT RETURN TO CONTINUE ("?" FOR HELP)

? <----- enter "?" for help

===== next screen =====

LIST DATABASE OPTIONS

- Q - QUIT return to previous menu
- RETURN - TO CONTINUE
- R - REPEAT listing (from beginning)
- E - EXTENDED listing (Hf S Cp)
- REF- EXTENDED listing with references

enter option (continue)

REF <----- enter "REF" to review group data with references

ENTER RANGE OF GROUPS TO VIEW

199 216 <----- specify the range to display
(this will display groups
199 (VIN) to 216 (ALLYLT)
as shown above. Group names could be
entered instead (VIN ALLYLT) to specify
the range.

===== on-line review of group values and references =====

Hf { Kcal/mol }		S & Cp { cal/mol K }							
GROUP ID	Hf	S	Cp 300	400	500	600	800	1000	
VIN	105.54	1.06	-.16	-.67	-1.17	-1.65	-2.55	-3.31	
Stein , 22nd Symp (International) on Combustion : Seattle 1988									
CHD	76.56	.48	-1.87	-2.26	-2.63	-2.96	-3.56	-4.11	
W. Tsang J Phys Chem 1986, 90, 1152									
CHD14	75.80	1.21	-1.83	-2.09	-2.37	-2.67	-3.30	-3.93	
W. Tsang J Phys Chem 1986, 90, 1152									
CYPD	74.00	4.62	-.40	-.44	-.61	-.95	-1.83	-2.68	
CYPENE	84.17	4.13	-.38	-.42	-.59	-.96	-1.90	-2.80	
CLBZ	112.12	1.12	-.87	-1.61	-2.22	-2.70	-3.41	-3.84	
bd lowered by 1 kcal over benzene (bz) : Louw, Mulder									
CHENE	98.98	5.78	-.12	-.71	-1.25	-1.74	-2.57	-3.22	
CHENEA	83.83	4.71	-.13	-.74	-1.29	-1.78	-2.61	-3.28	
BZ	113.65	1.12	-.87	-1.61	-2.22	-2.71	-3.41	-3.84	
W. Tsang J Phys Chem 1986, 90, 1152									
P	100.64	2.30	-.78	-1.19	-1.62	-2.09	-3.01	-3.80	
W. Tsang I J Chem Kin 1987, 10, 821. JACS 1985, 107, 2822									
S	98.10	4.50	-1.50	-2.33	-3.10	-3.39	-3.75	-4.45	
W. Tsang I J Chem Kin 1987, 10, 821. JACS 1985, 107, 2822									
T	95.87	6.48	-5.22	-5.52	-5.71	-5.77	-5.69	-5.54	
Russell and Gutman JACS 1988, 110, 3084 & 3092									

{ HIT RETURN TO CONTINUE } <----- press return

Hf { Kcal/mol }		S & Cp { cal/mol K }							
GROUP ID	Hf	S	Cp 300	400	500	600	800	1000	
ALPEROX	88.50	-2.10	-2.00	-2.65	-3.10	-3.40	-3.64	-3.60	
ALKOXY	104.06	-2.60	-1.47	-1.82	-2.12	-2.36	-2.72	-2.97	
PHENOXY	86.50	-2.60	-1.38	-2.02	-2.53	-2.91	-3.44	-3.81	
Burcat, Zelznik, McBride nasa tech memo #83800 January 1985									
ALLYLP	88.20	-1.60	-.51	-.72	-.99	-1.33	-2.08	-2.81	
avg {(C*CC --> C*CC. + H) + (CC*CC --> CC*CC. + H)}/2									
ALLYLS	84.40	-.62	-.78	-1.19	-1.62	-2.09	-3.01	-3.78	
C*CCC --> C*CC.C + H									
ALLYLT	81.80	.88	-1.50	-2.36	-3.10	-3.49	-3.95	-4.45	
Bozzelli : calc from alkyl bond trends & data in McMillian/Golden (1983)									

{ HIT RETURN TO CONTINUE }

NOTE: reference appears on the line following the group data if there is no reference, none is listed. Most groups with no reference are from Benson.

LIST DATABASE OPTIONS

- Q - QUIT return to previous menu
- RETURN - TO CONTINUE
- R - REPEAT listing (from beginning)
- E - EXTENDED listing (Hf S Cp)
- REF- EXTENDED listing with references

enter option {continue}

Q <----- return to previous menu

===== next screen =====

LIST GROUPS MENU

- 1 - HC
- 2 - CYCH
- 3 - CDOT
- 4 - BD
- 5 - CLC
- 6 - HCO
- 7 - HCN
- A - All Groups in DataBase
- Q - QUIT { return to previous menu}

enter option : { Q }

Q <----- "quit" back to previous menu

===== next screen =====

SPECIES ESTIMATION OPTIONS MENU

Units: Kcal/mol (cal/mol K)

- R - CALCULATE RADICAL BASED UPON PREVIOUS SPECIES
- F - ADD CURRENT SPECIES TO OUTPUT FILE
- H - TOGGLE (SHORT/LONG) MENU
- P - RETURN TO PREVIOUS SPECIES SCREEN
- M - RETURN TO PREVIOUS PARENT MOLECULE
- RETURN - ENTER A NEW SPECIES
- L - LIST GROUPS
- Q - RETURN TO MAIN MENU {choose "F"
first; current species is discarded
when you return to MAIN menu}
- X - EXIT PROGRAM
- S - GET SPECIES FROM { *.DOC } FILE
- ? - HELP
- U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)

LAST SPECIES FILED: C6H5C6H4.

enter option : { ENTER NEW SPECIES }

Q <----- "quit" back to MAIN menu

===== next screen =====

THERM MAIN MENU

Units: Kcal/mol (cal/mol K)

3/ 5/89

-
- 1 - ENTER/ESTIMATE SPECIES
 - 2 - VIEW GROUPS
 - 3 - SELECT SHORT MENU
 - 4 - SELECT LIST FILE (*.LST)
 - 5 - REVIEW (LST FORMAT FILE)
 - 6 - GET SPECIES FROM FILE (*.DOC)
 - 7 - ReWrite THERMO FILES (*.DOC, *.LST)
 - 8 - RUN THERMFIT create NASA (*.DAT)
 - 9 - RUN THERMRXN (calculate dU, dH, dS, dG for reaction)
 - 10 - Sort & ReWrite THERMO FILES (*.DOC, *.LST)
 - 11 - Sort/Write *.LST file (no *.DOC is needed)
 - 12 - RUN THERMLST (LIST NASA FORMAT FILE) /create *.LST
 - 13 - DOS utilities
 - U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)
 - * - CLOSE ALL OPENED FILES
 - X - EXIT PROGRAM
 - ? - HELP

enter option : { 1 }

6 <----- choose "6" to get species data from a "DOC" file

===== next screen =====

enter document filename

for species input

TEST <----- enter filename for input "TEST.DOC"
the file extension ".DOC" is understood.

INITIALIZING
THERMO DOCUMENTATION FILE

PLEASE WAIT

1	FBZ	C	6	H	5	F	1	0
2	BZ	C	6	H	6		0	0
3	CLBZ	CL	1	C	6	H	5	0
4	C6H5CH3	C	7	H	8		0	0
5	IBZ	C	6	H	5	I	1	0
6	BIPHENYL	C	12	H	10		0	0
7	CLBIPHENY	CL	1	C	12	H	9	0
8	PHENOL	C	6	H	6	O	1	0
9	PHENOXY	C	6	H	5	O	1	0
10	C6F6	C	6	F	6		0	0
11	PHENYL	C	6	H	5		0	0
12	C6H5.	C	6	H	5		0	0
13	CH3OCH3	C	2	H	6	O	1	0
14	C2H6	C	2	H	6		0	0
15	C2H5	C	2	H	5		0	0
16	C2H5CL	CL	1	C	2	H	5	0
17	C2H4	C	2	H	4		0	0
18	C2H3	C	2	H	3		0	0
19	C2H3CL	CL	1	C	2	H	3	0
20	PHPH	C	12	H	10		0	0
21	PHPH.	C	12	H	9		0	0
22	CY13HD	C	6	H	8		0	0
23	CYC5E	C	5	H	8		0	0
24	C5DE14	C	5	H	8		0	0
25	CYPD	C	5	H	6		0	0
26	C5DE23	C	5	H	8		0	0
27	ANILINE	C	6	H	7	N	1	0
28	C2H4O	C	2	H	4	O	1	0
29	C20H42	C	20	H	42		0	0
30	C2H5F	C	2	H	5	F	1	0
31	CH2CF2	C	2	H	2	F	2	0

===== next screen =====

1 FBZ	2 BZ	3 CLBZ	4 C6H5CH3
5 IBZ	6 BIPHENYL	7 CLBIPHENY	8 PHENOL
9 PHENOXY	10 C6F6	11 PHENYL	12 C6H5.
13 CH3OCH3	14 C2H6	15 C2H5	16 C2H5CL
17 C2H4	18 C2H3	19 C2H3CL	20 PHPH
21 PHPH.	22 CY13HD	23 CYC5E	24 C5DE14
25 CYPD	26 C5DE23	27 ANILINE	28 C2H4O
29 C2OH42	30 C2H5F	31 CH2CF2	32

enter "D" to delete; "U" to undelete; "V" to view; or hit return to continue
D <----- enter "D" to delete a species

DELETE which species { 0 to abort }
or enter species number to delete)

1 <----- choose to delete FBZ, enter "1"
species # 1
has been deleted

===== next screen =====

1	2 BZ	3 CLBZ	4 C6H5CH3
5 IBZ	6 BIPHENYL	7 CLBIPHENY	8 PHENOL
9 PHENOXY	10 C6F6	11 PHENYL	12 C6H5.
13 CH3OCH3	14 C2H6	15 C2H5	16 C2H5CL
17 C2H4	18 C2H3	19 C2H3CL	20 PHPH
21 PHPH.	22 CY13HD	23 CYC5E	24 C5DE14
25 CYPD	26 C5DE23	27 ANILINE	28 C2H4O
29 C2OH42	30 C2H5F	31 CH2CF2	32

enter "D" to delete; "U" to undelete; "V" to view; or hit return to continue
U <----- choose to replace FBZ by entering "U"

===== next screen =====

1 - FBZ <----- all species that have been deleted
but are retained are listed here

undelete which species { 0 to abort }
or enter species number to undelete

1 <----- enter "1" to UNDELETE FBZ

===== next screen =====

1 FBZ	2 BZ	3 CLBZ	4 C6H5CH3
5 IBZ	6 BIPHENYL	7 CLBIPHENY	8 PHENOL
9 PHENOXY	10 C6F6	11 PHENYL	12 C6H5.
13 CH3OCH3	14 C2H6	15 C2H5	16 C2H5CL
17 C2H4	18 C2H3	19 C2H3CL	20 PHPH
21 PHPH.	22 CY13HD	23 CYC5E	24 C5DE14
25 CYPD	26 C5DE23	27 ANILINE	28 C2H4O
29 C2OH42	30 C2H5F	31 CH2CF2	32

enter "D" to delete; "U" to undelete; "V" to view; or hit return to continue
V <----- choose "V" to view data in the file

view which species { enter species number }

9 <----- choose species #9 : phenoxy radical
===== next screen =====

SPECIES

PHENOXY

Thermo estimation for radical

PHENOXY

C6H5O

RADICAL BASED UPON PARENT PHENOL

PARENT FORMULA

C6H5OH

PARENT SYMMETRY 2

UNITS:KJ

GROUPS 4

Gr # - GROUP ID - Quantity

1 - O/CB/H - 1

2 - CB/O - 1

3 - CB/H - 5

4 - PHENOXY - 1

Hf S Cp 300 400 500 600 800 1000 1500

50.63 303.64 96.32 125.02 149.75 169.12 197.40 216.52 .00

CPINF = 282.66

SYMMETRY 2

R ln(2) has been added to S to account
for unpaired electron

BOND 361.92

ENDSPECIES

{ hit return to continue }

NOTE: this is only an image of the data recorded in the "DOC" file.
This option allows one to view species data before choosing to load
the data into memory.

===== next screen =====

1 FBZ	2 BZ	3 CLBZ	4 C6H5CH3
5 IBZ	6 BIPHENYL	7 CLBIPHENY	8 PHENOL
9 PHENOXY	10 C6F6	11 PHENYL	12 C6H5.
13 CH3OCH3	14 C2H6	15 C2H5	16 C2H5CL
17 C2H4	18 C2H3	19 C2H3CL	20 PHPH
21 PHPH.	22 CY13HD	23 CYC5E	24 C5DE14
25 CYPD	26 C5DE23	27 ANILINE	28 C2H4O
29 C2OH42	30 C2H5F	31 CH2CF2	32

enter "D" to delete; "U" to undelete; "V" to view; or hit return to continue

<----- press return to continue

enter species id ("?" for options)

CLBZ <----- enter "CLBZ" and groups and other data are loaded
into memory for recalculation/editing

{ hit return to continue : ? for options }

===== next screen =====

Thermo estimation for molecule

CLBZ

C6H5CL

Gr # - GROUP ID - Quantity

1 - CB/H - 5

2 - CB/CL - 1

UNITS: Hf{Kcal/mol} S & Cp {cal/mol K}

Hf	S	Cp	300	400	500	600	800	1000	1500
----	---	----	-----	-----	-----	-----	-----	------	------

12.39	74.82	23.37	30.55	36.46	41.21	48.04	52.73		
-------	-------	-------	-------	-------	-------	-------	-------	--	--

CPINF 67.56

Symmetry number used to correct S value is 2

EDIT THESE RESULTS? { "Y" OR "N" }

NOTE: Properties have actually been recalculated from
group database and data is in memory as if the user had just typed it in.

Literature data is not recalculated. The keyword "NOCALC" appears with
every literature entry.

USING THERMFIT

Cp EXTRAPOLATION AND POLYNOMIAL FITTING PROGRAM

This stand alone program may be run from the THERM main menu or may be run independent from THERM. Input file is LST format and output is DAT format (thermo property polynomials). To run independent enter "THERMFIT" at the DOS prompt and press return.

THERMFIT : Polynomial Fitting & Cp Extrapolation Method

ENTER FILENAME FOR INPUT (.LST)

EXAMPLE <----- enter input filename (extension "LST" is assumed.

ENTER FILENAME FOR OUTPUT (.DAT)

EXAMPLE <----- enter output filename (extension "DAT" is assumed.

GENERATING NASA FORMAT DATABASE FROM
TEST.LST

please wait

C6H5F

C6H6

C6H5CL

C6F6

C6CL6

C6H5CH3 <----- species names are listed as each is processed.

C6H5I

C6H5C6H5

C6H5OH

C6H5O.

EXAMPLE LIST FILE (LST)

SPECIES	Hf	S	Cp 310	400	500	600	800	1000	1500	DATE	ELEMENTS		
C6H5F	-26.30	72.37	22.50	29.80	35.80	40.60	47.50	52.25	.00	1/23/89	C 6 H 5 F	1	0 G 0
C6H6	19.80	64.24	19.44	26.64	32.76	37.80	45.24	50.46	58.38	1/23/89	C 6 H 6	0	0 G 0
C6H5CL	12.70	75.17	24.60	29.60	37.00	40.70	47.90	52.45	.00	1/23/89	CL 1 C 6 H 5	5	0 G 0
C6F6	-228.64	91.59	37.56	43.88	48.78	52.55	57.62	60.63			STULL C 6 F 6	0	0 G 0
C6CL6	-8.10	105.45	41.36	46.00	50.52	53.00	57.74	60.28			THERM CL 6 C 6	0	0 G 0
C6H5CH3	11.81	76.81	25.06	33.18	40.38	46.44	55.68	62.26	72.21	1/23/89	C 7 H 8	0	0 G 1
*C6H5I	39.00	79.97	24.20	31.10	36.90	41.40	49.00	52.55	.00	1/23/89	C 6 H 5 I	1	0 G 0
C6H5C6H5	42.92	93.89	39.06	52.84	64.38	73.54	86.92	96.00	109.40	1/23/89	C 12 H 10	0	0 G 1
PHENDL	-22.30	75.17	24.40	31.90	38.32	43.33	50.62	55.56	.00	1/23/89	C 6 H 6 O	1	0 G 1
PHENOXY	12.10	72.57	23.02	29.88	35.79	40.42	47.18	51.75	.00	1/23/89	C 6 H 5 O	1	0 G 0

NOTE: this is a sample LST format file (*.LST) as created by the group additivity code. LST files produced by THERMLST have essentially the same format, except Cp 1500 K is never blank or zero.

- o If Cp 1500 K is blank or zero that means one or more groups considered had no data available at this temperature. Once data has been fit using this program, Cp data will be calculated to 5000 K unless an asterisk appears in column 1. An asterisk in column 1 "*" indicates that the desired temperature range is limited to 2000 K or that extrapolation was not successful.
- o The last column contains the number of rotors which can be considered free rotors at high temperature. This is used to adjust the high temp limiting heat capacity (Cp infinity).

```

----- THIS IS THE FORMAT OF OUTPUT FROM THERMFIT -----
THERMO <----- first two lines are padded with
300.000 1500.000 5000.000 blanks to column 80
FBZ 1/23/89 C 6H 5F 1 OG 300.000 5000.000 1394.000 01
1.61833718E+01 1.55046197E-02-5.43776755E-06 8.58686527E-10-5.04169920E-14 2
-2.11896966E+04-6.54224811E+01-4.64588189E+00 6.87643930E-02-5.85165373E-05 3
2.52183330E-08-4.35564823E-12-1.44380166E+04 4.47766797E+01 4
BZ 1/23/89 C 6H 6 0 OG 300.000 5000.000 1387.000 01
1.39935036E+01 1.74971856E-02-6.15476220E-06 9.73716969E-10-5.72415007E-14 2
2.47175791E+03-5.77602198E+01-5.39447911E+00 6.37500472E-02-4.90152689E-05 3
1.93648825E-08-3.13307408E-12 9.13590251E+03 4.60723136E+01 4
CLBZ 1/23/89 CL 1C 6H 5 OG 300.000 5000.000 1402.000 01
1.76097340E+01 1.39051666E-02-4.81202456E-06 7.54213602E-10-4.40866883E-14 2
-2.09013038E+03-7.20465247E+01-2.22953876E-01 4.92544675E-02-2.68122926E-05 3
4.13248078E-09 5.27159680E-13 4.49728146E+03 2.55701514E+01 4
C6F6ST STULL C 6F 6 0 OG 300.000 5000.000 1399.000 01
2.58396239E+01 7.52573639E-03-2.73763134E-06 4.42881600E-10-2.64426394E-14 2
-1.25330418E+05-1.08117770E+02 3.78000514E+00 6.79621910E-02-6.65244670E-05 3
3.09697946E-08-5.56965091E-12-1.18686491E+05 6.98893678E+00 4
C6CL6TH THERM CL 6C 6 0 OG 300.000 5000.000 1388.000 01
2.55178960E+01 7.73146882E-03-2.79189838E-06 4.49470408E-10-2.67455853E-14 2
-1.38549596E+04-9.84421553E+01 9.57209477E+00 4.87056064E-02-4.35234301E-05 3
1.89791732E-08-3.26102369E-12-8.74666935E+03-1.42163133E+01 4
C6H5CH3 1/23/89 C 7H 8 0 OG 300.000 5000.000 1382.000 11
1.61733987E+01 2.32878469E-02-8.15197962E-06 1.28545400E-09-7.53928226E-14 2
-2.87513958E+03-6.63277432E+01-3.90646567E+00 6.70276172E-02-4.42253282E-05 3
1.48118855E-08-2.04209181E-12 4.49160027E+03 4.27682967E+01 4
IBZ 1/23/89 C 6H 5I 1 OG 300.000 5000.000 1397.000 01
1.65325962E+01 1.49823586E-02-5.20668476E-06 8.17232192E-10-4.77828786E-14 2
1.18034749E+04-6.30109665E+01-3.13809856E+00 6.61721608E-02-5.70980103E-05 3
2.49774647E-08-4.36424464E-12 1.80792156E+04 4.07227701E+01 4
BIPHENYL 1/23/89 C 12H 10 0 OG 300.000 5000.000 1393.000 11
2.78999627E+01 3.12250127E-02-1.09076740E-05 1.71779966E-09-1.00667229E-13 2
7.36037385E+03-1.30290245E+02-1.05041920E+01 1.29491922E-01-1.09365524E-04 3
4.73171544E-08-8.25035721E-12 1.98533421E+04 7.29519852E+01 4
PHENOL 1/23/89 C 6H 6O 1 OG 300.000 5000.000 1399.000 11
1.65690590E+01 1.72953159E-02-5.95971999E-06 9.30134800E-10-5.41699078E-14 2
-1.93122929E+04-6.66265382E+01-4.30712135E+00 7.12378295E-02-6.01302959E-05 3
2.58824065E-08-4.46320704E-12-1.26228735E+04 4.35843352E+01 4
PHENOXY 1/23/89 C 6H 5O 1 OG 300.000 5000.000 1399.000 01
1.58794328E+01 1.54008223E-02-5.32171061E-06 8.32198383E-10-4.85354318E-14 2
-1.58383272E+03-6.31930634E+01-3.64980357E+00 6.52692783E-02-5.45970495E-05 3
2.31094723E-08-3.91027027E-12 4.71529505E+03 4.00876924E+01 4
END <----- padded with blanks to column 80.

```

NOTE: This is a sample thermo property polynomial file created by THERMFIT. Some slight differences exist between this file format and that supplied with the CHEMKIN code.

Perhaps the most significant difference is the break point (or common) temperature. This fitting method determines the best position for the breakpoint rather than holding it constant at 1000 K.

The number of rotors appears in column 79 (unused by CHEMKIN). These differences are transparent to the CHEMKIN code

USING THERMRXN

THERMODYNAMIC ANALYSIS FOR REACTION

This stand alone program may be run from the THERM main menu or may be run independent of THERM. Thermo property polynomials are required input (DAT format). Reactions may either be entered interactively or entire CHENKIN inout files may be processed. To run this program independent of THERM, enter "THERMRXN" at the DOS prompt and press return.

ThERM RXN:

Thermodynamic Property Analysis for Reactions

ENTER FILENAME FOR NASA FORMAT COEFFICIENTS (*.DAT)

EXAMPLE <----- enter filename containing thermodynamic
property data in polynomial format.
(file extension DAT is assumed)

NOTE: If one wants to use a polynomial file which was not created by this package, it will be necessary to run the utility program "STOD.EXE" to verify the record length is 80 characters per line. THERMRXN requires the first two lines of the polynomial format file to be padded with blanks to 80 characters (required record length). STOD will do this automatically. This is called DIRECT ACCESS FILE FORMAT. STOD stands for Sequential TO Direct conversion.

Failure to pad each line to 80 characters will result in an error message. The polynomial file supplied with Sandia's "CHEMKIN" requires this change before it can be read. This format change is transparent to the CHEMKIN code, and allows quicker operation when used with THERM.

===== next screen =====

current units: Kcal/mol (cal/mol K)

To Calculate Property Change of Reaction for
enthalpy (del H), entropy (del S), and
gibbs free energy (del G)
enter a Reaction expression as follows:

" A+B=C+D " or " A+B=C " or " A=B+C "
(ad'n/abstr) (ad'n/recomb) (dissoc)
where A, B, C, etc. are species defined
in the current Thermo D Base (*.DAT) file
EXAMPLE: C6H5CL=C6H5.+CL (blanks are ignored)

NOTE: Reaction expression MUST BALANCE
no quote marks are needed

enter " L " to list defined species
" C " to process a "CHEMKIN" input file <--- CHEMKIN input files
" Q " to return to the MAIN MENU can be processed.
" ? " to suppress this information
" U " change units to Kcal/mol (cal/mol K)

C6H5CL=C6H5.+CL <----- enter reaction expression (blanks are
ignored; H +H+M = H2+M and 2H+M=H2+M are equivalent)

===== next screen =====

THERMODYNAMIC ANALYSIS for REACTION

Rx C6H5CL = C6H5. + CL
Hf {Kcal/mol} 12.390 81.350 28.900
S {cal/mol K} 74.820 68.920 39.500

dHr (298K) = 97.860 Kcal/mol
dU (dE) (") = 97.268 Kcal/mol
dSr (") = 33.600 cal/mol K
dGr (") = 87.842 Kcal/mol
Af/Ar (") = 3.320E+02

T (K)	dH(Kcal/mol)	dU(Kcal/mol)	dS(cal/mol K)	(Af/Ar)	dG(Kcal/mol)
300.000	9.786E+01	9.726E+01	3.360E+01	3.304E+02	8.778E+01
400.000	9.787E+01	9.708E+01	3.364E+01	2.522E+02	8.442E+01
500.000	9.783E+01	9.683E+01	3.354E+01	1.923E+02	8.106E+01
600.000	9.775E+01	9.656E+01	3.340E+01	1.495E+02	7.771E+01
800.000	9.756E+01	9.597E+01	3.313E+01	9.786E+01	7.106E+01
1000.000	9.738E+01	9.540E+01	3.293E+01	7.071E+01	6.445E+01
1200.000	9.723E+01	9.485E+01	3.279E+01	5.495E+01	5.788E+01
1500.000	9.703E+01	9.405E+01	3.265E+01	4.085E+01	4.806E+01
2000.000	9.673E+01	9.276E+01	3.247E+01	2.805E+01	3.179E+01

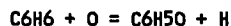
Q (quit) F (file) N (new input file) U (change units)
enter option { enter new reaction }

<----- press return to enter
 a new reaction

NOTE: OPTIONS

- Q - quit this program (return to THERM MAIN menu)
- F - save this data to a file.
- N - change the thermo property polynomial data file (DAT).
- U - switch units on display from kcal/mol (cal/mol K) to KJ/mol (J/mol K) or visa versa.

or enter Reaction expression here:



THERMODYNAMIC ANALYSIS for REACTION

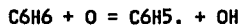
Rx	C6H6	+ O	= C6H5O	+ H
Hf (Kcal/mol)	19.800	59.550	11.370	52.100
S (cal/mol K)	64.240	38.470	72.730	27.390

dHr (298K) =	-15.880	Kcal/mol
dU (dE) (") =	-15.880	Kcal/mol
dSr (") =	-2.590	cal/mol K
dGr (") =	-15.108	Kcal/mol
Af/Ar (") =	2.716E-01	

T (K)	dH(Kcal/mol)	dU(Kcal/mol)	dS(cal/mol K)	(Af/Ar)	dG(Kcal/mol)
300.000	-1.587E+01	-1.587E+01	-2.567E+00	2.748E-01	-1.510E+01
400.000	-1.550E+01	-1.550E+01	-1.502E+00	4.695E-01	-1.490E+01
500.000	-1.516E+01	-1.516E+01	-7.347E-01	6.909E-01	-1.479E+01
600.000	-1.485E+01	-1.485E+01	-1.703E-01	9.179E-01	-1.475E+01
800.000	-1.435E+01	-1.435E+01	5.517E-01	1.320E+00	-1.479E+01
1000.000	-1.401E+01	-1.401E+01	9.331E-01	1.599E+00	-1.495E+01
1200.000	-1.381E+01	-1.381E+01	1.124E+00	1.761E+00	-1.516E+01
1500.000	-1.365E+01	-1.365E+01	1.245E+00	1.871E+00	-1.551E+01
2000.000	-1.356E+01	-1.356E+01	1.298E+00	1.922E+00	-1.615E+01

Q (quit) F (file) N (new input file) U (change units)
enter option { enter new reaction } <-----press return

enter Reaction expression here:



THERMODYNAMIC ANALYSIS for REACTION

Rx	C6H6	+ O	= C6H5	+ OH
Hf (Kcal/mol)	19.800	59.550	81.350	9.500
S (cal/mol K)	64.240	38.470	68.920	43.880

dHr (298K) =	11.500	Kcal/mol
dU (dE) (") =	11.500	Kcal/mol
dSr (") =	10.090	cal/mol K
dGr (") =	8.492	Kcal/mol
Af/Ar (") =	1.605E+02	

T (K)	dH(Kcal/mol)	dU(Kcal/mol)	dS(cal/mol K)	(Af/Ar)	dG(Kcal/mol)
300.000	1.150E+01	1.150E+01	1.010E+01	1.611E+02	8.473E+00
400.000	1.159E+01	1.159E+01	1.036E+01	1.834E+02	7.448E+00
500.000	1.161E+01	1.161E+01	1.041E+01	1.888E+02	6.408E+00
600.000	1.159E+01	1.159E+01	1.037E+01	1.845E+02	5.369E+00
800.000	1.143E+01	1.143E+01	1.014E+01	1.643E+02	3.317E+00
1000.000	1.116E+01	1.116E+01	9.845E+00	1.418E+02	1.318E+00
1200.000	1.084E+01	1.084E+01	9.550E+00	1.223E+02	-6.212E-01
1500.000	1.029E+01	1.029E+01	9.140E+00	9.946E+01	-3.423E+00
2000.000	9.284E+00	9.284E+00	8.564E+00	7.444E+01	-7.844E+00

SECTION IV

FITTING / EXTRAPOLATION METHODS FOR
THE HEAT CAPACITY OF AN IDEAL GAS

EXTRAPOLATION & INTERPOLATION OF $C_p(T)$ FOR AN IDEAL GAS USING AN EXPONENTIAL FUNCTION

We have developed a linear relationship with respect to temperature which can be used to interpolate/extrapolate $C_p(T)$ estimates obtained with group additivity to cover the range from 300 - 5000 K. Data is generated in a piecewise fashion with an maximum error near 5% when compared to literature data. Group additivity estimates between 300 and 1000 K are all that are required. These C_p estimates can then be used to generate thermodynamic property expressions for use with CHEMKIN and other codes requiring thermo property functions in NASA polynomial format.

We start with the following approximation for C_p :

$$C_p(T) = C_{p_{inf}} (1 - \exp (- BT)) \quad (1).$$

Where B is a parameter obtained by regression or estimated by solving for B using known C_p data at 298 or 300 K. $C_{p_{inf}}$ is the high temperature limiting heat capacity. This expression may be transformed to the following linear expression in temperature:

$$Y = - \ln (1 - C_p(T)/C_{p_{inf}}) = BT \quad (2).$$

Equation (2) may be used to obtain rapid estimates of $C_p(T)$ over the entire T range (100 - 5000 K) with a typical maximum error near 10%. This is the best one can obtain with a one parameter model, as will be shown. Only a single C_p estimate at one temperature (298 or 300 K) is required. Accuracy may be improved slightly if more data is available for regression (see figure 4.1), but for

significant improvement another parameter is required.

Equation 1 may be thought of as a simplification of the equation of Yuan and Mok^{6,7} who developed the following four parameter exponential function to describe the temperature dependence of an ideal gas:

$$C_p(T) = A + B \exp (C / T^n) \quad (3)$$

where A, B, C, and n are the parameters determined by non-linear regression.

$$\text{If we define } A = -B = C_{p_{\text{inf}}} = \begin{cases} (3N-2)R & \text{non-linear} \\ & \text{molecule} \\ (3N-1.5)R & \text{linear} \\ & \text{molecule} \end{cases}$$

and define $n = -1$ then equation (3) reduces to equation (1).

We can improve the predictive ability of equation (2) by adding a parameter. Equation (2) now becomes the following:

$$Y = - \ln (1 - C_p(T)/C_{p_{\text{inf}}}) = A + BT \quad (4).$$

This expression can yield estimates within 6% over the temperature range 300 - 5000 K given only 2 reliable data points as close together as 100 K. Data must be at low temperature (300 or 400 K) for the expression to yield accurate values.

At this point it should be noted that the error between equations (3 or 4) and literature is not random. Predictions are either above or below the literature values across the entire temperature range. Since we are interested in the integral of the heat capacity for the enthalpy

function $(H(T)-H^0(T))$, we must see if the integrated error is acceptable. We note that the integrated error (or the error in the enthalpy function) is a better measure of accuracy than the percent error in C_p at any given temperature. The integrated error increases the limits of uncertainty on calculated property changes for reaction at elevated temperatures.

Figures 4.2 (a - j) compare C_p , H_f , and S estimates for ethylene oxide using equation (4) and data at 300, 400, 500, 600, 800, and 1000 K that was estimated using group additivity (the THERM program). The error at 2000 K and 3000 K are -2.5 KJ/mol (1.2%) and -5.25 KJ/mol (1.5%) respectively for $(H(T)-H(298K))$; -1.75 J/mol K (1.4%) and -2.75 J/mol K (1.2%) respectively for $(S(T)-S(298K))$; and -2.5 J/mol K (1.8%) and -2.5 J/mol K (1.67%) respectively for C_p . Results obtained using the harmonic oscillator equation (HOE) are shown figures 4.1 (a-j) for comparison. This method will be discussed in detail later.

If one plots C_p data from the JANAF tables^{<8>} in the form $-\ln(1 - C_p(T)/C_{p_{inf}})$ vs. T , it can be seen that this is not really a linear relationship (see figure 4.3). Even so, a chord drawn between data points at 300 and 400 K and projected to 5000 K (equation 4) results in less than 2% error when transformed to $C_p(5000 K)$. Equation (4) can be used to linearly interpolate smooth data at 100 K (or wider) temperature intervals with remarkable accuracy. Data points generated using Benson's group additivity

method (the THERM program) may be used to generate C_p estimates in a piecewise fashion using equation (4). Typical maximum error from this method is less than 4 %.

We determined that extrapolation above 2000 K is best achieved by assuming that $C_p(20\ 000\ K) = 99.999\% C_{p_{inf}}$. This temperature (20 000 K) has no physical significance, and is only used as a tie point to improve extrapolations.

Heat capacity data are estimated at 1500 and 2000 K using an empirically derived relationship which relates the heat capacity at these temperatures to that at 1000K and $C_{p_{inf}}$. The following relationships have been determined empirically to approximate C_p at 1500 K and 2000 K, and typically result in less than 5% error:

$$C_p(1500K) = C_p(1000K) + 0.37(C_{p_{inf}} - C_p(1000K)) \quad (5)$$

$$C_p(2000K) = C_p(1500K) + 0.37(C_{p_{inf}} - C_p(1500K)) \quad (6).$$

These estimates along with the tie point at 20 000 K are used to extrapolate equation (4) to 6000 K and generate data required to create NASA polynomials.

A computer program has been developed to perform C_p extrapolation and polynomial determination using estimates obtained from THERM and the method described above. The program is called THERMFEX (THERM Fit EXponential), and a listing appears in appendix IV-C.

The method for polynomial fitting is discussed in the next section.

GENERATION OF THERMODYNAMIC PROPERTY DATA IN POLYNOMIAL FORM:

The NASA polynomial format has become a standard method for expressing thermodynamic properties. It is well known that 3rd and 4th order polynomials do a rather poor job of fitting the heat capacity function for an ideal gas over an extended temperature range (300 - 5000 K).^{<9>} In 1967 McBride and Gordon, at NASA,^{<4>} developed a method to fit Cp data using two 4th order polynomials which are tangent at 1000K, the break point temperature (T_{bk}). Fourteen coefficients are determined simultaneously. Ten coefficients are for Cp. Five are for the low temperature region ($T < T_{bk}$) and five for the high temperature region ($T > T_{bk}$). The remaining four coefficients are used for Hf and S over the two temperature regions. In this method H, S, and Cp data are regressed simultaneously. The regression is constrained so that Hf, S, Cp, and their first derivatives match at 1000 K, the break point temperature (T_{bk}).

A second and more efficient method was developed by Hanson and Haskell at Sandia National Laboratory in 1978 to fit thermo property data and generate polynomials in the NASA format.^{<2,3>} The chief difference with their method is that the 10 Cp coefficients are determined first, and then the 4 remaining coefficients (integration constants for Hf and S) are determined using Hf and S data at 298 K only. This method is also a constrained linear regression which must match the Cp its first derivative at 1000 K or

some other break point temperature.

A new method is developed here to fit C_p and generate thermo property polynomials in NASA format using group additivity estimates obtained from the program THERM. The methods discussed above perform constrained linear regression to simultaneously determine 14 or 10 parameters for two polynomials which are tangent at a predetermined T_{bk} . Our method, on the other hand, performs two unconstrained linear regressions to determine 5 C_p coefficients at a time and then solves for the point of tangency. In order for this method to be successful, the data for high and low temperature polynomials must overlap. We generate 45 data points between 300 and 6000 K using estimates from THERM and either an harmonic oscillator equation, developed in the next section, or an exponential function, developed in the previous section. The temperature range is divided into 3 regions. For example the temperature range may be divided into 15 points between 273 and 1000 K (group A), 15 points between 1000 and 1500 K (group B), and 15 points between 1500 and 6000 K (group C). Two unconstrained linear regressions are performed and two polynomials determined. Regression of data groups A and B gives the low temperature polynomial, while regression of data groups B and C gives the high temperature polynomial. A point of tangency is then determined in the region described by data group B (the overlap region) using the Newton/Raphson method.

The coefficients for H_f and S are determined from properties at 298 K in a fashion similar to that of Hanson.<2,3,10>

Properties at T_{bk} are matched to within 0.005% error and their temperature derivatives are matched to within an absolute tolerance of 0.005.

In the event that T_{bk} cannot be determined to satisfy the tolerance for property values and derivatives, the overlap region is moved and/or weighted differently (a different number of data points are used in that region) and the regressions are repeated. In most cases T_{bk} is determined on the first iteration making this a very effective and efficient regression method when sufficient data is available or when it can be extrapolated.

Figure 4.4 compares the polynomials with the C_p estimates used in their determination. The break point temperature is shown at a point of tangency and labeled T_{bk} . For temperatures below T_{bk} the low temperature coefficients are used and above T_{bk} the high temperature coefficients are used. Figures 4.5 (a-f) compare the polynomial fit of C_p data, enthalpy function ($H(T)-H^O(T_{ref})$), and entropy function ($S(T)-S^O(T_{ref})$) extrapolated from group additivity estimates with literature data for biphenyl radical. Figures 4.6 (a-f) are similar comparisons for phenoxy radical, while figures 4.7 (a-b) are comparisons of $C_p(T)$ for furan. Also shown for comparison in these figures are the extrapolations obtained using the harmonic oscillator equation

which will be discussed in the next section.

This method has been compared with literature for more than 40 species and in all cases agreement is excellent with typical maximum error less 5%.

We have developed a computer code which takes H_f , S , and C_p estimates from group additivity (using the computer program THERM), extrapolates them to high temperature, and then uses the method described above to generate thermo property functions in polynomial form. The extrapolation methods are developed in other sections. One computer program is called THERMFEX, and uses an exponential function to generate the required C_p data for regression (listing appears in appendix IV-C). The second program is called THERMFIT and uses an harmonic oscillator equation (HOE) to generate the required C_p data for regression (listing appears in appendix IV-D). An example of the usage of these programs appears in the THERM Users Manual in appendix III-C.

Table IV.ii shows the polynomial output in NASA compatible format phenoxy radical and dimethyl ether. Although this format can be read by CHEMKIN and other codes which allow T_{bk} to vary from one species to the next, there are several small modifications which have been incorporated for use with the programs developed here. Table IV.i explains what information is contained in these polynomials column by column for each of the four lines required per species. The chief modification to the standard format

used by CHEMKIN is that the number of rotors in a molecule appears in column 79 on the first line of data for each species. In addition, the first two lines in the file must be padded with blanks to column 80 to allow direct access for use with the program THERMRXN (thermodynamic property analysis for reaction) which is described in the THERM Users Manual (see appendix III-C).

Table IV.i gives the polynomial equations for $H(T)$, $S(T)$, and $C_p(T)$ with coefficients as described in table IV.ii.

HEAT CAPACITY DATA FROM STATISTICAL MECHANICS:

The heat capacity (C_p) of an ideal gas can be calculated from spectroscopic data using standard formulas from statistical mechanics. <5,11,12,13,14>

Each degree of freedom in a molecule makes a contribution to the total heat capacity (C_{p_t}). The translational contribution to the heat capacity at constant volume ($C_{v_t}(T)$) is given by the following expression:

$$C_{\text{trans}} = 5/2 R \quad (7)$$

where R is the universal gas constant. Rotational contributions are different for linear and non-linear molecules. The following expressions are used for rotational contributions to C_{v_t} :

$$C_{\text{rot}} = R \text{ (for linear molecules)} \quad (8a)$$

$$C_{\text{rot}} = (3/2)R \text{ (for non-linear molecules)} \quad (8b)$$

The temperature dependence for the heat capacity of an ideal gas arises from the vibrational contribution alone for molecules with no hindered internal rotors and negligible electronic contribution. The vibrational contribution must be summed over the number of vibrational degrees of freedom (S) in a molecule and is given by the following expressions:

$$C_{\text{vib}} = R \cdot \sum_i^S f(u_i, T)$$

$$\text{where } f(u_i/T) = (u_i/T)^2 \frac{\exp(u_i/T)}{(\exp(u_i/T) - 1)^2} \quad (9)$$

$$S = 3N - 6 \text{ for non-linear molecules or} \\ = 3N - 5 \text{ for linear molecules.}$$

N = the number of atoms in the molecule.

$$u_i = (hcw_i / k) \quad (10)$$

where h is Plank's constant, c is the speed of light, k is Boltzman's constant, and w_i is the vibrational wavenumber (cm^{-1}) for the i^{th} vibrational mode (degree of freedom) in the molecule.

The total heat capacity at constant volume ($C_{v_t}(T)$) is then given as the sum of the individual contributions as follows:

$$C_{v_t}(T) = C_{\text{trans}} + C_{\text{rot}} + C_{\text{vib}} + C_{\text{elec}}$$

where C_{trans} , C_{rot} , C_{vib} are the translational, rotational, and vibrational contributions to C_v . The electronic contribution (C_{elec}) can typically be neglected.

The heat capacity at constant pressure can then be written as follows:

$$C_{p_t}(T) = C_{v_t} + R = R + C_{\text{trans}} + C_{\text{rot}} + C_{\text{vib}} \quad (11)$$

$$= 4R + C_{\text{vib}} \quad (\text{non-linear molecule}) \quad (12a)$$

$$= (7/2)R + C_{\text{vib}} \quad (\text{linear molecule}) \quad (12b)$$

Using equation 9, one can calculate C_{vib} . Equations 11 and 12 can be used only for simple polyatomic molecules that have no contribution from free or hindered internal rotations (such as those found in dimethyl acetylene (free) or ethane (hindered)), and where electronic and anharmonic effects can be neglected.

The limit of equation 9, as temperature (T) tends to infinity is unity. Each vibrational mode, therefore, contributes a maximum of R (gas constant) to C_{p_t} . The high temperature limiting heat capacity ($C_{p_{inf}}$) is therefore obtained from equation 12 as follows:

$$C_{p_{inf}} = R (3 N - 2) \quad (\text{non-linear molecule}) \quad (13a)$$

$$= R (3 N - 1.5) \quad (\text{linear molecule}) \quad (13b).$$

These expressions must be modified to account for free internal rotations if they need to be considered. Each free rotor (a functional group which may rotate with no potential barrier) contributes $1/2 R$ to C_{p_t} at the expense of one vibrational degree of freedom. For a molecule having one or more free rotors, equations 11 - 13 become the following:

$$C_{p_t}(T) = C_{v_t} + R = C_{trans} + C_{rot} + C_{vib} + (N_{frot}/2)R \quad (14)$$

$$= 4 R + C_{vib} + (N_{frot}/2)R \quad (\text{non-linear molecule}) \quad (15)$$

$$C_{p_{inf}} = R (3N - (2 + N_{frot}/2)) \quad (\text{non-linear molecule}) \quad (16)$$

Equation 9 is used to calculate the vibrational contribution to C_{p_t} , except that $S = 3N - (6+N_{frot})$ where N_{frot} is equal to the number of free rotors in the molecule.

The situation is significantly complicated when hindered internal rotations need to be considered.^{<13>} A detailed discussion of the contribution of hindered internal rotations to C_{p_t} is beyond the scope of this work.

The interested reader is referred to the work of Pitzer,^{<15>} Pitzer and Gwinn,^{<16>} Pitzer and Brewer,^{<17>} Price,^{<18>} and Crawford.^{<19>} Detailed consideration of hindered internal rotations requires the solution of the Schrodinger wave equation given the appropriate potential function for internal rotation. Pitzer and Gwinn^{<16>} have performed a detailed analysis on this problem and correlated the contributions to thermodynamic properties from hindered internal rotations with the maximum potential barrier (V/RT) and the reciprocal of the rotational partition function for free rotation ($1/Q_f$). These tables have been widely used to estimate the contribution to C_{p_t} from hindered internal rotors.

An example is now presented to illustrate the calculation of $C_p(T)$ for a molecule where internal rotations need to be considered:

Hexafluoroethane has eight atoms and one hindered internal rotation. Using equation 8 and assuming that the hindered rotation acts essentially as a free rotor in the high temperature limit (this is a very good assumption) we find that $C_{p_{inf}} = 178.7$ KJ/mol. Hexafluoroethane has 17 vibrational degrees of freedom and one hindered internal rotation. The JANAF Tables^{<8>} list the frequencies for the 17 oscillators and gives the maximum potential barrier to internal rotation (V) to be 16.57 KJ/mol. Using equations 7-16 we can obtain the vibrational contribution to C_{p_t} (see appendix IV-E for this calculation). A computer program

named Cpideal was written to facilitate these calculations. A listing appears in appendix IV-E. To apply the method of Pitzer and Gwinn it is necessary to calculate the reduced moment of inertia for rotation about the C/C bond in this molecule. The moment of inertia for rotation of a CF₃ group about the C - C axis is given by the following expression, with bond distances and bond angle from the JANAF Tables:

$$I_{CF_3} = \frac{3 \times 19. \times (1.33 \sin 68.5^\circ)^2}{6.023 \text{ E}+23 \times 1.0 \text{ E}+16}$$

$$= 144.9 \text{ E}-40 \text{ gm cm}^2$$

The reduced moment of inertia is given by the following expression:

$$1/I_r = 1/I_a + 1/I_b \quad (17)$$

where I_a and I_b are the moments of inertia for each group. In the case of hexafluoroethane $I_a = I_b = I_{CF_3} = 1.449 \text{ E}-38 \text{ gm cm}^2$. Equation 11 then gives $I_r = 7.32 \text{ E}-39 \text{ gm cm}^2$. The partition function for free rotation is given by the following expression:

$$1/Q_f = \frac{h \sigma_r}{(8 \pi^3 I_r k T)^{1/2}} = \frac{n}{2.7935 \text{ E}+19 (I_r T)^{1/2}} \quad (18)$$

where n is the number of potential maxima which occur during one rotation of the group (for CF₃/CF₃, $n = 3$). From equation 12 we obtain $1/Q_f = 0.07247$ at 300 K. Using the tables of Pitzer and Brewer ^{<17>} we obtain a contribu-

tion to C_p from internal rotation of the CF_3 group (at 300 K) equal to 9.414 J/mol. The C_p for C_2F_6 at 300 K is then given as the sum of contributions from each degree of freedom in the molecule or 106.7 J/mol. This is in excellent agreement with the tabulated value of 106.8 J/mol given in the JANAF Tables. The 0.1 J/mol difference is due to interpolation error for values in the Pitzer/Brewer tables. This calculation is presented in more detail with results tabulated in appendix IV-E. A similar calculation for internal rotational contribution to C_p for biphenyl is also presented in appendix IV-E. These examples are presented to illustrate the current literature method used to calculate C_p for an ideal gas.

In the next section, a model is developed which will allow accurate extrapolation of low temperature heat capacity estimates from group additivity or available experimental data (< 1000 K) to high temperatures (5000 K). While, this model is based upon the principles of statistical mechanics which have been reviewed here, it does not require input of moments of inertia or barriers to internal rotation. All that is required is low temperature C_p data and the number of rotors.

DEVELOPMENT OF A Cp EQUATION BASED UPON STATISTICAL MECHANICS:

For molecules where no internal rotations need be to considered, equations 1 - 10 show us that the only temperature dependent term for contributions to Cp is that for vibrations (C_{vib}) given by equation 3. One may attempt to fit Cp data using a single term from equation 3 and some mean vibrational frequency (w_{mean} (cm^{-1})). In this case the summation is replaced by the constant factor S (the number of oscillators) as follows for non-linear molecules:

$$C_p(T)/R = 4 + S \cdot (u_{mean}/T)^2 \frac{\exp(u_{mean}/T)}{(\exp(u_{mean}/T) - 1)^2} \quad (19)$$

It can be easily shown that equation 19 gives generally poor results even if u_{mean} is determined by fitting reliable Cp data. The reason for this is that the contribution to Cp from each vibrational mode is a function of frequency and temperature. The relative contribution from any one vibrational frequency varies with temperature. The mean frequency which reproduces Cp at one temperature is different from that required to fit Cp at another temperature. Therefore, it is not surprising that a single mean vibrational frequency does a poor job of representing the complex behavior of Cp as a function of temperature. Figures 4.8 and 4.9 illustrate how poorly the geometric and arithmetic mean frequencies reproduce Cp(T) using equation 19 for cyclopentadiene when compared with the data of Dorafeeva, et al. <20>

In order to improve this calculation, one may attempt to increase the number of terms (n_t) considered. Equation 19 can then be rewritten as:

$$C_p(T)/R = 4 + \frac{S}{n_t} \sum_i^{n_t} (u_i/T)^2 \frac{\exp(u_i/T)}{(\exp(u_i/T) - 1)^2} \quad (20)$$

It can be shown that equation 14 is only able to fit the C_p behavior in the limit as the number of terms considered (n_t) approaches the number of oscillators in the molecule. For cyclopentadiene, which has 27 vibrational modes, we may require nearly 27 parameters (or at least half that many) to fit C_p using equation 20. In this limit, equation 20 reduces to equation 3. Since vibrational frequency data is typically not readily available for many molecules whose C_p are required, equations 9 and 20 offer no solution to fitting or extrapolation of C_p data.

The solution to this problem is to replace the summation over the number of vibrational degrees of freedom in the molecule with a 3 term expression based upon equation 3, but with weighting factors as coefficients to these terms. These coefficients need not have integer values.

We have chosen a three term equation as follows (for a non-linear molecule):

$$C_p(T)/R = 4 + A_1 \cdot f(u_1/T) + A_2 \cdot f(u_2/T) + A_3 \cdot f(u_3/T) \quad (21)$$

where $f(u_i/T)$ is given by equation 3 with u_i and A_i determined from non-linear regression using the method of Marquardt^{<21>}. Equation 21 is a six parameter non-linear model for $C_p(T)$ for any non-linear molecule having no internal rotations.

Making use of the fact that the coefficients A_i must sum to S (the number of oscillators) we can reduce equation 21 to a 5 parameter expression which we call an Harmonic Oscillator Equation (HOE):

$$C_p(T)/R = 7/2 + A_1 \cdot f(u_1/T) + A_2 \cdot f(u_2/T) + (S - (A_1 + A_2)) \cdot f(u_3/T)$$

Harmonic Oscillator Equation (HOE) (22a)
linear molecule

$$C_p(T)/R = 4 + A_1 \cdot f(u_1/T) + A_2 \cdot f(u_2/T) + (S - (A_1 + A_2)) \cdot f(u_3/T)$$

Harmonic Oscillator Equation (HOE) (22b)
non-linear molecule

This equation is based upon the harmonic oscillator model for vibrational contribution to the heat capacity of an ideal gas. This equation has been found to give an excellent fit for C_p data across the temperature range 300 - 6000 K. Equations 22 have the fundamentally correct functional form for the heat capacity of an ideal gas. This allows C_p data to be extrapolated from low temperature to high temperature with a high degree of accuracy. Figure 4.10 illustrates how well this expression fits C_p data for cyclopentadiene. The solid line is the C_p func-

tion described by equation 22b. Only six data points between 300 and 1000 K in addition to the high temperature limiting heat capacity $C_{p_{inf}}$ (described by equation 13b) are required to determine parameters for equations 22. Figures 4.11 (a-b) demonstrate how well equation 22b does in extrapolating C_p data to high temperature for benzene. Again, only data at 300, 400, 500, 600, 800, and 1000 K were used to determine the parameters of equation 22b. The data points labeled () in figure 4.11a are those of Burcat^{<1>}. Those points labeled (*) are the group additivity data points obtained with the THERM computer program and used to project the C_p to high temperature. There is excellent agreement between extrapolated C_p values and those from literature. The maximum error is less than 0.3% when C_p data from group additivity are used, and less than 0.05 % when Burcat's C_p data at 300, 400, 500, 600, 800, and 1000 K are used for the regression (see figure 4.11c).

Equation 22b implies that the 30 non-degenerate vibrational frequencies of benzene can be represented as the weighted average of only three frequencies. Term 1 represents the low frequency vibrations, term 2 represents the mid frequency vibrations, and term 3 represents the high frequency vibrations occurring in a molecule.

The use of equation 22b for molecules which contain free or hindered internal rotations requires only a small modification to the high temperature limiting heat capacity and the number of oscillators.

All hindered rotations are considered to become free rotors in the high temperature limit. Few exceptions to this rule have been found. Three molecules which violate assumptions of equations 22 are now presented to illustrate the maximum errors encountered when these equations are used to extrapolate Cp data.

Hexachloroethane has a severely hindered rotation with a potential barrier in excess of 42 KJ/mol.^{<8>} Rigorous calculation of the contribution of this hindered rotation to Cp for C₂Cl₆ show a maximum in Cp(T) near 2000 K.^{<8>} This maximum is not predicted by equation 22b, however, the maximum error in neglecting this is less than 4% (see figures 4.12 a-f). Two additional molecules which do not adhere to equations 22 are acetylene (which requires significant anharmonic corrections) and ammonia (which undergoes inversion between two pyramidal conformations). In these cases, equation 22b produces less than 5% error in high temperature Cp extrapolations (see figures 4.12-4.14). Acetylene, however (equation 22a), has larger errors due to the required corrections to the rigid rotator harmonic oscillator model for this molecule. Acetylene is a unique molecule in this respect; ethynl radical and substituted acetylenes produce no such violation of the HOE model.

Hexafluoroethane, which has a more typical barrier to internal rotation, is fit with a maximum error of 0.3% (see figures 4.15 a-f).

The required modifications to equation 16 for $C_{p_{inf}}$ have been determined empirically as follows:

$$C_{p_{inf}} = R (3N - (2 + N_{rot}/4)) \text{ (non-linear molecule) } \quad (23)$$

$$\text{with } S = 3 N - (6 + N_{rot}/2) \quad \text{(non-linear molecule) } \quad (24) .$$

Equations 23 and 24 sacrifice some realism for the sake of a more generally applicable expression. Each internal rotation is weighted as 1/2 of a vibrational degree of freedom instead of the theoretically correct value of 1 vibrational degree of freedom. Statistical mechanics tells us that $C_{p_{inf}}/R$ should be reduced by 1/2 for each free rotor. Equation 23, however, yields results which are more consistent with available experimental data. It is recognized that the use of equations 23 and 24 will result in a slight overestimate (typically less than 1%) for molecules which contain truly free internal rotations.

C_p extrapolations have been compared with literature for more than 50 species using this method. Agreement is generally excellent, with maximum errors less than 0.1% when the literature C_p data are used for the non-linear regression.

As stated earlier, the motivation to develop an extrapolation method for C_p data arises from the need to determine thermodynamic properties in polynomial form which are valid outside the temperature range for which Benson's group estimates are available. Equations 22 - 24 provide

such a method. In figures 4.16 - 4.18 (a-f), Cp, Hf, and S data estimated using the THERM program (extrapolated with equation 22b) are compared with data from Burcat, et al^{<1>} for phenyl radical, phenol, and biphenyl. Here we are comparing data from two different sources, and the agreement is excellent.

An important and valuable benefit to the use of equations 22 for Cp data extrapolation is that the parameters determined from regression have physical significance. The parameters obtained from fitting Cp data can be used to estimate the vibrational distribution, geometric and arithmetic mean frequencies, the density and sum of vibrational quantum states, and the vibrational partition function for molecules. These applications will be discussed further in the next section.

A computer program called CPFIT has been developed to apply equations 22 to fit Cp data for linear as well as non-linear molecules (with or without hindered internal rotations). The code employs Marquardt's method ^{<21>} for the non-linear regression. A numerically determined Jacobian matrix has been replaced with an explicit matrix of partial derivatives to substantially improve computational efficiency (source code listing appears in appendix IV-F).

The code does not require any estimate for potential barriers or reduced moments of inertia for molecules having hindered internal rotations, however, we still need accurate low temperature data.

The chief weakness for this method is the sensitivity to the initial parameter guesses and parameter constraints. Molecules which contain only low frequency oscillators, such as CCl_4 , will not be fit well if initial parameter values contain a high frequency oscillator. Regression will converge to a solution which is in significant error (as much as 25%). If calculated frequencies are too high, the error will be negative (Cp estimates will fall below Cp data). If, on the other hand, calculated frequencies are too low, the error will be positive (Cp estimates will be larger than the Cp data points). This fact is used to perform a systematic restart of the regression to insure an adequate fit. A new starting point and feasible region are determined if an adequate fit (max error < 4%) is not achieved with the first solution.

A listing of this computer program CPFIT appears in appendix IV-F. A listing of the program THERMFIT (which incorporates NASA polynomial determination) appears in appendix IV-D.

APPLICATION OF HARMONIC OSCILLATOR EQUATION PARAMETERS
TO CALCULATIONS REQUIRING VIBRATIONAL FREQUENCIES

The harmonic oscillator equation (HOE) was shown to be an effective method to extrapolate heat capacity data from low temperature (< 1000 K) to high temperature (5000 K). In this section we shall demonstrate that group additivity and the HOE (equations 22) can be used to estimate properties and functions which require vibrational frequency data. We shall compare vibrational partition functions, sum of vibrational quantum states, and mean frequencies (geometric, arithmetic, and root mean square) estimated using HOE and Cp data from group additivity with those calculated from experimental frequencies available in literature. Unimolecular QRRK calculations performed with estimated geometric mean frequencies will be compared with those calculated using experimental mean frequencies as well as RRKM calculations from literature.

VIBRATIONAL PARTITION FUNCTION: We consider first the vibrational partition function which can be written as follows for a polyatomic molecule: <12,22>

$$Q_{\text{vib}}(T) = \sum_{i=1}^S \frac{1}{1 - \exp \{ - hcw_i/kT \}} \quad (25)$$

where h is Plank's constant, c is the speed of light, k is Boltzman's constant, T is absolute temperature, and w_i is

the vibrational wavenumber for the i^{th} vibrational degree of freedom.

Figure 4.19 compares the natural logarithm of the vibrational partition function for cyclohexa-1,3-diene estimated from Cp data with that calculated from experimental frequency data.^{<46>} Also included for comparison, are estimates using arithmetic and geometric mean frequencies. The predictive ability of HOE is quite good. Maximum error for cyclohexa-1,3-diene is 1 unit in $\ln(Q_{\text{vib}})$ at 298 K using HOE frequencies determined from group additivity estimates for Cp. In comparison, the literature geometric mean frequency produces a maximum error of 3 units in $\ln(Q_{\text{vib}})$ at 1000 K, while the literature arithmetic mean produces a maximum error of 8 units at 6000 K.

Prediction of $\ln(Q_{\text{vib}})$ for molecules having hindered internal rotations is not necessarily improved by subtracting the contribution to Cp due to the hindered internal rotation before fitting with the HOE (equation 22b). For C_2F_6 we remove the internal rotational contribution from Cp (calculation of internal rotation contribution for C_2F_6 appears in appendix IV-E). Fitting the corrected Cp(T) we then obtain frequencies and degeneracies which produce similar error in $\ln(Q_{\text{vib}})$. Figure 4.20 demonstrates estimates of vibrational partition function for C_2F_6 with and without corrections for the hindered internal rotation are within the uncertainty for properties derived from group additivity values.

SUM AND DENSITY OF VIBRATIONAL QUANTUM STATES

The next calculation that we shall examine is the sum and density of vibrational quantum states. The sum ($W(E_{\text{vib}})$) and density ($N(E_{\text{vib}})$) of vibrational quantum states can be calculated using the Whitten-Rabinovitch modification to the Marcus-Rice semiclassical approximation.^{<22,23,24>} This approximation can be written as follows:

$$W(E_{\text{vib}}) = \frac{(E_{\text{vib}} + a E_z)^S}{S! \prod_i h c w_i} \quad (26)$$

and

$$N(E_{\text{vib}}) = \frac{(E_{\text{vib}} + a E_z)^{S-1}}{(S-1)! \prod_i h c w_i} \left[1 - B(du/dE') \right] \quad (27)$$

where

$$E_z = \sum_{i=1}^S (h c w_i / 2) ; \quad E' = E_{\text{vib}} / E_z$$

$$a = 1 - B u(E') ; \quad B = \frac{S-1}{S} \cdot \frac{\langle w^2 \rangle}{\langle w \rangle^2}$$

$$\langle w^2 \rangle = (1/S) \cdot \sum_i (w_i^2) ; \quad \langle w \rangle^2 = \left\{ (1/S) \cdot \sum_i (w_i) \right\}^2$$

$$u(E') = \begin{cases} (5.0 E' + 2.73 E'^{0.5} + 3.51)^{-1} & \text{for } 0.1 < E' < 1.0 \\ \exp \{ -2.4191 E'^{0.25} \} & \text{for } 1.0 < E' < 8.0 \end{cases}$$

$$du(E')/dE' = \begin{cases} -(5.00 + 1.365 E'^{-0.5}) u^2 & \text{for } (0.1 < E' < 1.0) \\ -(0.60478 E'^{-0.75}) u & \text{for } (1.0 < E' < 8.0) \end{cases}$$

Figure 4.21 compares $\ln\{W(E_{vib})\}$ calculated using literature frequencies with those calculated from HOE parameters obtained from fitting C_p data for cyclohexa-1,3-diene. For comparison $\ln\{W(E_{vib})\}$ estimated with geometric and arithmetic mean frequencies are also shown. As can be seen, HOE frequency parameters can be used to estimate this function with much higher accuracy than the geometric mean frequency. Hindered internal rotor effects need not be removed from C_p estimates in order to approximate these functions accurately. Figure 4.22 compares estimates based upon HOE parameters with calculations using literature frequencies for biphenyl. With or without hindered internal rotational contributions removed from group additivity C_p estimates, the HOE parameters which are obtained approximate the sum of vibrational quantum states rather well.

ESTIMATING GEOMETRIC AND ARITHMETIC MEAN VIBRATIONAL FREQUENCIES:

The geometric mean vibrational frequency is required for QRRK calculations presented throughout this thesis. An harmonic oscillator equation (equations 22) may be used to obtain an estimate of mean vibrational frequencies by fitting C_p data from THERM (group additivity). One uses the parameters of equations 22 to determine mean frequen-

cies. The geometric (w_{gm}) and arithmetic (w_{am}) mean vibrational frequencies may be obtained using the following expressions:

$$\bar{w}_{gm} = \sqrt[S]{w_1^{A_1} \cdot w_2^{A_2} \cdot w_3^{(S-(A_1+A_2))}} \quad (28)$$

$$\bar{w}_{am} = \frac{1}{S} \left[A_1 \cdot w_1 + A_2 \cdot w_2 + (S-(A_1+A_2)) \cdot w_3 \right] \quad (29)$$

with parameters A_i and w_i described by equations 22. The computer program CPFIT performs these estimations (see appendix IV - F).

Table IV.iii compares estimated and literature mean frequencies for 50 species (more than 30 of which are based upon group additivity Cp estimates). Maximum error in estimating the geometric mean frequency is estimated as 50 cm^{-1} which is rarely greater than 10% error with error for most species within 2%.

Geometric mean frequencies obtained from literature range anywhere from 400 cm^{-1} for CCl_4 to near 2000 cm^{-1} for CH_4 . Predictions in table IV.iii have a typical accuracy better than $\pm 25 \text{cm}^{-1}$ when compared with literature values for geometric mean frequencies. This is actually quite good. Let us consider how well literature frequency data from two sources compare. Frequency data may be obtained for furan ($\text{C}_4\text{H}_4\text{O}$) from Chao et.al.^{<25>} or from Simandiras^{<26>}. These sources give geometric mean's of

1221 and 1244.5 cm^{-1} respectively or a difference of nearly 25 cm^{-1} . The estimate from THERM (group additivity) Cp data is obtained using the HOE as 1215 cm^{-1} which is closer to the value from Chao than the value from Simandiras is. This demonstrates that mean frequencies estimated in this manner have uncertainties on the same order as those derived from literature frequency data.

A comparison of mean frequencies estimated from literature Cp data with those estimated from group additivity Cp data shows that HOE parameters are only as reliable as the Cp estimates which one uses. Mean frequencies based upon group additivity data typically have larger errors than those based upon literature Cp data. Even so, group additivity Cp estimates do a remarkably good job in predicting the functions described in this section. It is our feeling that the HOE (equations 22) presents us with an easy and effective method to estimate mean vibrational frequencies from group additivity Cp data. QRRK calculations presented in other sections of this work utilized geometric mean frequencies estimated in this manner.

Unimolecular QRRK calculations using the method of Dean^{<27>} are now presented for three species to illustrate how good of an approximation mean frequencies obtained using the HOE and Cp are.

The first case to be considered is that for unimolecular dissociation of SF_6 at 1750 K. Required input data come from Lyman^{<28>} and appear in table IV.iv. Using Cp

data from Benson^{<30>} the geometric mean vibrational frequency is estimated from the HOE as 596/cm as compared to 591/cm given by Lyman. Figure 4.23 compares calculated fall-off behavior for this reaction using these two frequencies. Results are identical. QRRK results are shown to be in good agreement with the RRKM results of Lyman.

The second example will be unimolecular dissociation of phenyl radical (C_6H_5) at 1700 K. Required input data are taken from Rao and Skinner^{<29>} and are presented in table IV.v. Using group additivity (THERM) and the HOE we estimate the geometric mean vibrational frequency for C_6H_5 to be 1204 cm^{-1} while that obtained from the data of Skinner is 1180 cm^{-1} . Figure 4.24, again, shows QRRK calculations using these two frequencies to be virtually identical. Skinner's RRKM calculations are also reproduced for comparison. QRRK using this estimated mean frequency matches Skinner's results rather well.

The final example presented is unimolecular dissociation of benzene (C_6H_6) to form phenyl + H atom. Group additivity and the HOE estimate the geometric mean frequency to be 1216 cm^{-1} while the data of Burcat give 1205.8 cm^{-1} . Again, required input parameters for QRRK are taken from Skinner and are presented in table IV.vi. Figure 4.25, shows once again that the estimated mean frequency reproduces fall-off results calculated with actual mean frequency. In addition, the QRRK results are in good agreement with Skinners RRKM calculations. Figures

4.23 - 4.25 not only show how well frequencies obtained from group additivity do when applied to QRRK calculations, but also how good the QRRK theory is at approximating the more rigorous RRKM calculations.

CONCLUSION: In this section we have shown that parameters obtained for the Harmonic Oscillator Equation (HOE) by fitting estimated Cp data not only have physical significance, but can be used to estimate functions requiring vibrational frequency data with a high degree of success. The harmonic oscillator equation is a valuable tool allowing the extrapolation of low temperature (< 1000 K) Cp data to 5000 K and in addition giving frequencies and degeneracies which can be used further to approximate statistical mechanics functions for species where the vibrational frequency data are not available.

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APPENDIX IV - A

TABLES FOR SECTION IV

TABLE IV.i

POLYNOMIAL REPRESENTATION OF THERMODYNAMIC PROPERTY DATA

Heat capacity:

$$C_p(T) = R (a_1 + a_2 T + a_3 T^2 + a_4 T^3 + a_5 T^4) \quad T > T_{bk}$$

$$C_p(T) = R (a_8 + a_9 T + a_{10} T^2 + a_{11} T^3 + a_{12} T^4) \quad T < T_{bk}$$

Enthalpy of formation:

$T > T_{bk}$

$$H(T) = R (a_1 T + \frac{a_2}{2} T^2 + \frac{a_3}{3} T^3 + \frac{a_4}{4} T^4 + \frac{a_5}{5} T^5 + a_6)$$

$T < T_{bk}$

$$H(T) = R (a_8 T + \frac{a_9}{2} T^2 + \frac{a_{10}}{3} T^3 + \frac{a_{11}}{4} T^4 + \frac{a_{12}}{5} T^5 + a_{13})$$

Entropy:

$T > T_{bk}$

$$S(T) = R (a_1 \ln(T) + a_2 T + \frac{a_3}{2} T^2 + \frac{a_4}{3} T^3 + \frac{a_5}{4} T^4 + a_7)$$

$T < T_{bk}$

$$S(T) = R (a_8 \ln(T) + a_9 T + \frac{a_{10}}{2} T^2 + \frac{a_{11}}{3} T^3 + \frac{a_{12}}{4} T^4 + a_{14})$$

TABLE IV.ii

NASA FORMAT EXPLAINED

```

THERMO
300., 1000., 5000.
C6H5O    3/20/89 THERMC  6H  50  1  0G  300.000  5000.000  1404.000  01
1.57324764E+01 1.54394760E-02-5.31383756E-06 8.28591116E-10-4.82238305E-14  2
-1.76799222E+03-6.20052317E+01-3.73072513E+00 6.71840729E-02-5.88121307E-05  3
2.61335718E-08-4.61968583E-12 4.31827564E+03 4.02213334E+01  4
CH3OCH3  3/20/89 THERMC  2H  60  1  0G  300.000  5000.000  1364.000  21
8.43631162E+00 1.30235626E-02-4.45885307E-06 6.93233262E-10-4.02757540E-14  2
-2.62777965E+04-2.24530764E+01 1.53263200E+00 2.37669572E-02-8.14177550E-06  3
-5.29451929E-10 5.96605679E-13-2.32831259E+04 1.66340885E+01  4
END
    
```

column numbers:

```

1      10      20      30      40      50      60      70      80
|-----|-----|-----|-----|-----|-----|-----|
|23456789|123456789|123456789|123456789|123456789|123456789|123456789|
    
```

```

|<-name>|<-date->|<ref>|<---- elements ---->G|<- Tlow >|<- Thi->|<- Tbk->| 21
|<---- a1 ---->|<---- a2 ---->|<---- a3 ---->|<---- a4 ---->|<---- a5 ---->| 2
|<---- a6 ---->|<---- a7 ---->|<---- a8 ---->|<---- a9 ---->|<---- a10 ---->| 3
|<---- a11 ---->|<---- a12 ---->|<---- a13 ---->|<---- a14 ---->| 4
    
```

- 4 lines per species
- number of rotors appears in column 79 of first line

line 1:

- species name column 1-9
- date : column 11-19
- reference: column 20-24
- elements : columns 26-44
- phase : column 45
- low temperature limit
- high temperature limit
- break point temperature
- number of rotors : column 79
- line number "1" for first line of species :column 80

line 2:

- coefficients 1-5 : columns 1 - 75
- line number "2" for second line of species :column 80

line 3:

- coefficients 6-10 : columns 1 - 75
- line number "3" for third line of species :column 80

line 4:

- coefficients 11-14 : columns 1 - 60
- line number "4" for fourth (last) line for this species :column 80

TABLE IV.iii

SPECIES	LIT $w_{am}(cm^{-1})$	Cpfit $w_{am}(cm^{-1})$	LIT $w_{gm}(cm^{-1})$	Cpfit $w_{gm}(cm^{-1})$	source Cp data
C_3H_6	1646.9	1648.4	1429.7	1430.5	(a)dorafeeva
"	"	1614.3	"	1415.1	(b)therm
CY-1,3-HD	1436.7	1442.3	1183.2	1209.7	a
"	"	1449.1	"	1196.0	b
C_2F_6	745.77	725.0	637.7	668.9	c: therm (subtr. rotor)
"	"	637.0	"	601.3	d: therm (ignore rotor)
BIPHENYL	1308.5	1323.23	1038.4	1091.13	c
"	"	1266.65	"	1034.54	d
CY- C_5H_{10}	1570.7	1540.76	1339.5	1324.5	c
"	"	1523.17	"	1294.10	d
CY- C_4H_8O	1546.34	1524.12	1339.2	1345.6	c
"	"	1505.52	"	1317.43	d
C_6H_6	1426.2	1427.3	1205.8	1213.1	(e) Burcat
"	"	1415.48	"	1218.35	b
C_2H_4	1799.58	1798.57	1585.99	1586.1	(f) JANAF
"	"	1779.02	"	1578.3	b
C_6H_5Cl	1288.57	1291.65	1033.74	1057.72	(g) Skinner
"	"	1269.60	"	1054.32	b
CY- C_2H_4O	1637.4	1636.7	1443.97	1443.07	f
"	"	1625.91	"	1440.03	b
CY- C_3H_4	1573.9	1573.6	1345.2	1346.8	a
"	"	1575.4	"	1353.1	b
CY- C_7H_{14}	1460.79	1467.87	1174.6	1215.9	a
"	"	1443.16	"	1205.26	b

SPECIES	LIT $\omega_{\text{am}}(\text{cm}^{-1})$	Cpfit $\omega_{\text{am}}(\text{cm}^{-1})$	LIT $\omega_{\text{gm}}(\text{cm}^{-1})$	Cpfit $\omega_{\text{gm}}(\text{cm}^{-1})$	source Cp data
$\text{C}_6\text{H}_5\text{Br}$	1280.97	1285.18	1013.53	1044.32	g
"	"	1273.72	"	1052.36	b
C_2HCl	1152.29	1154.47	798.27	823.48	f
"	"	1134.59	"	795.04	b
C_2Cl_2	660.71	611.82	441.70	401.55	f
"	"	598.82	"	352.30	b
Cy-1,3- C_8H_{12}	1404.6	1412.09	1108.14	1152.73	a
"	"	1404.37	"	1150.5	b
Cy-1,5- C_8H_{12}	1401.85	1408.27	1107.95	1149.08	a
"	"	1373.52	"	1142.84	b
Cy- C_7H_8	1405.77	1409.22	1139.56	1162.22	a
"	"	1408.66	"	1171.82	b
C_2F_2	799.86	801.42	635.32	644.34	f
Cy- C_4H_4	1455.28	1452.75	1239.8	1240.26	a
Cy- $\text{C}_4\text{H}_4\text{S}$	1353.7	1351.74	1131.97	1132.69	(h) Simandiras
Cy- $\text{C}_4\text{H}_5\text{N}$	1465.0	1462.8	1231.4	1233.0	"
C_2HF	1223.43	1226.02	865.26	883.39	f
C_2F_4	778.17	784.02	619.62	646.87	"
SiBr_4	255.46	256.96	199.91	202.07	"
SF_6	623.6	631.51	591.0	598.1	(i) Lyman
SiH_2Cl_2	989.78	1048.39	777.55	840.64	f
SiH_2F_2	1112.44	1116.47	953.99	970.05	"
SiH_4	1493.0	1494.1	1365.5	1366.0	"
CH_3F	1865.3	1862.2	1708.0	1700.3	"
CHCl_3	951.62	953.59	727.99	728.73	"

SPECIES	LIT $w_{am}(cm^{-1})$	Cpfit $w_{am}(cm^{-1})$	LIT $w_{gm}(cm^{-1})$	Cpfit $w_{gm}(cm^{-1})$	source Cp data
CHF ₃	1216.0	1217.1	1051.12	1053.68	"
H ₂ SO ₄	1107.3	1110.6	788.01	807.4	"
CH ₄	2106.5	2128.7	1956.74	1958.45	"
N ₂ H ₄	1736.25	1741.86	1387.12	1402.95	f
CCl ₃ F	549.09	553.08	479.5	429.6	"
CCl ₄	462.7	460.5	408.2	401.9	"
CF ₄	835.6	828.8	766.36	757.4	"
CH ₂ Cl ₂	1398.0	1399.9	1116.3	1141.8	"
CH ₂ F ₂	1564.2	1570.3	1381.78	1391.10	"
B ₃ H ₂ O ₃ F	992.38	996.51	796.96	820.04	"
B ₃ O ₃ Cl ₃	596.52	603.93	456.34	492.25	"

TABLE IV.iv

SF6 DISSOCIATION Re: LYMAN jcp 67 P1808 1977
 ****DISSOCIATING SPECIES****
 SF6
 ****PRODUCT CHANNEL 1 (LOWEST ENERGY)****
 SF5 + F
 ****PRODUCT CHANNEL 2 ****
 ****PRODUCT CHANNEL 3 ****

GEOMETRIC MEAN FREQUENCY; # OF OSCILLATORS (S)*
 591.0 15
 COLLISION COMPLEX MASS; DIAMETER; WELL DEPTH*
 146.0 5.128, 222.1
 THIRD BODY (COLLISION PARTNER)*
 AR
 THIRD BODY MASS; DIAMETER; WELL DEPTH; ENERGY TRANSFERRED*
 40.0, 3.54, 93.3, 500.
 ****COLLISION COEFFICIENT****
 0.
 ****CHANNEL 1: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)****
 1.2E+16 92.0,
 ****CHANNEL 2: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)****
 0.0, 0.0
 ****CHANNEL 3: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)****
 0.0, 0.0

							53
NUMBER OF TEMPERATURES	T1	T2	T3	T4	T5	T6 (K)	54
4,	1000.,	1300.,	1500,	1750.,			
							56
NUMBER OF PRESSURES	P1	P2	P3	P4	P5	P6 (TORR)	
6,	2.0,	10.,	100.,	1000.,	10000.,	100000.,	

Tout (FOR DISTRIBUTION $K(E,T)*K_i(E)$ vs. E AT THIS TEMP (K))
 1750.,

Pout
 760.,

OUTPUT OPTION (0,1,2,3)
 1,
 NOTE: CALCULATION/OUTPUT OPTION
 0 - GAMMA FUNCTION : SHORT OUTPUT
 1 - GAMMA FUNCTION : LONG OUTPUT
 2 - FACTORIAL : SHORT OUTPUT
 3 - FACTORIAL : LONG OUTPUT

TABLE IV.v

CYC6H5 DISSOCIATION

****DISSOCIATING SPECIES****

CYC6H5

****PRODUCT CHANNEL 1 (LOWEST ENERGY)****

LINC6H5

****PRODUCT CHANNEL 2 ****

****PRODUCT CHANNEL 3 ****

GEOMETRIC MEAN FREQUENCY; # OF OSCILLATORS (S)*

1104.25, 27

COLLISION COMPLEX MASS; DIAMETER; WELL DEPTH*

77.0, 5.349, 412.30

THIRD BODY (COLLISION PARTNER)*

AR

THIRD BODY MASS; DIAMETER; WELL DEPTH; ENERGY TRANSFERRED*

40.0, 3.54, 93.3, 630.

COLLISION COEFFICIENT*

0.028

CHANNEL 1: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)*

1.3E+15, 81.3,

CHANNEL 2: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)*

0.0, 0.0

CHANNEL 3: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)*

0.0, 0.0

								53
NUMBER OF TEMPERATURES	T1	T2	T3	T4	T5	T6 (K)		54
4,	1600.,	1700.,	1800.,	1900.,	.,	55		56
NUMBER OF PRESSURES	P1	P2	P3	P4	P5	P6 (TORR)		57
6,	10.,	31.62,	100.,	316.23,	1000.,	10000.,		58
								59
Tout (FOR DISTRIBUTION K(E,T)*Ki(E) vs. E AT THIS TEMP (K))								60
1700.,								61
								62
Pout								63
760.,								64
								65
OUTPUT OPTION (0,1,2,3)								66
1,								

NOTE: CALCULATION/OUTPUT OPTION

0 - GAMMA FUNCTION : SHORT OUTPUT

1 - GAMMA FUNCTION : LONG OUTPUT

2 - FACTORIAL : SHORT OUTPUT

3 - FACTORIAL : LONG OUTPUT

TABLE IV.vi

CYC6H6 DISSOCIATION

****DISSOCIATING SPECIES****

CYC6H6

****PRODUCT CHANNEL 1 {LOWEST ENERGY}****

CYC6H5 + H

****PRODUCT CHANNEL 2 ****

****PRODUCT CHANNEL 3 ****

GEOMETRIC MEAN FREQUENCY; # OF OSCILLATORS (S)*

1205.8, 30

COLLISION COMPLEX MASS; DIAMETER; WELL DEPTH*

78.0, 5.349, 412.30

THIRD BODY (COLLISION PARTNER)*

AR

THIRD BODY MASS; DIAMETER; WELL DEPTH; ENERGY TRANSFERRED*

40.0, 3.54, 93.3, 630.0

****COLLISION COEFFICIENT****

0.0

****CHANNEL 1: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)****

1.3E+16, 113.6,

****CHANNEL 2: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)****

0.0, 0.0

****CHANNEL 3: HIGH PRESSURE A FACTOR; EA(KCAL/MOL)****

0.0, 0.0

							53
NUMBER OF TEMPERATURES	T1	T2	T3	T4	T5	T6 (K)	54
4,	1600.,	1700.,	1800.,	1900.,	.,	55	56
NUMBER OF PRESSURES	P1	P2	P3	P4	P5	P6 (TORR)	57
6,	10.,	31.62,	100.,	316.23,	1000.,	10000.,	58
							59
Tout (FOR DISTRIBUTION $K(E,T)*K_i(E)$ vs. E AT THIS TEMP (K))							60
1700.,							61
							62
Pout							63
760.,							64
							65
OUTPUT OPTION (0,1,2,3)							66
0,							

NOTE: CALCULATION/OUTPUT OPTION

- 0 - GAMMA FUNCTION : SHORT OUTPUT
- 1 - GAMMA FUNCTION : LONG OUTPUT
- 2 - FACTORIAL : SHORT OUTPUT
- 3 - FACTORIAL : LONG OUTPUT

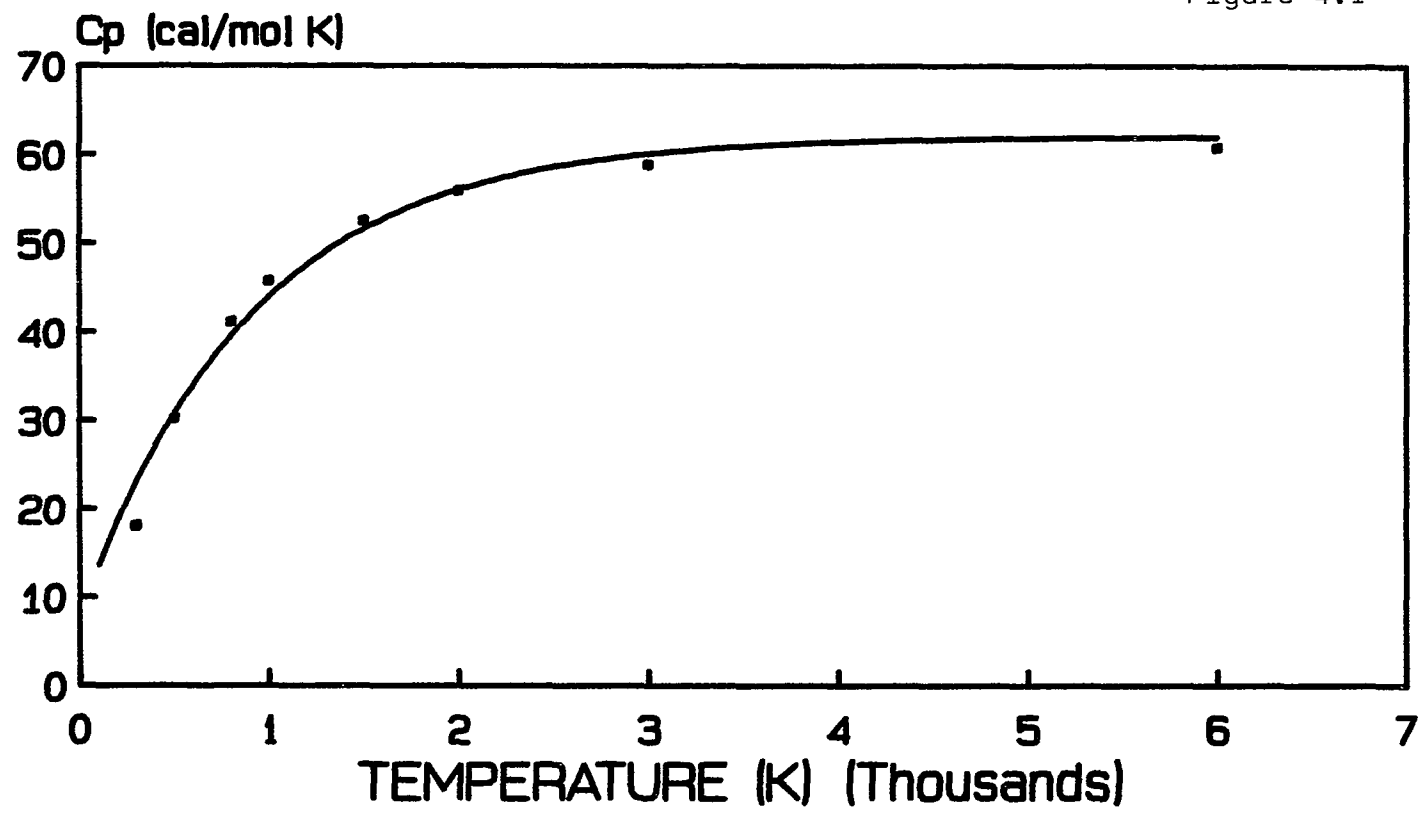
APPENDIX IV - B

FIGURES FOR SECTION IV

CYPD: Cp FIT vs. T

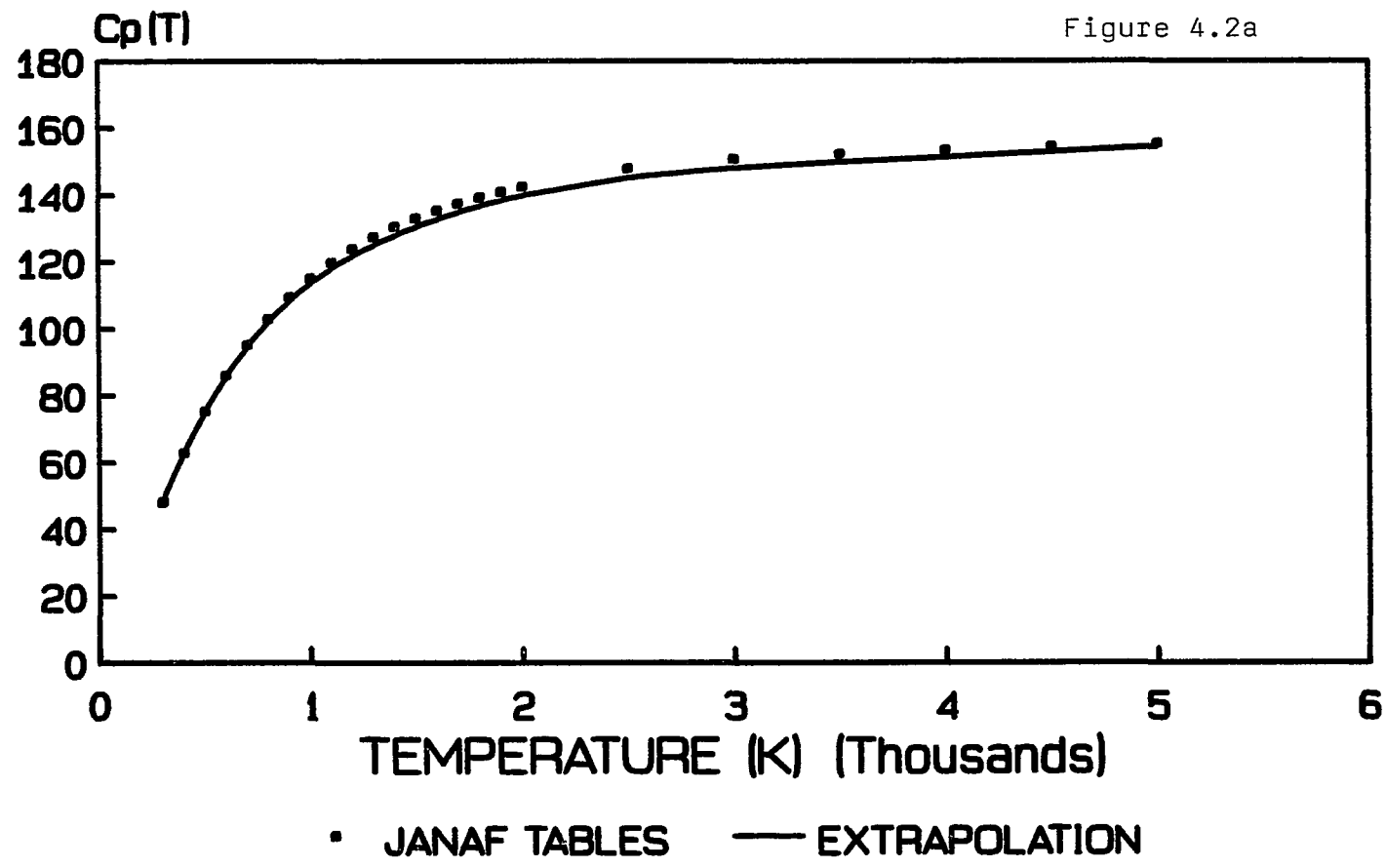
$C_p = C_{p\text{inf}} (1 - \text{EXP}(-B_1 * T))$ vs. LITERATURE

Figure 4.1



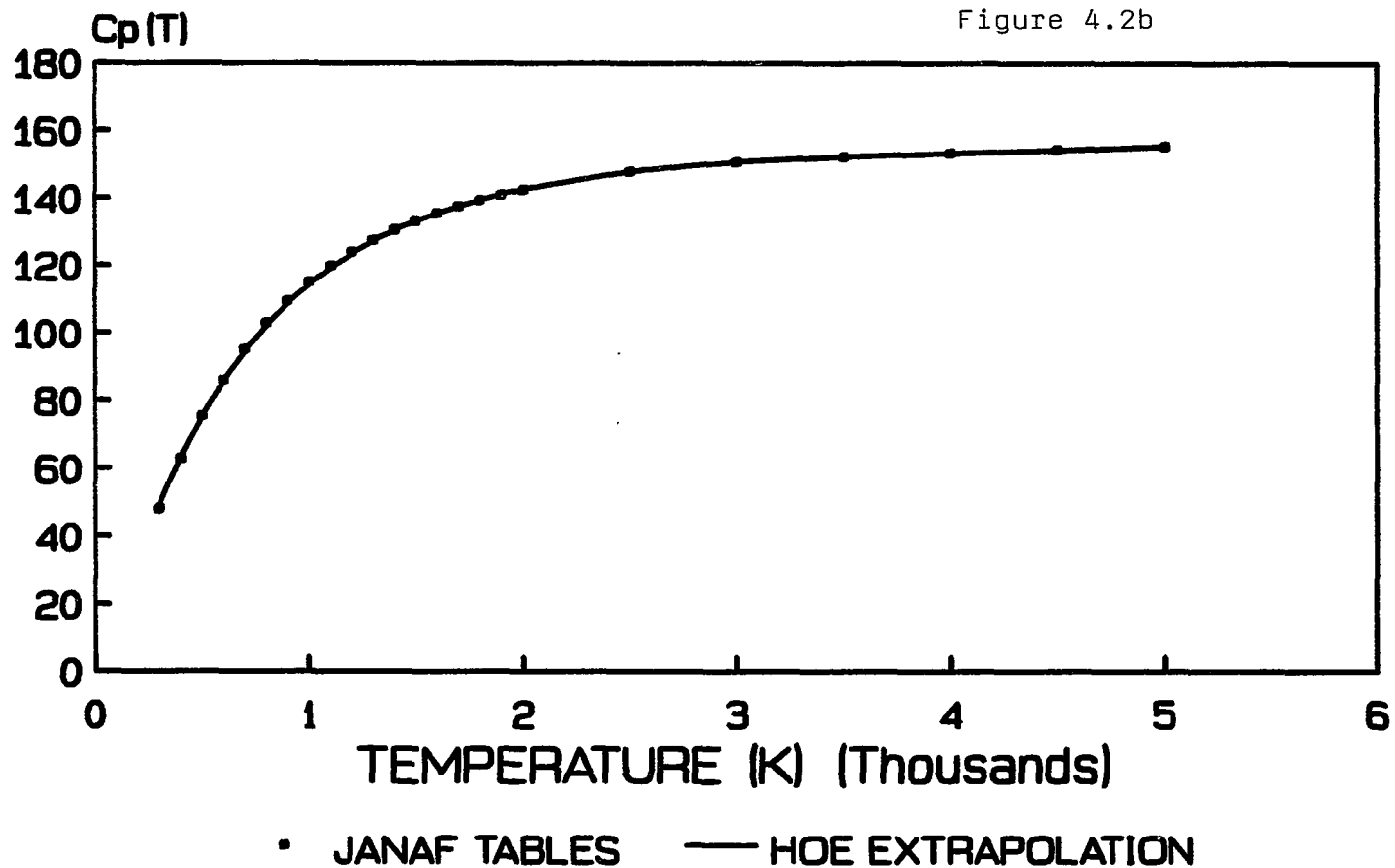
ETHYLENE OXIDE $C_p(T)$ FIT WITH EXPONENTIAL MODEL

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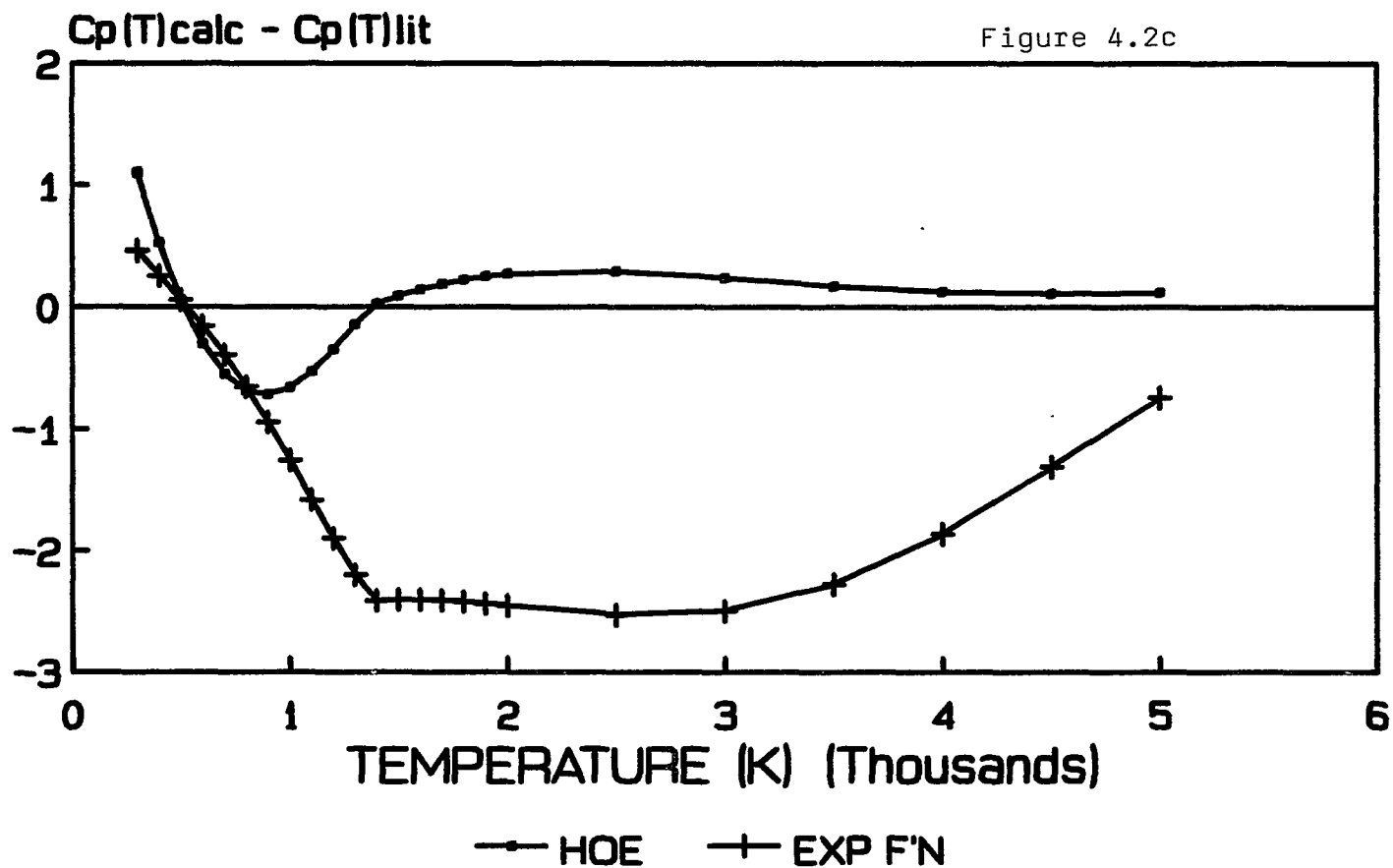


ETHYLENE OXIDE $C_p(T)$ FIT WITH HOE MODEL & THERM DATA

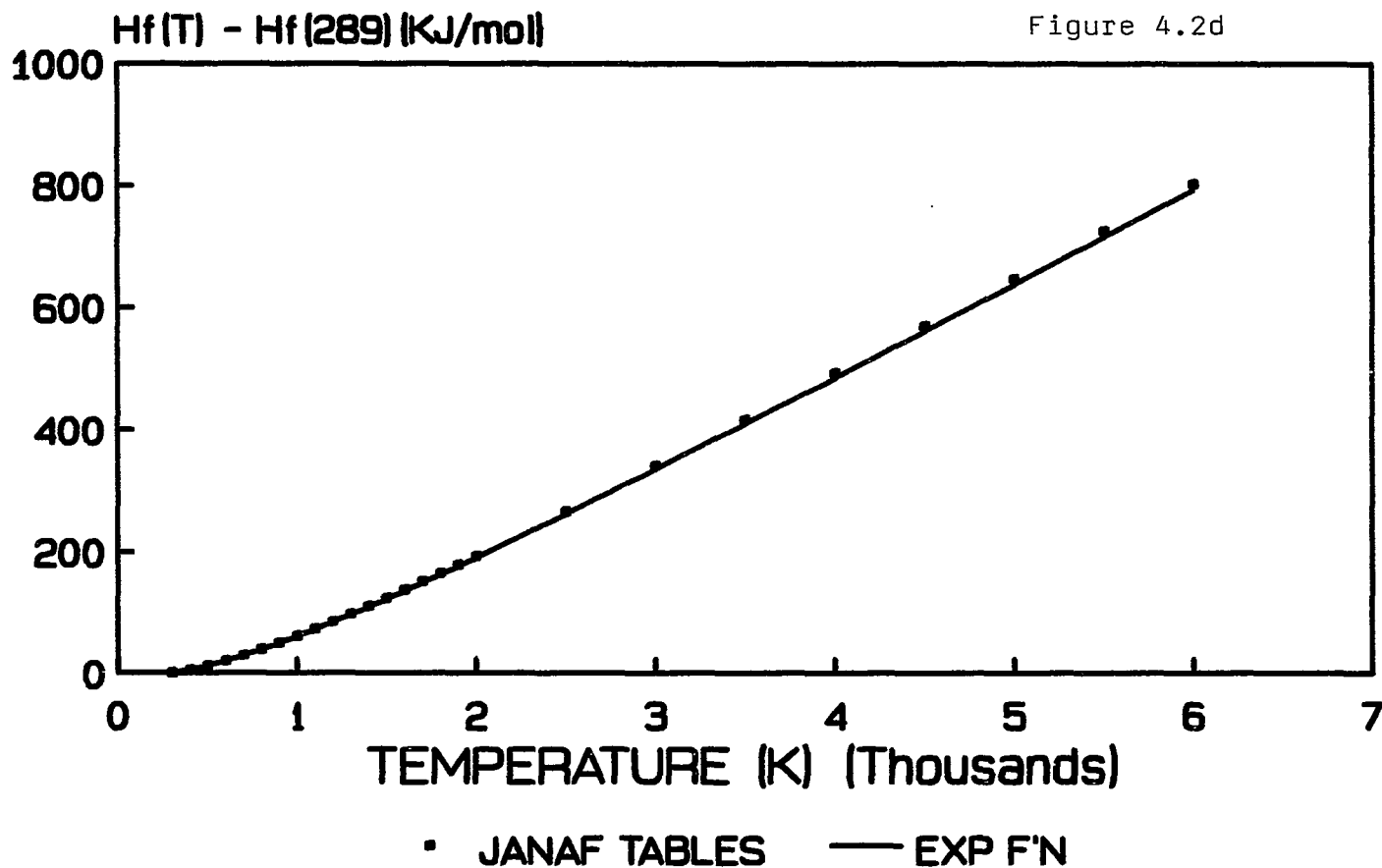
Figure 4.2b



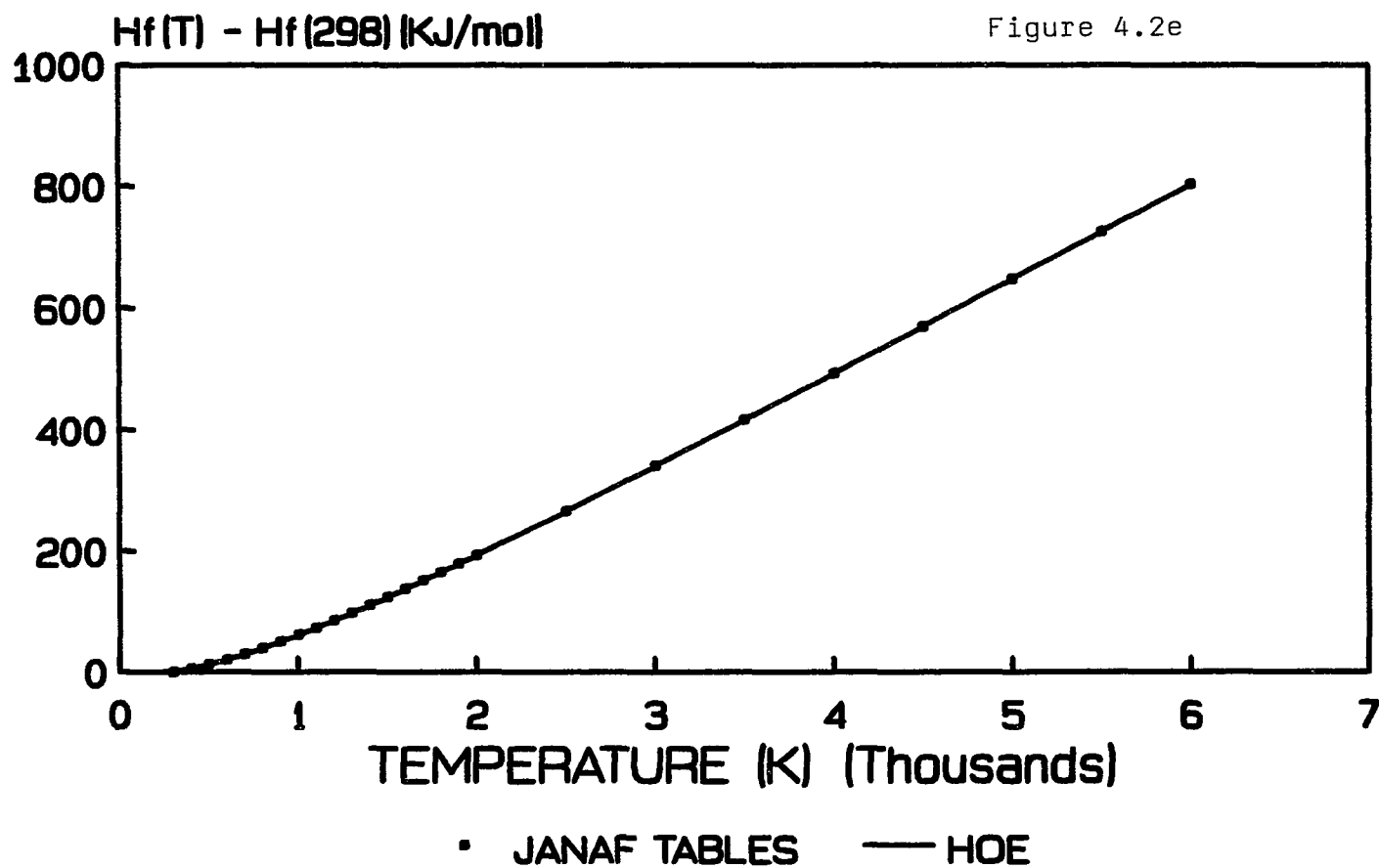
ETHYLENE OXIDE $C_p(T)$:RESIDUALS RESIDUALS FOR FIT OF HOE AND EXP MODELS



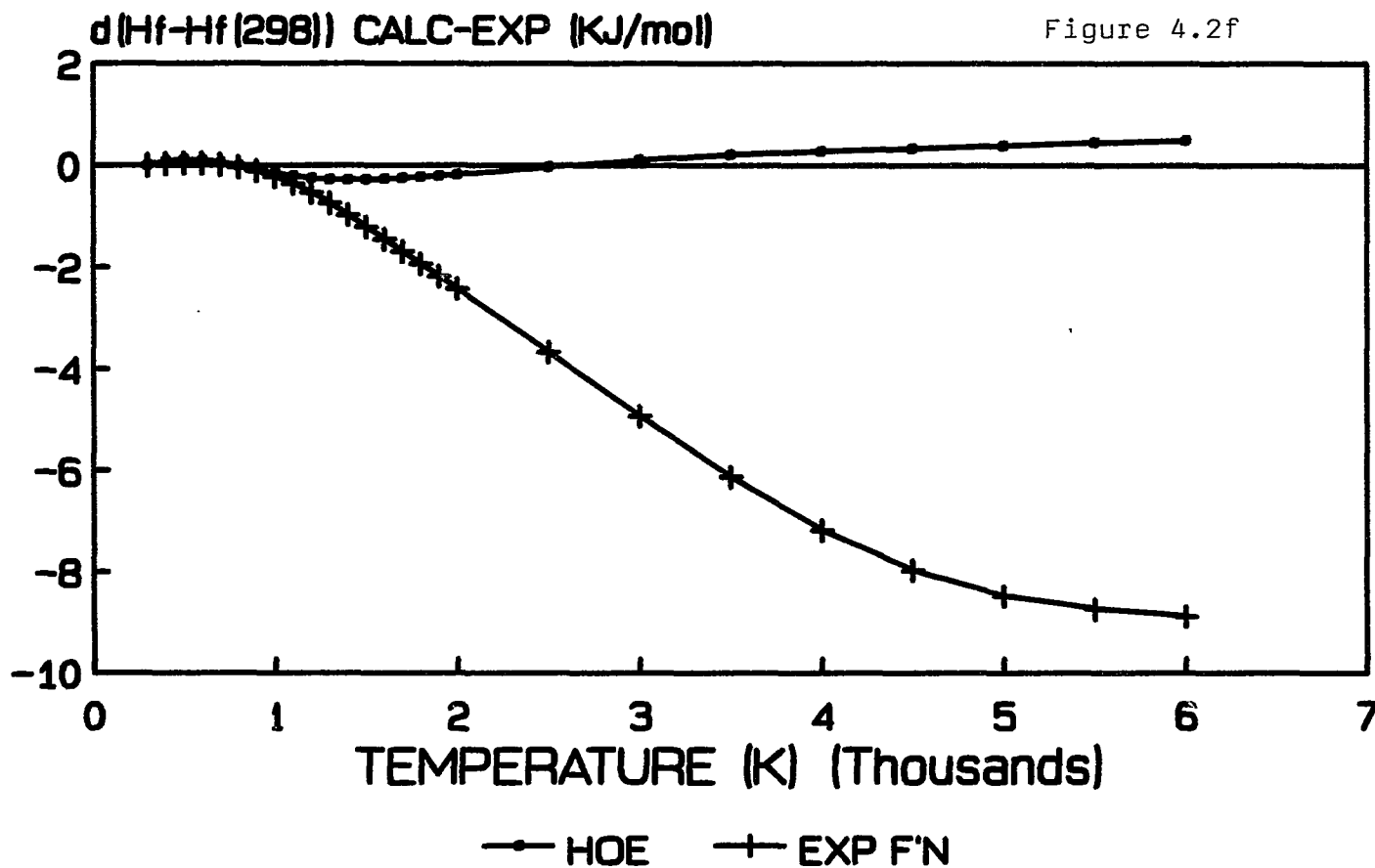
ETHYLENE OXIDE: $H_f(T) - H_f(298K)$ FIT FOR EXPONENTIAL EXTRAPOLATION: THER



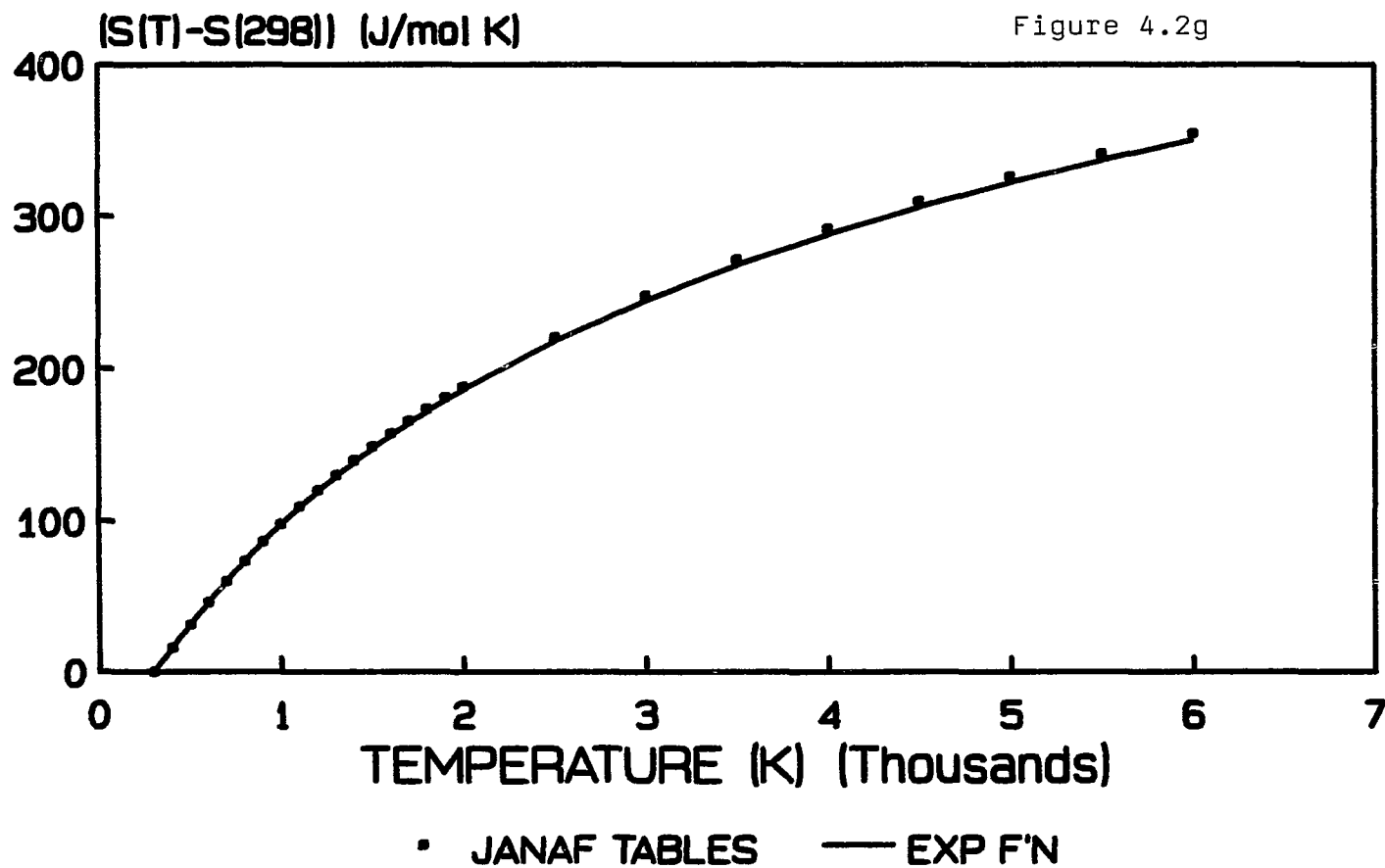
ETHYLENE OXIDE: $H_f(T) - H_f(298K)$ FIT FOR HOE EXTRAPOLATION: THERM



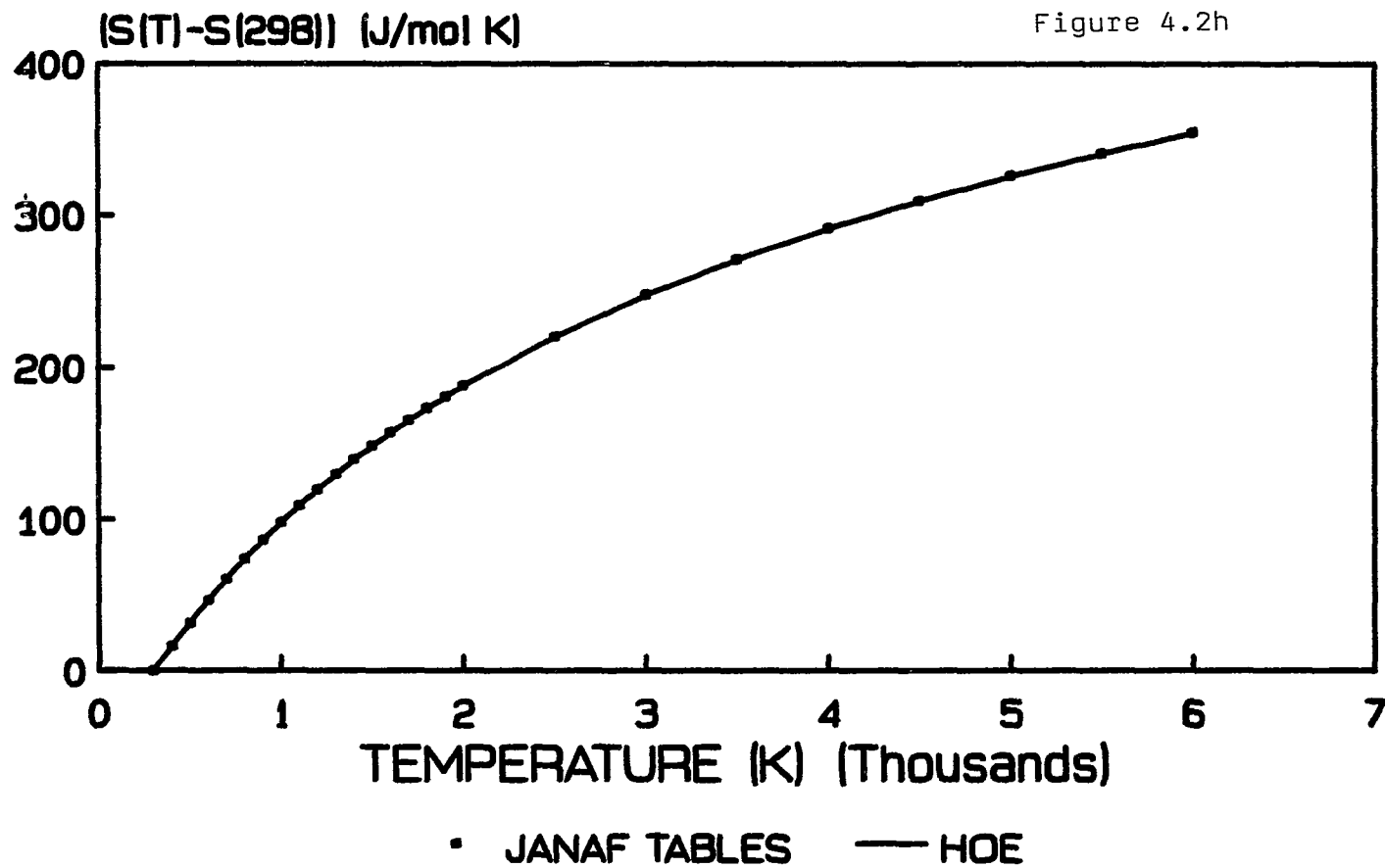
ETHYLENE OXIDE: $H_f(T) - H_f(298K)$ RESIDUALS FOR HOE AND EXP F'N MODELS



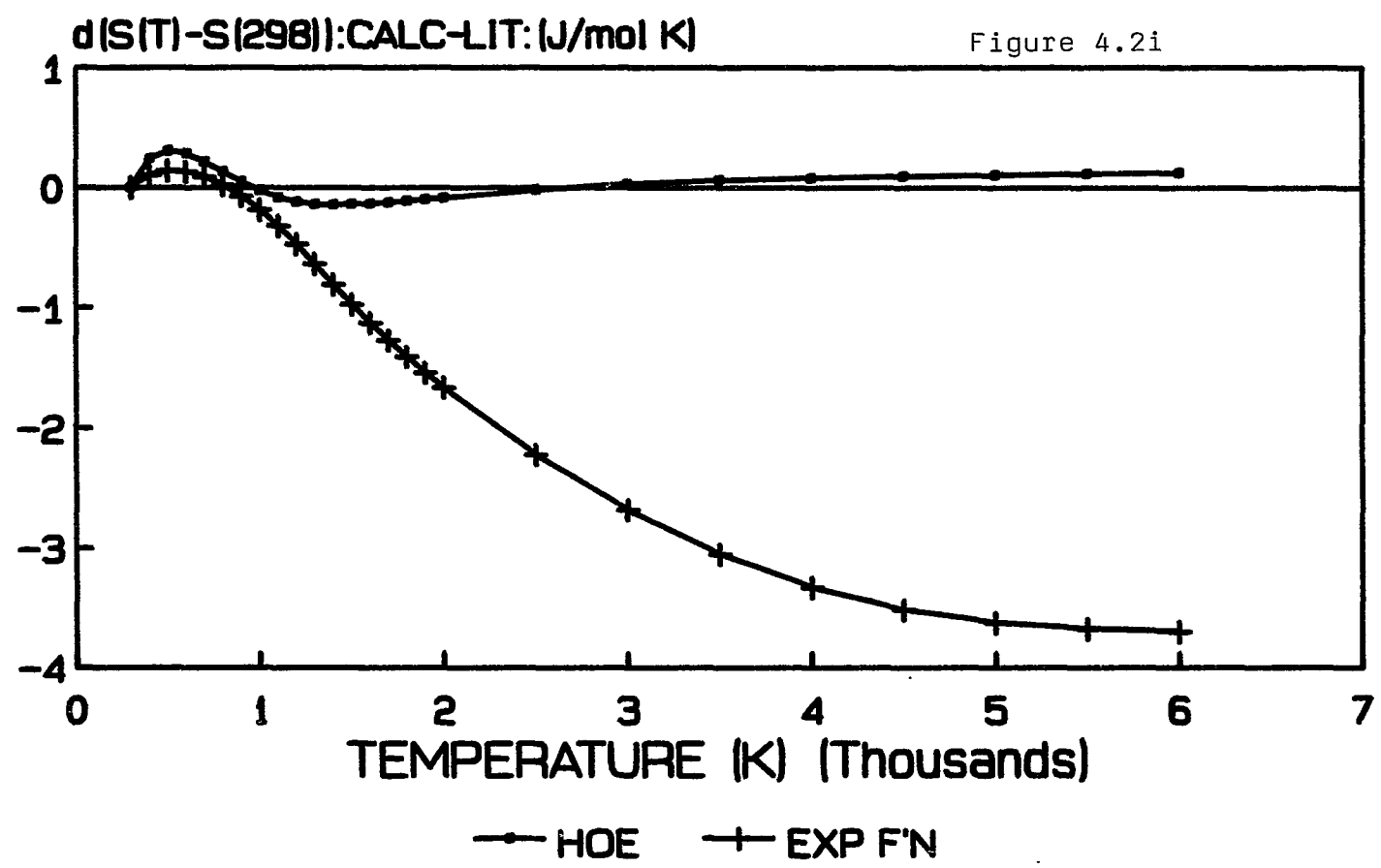
ETHYLENE OXIDE: $S(T) - S(298K)$ ENTROPY FUNCTION: EXP F'N MODEL



ETHYLENE OXIDE: $S(T) - S(298K)$ ENTROPY FUNCTION: HOE MODEL



ETHYLENE OXIDE: S(T)-S(298K) RESIDUALS ENTROPY FUNCTION

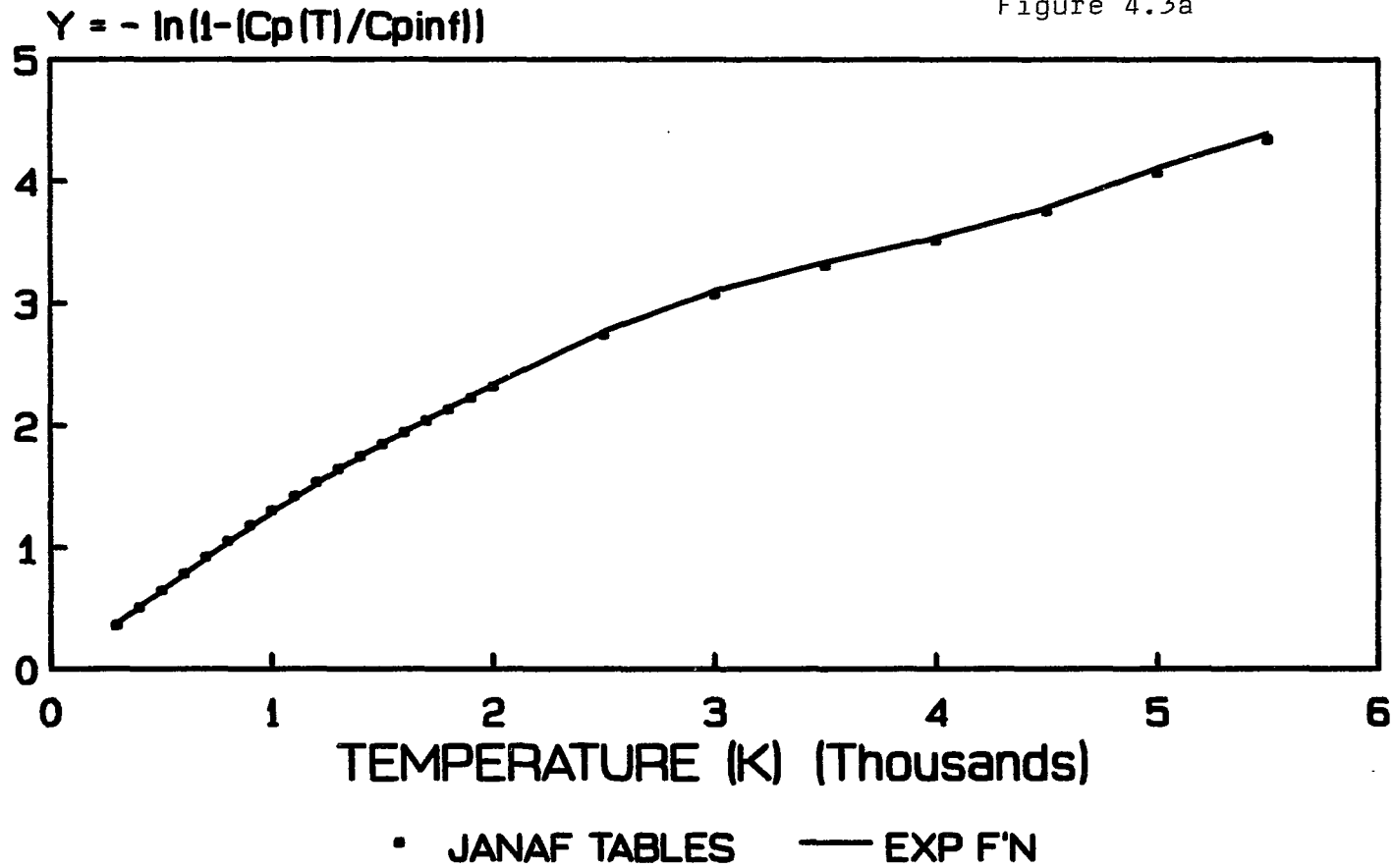


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ETHYLENE OXIDE: Cp EXP F'N

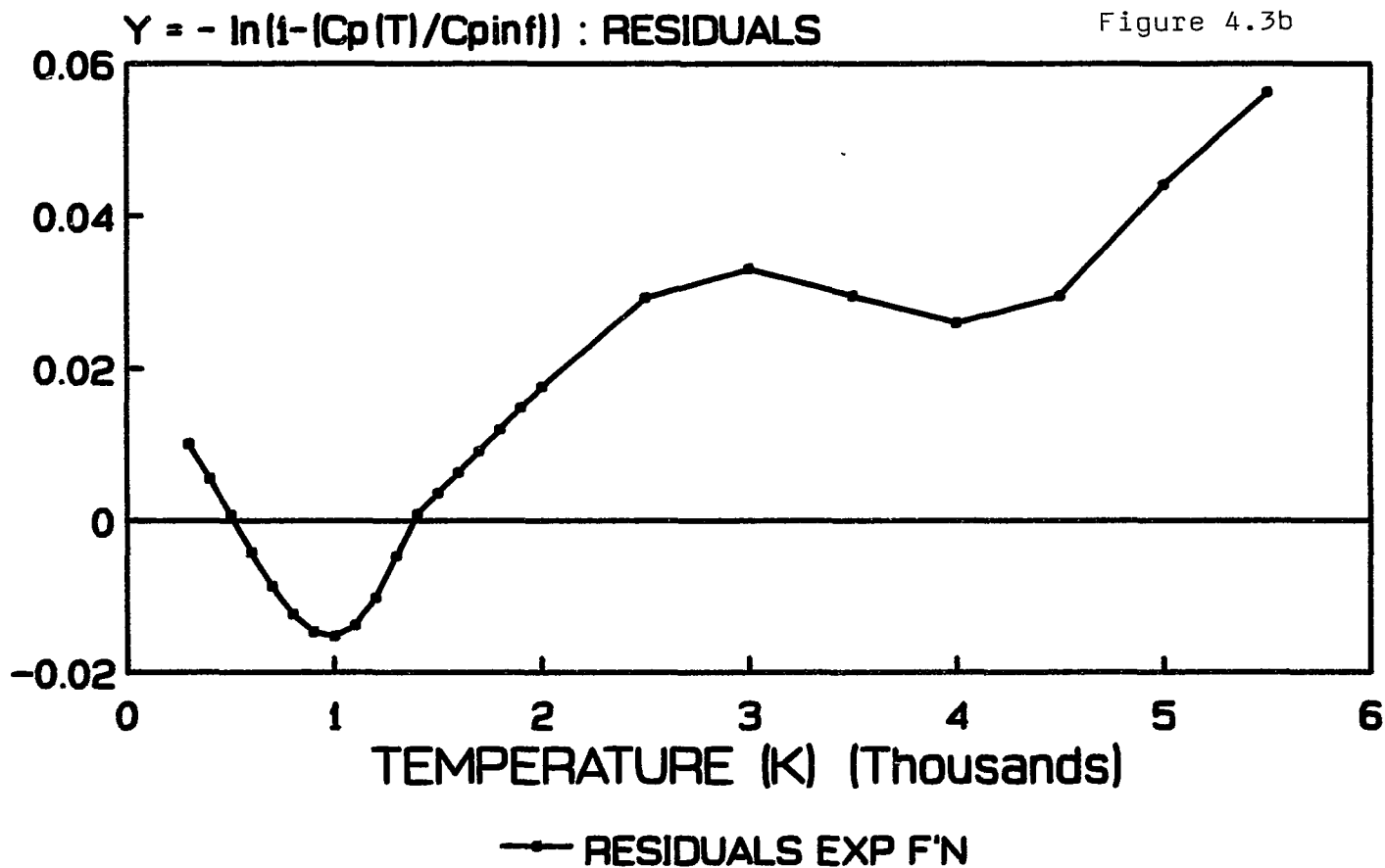
$$Y = -\ln(1 - C_p/C_{pinf}) = A + BT$$

Figure 4.3a

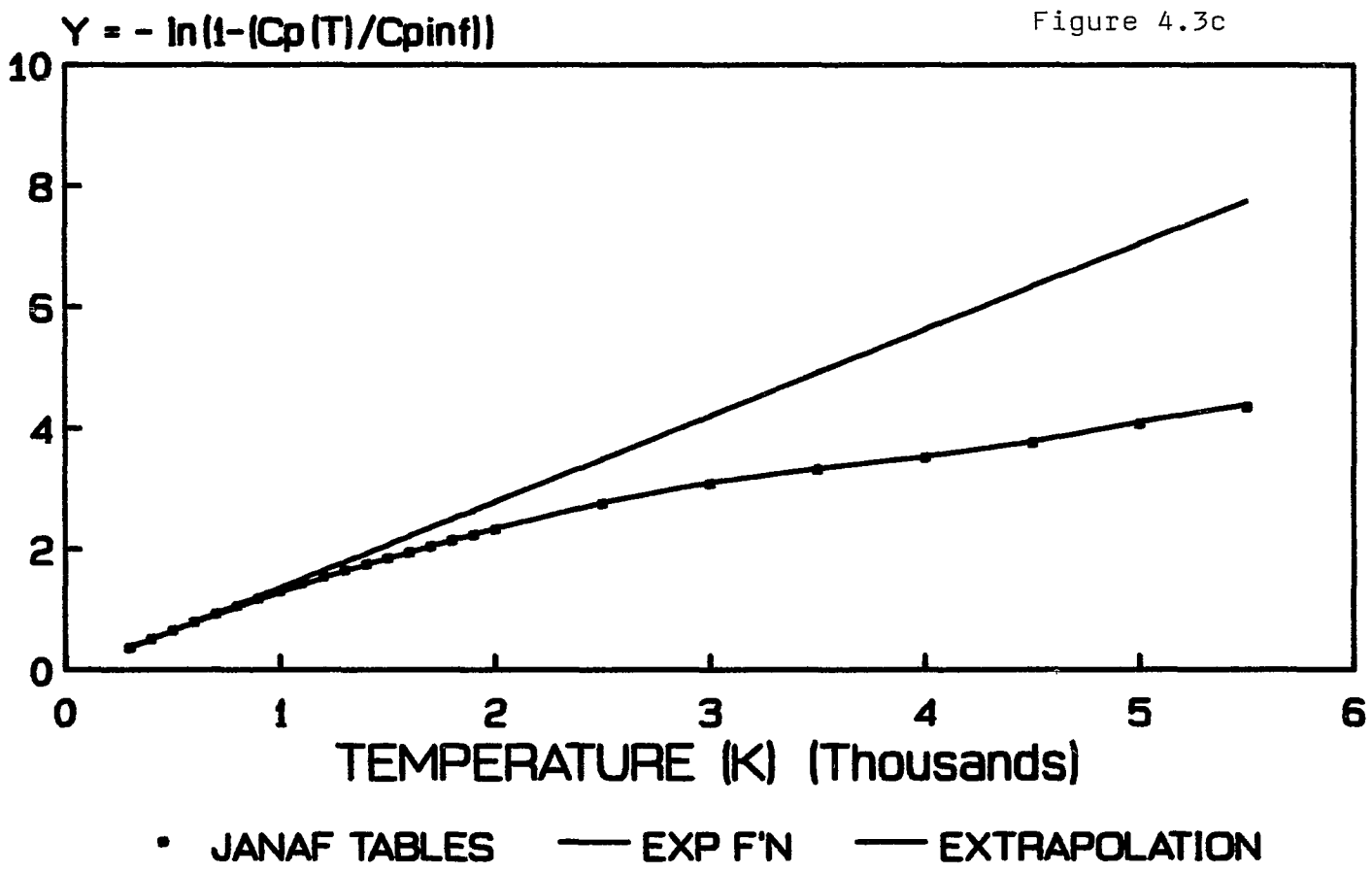


ETHYLENE OXIDE: Cp EXP F'N
Y = $-\ln(1 - C_p/C_{pinf}) = A + BT$: RESIDUALS

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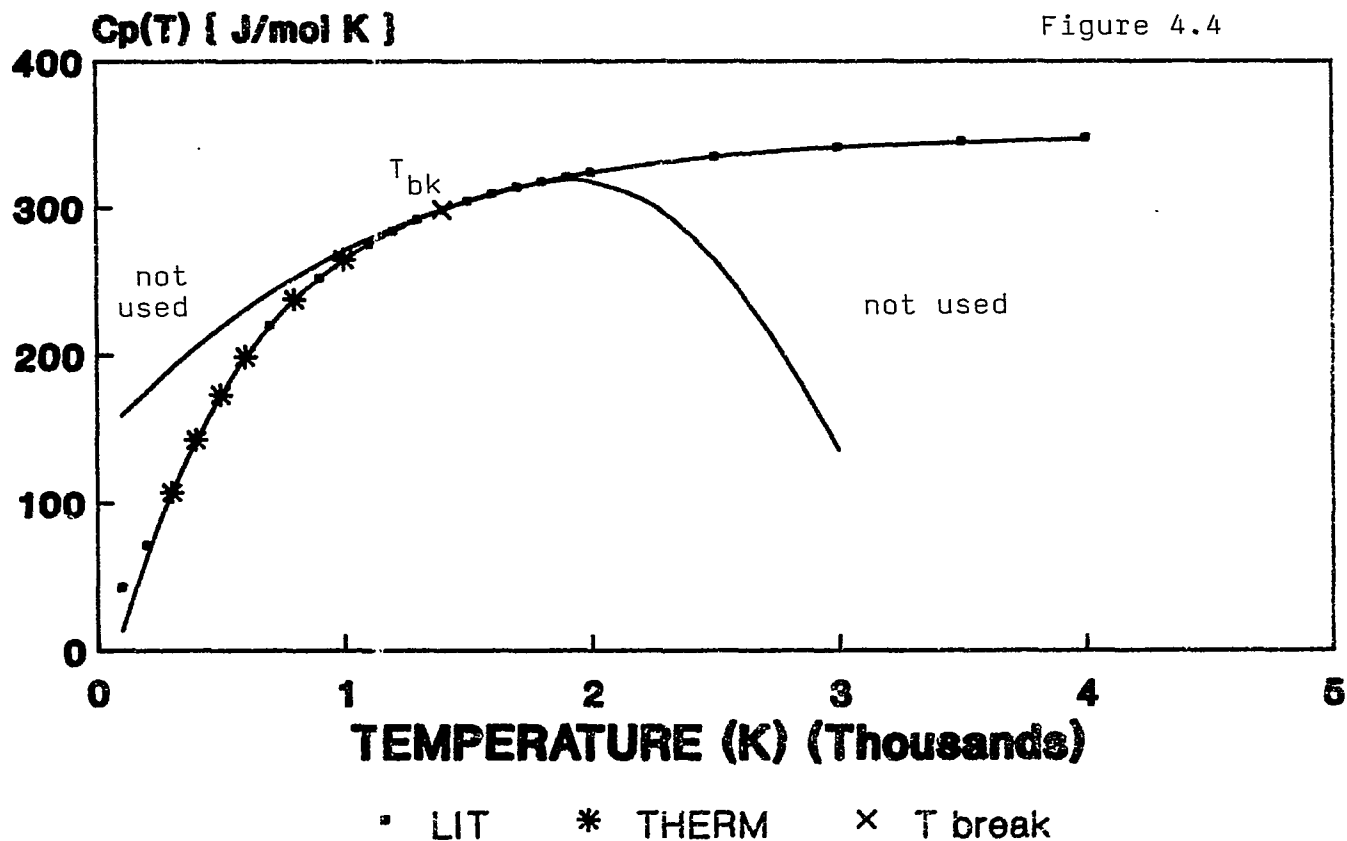


ETHYLENE OXIDE: Cp EXP F'N

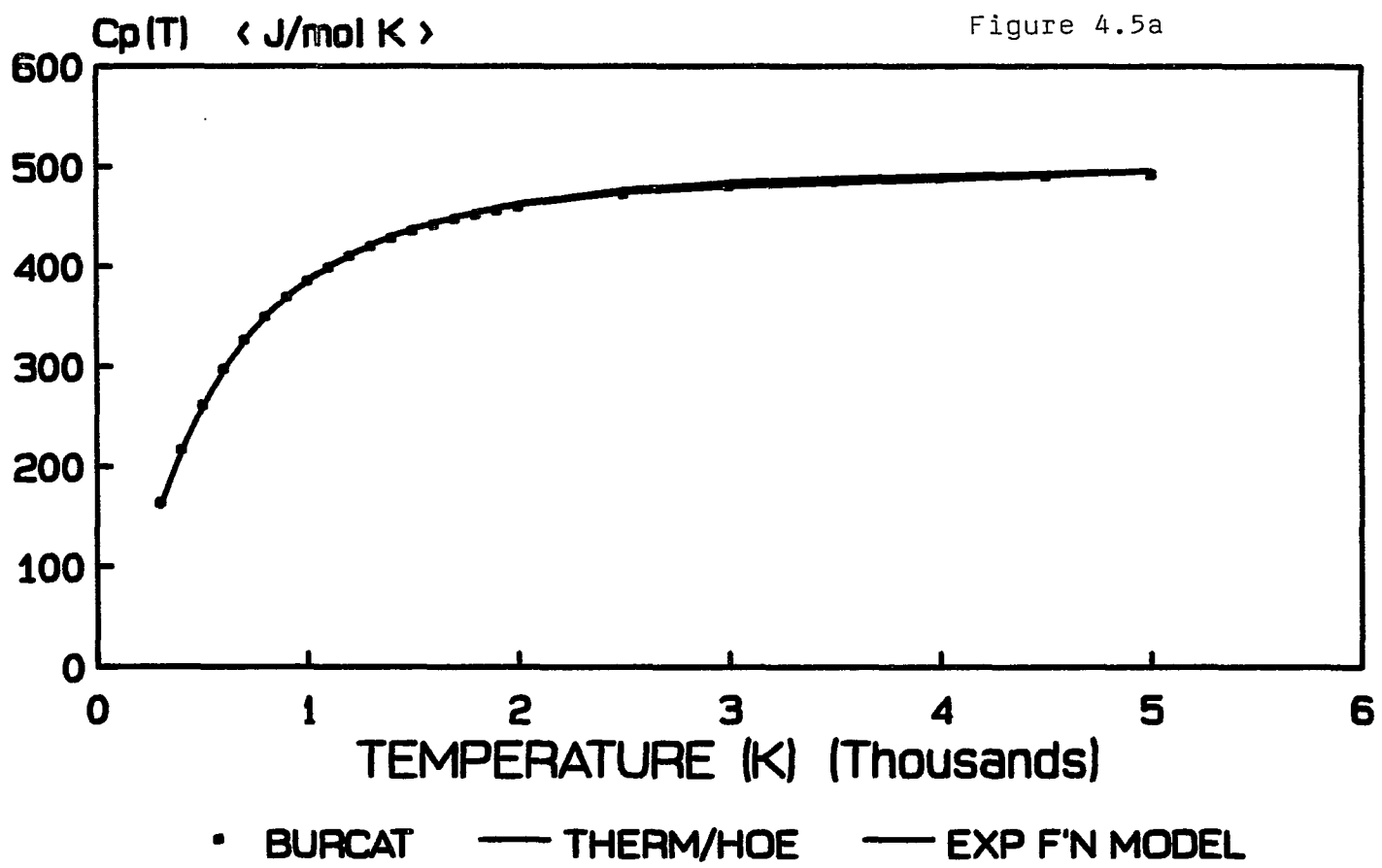
$$Y = -\ln(1 - C_p / C_{p\infty}) = A + BT$$


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CYCLOHEPTATRIENE : Cp(T) polynomials low and high Temp polynomials



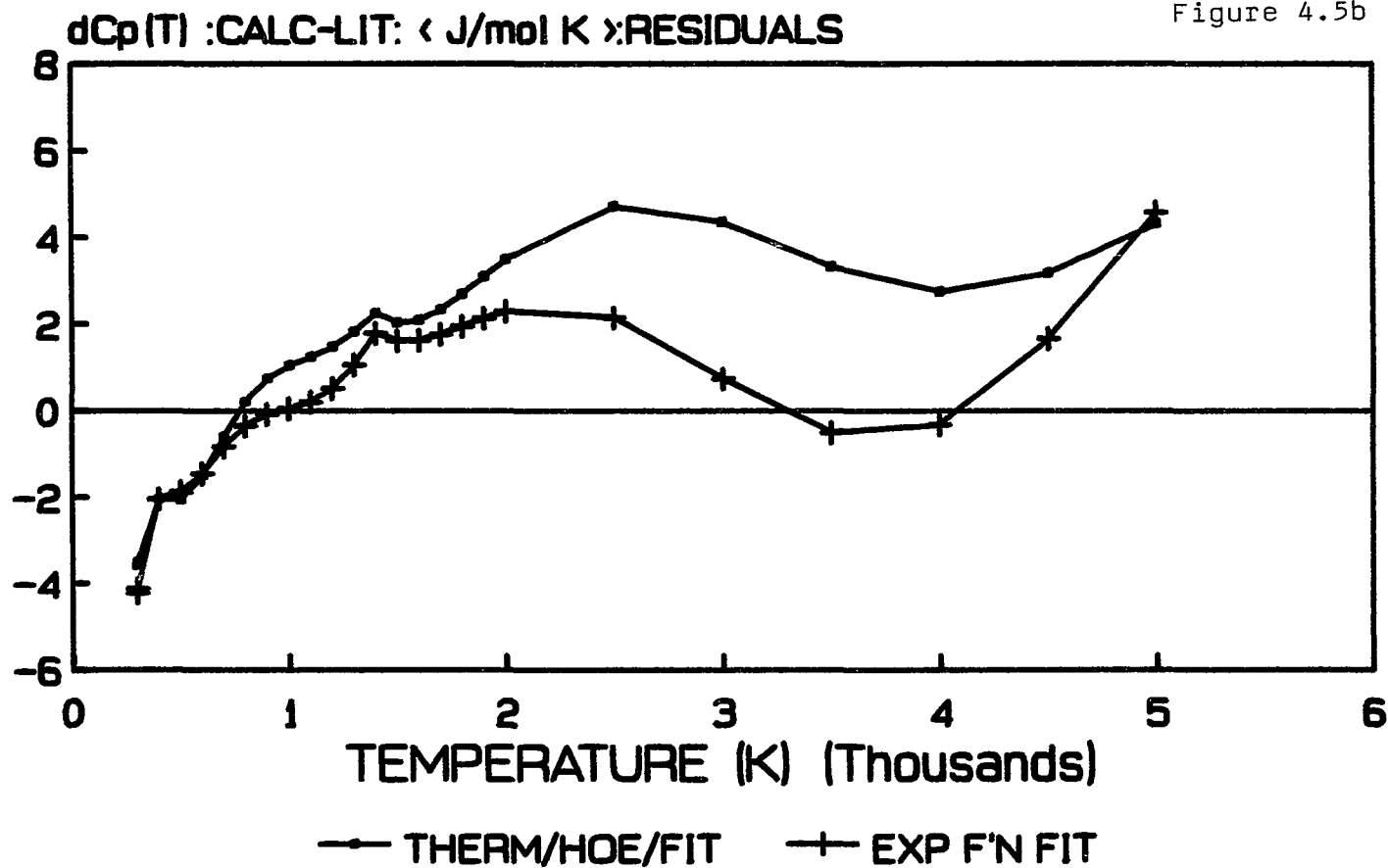
BIPHENYL RADICAL $C_p(T)$: EXP MODEL THERM DATA vs. BURCAT



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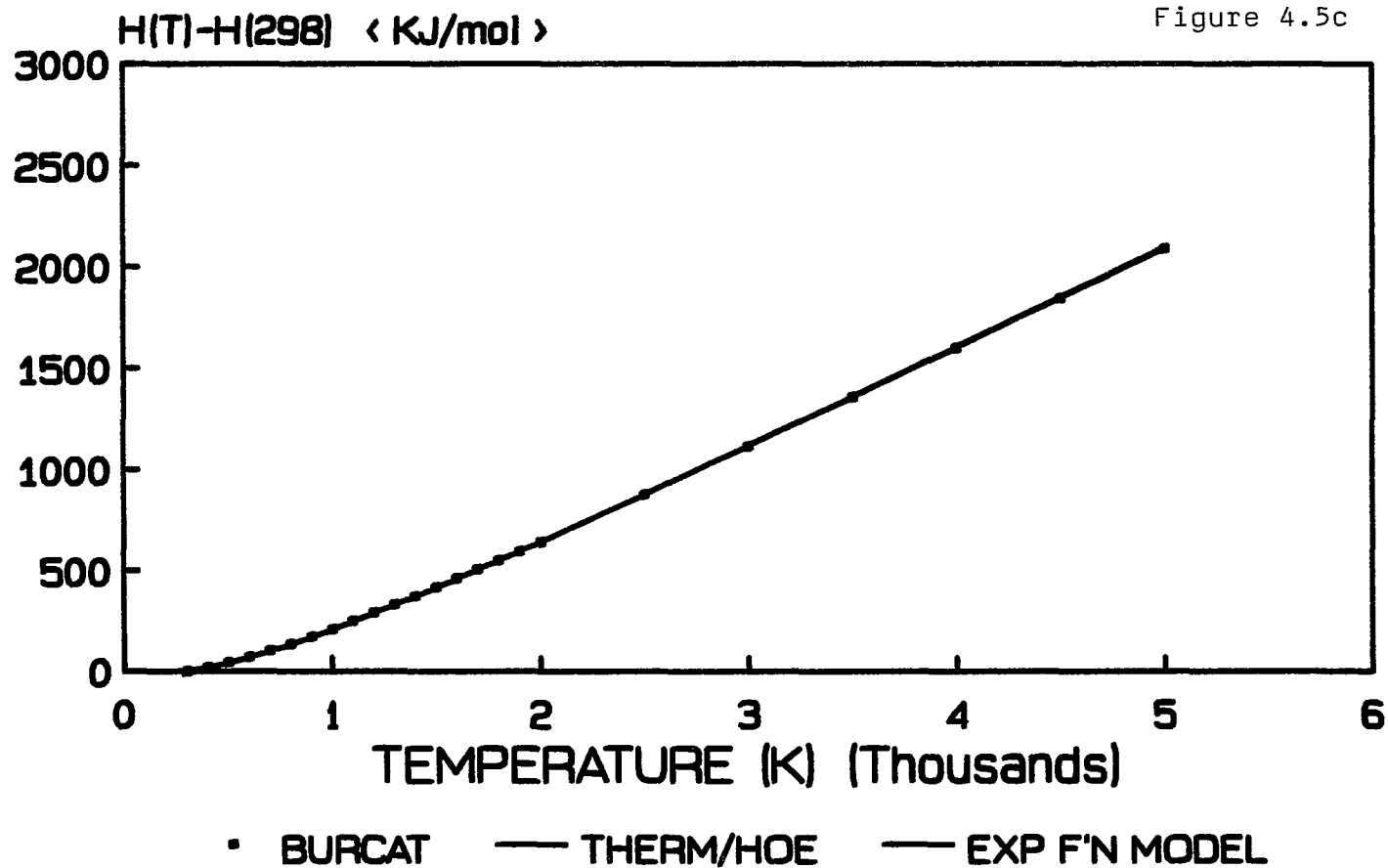
BIPHENYL RADICAL $C_p(T)$: RESIDUALS THERM DATA vs. BURCAT

Figure 4.5b



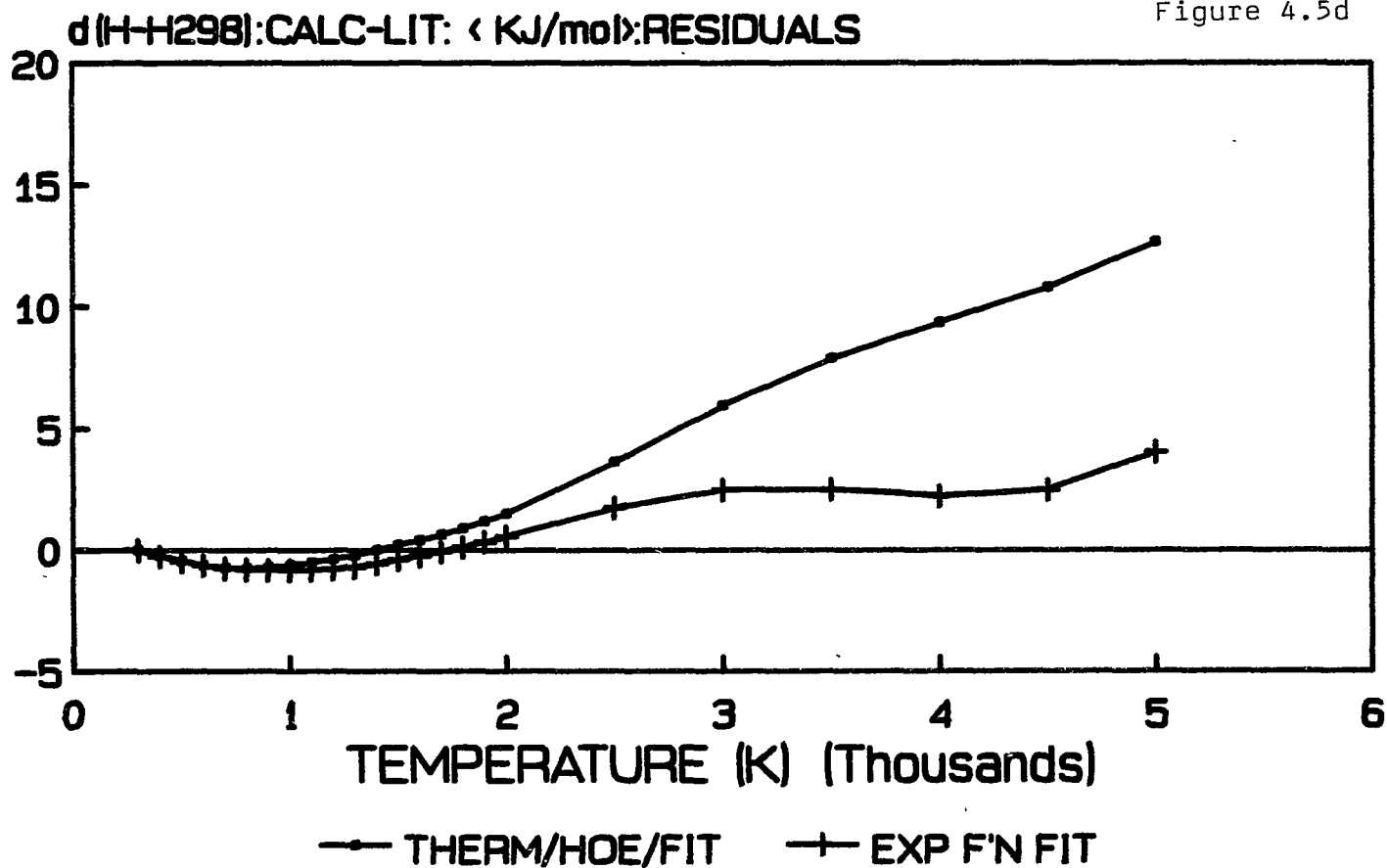
BIPHENYL RADICAL: H-H298: EXP MODEL THERM DATA vs. BURCAT

Figure 4.5c



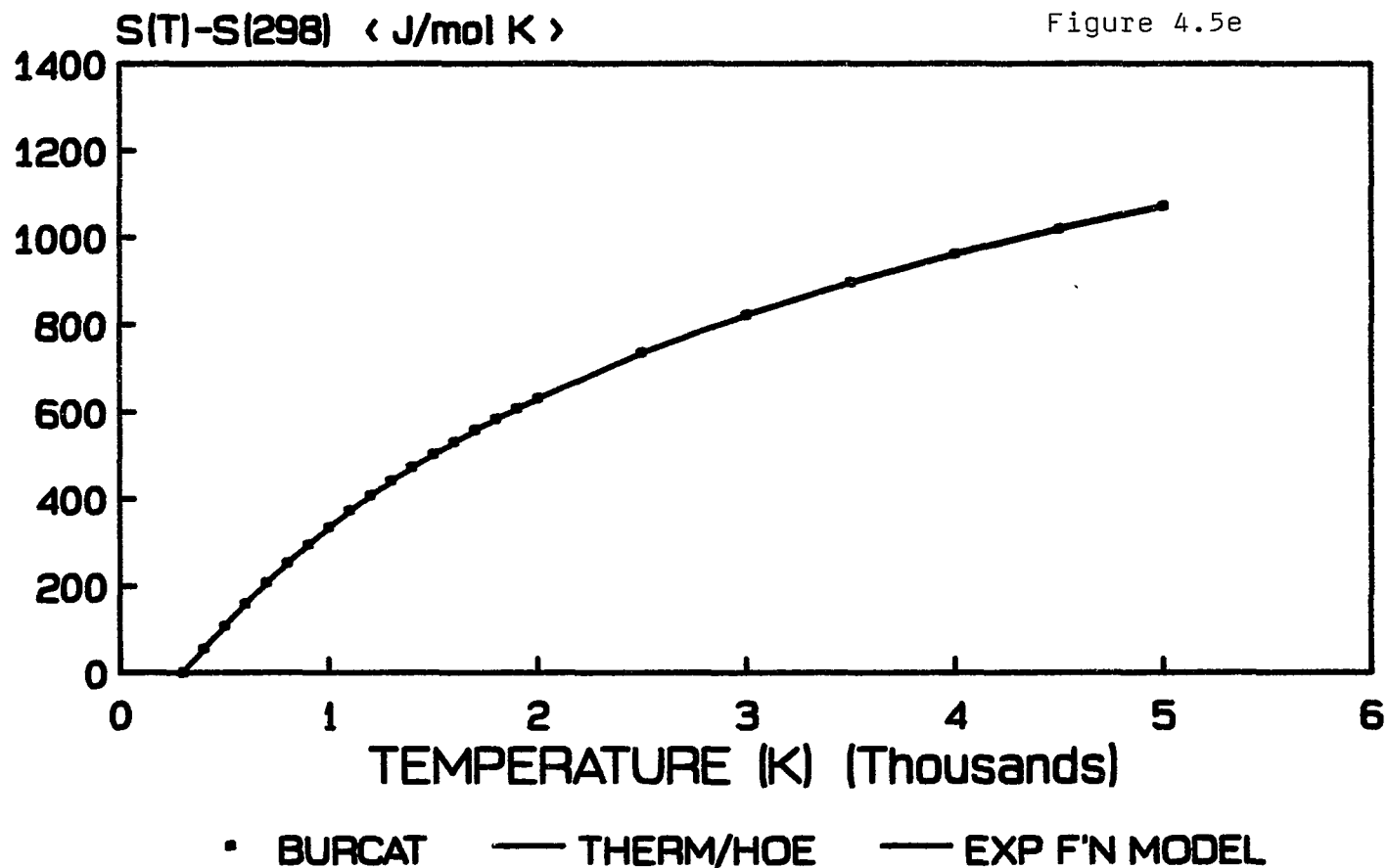
BIPHENYL RADICAL: H-H298: RESIDUALS THERM DATA vs. BURCAT

Figure 4.5d

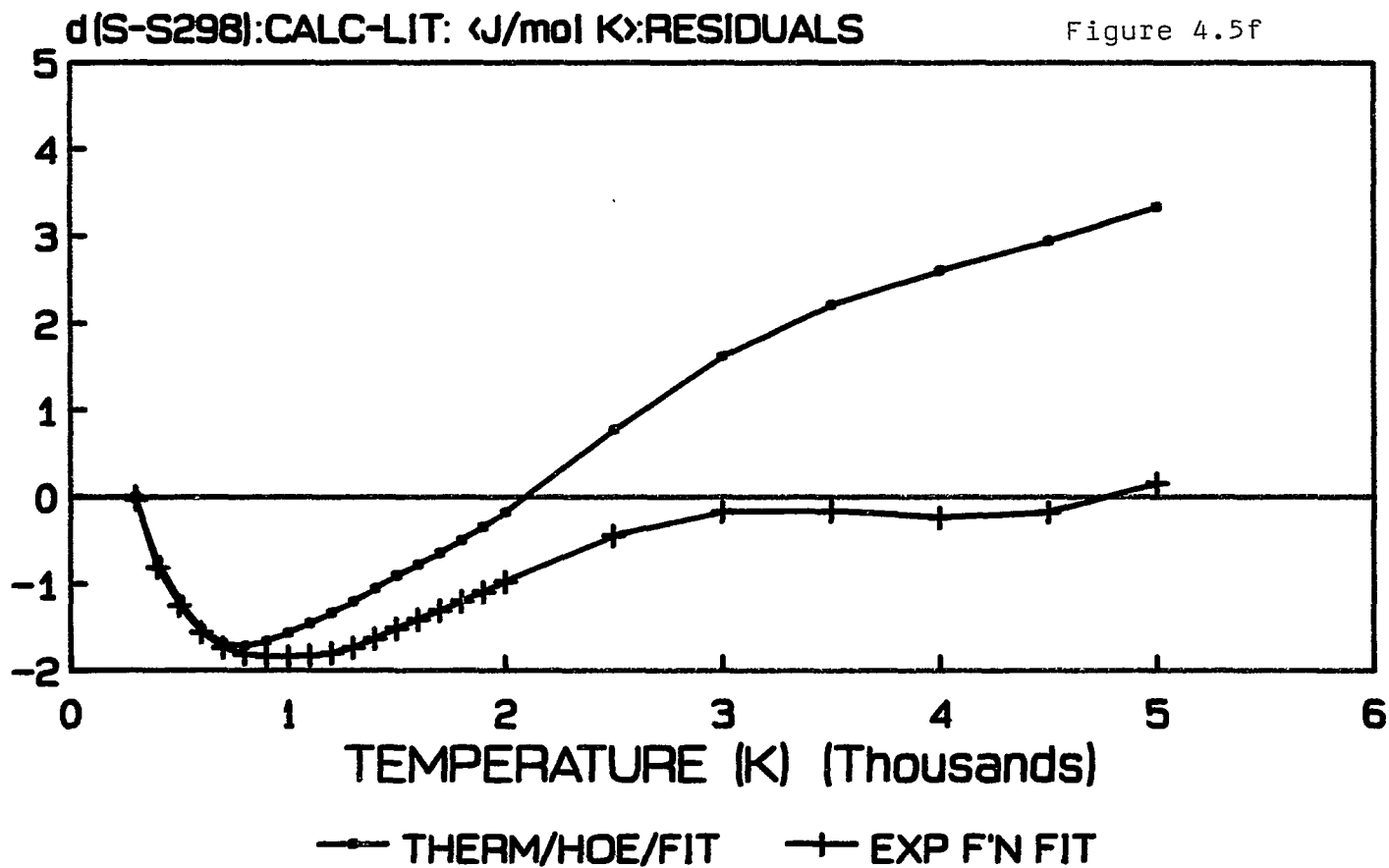


BIPHENYL RADICAL: S-S298: EXP MODEL THERM DATA vs. BURCAT

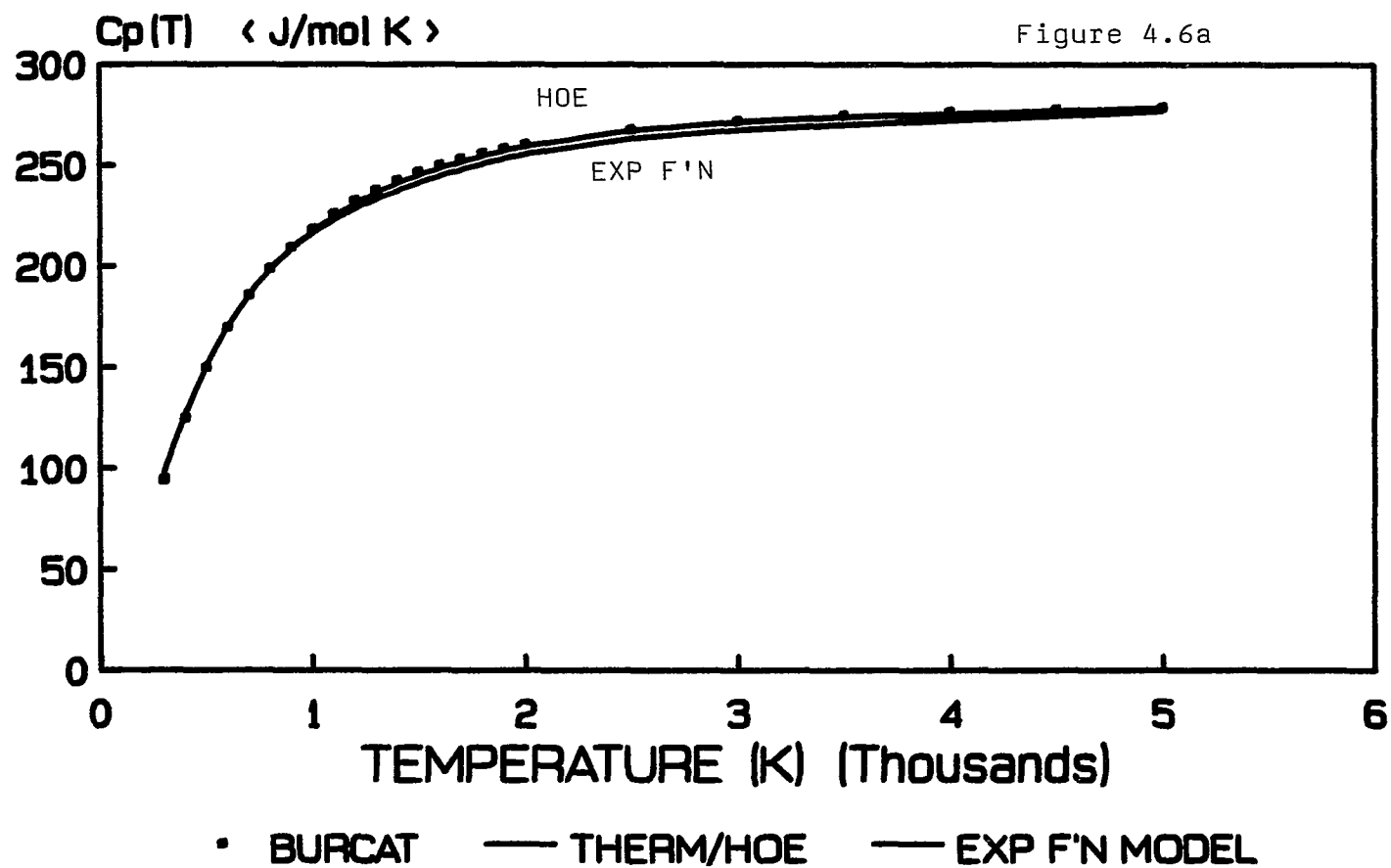
Figure 4.5e



BIPHENYL RADICAL: S-S298: RESIDUALS THERM DATA vs. BURCAT

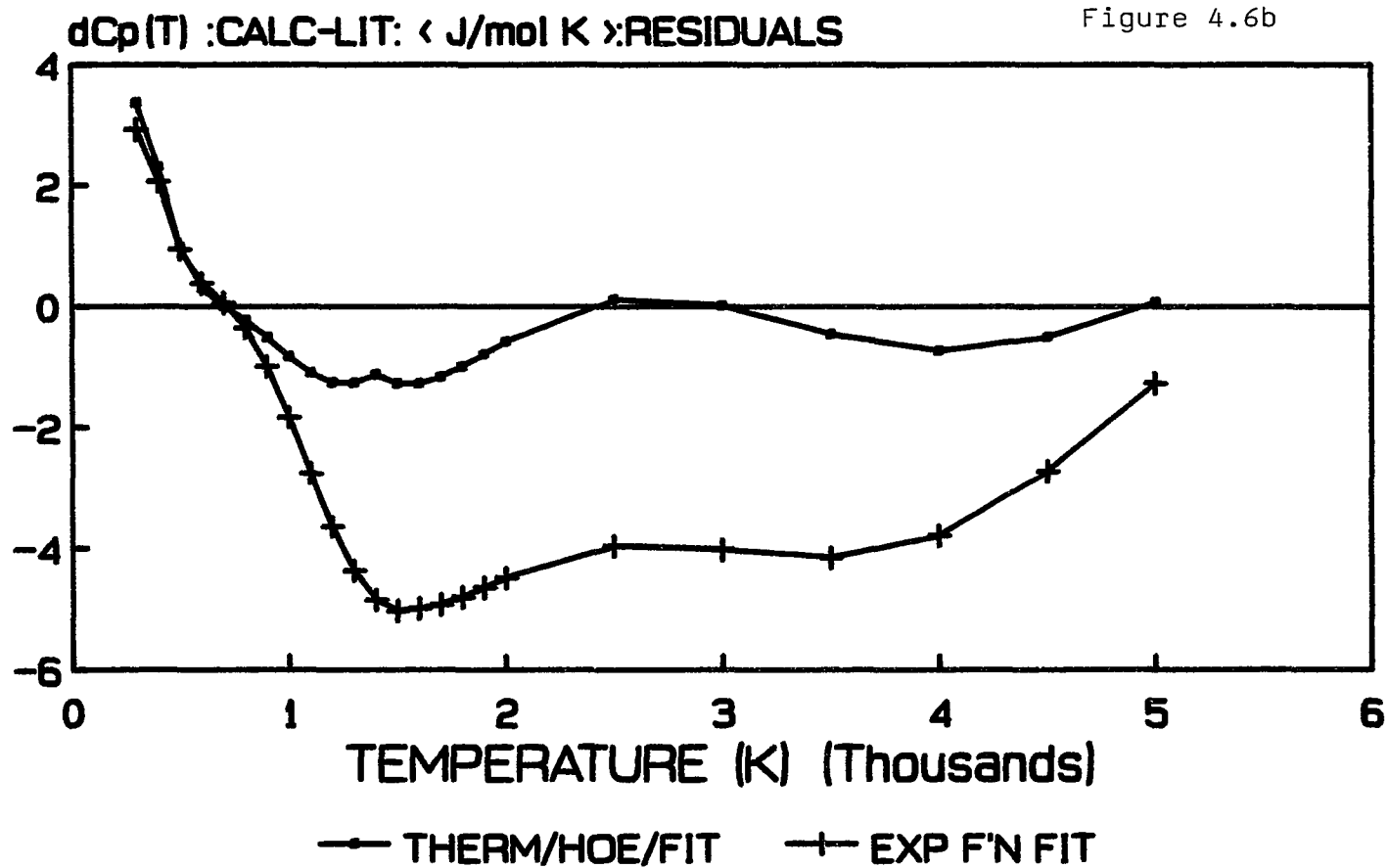


PHENOXY RADICAL $C_p(T)$: EXP MODEL THERM DATA vs. BURCAT



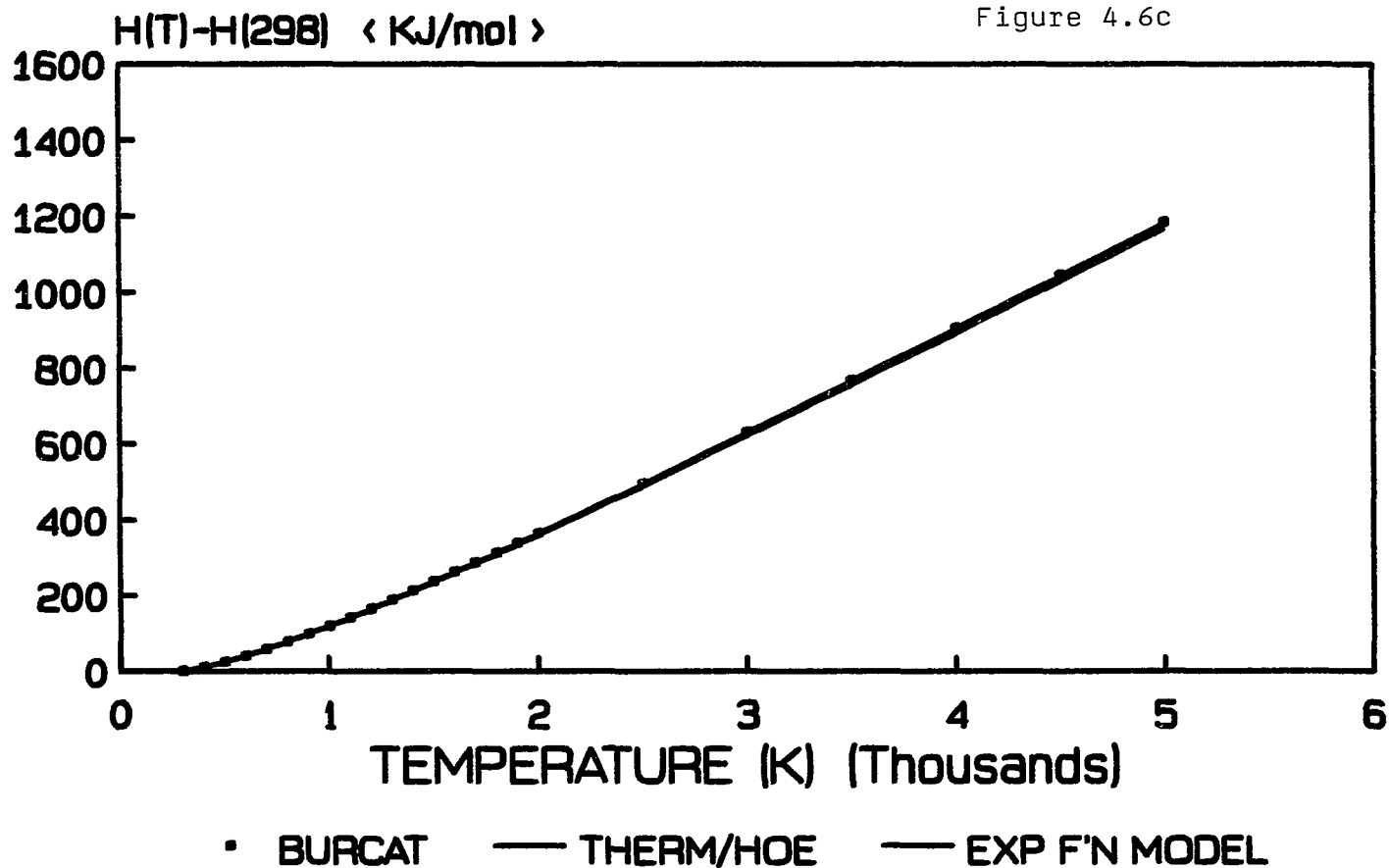
PHENOXY RADICAL $C_p(T)$: RESIDUALS THERM DATA vs. BURCAT

Figure 4.6b

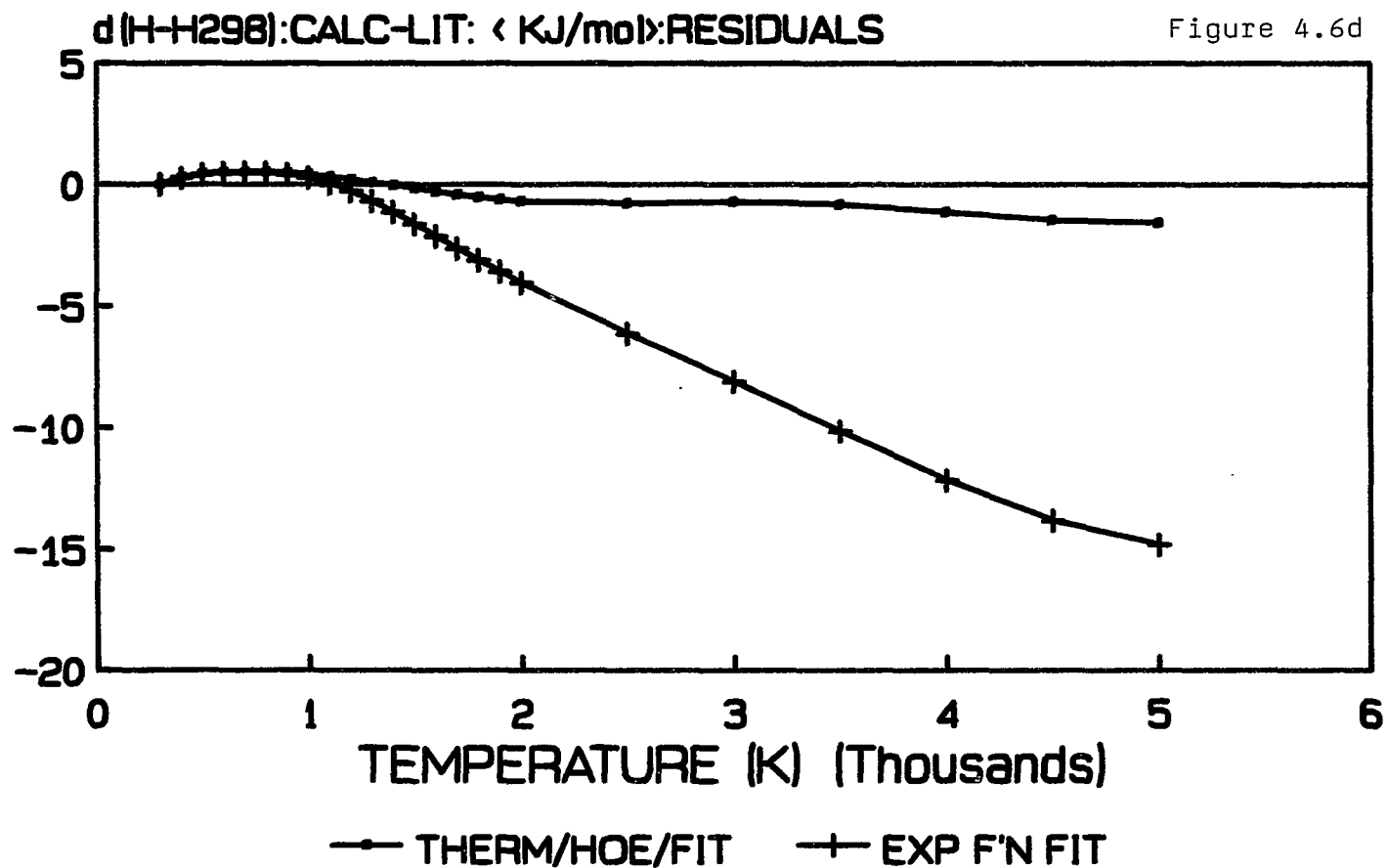


PHENOXY RADICAL: H-H298: EXP MODEL THERM DATA vs. BURCAT

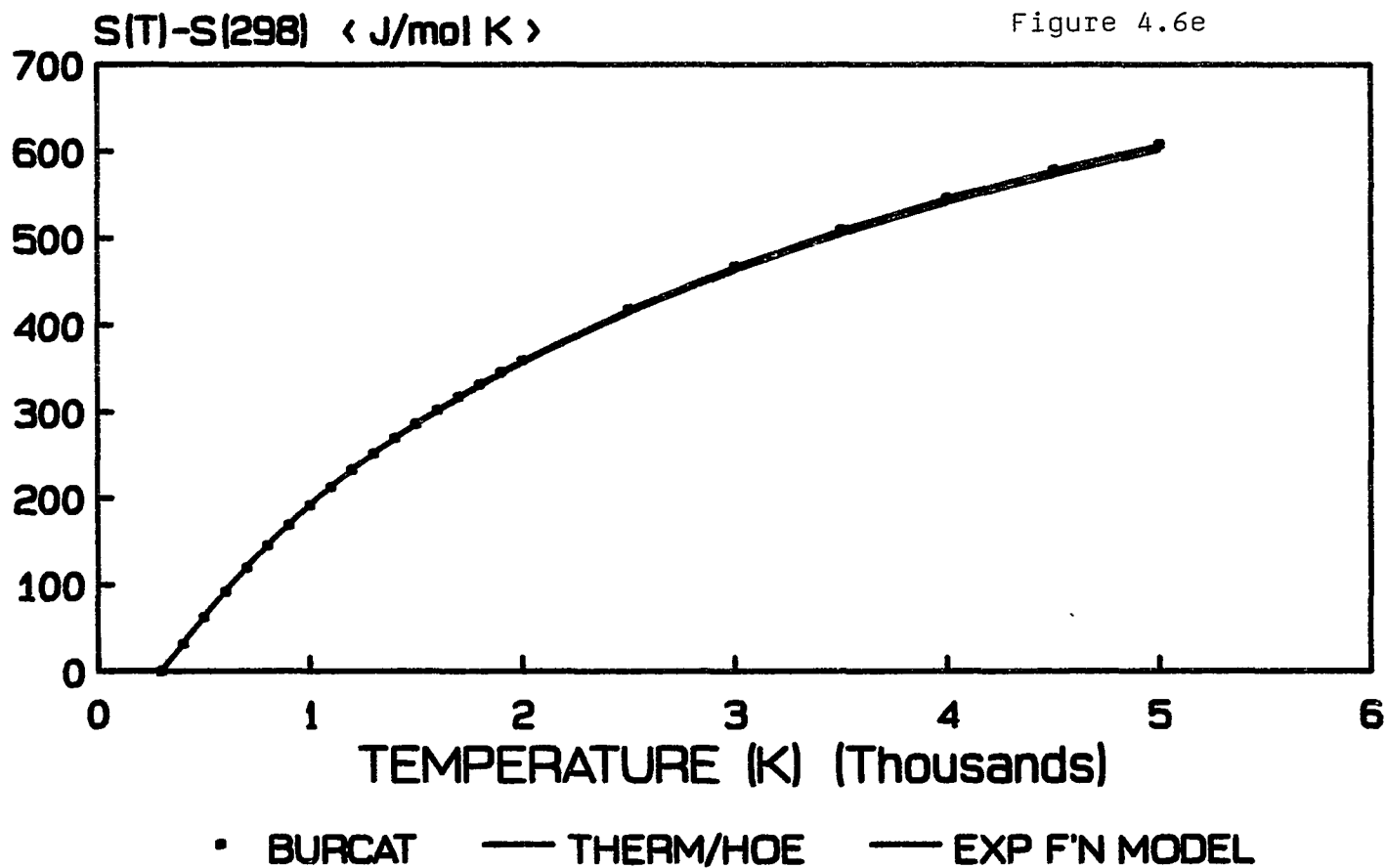
Figure 4.6c



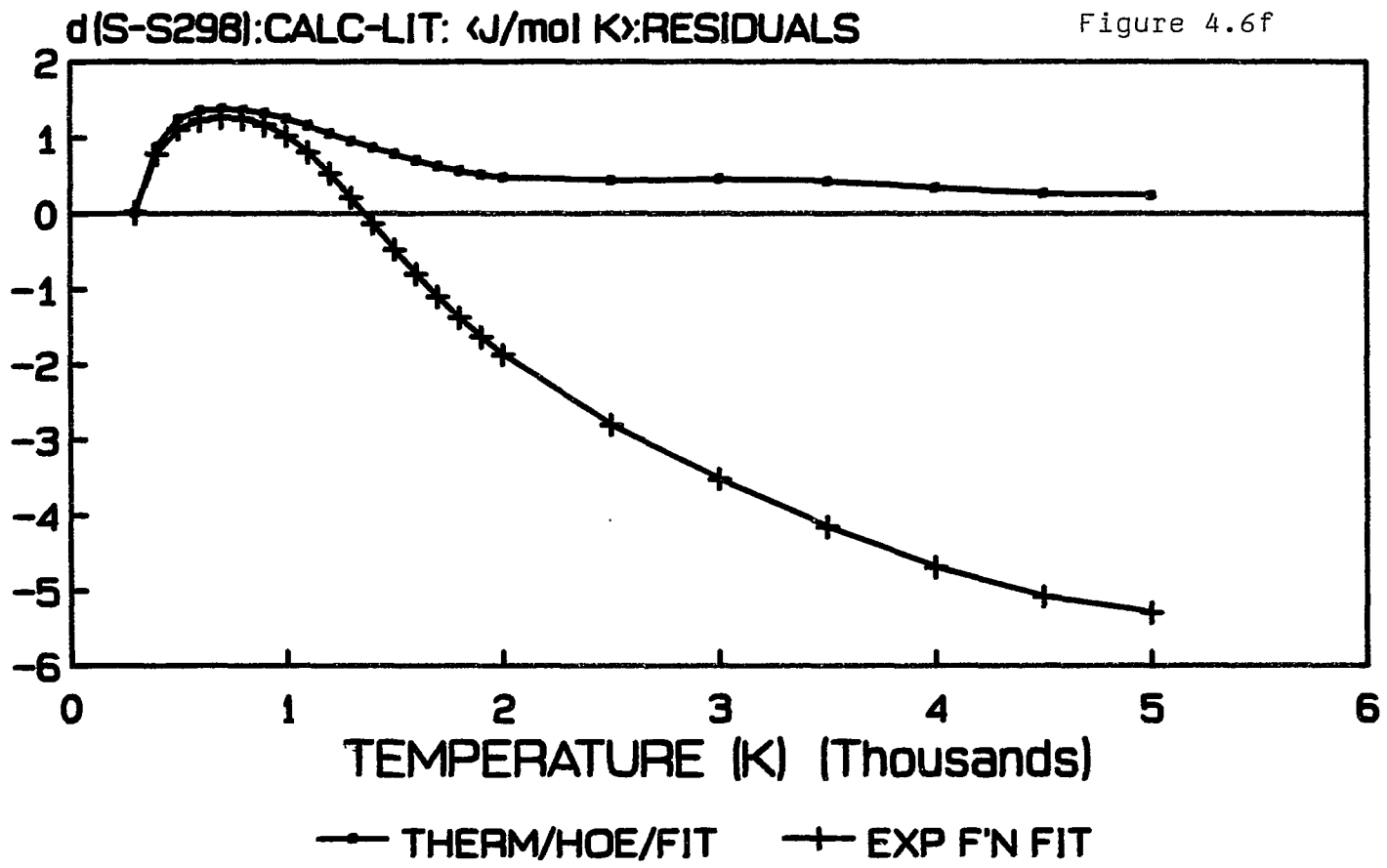
PHENOXY RADICAL: H-H298: RESIDUALS THERM DATA vs. BURCAT



PHENOXY RADICAL: S-S298: EXP MODEL THERM DATA vs. BURCAT

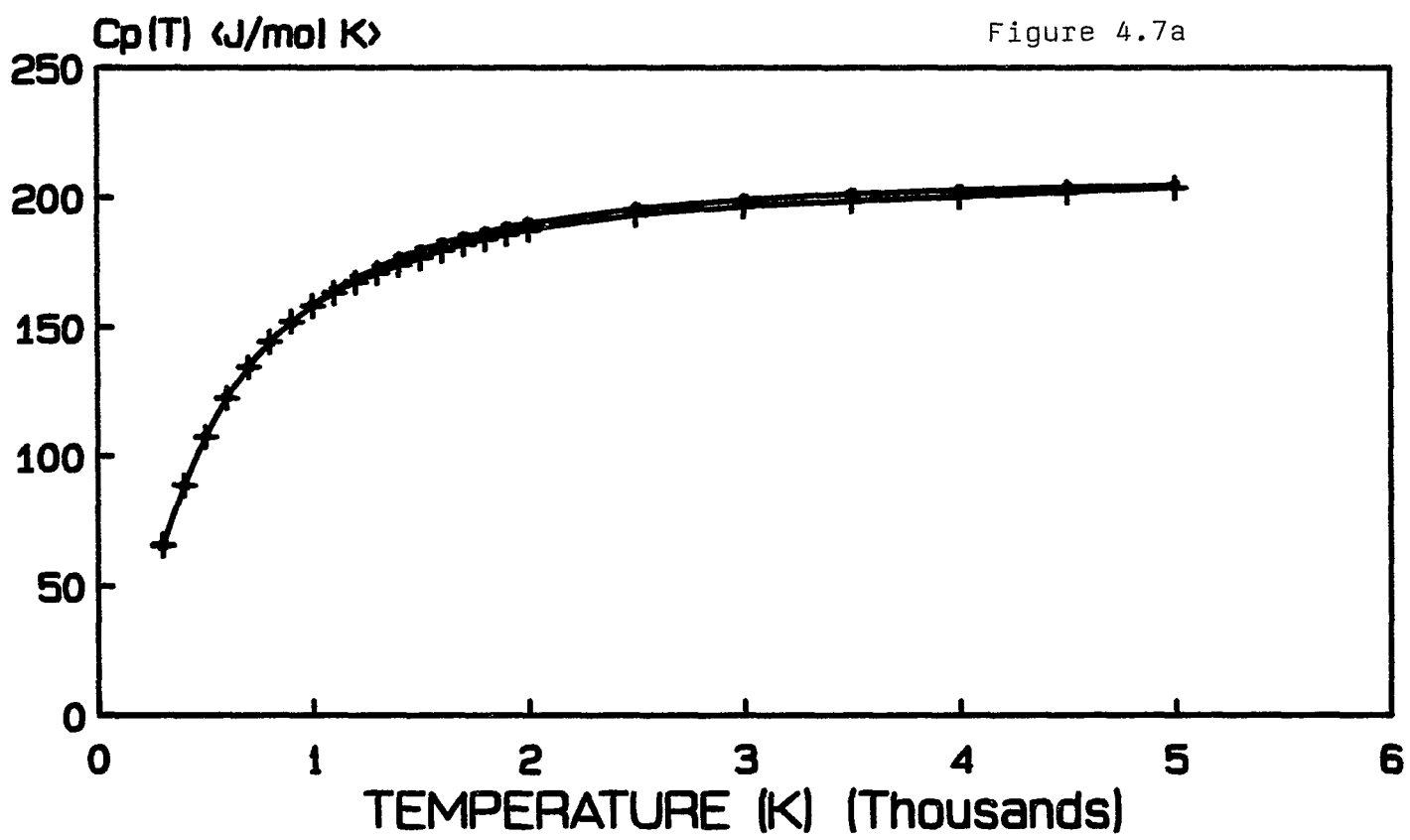


PHENOXY RADICAL: S-S298: RESIDUALS THERM DATA vs. BURCAT



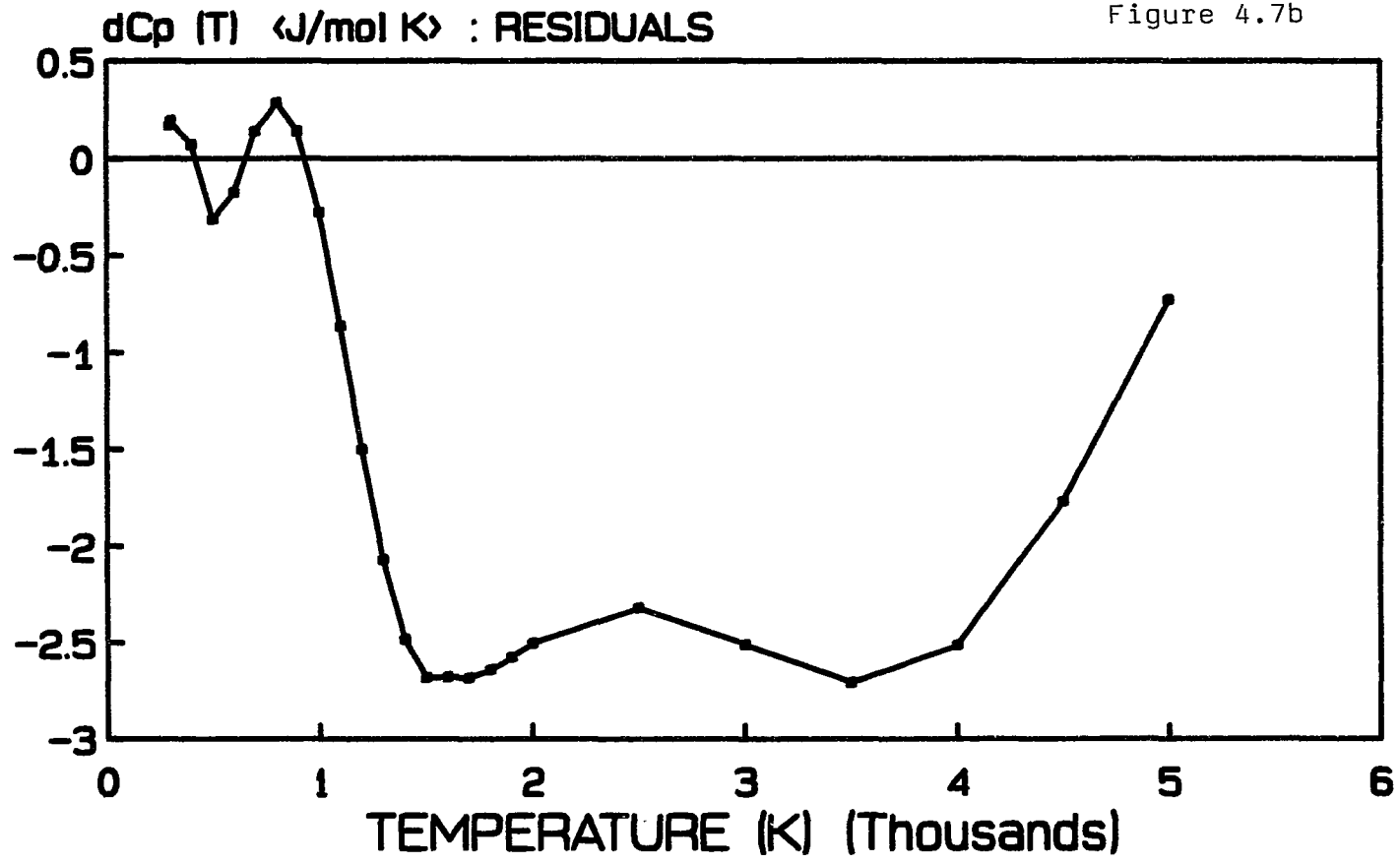
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FURAN : $C_p(T)$



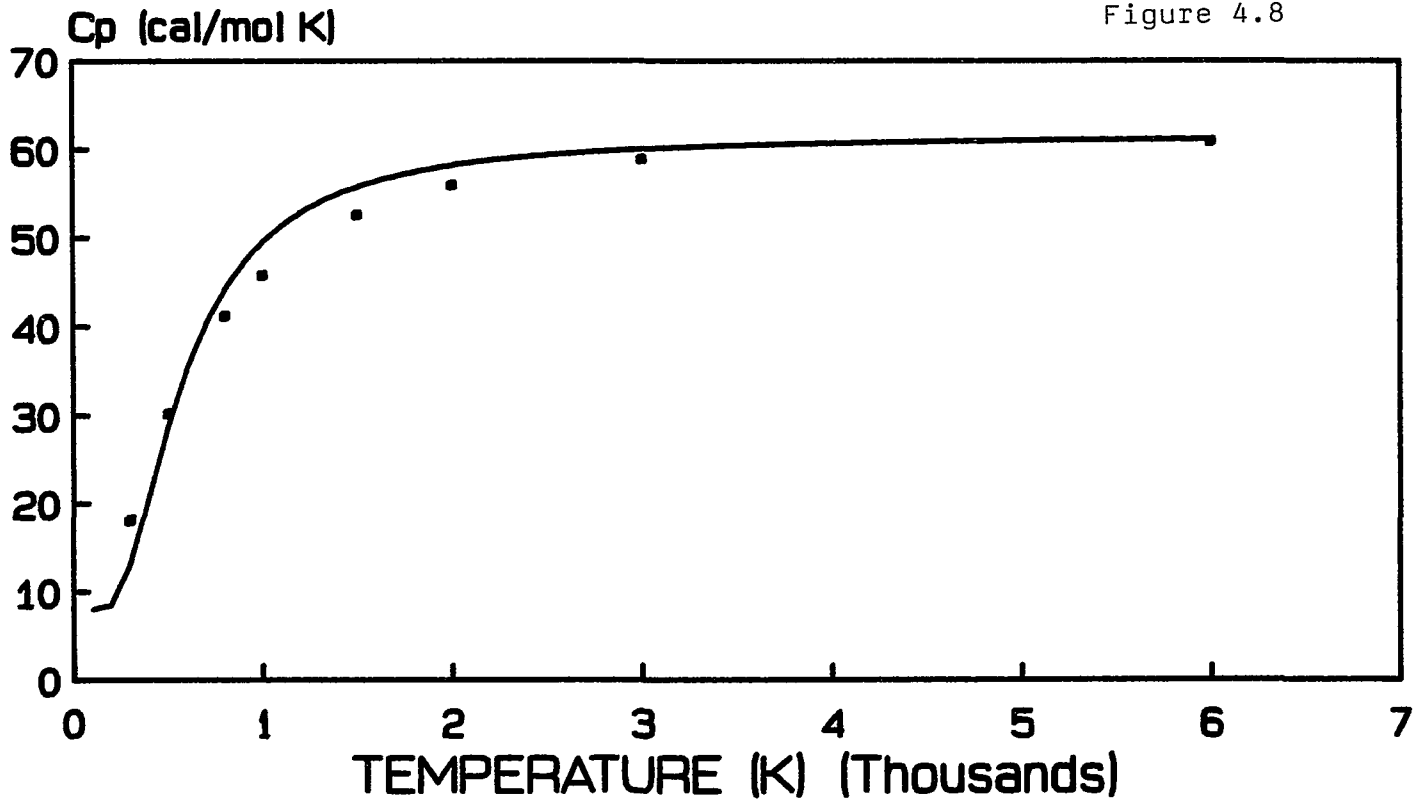
FURAN :Cp (T): RESIDUALS

Figure 4.7b



CYPD: Cp FIT vs. T GEOMETRIC MEAN APPROX vs. LITERATURE

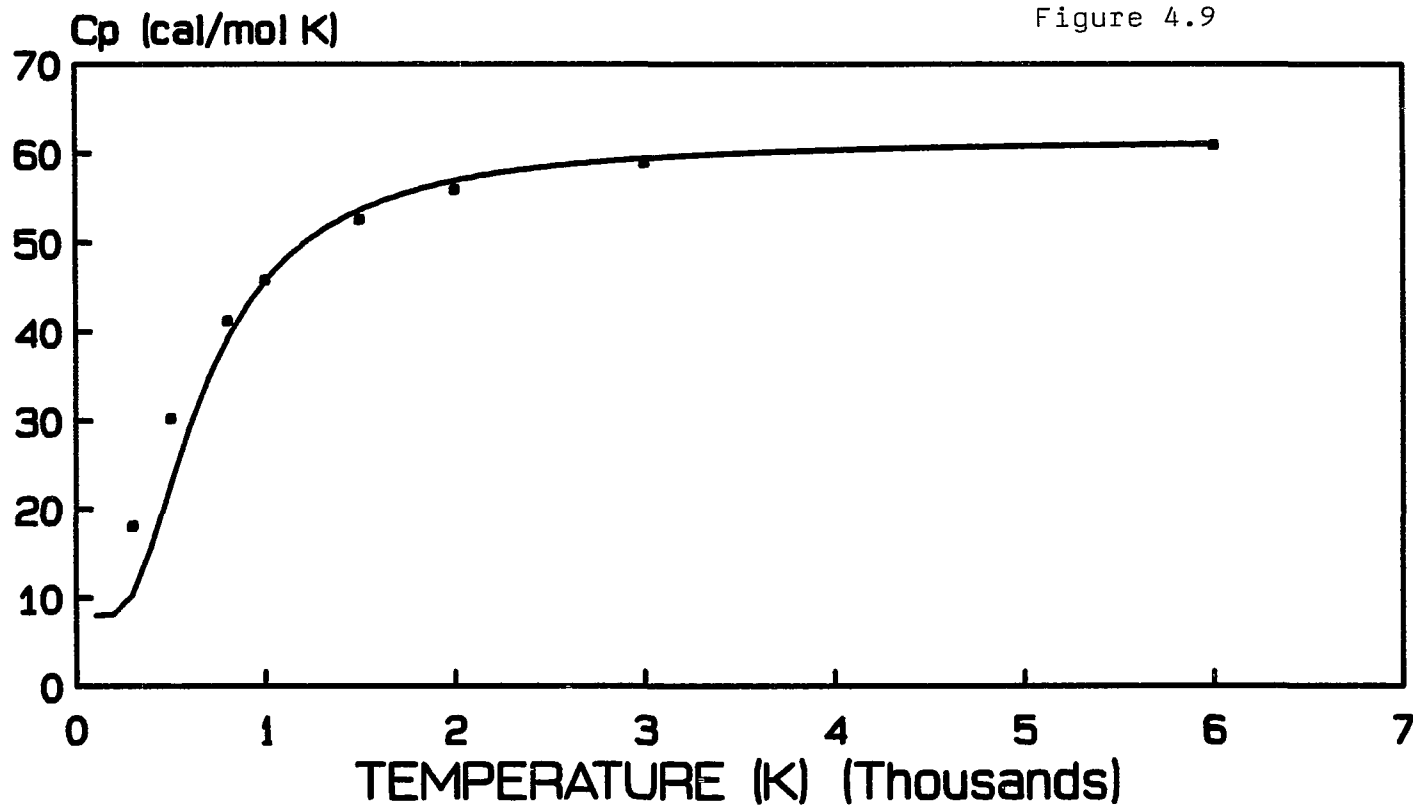
Figure 4.8



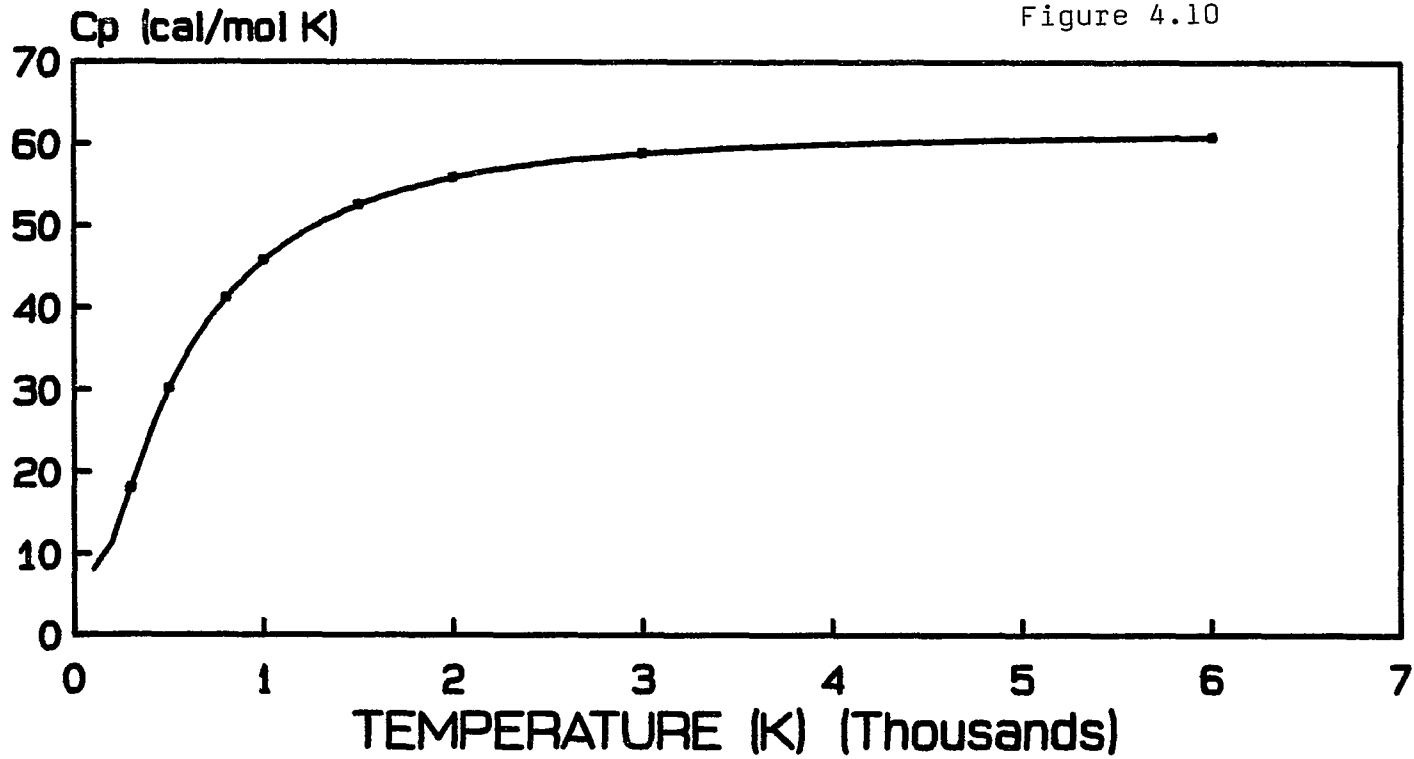
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CYPD: Cp FIT vs. T ARITHMETIC MEAN APPROX vs. LITERATURE

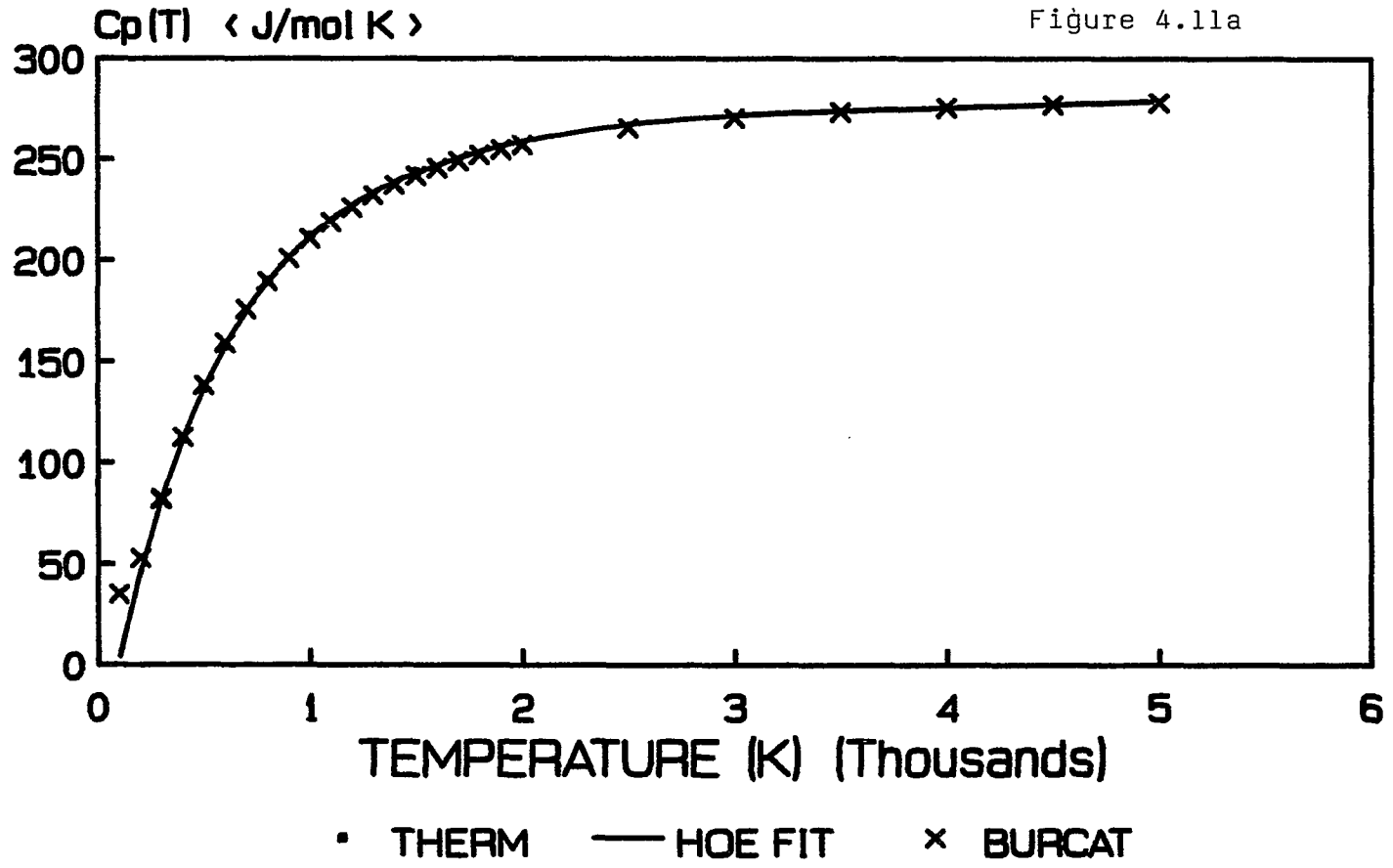
Figure 4.9



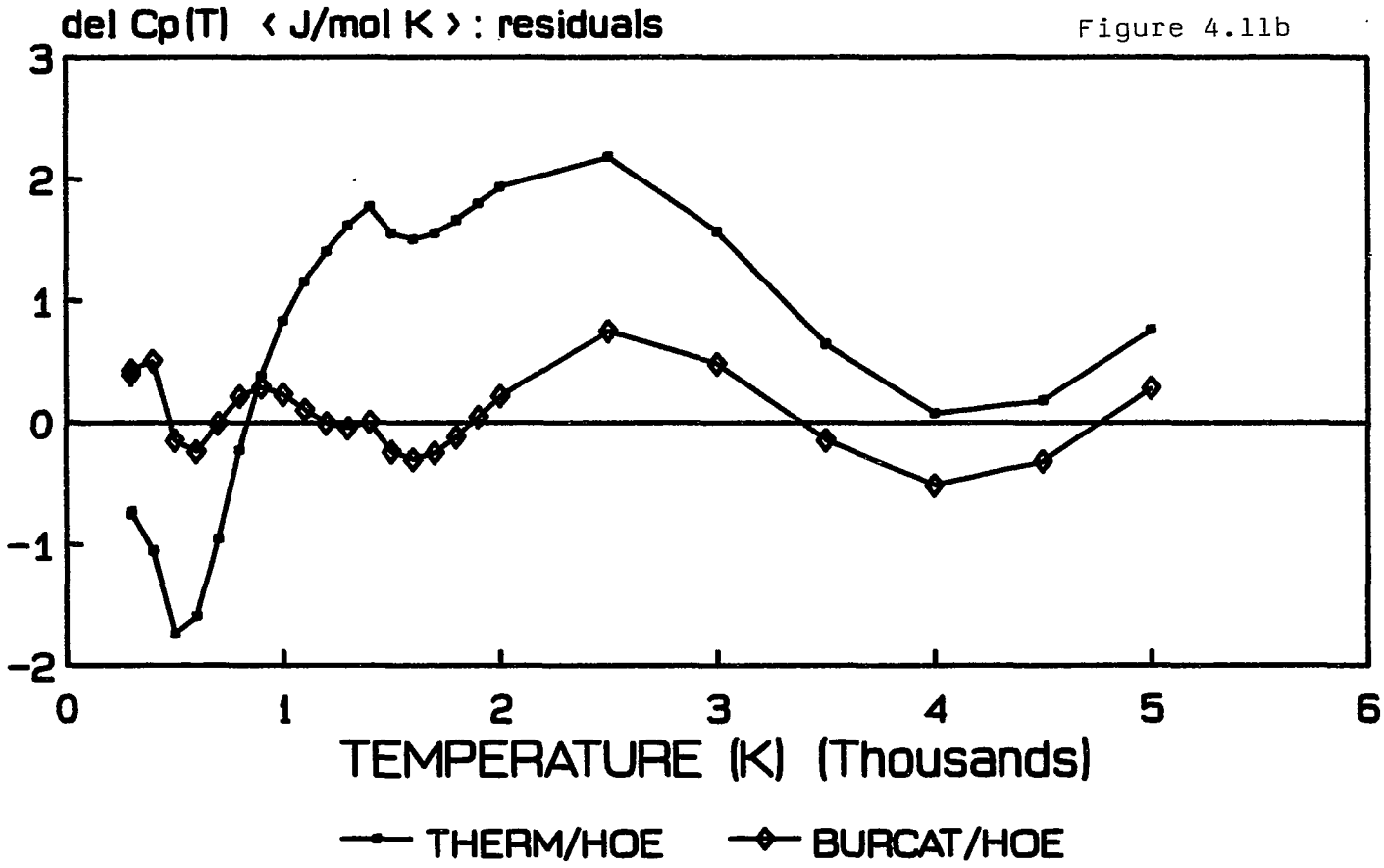
CYPD: Cp FIT vs. T HOE vs. LITERATURE



Cp (T) : BENZENE COMPARISON OF HOE EXTRAPOLATION W/ LIT

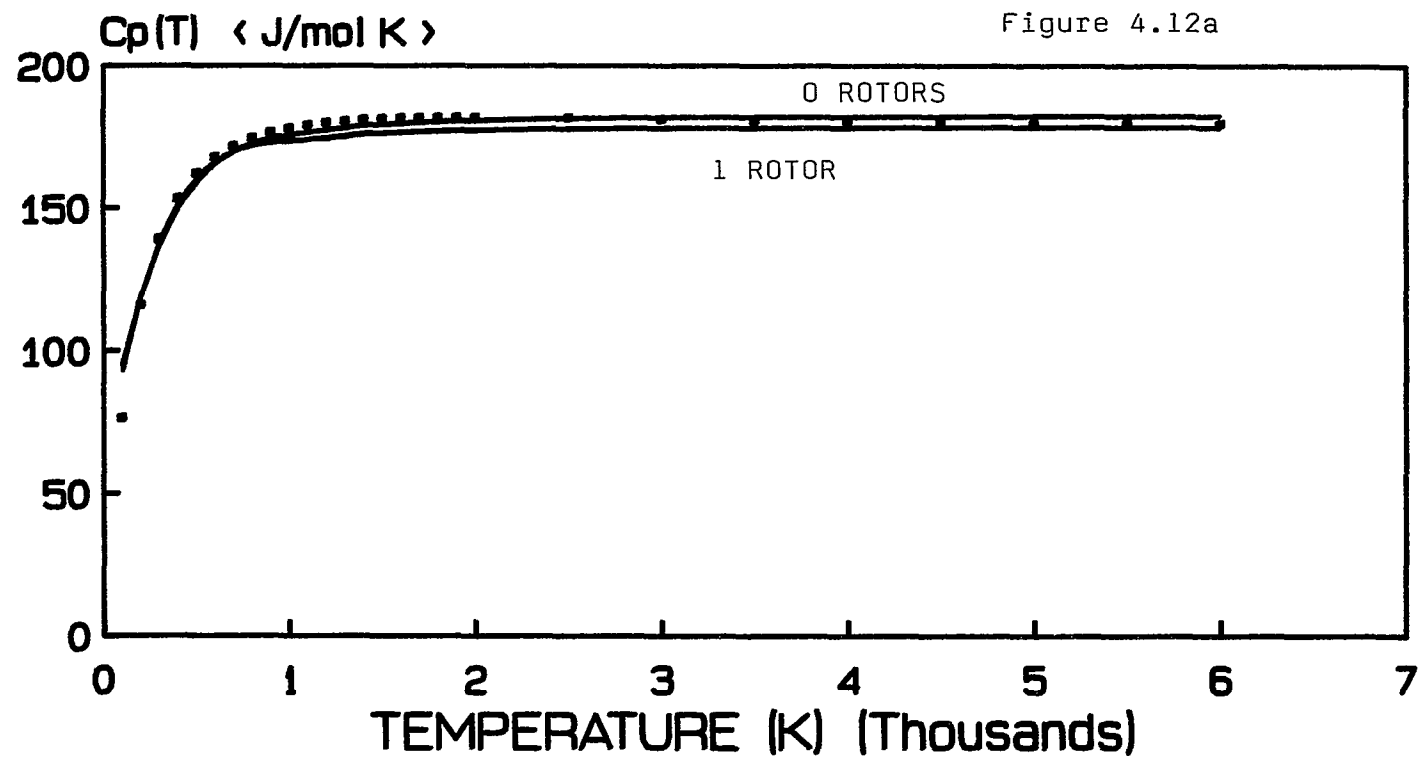


Cp (T) : BENZENE : RESIDUALS COMPARISON OF HOE EXTRAPOLATION W/ LIT



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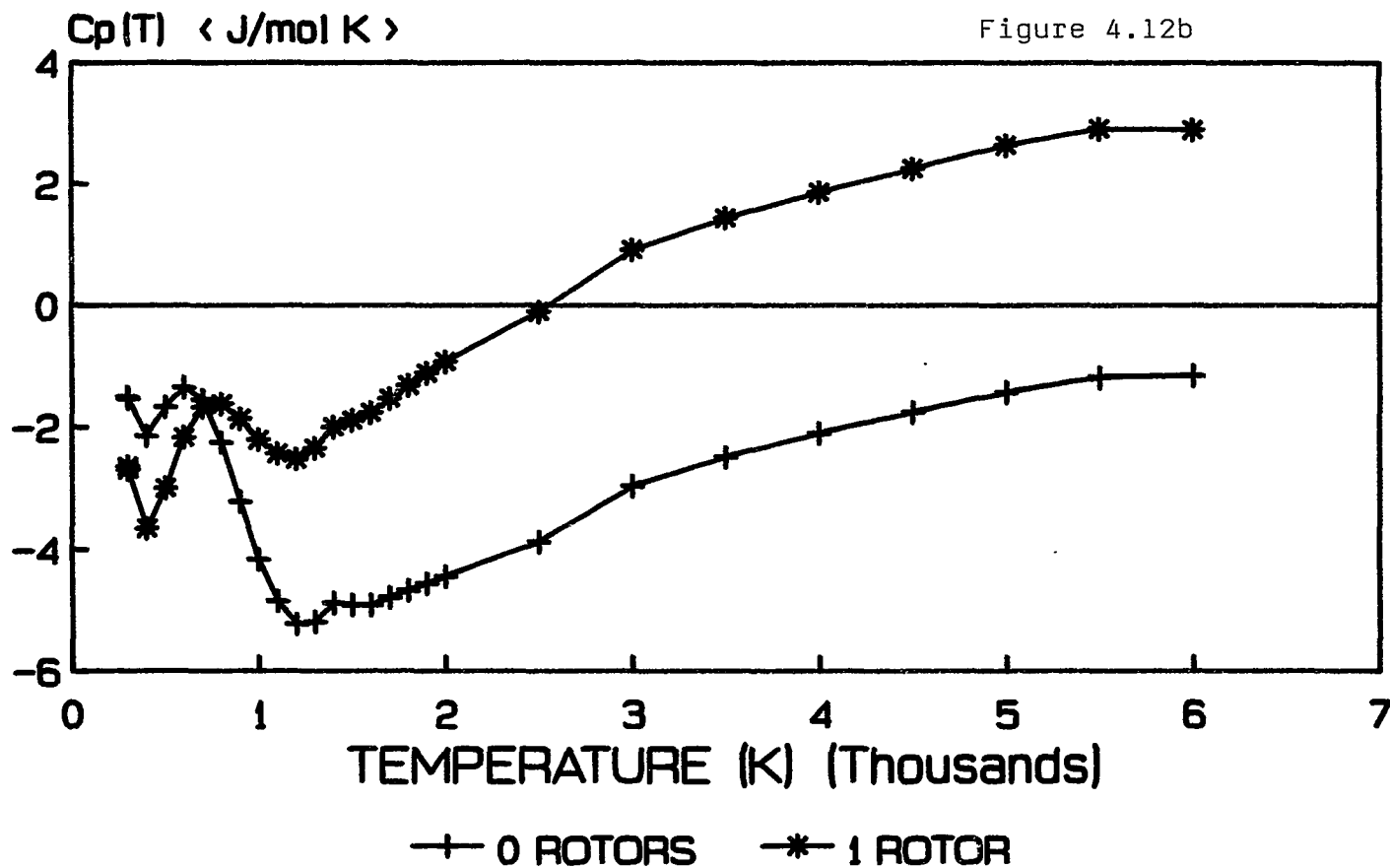
C2Cl6 : fit to HOE Cp (T) ASSUMING 0 AND 1 ROTOR



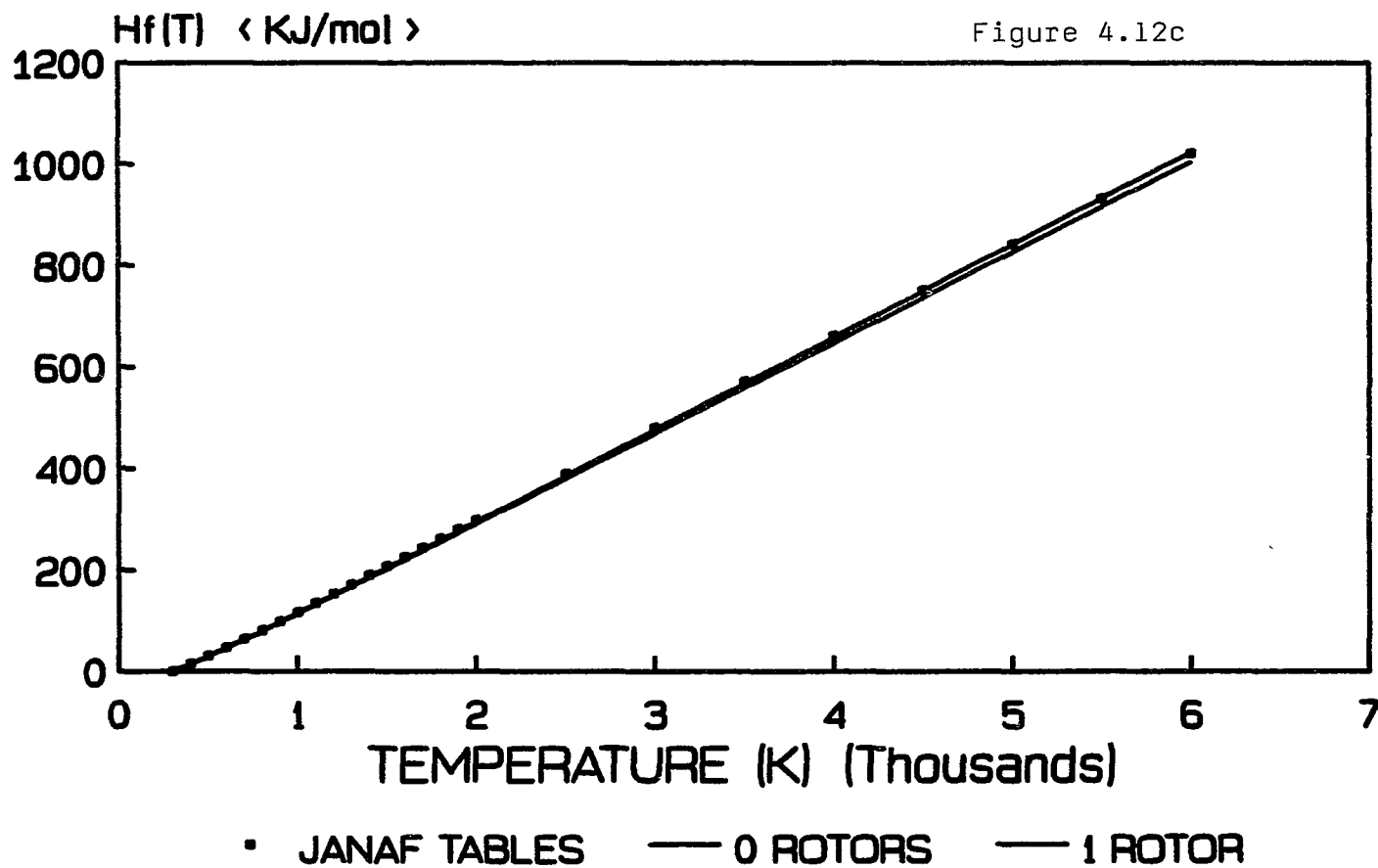
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• JANAF TABLES

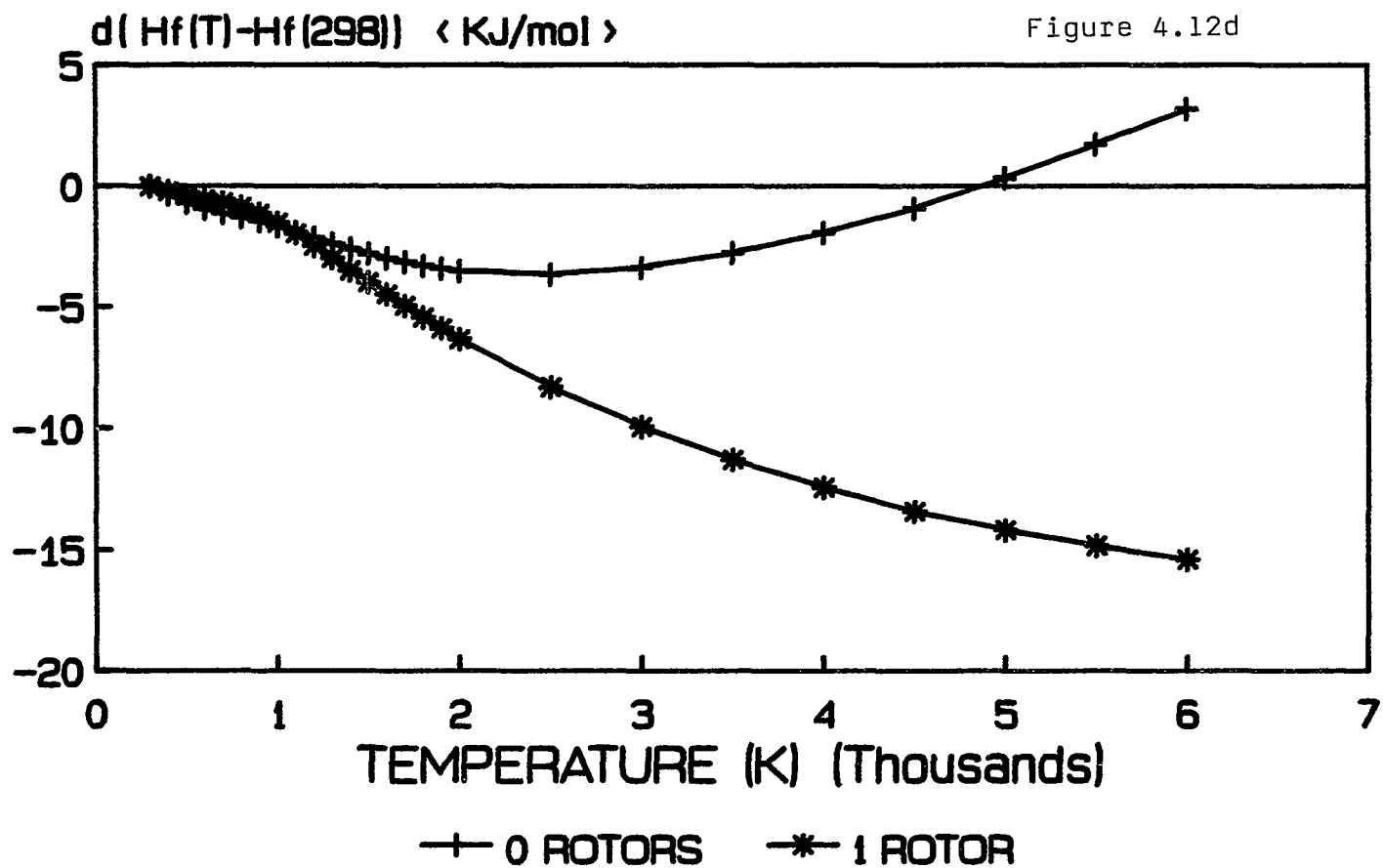
C2Cl6 residuals for HOE fit
Cp (T) ASSUMING 0 AND 1 ROTOR: RESIDUALS



C2Cl6 : ENTHALPY FUNCTION (H(T)-H(298))
Hf (T) ASSUMING 0 AND 1 ROTOR

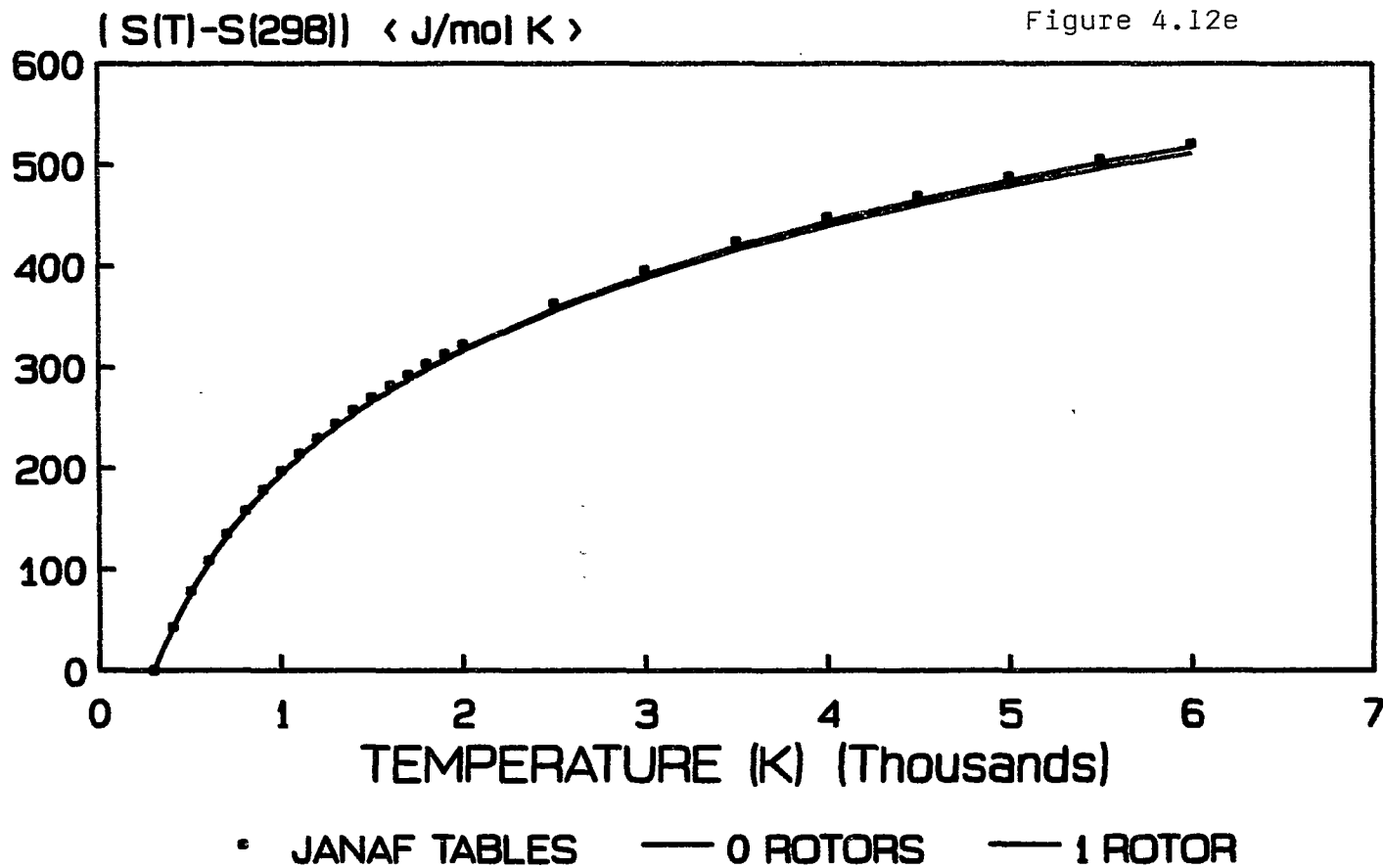


C2Cl6 : ENTHALPY F'N (H(T)-H(298)): RESID
Hf(T) ASSUMING 0 AND 1 ROTOR: RESIDUALS



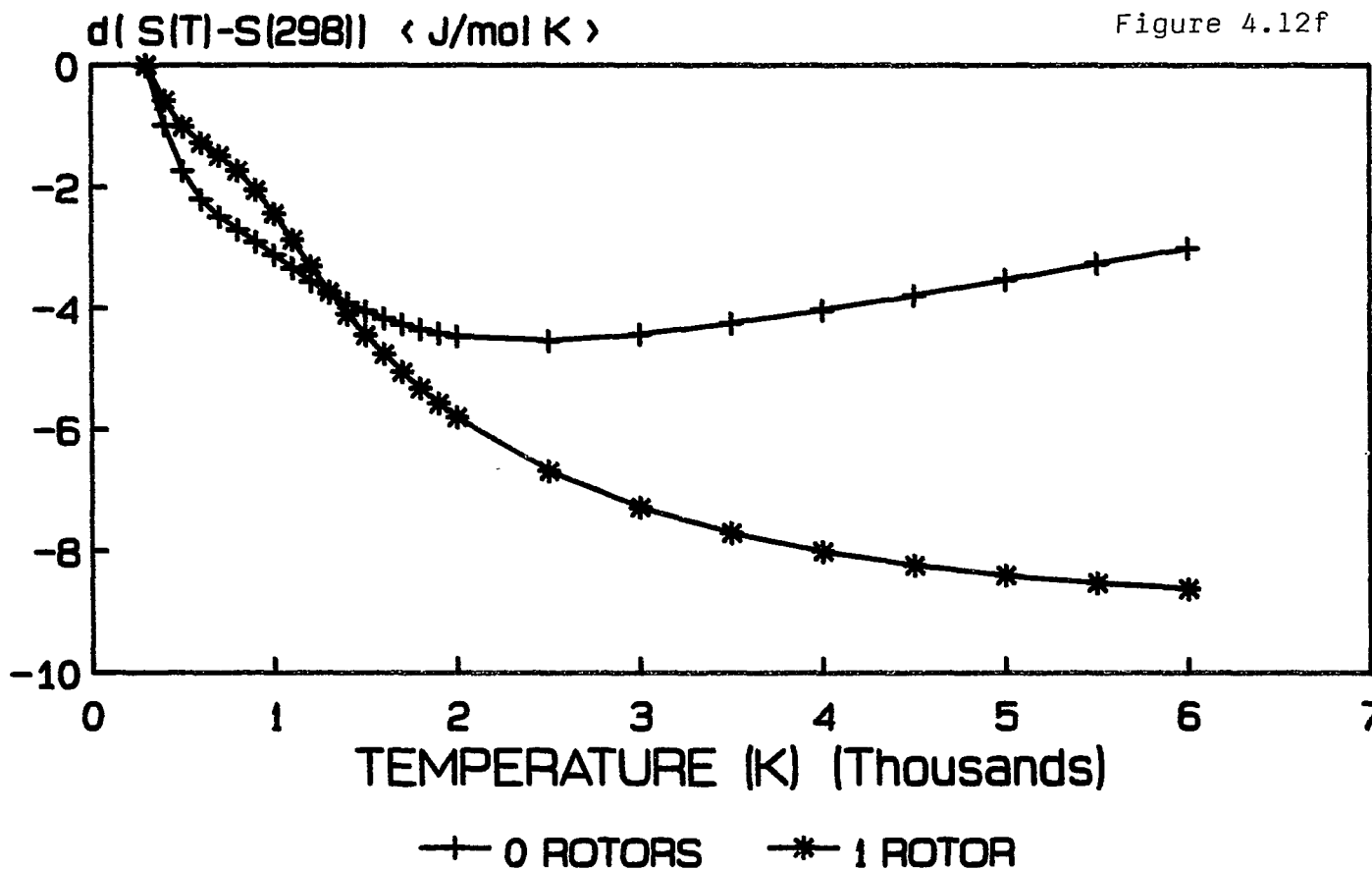
C2Cl6 : ENTROPY F'N (S(T)-S(298))
S(T) ASSUMING 0 AND 1 ROTOR

Figure 4.12e



C2Cl6 :ENTROPY F'N (S(T)-S(298)):RESID S(T) ASSUMING 0 AND 1 ROTOR: RESIDUALS

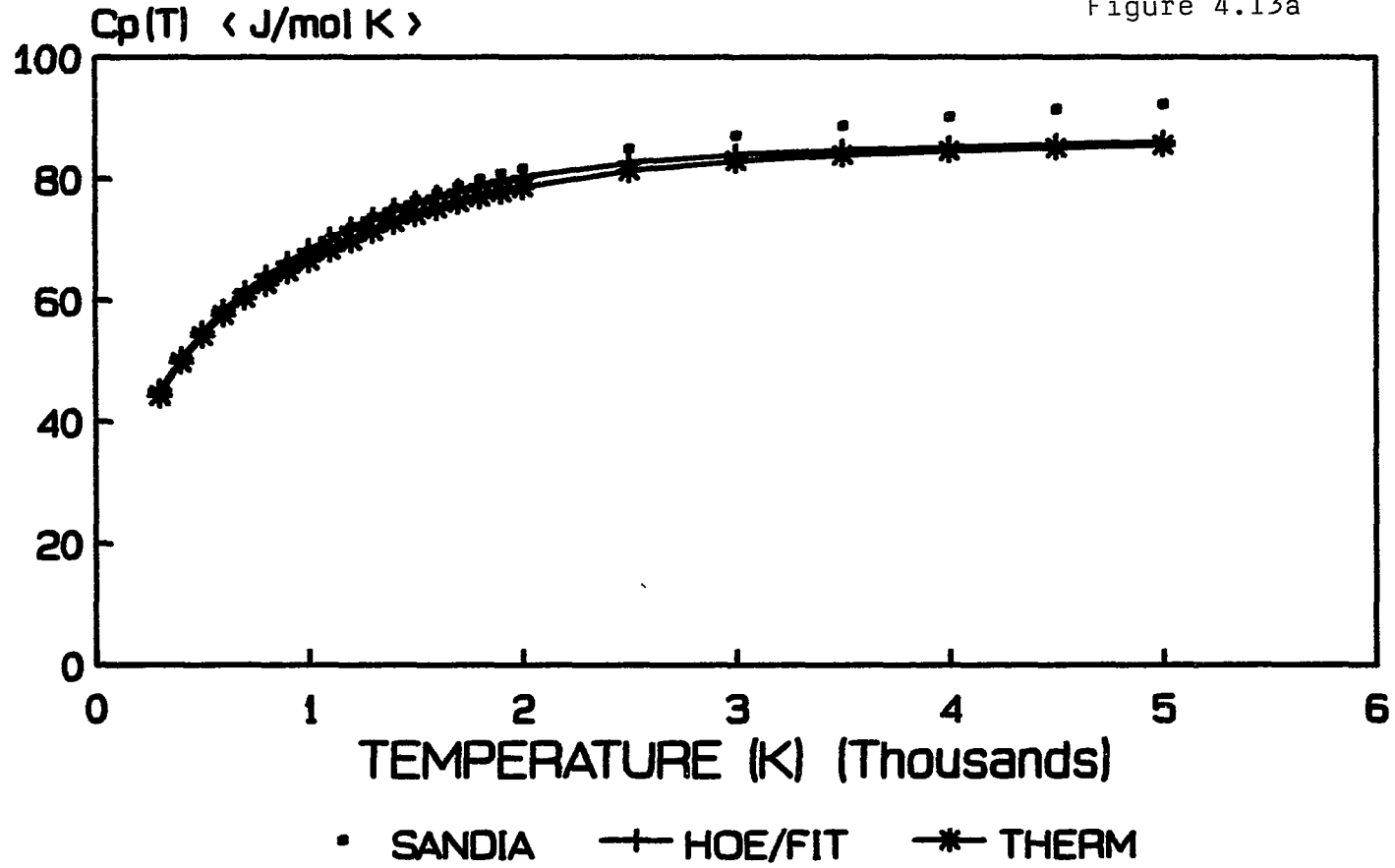
Figure 4.12f



300

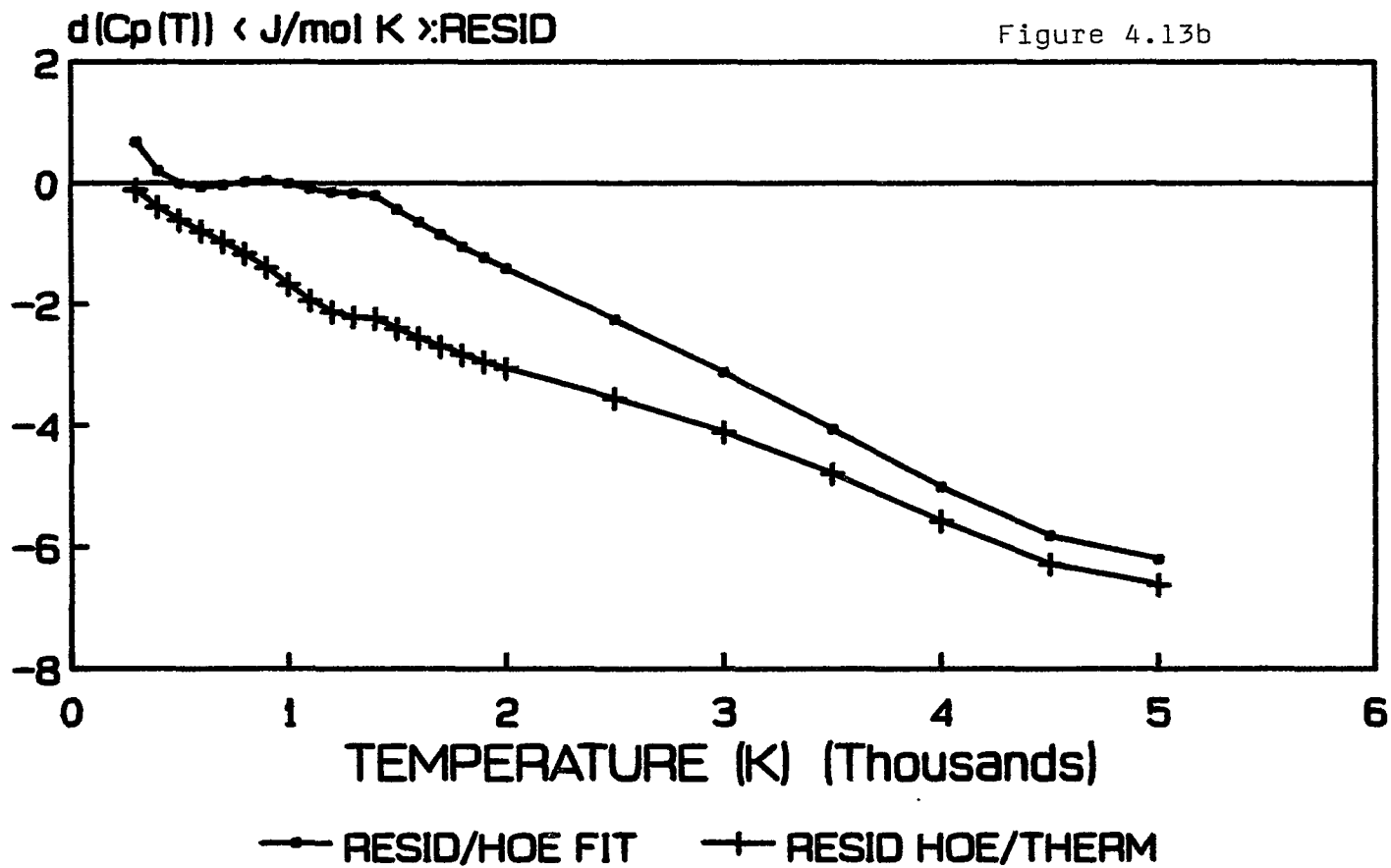
C2H2 : Cp(T) : FIT TO HOE COMPARE SANDIA DATA W/ FIT

Figure 4.13a

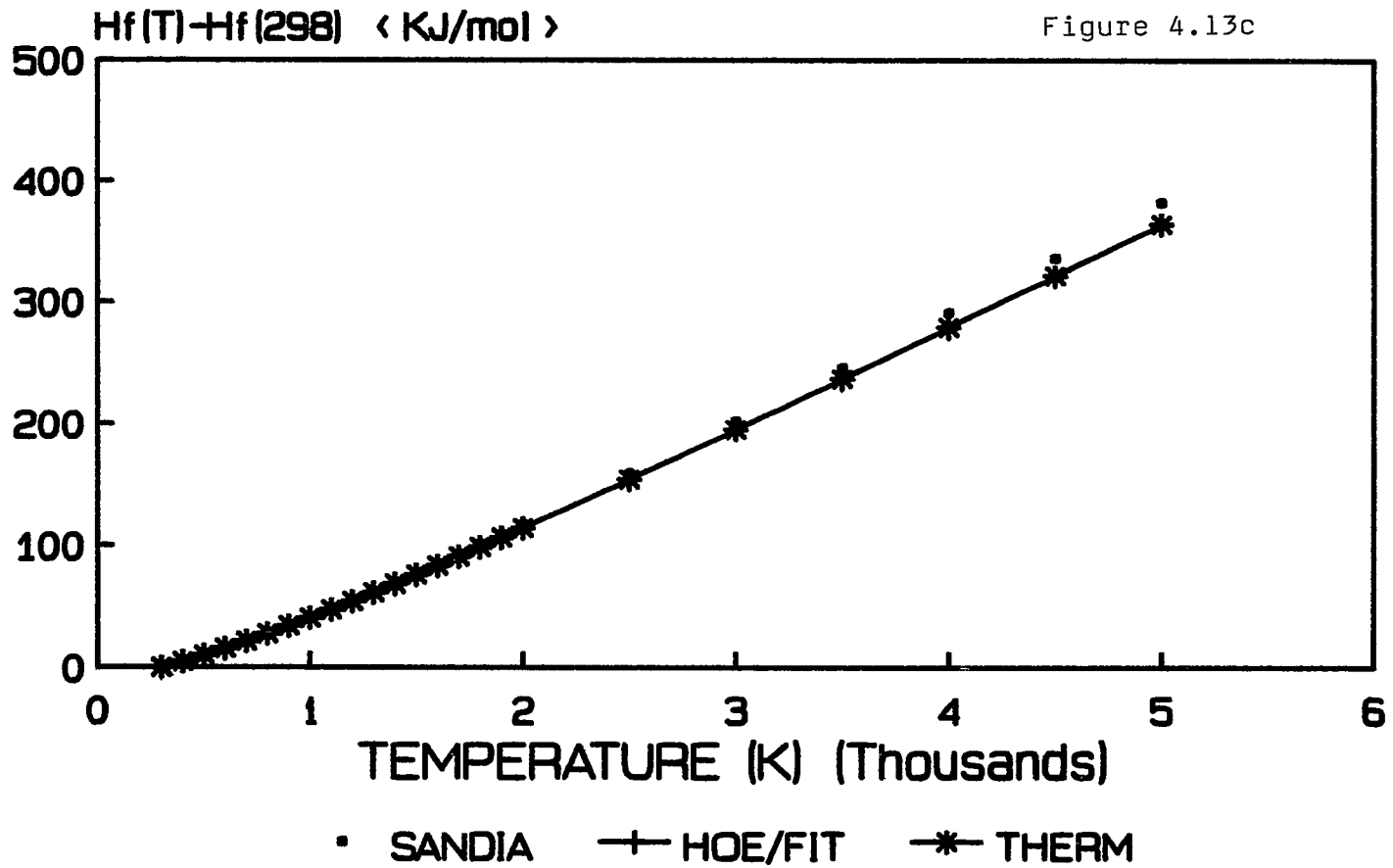


301.

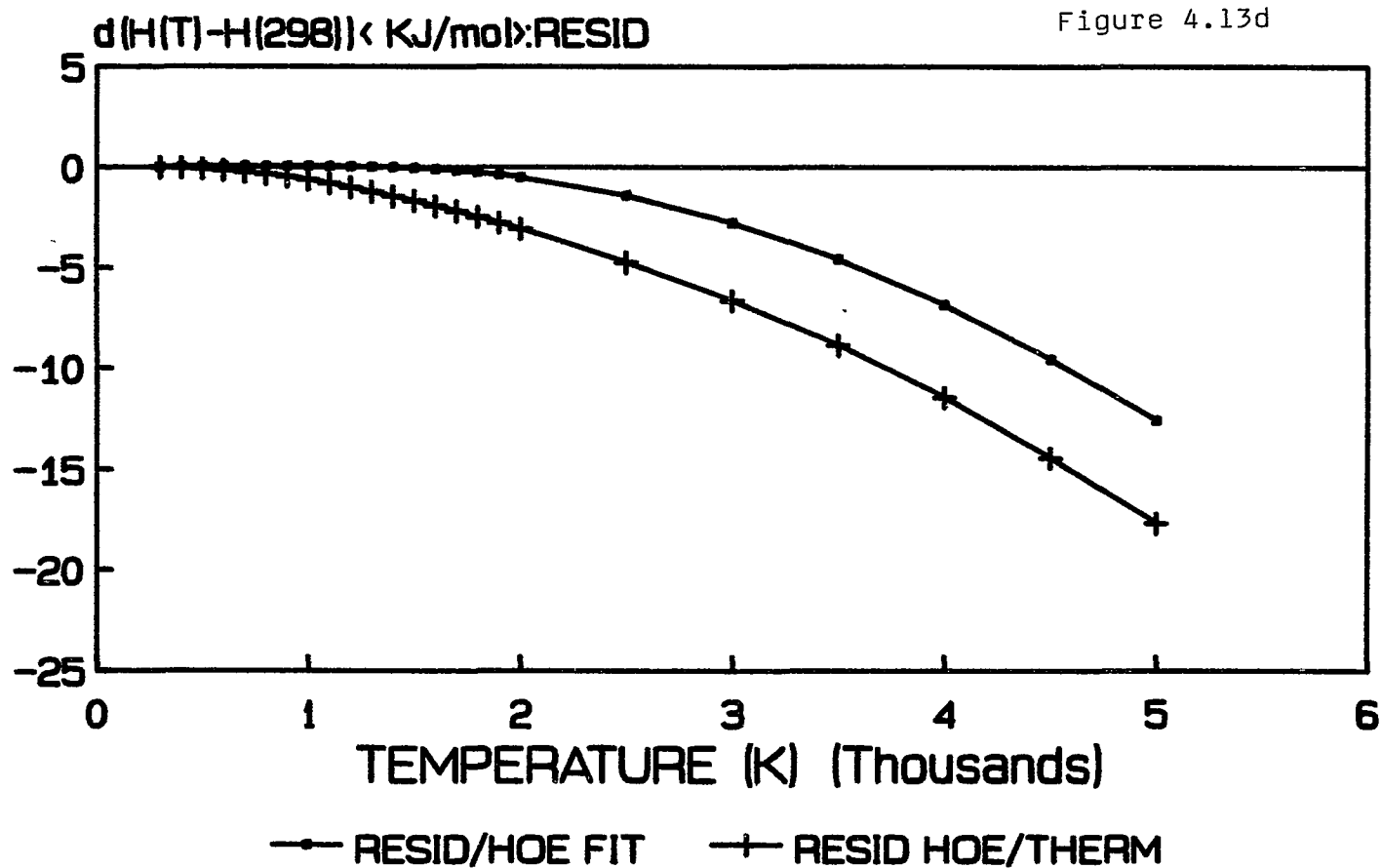
C2H2: Cp(T) : FIT TO HOE: RESIDUALS COMPARE SANDIA DATA W/ FIT



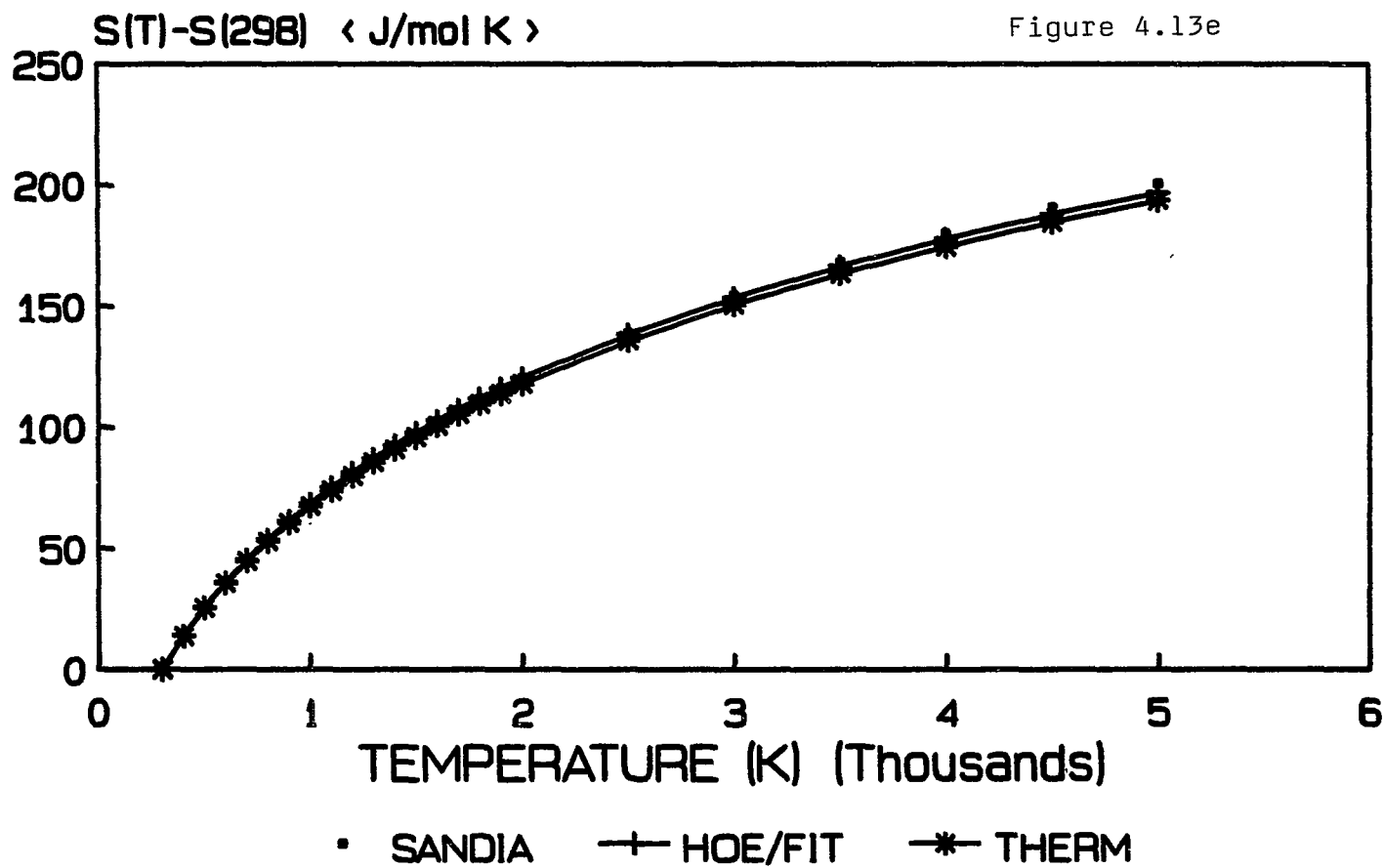
C2H2 : Hf (T)-Hf (298) : FIT TO HOE COMPARE SANDIA DATA W/ FIT



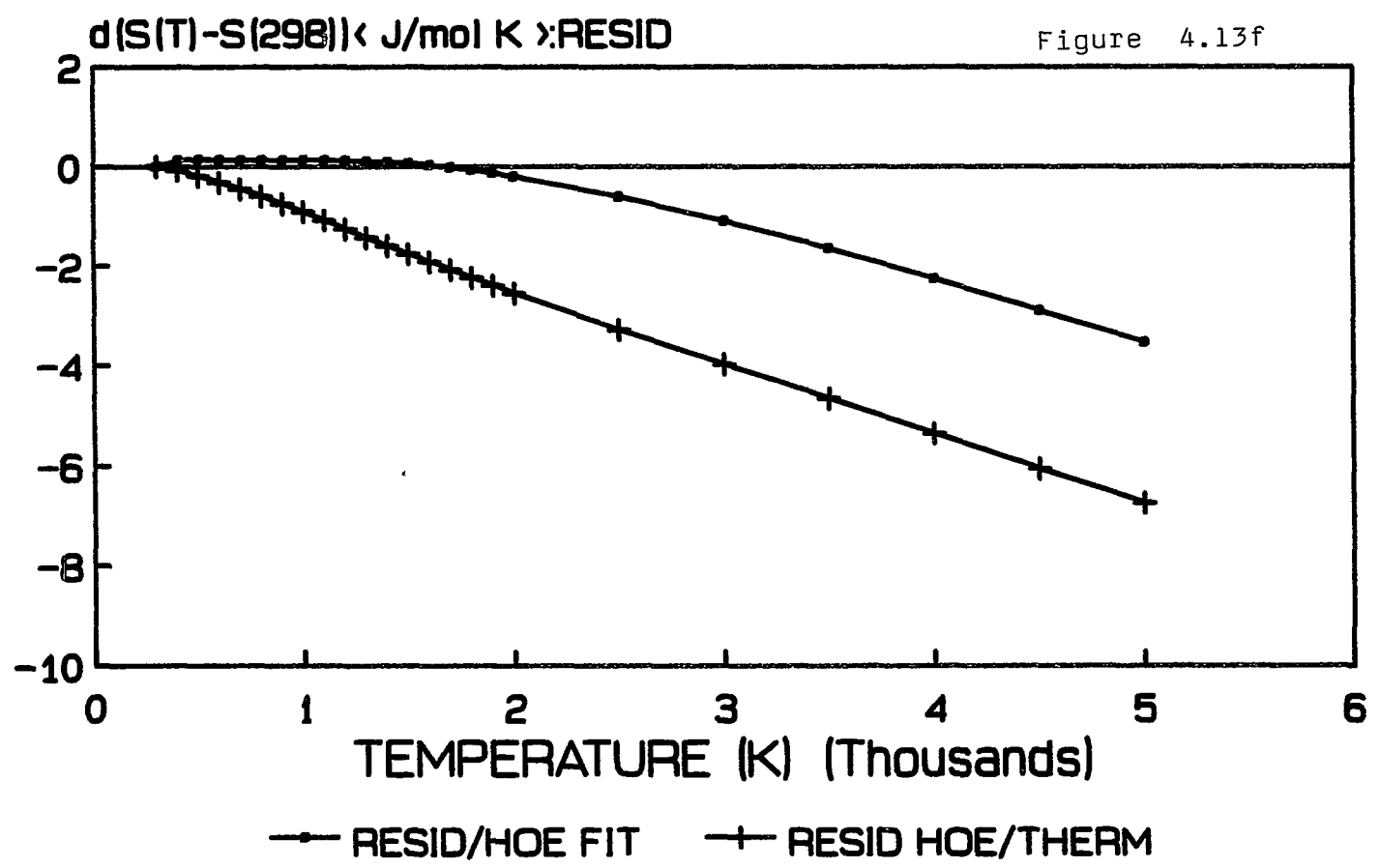
C2H2:H(T)-H(298): FIT TO HOE: RESIDUALS COMPARE SANDIA DATA W/ FIT



C2H2 : S(T)-S(298) : FIT TO HOE COMPARE SANDIA DATA W/ FIT

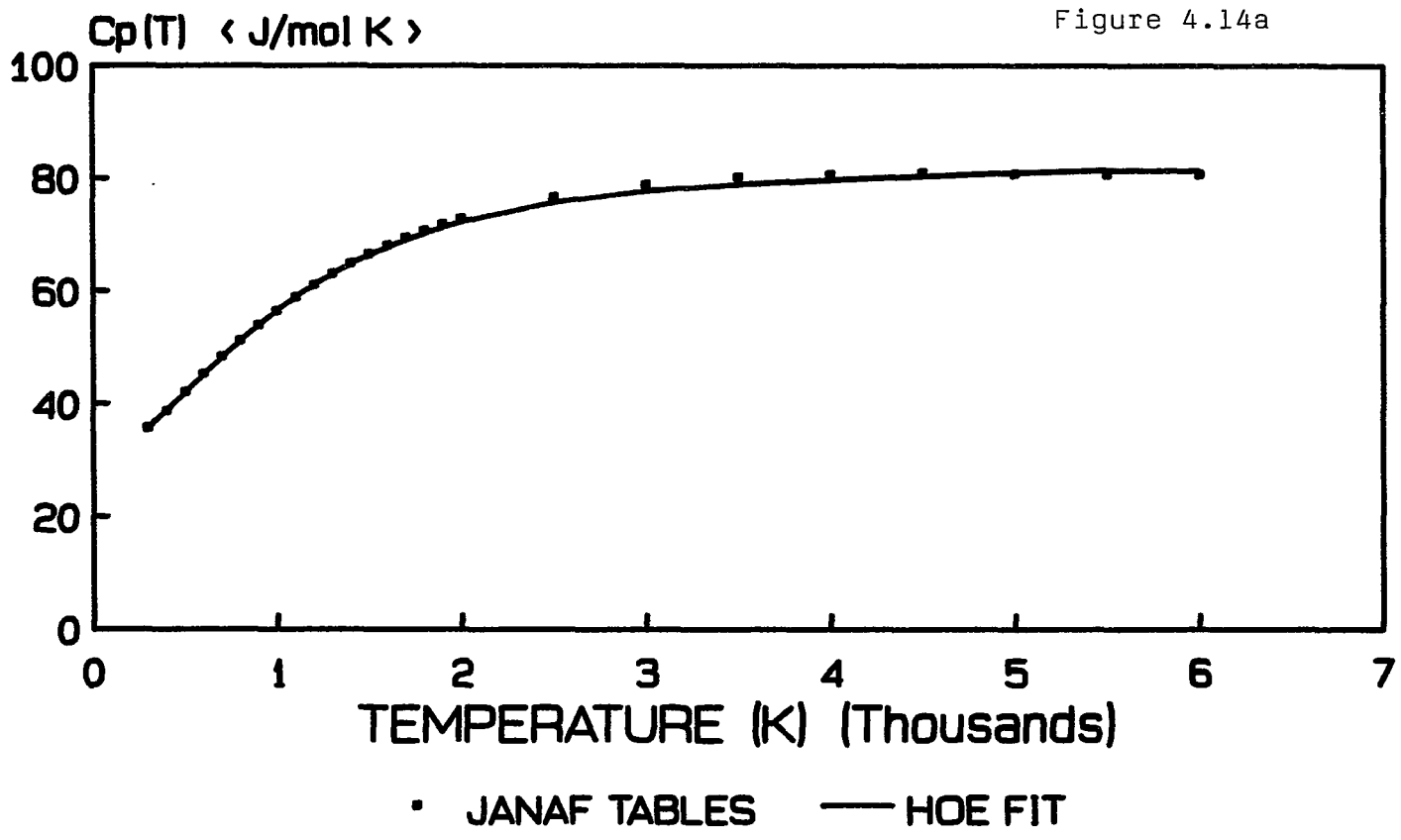


C2H2:S(T)-S(298): FIT TO HOE: RESIDUALS COMPARE SANDIA DATA W/ FIT



306

NH3 : Cp (T) FIT TO HOE COMPARE LITERATURE W/ FIT

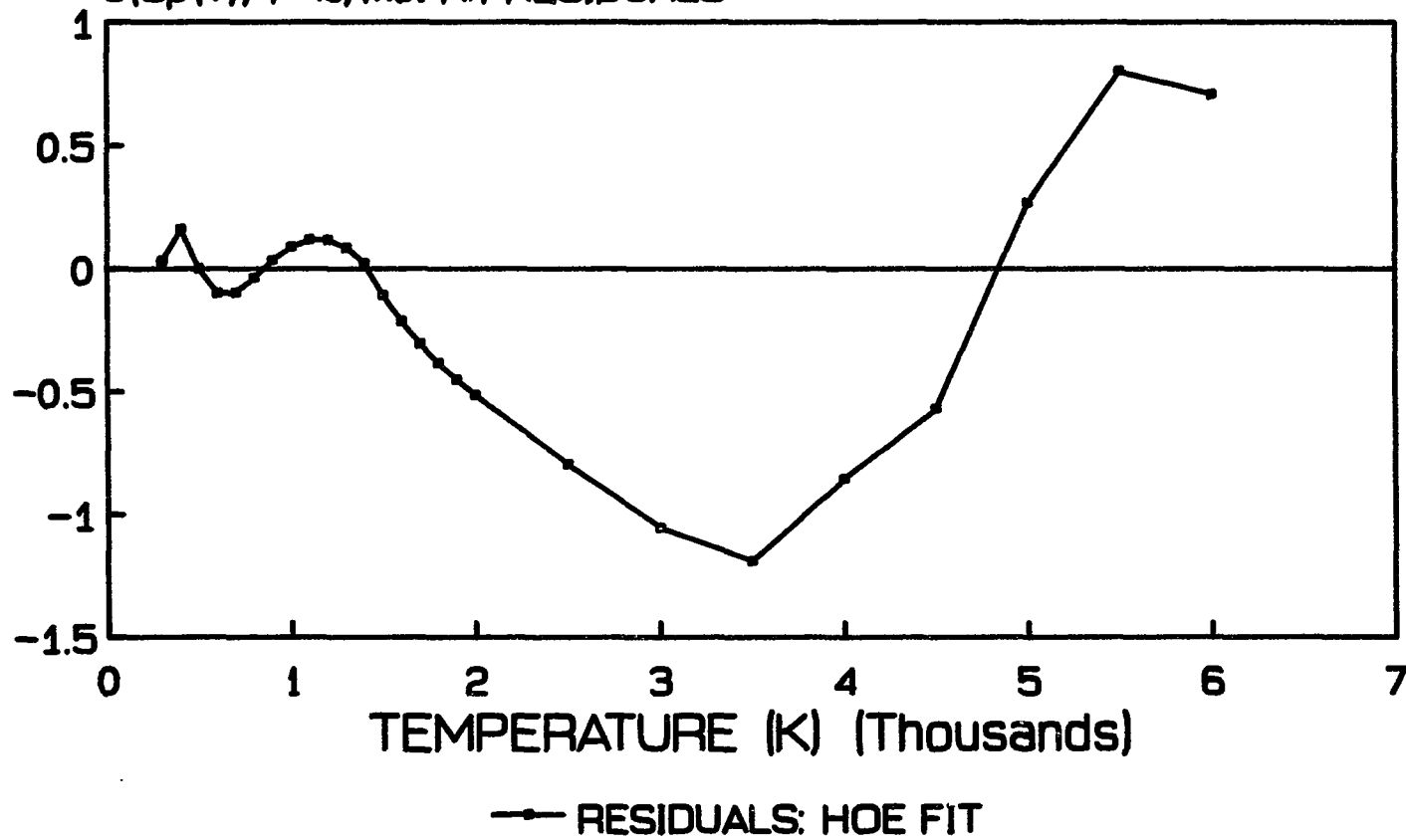


307

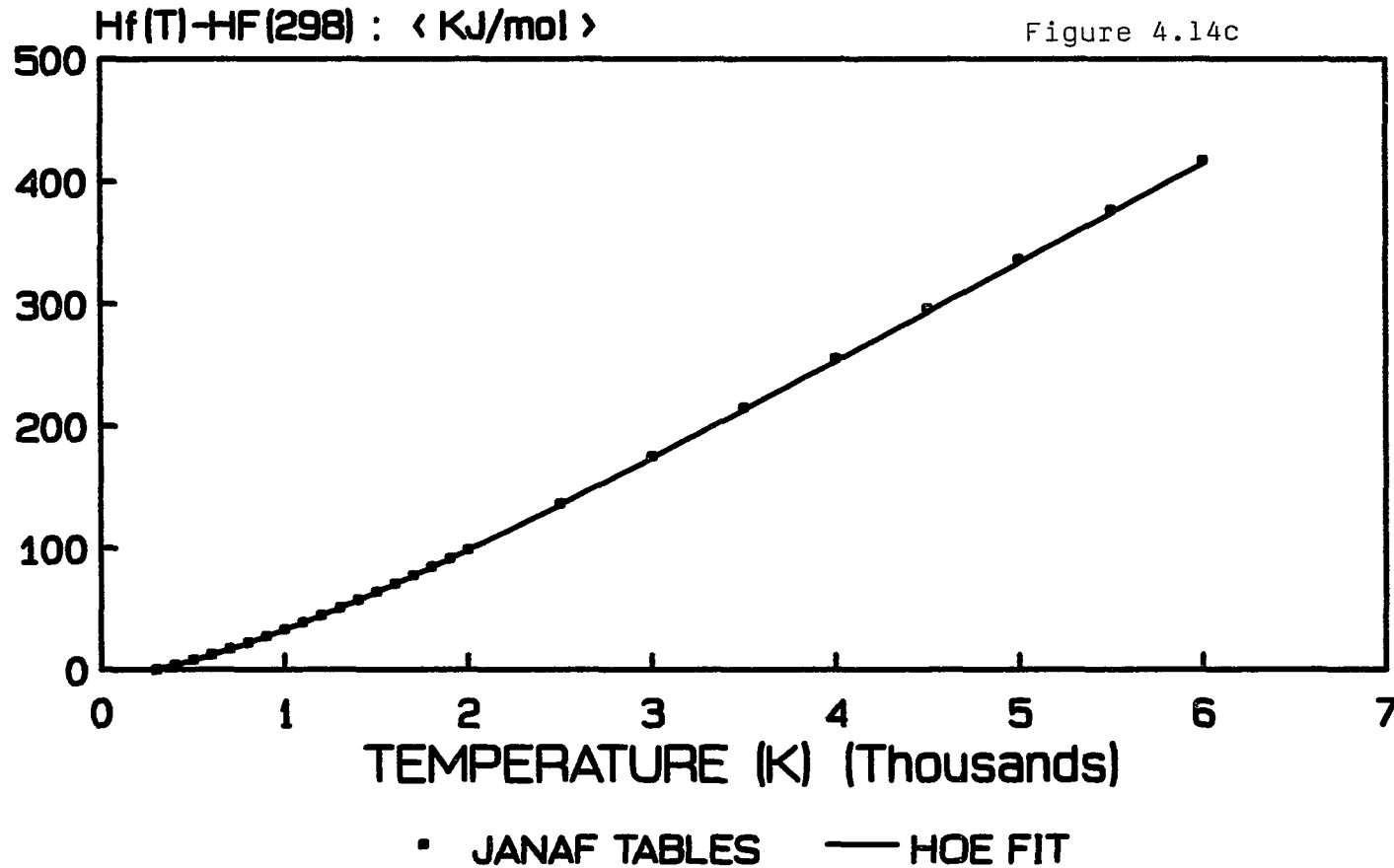
NH3: Cp(T) : FIT TO HOE: RESIDUALS COMPARE LITERATURE W/ FIT

d(Cp(T)) : <J/mol K>: RESIDUALS

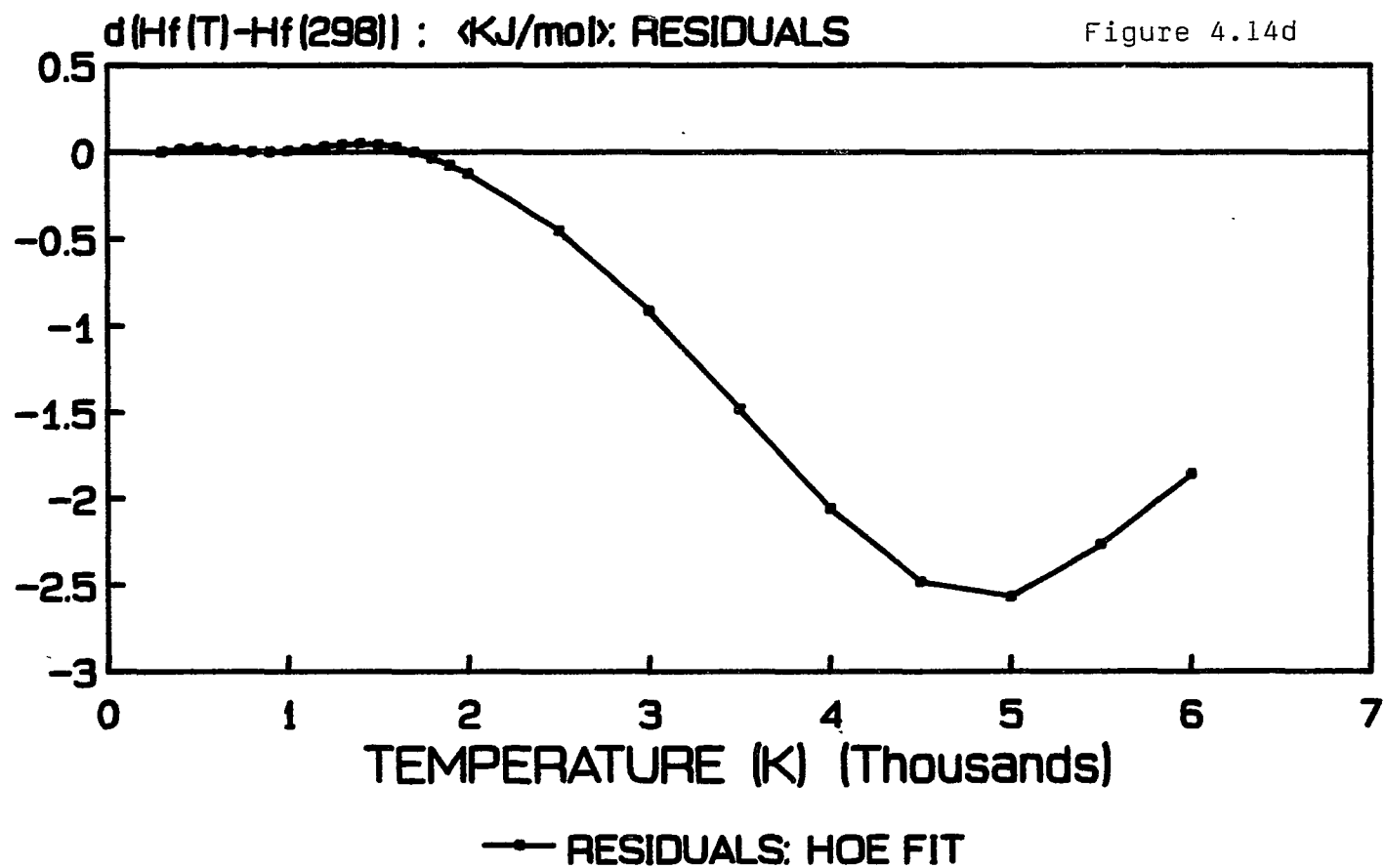
Figure 4.14b



NH3 : H(T)-H(298): FIT TO HOE COMPARE LITERATURE W/ FIT

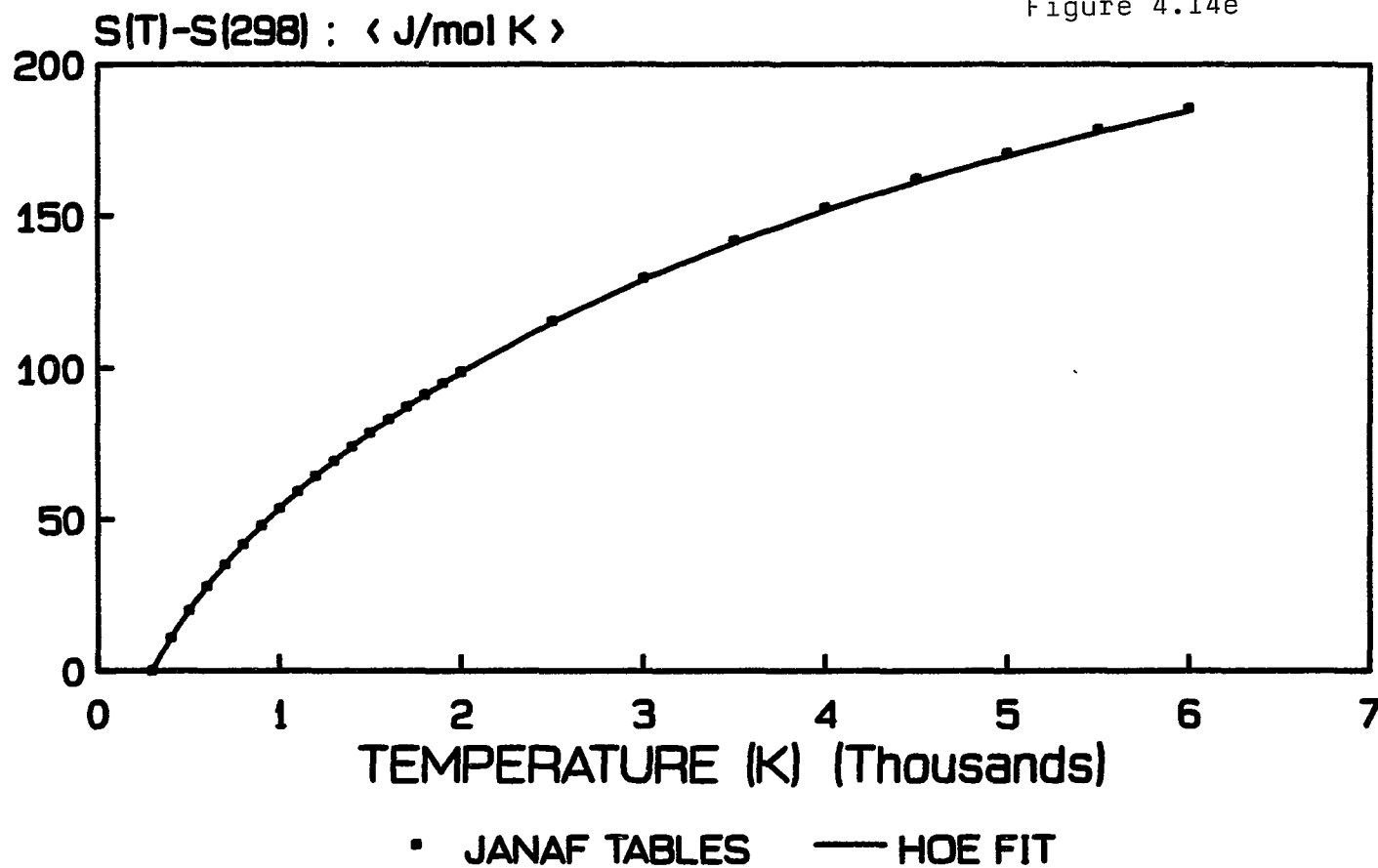


NH3: H(T)-H(298): FIT TO HOE: RESIDUALS COMPARE LITERATURE W/ FIT



NH3 : S(T)-S(298): FIT TO HOE COMPARE LITERATURE W/ FIT

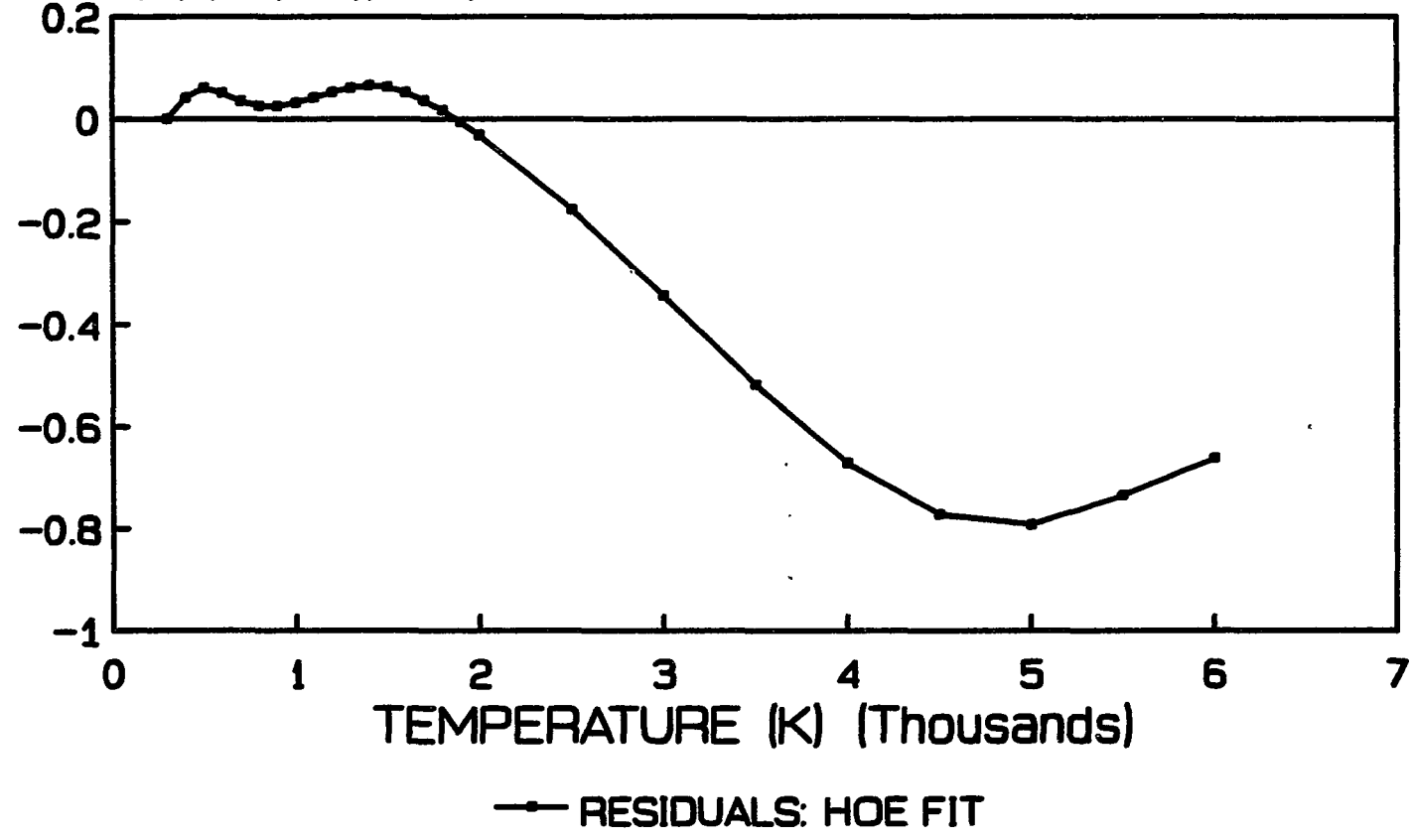
Figure 4.14e



NH3: S(T)-S(298): FIT TO HOE: RESIDUALS COMPARE LITERATURE W/ FIT

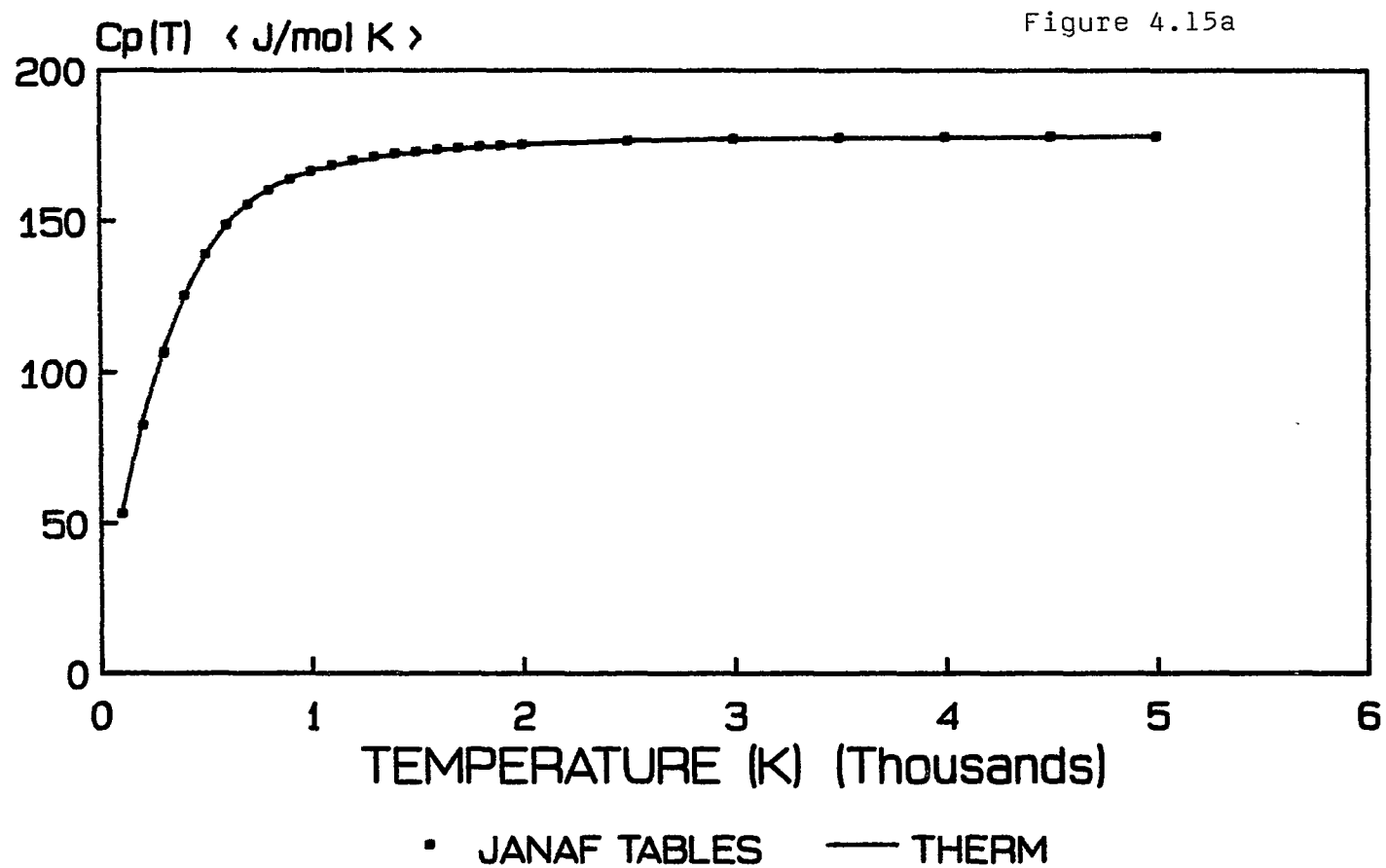
d(S(T)-S(298)) : <J/mol K>: RESIDUALS

Figure 4.14f



312

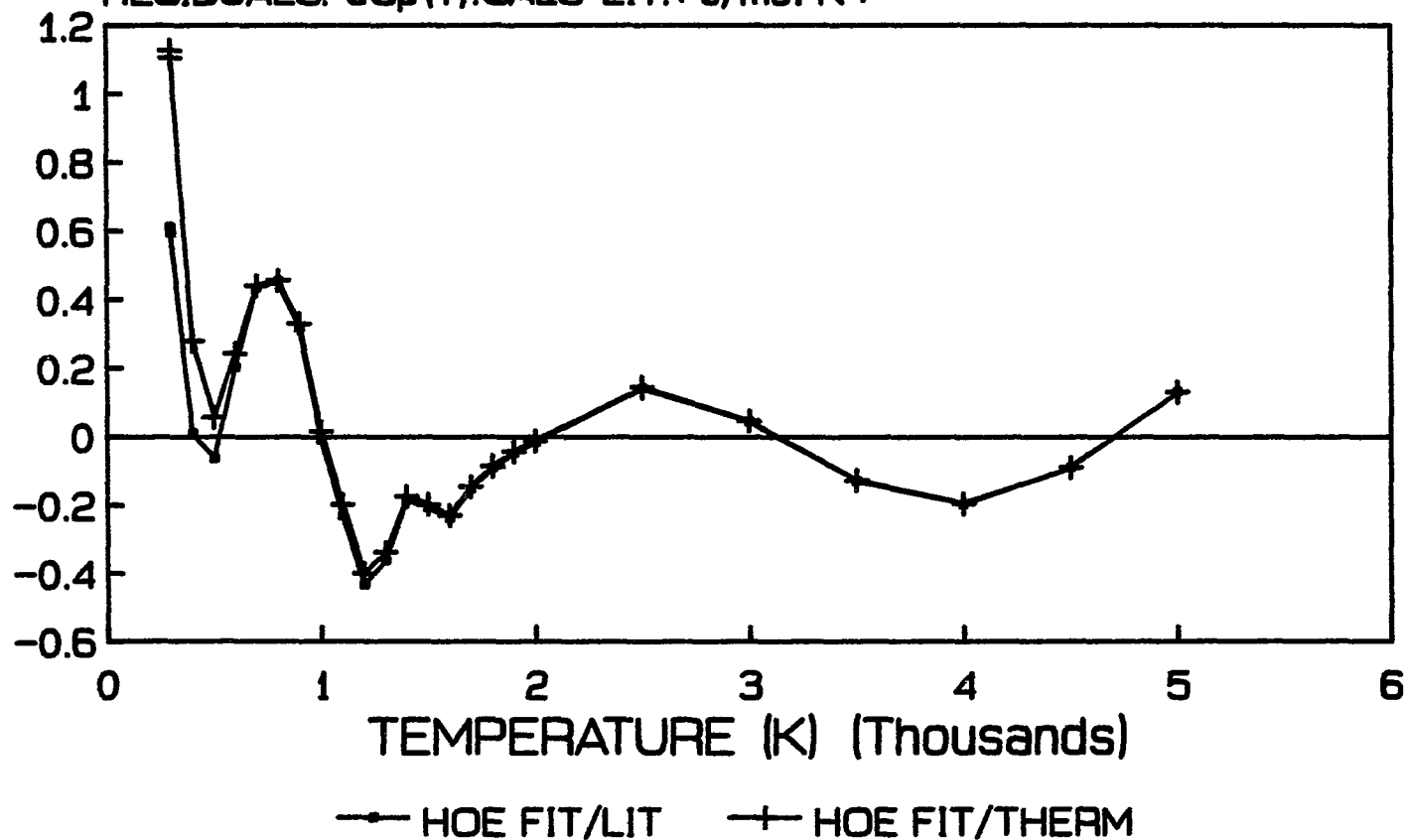
C2F6 : FIT of $C_p(T)$: LIT & ESTIMATED,
JANAF DATA vs. THERM ESTIMATE : HOE



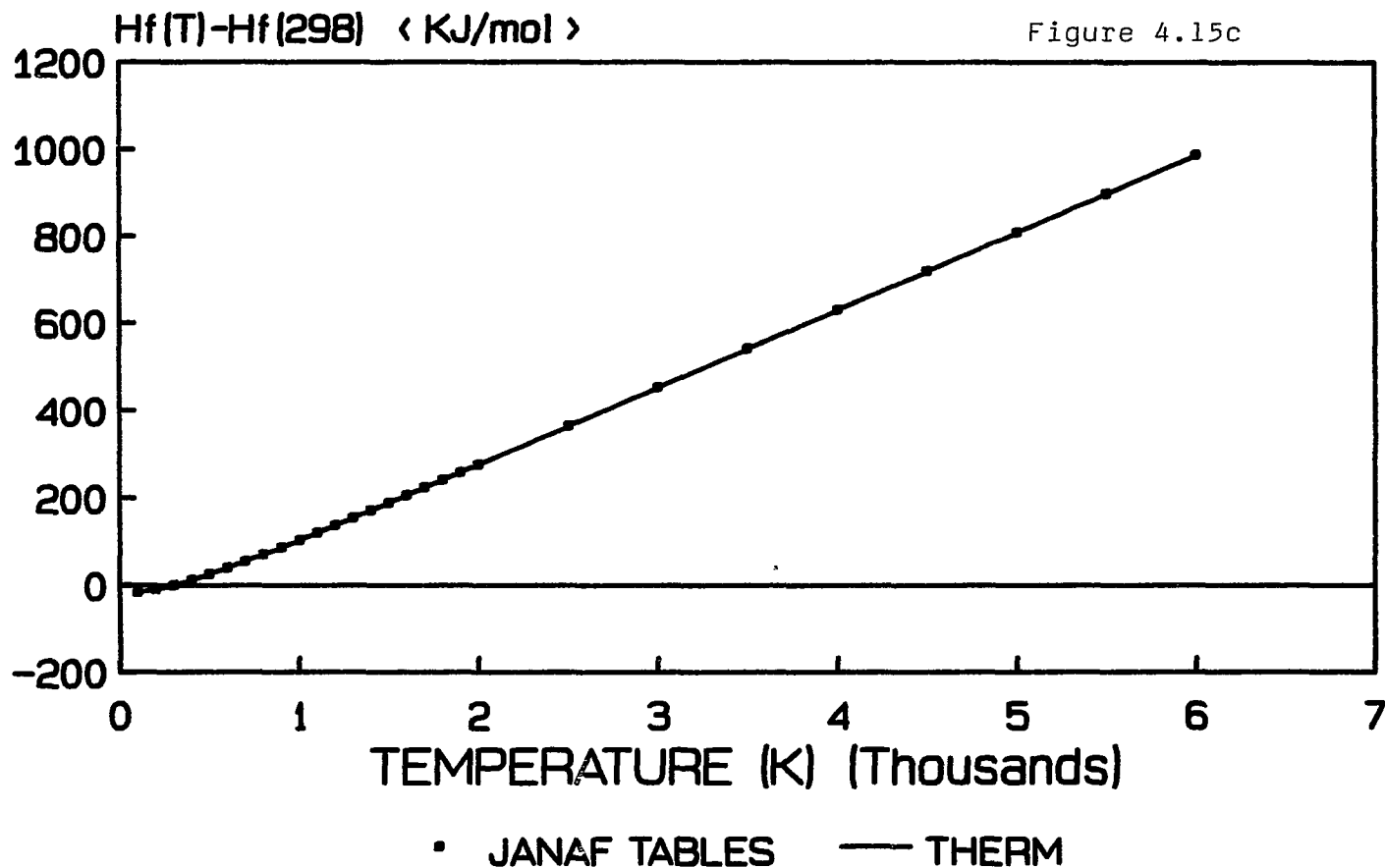
C2F6 : FIT of Cp(T) : LIT & ESTIMATED RESIDUALS : HOE FIT TO C2F6

RESIDUALS: dCp(T):CALC-LIT:< J/mol K >

Figure 4.15b

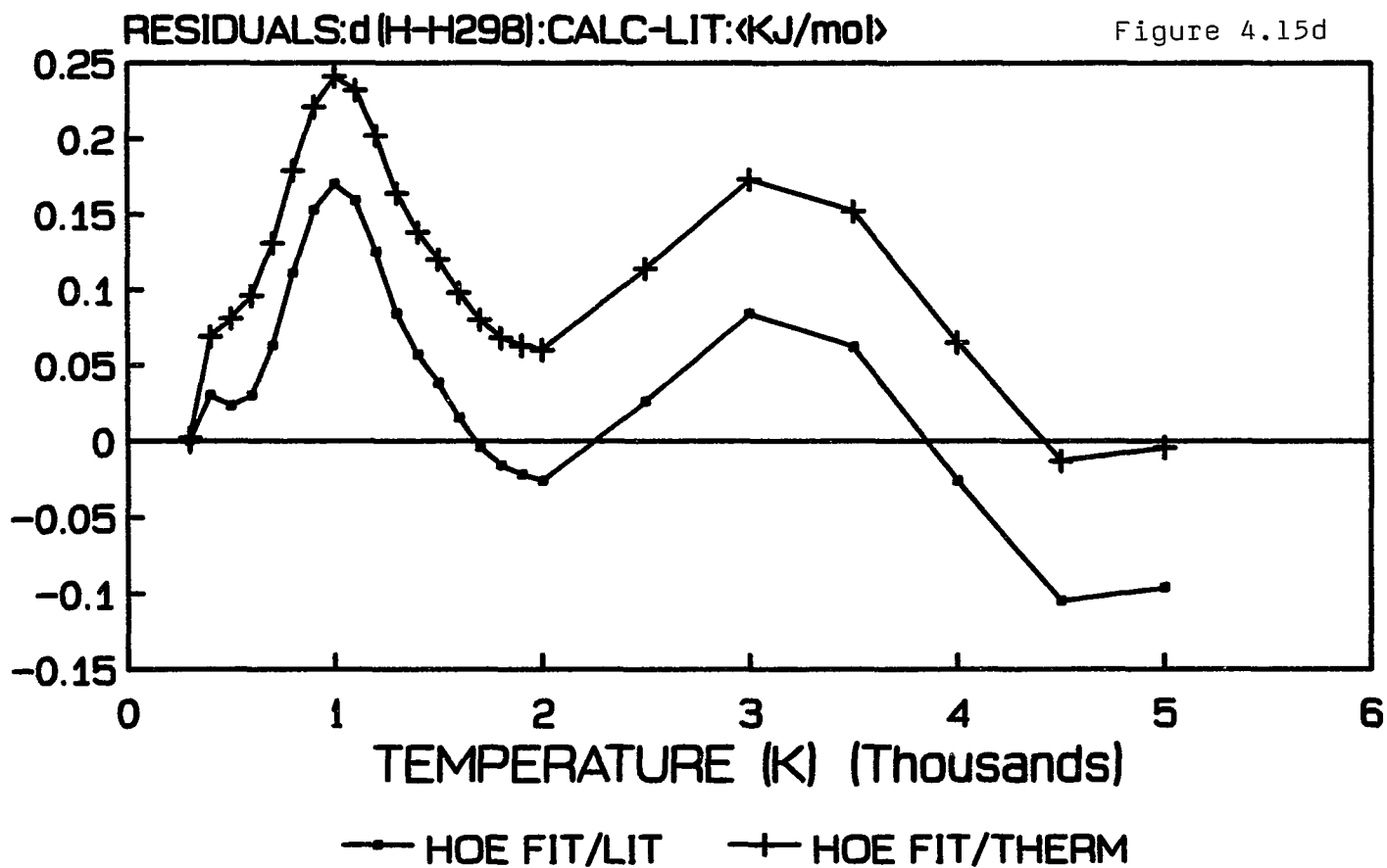


C2F6 : H(T)-H(298) : LIT & ESTIMATED
JANAF DATA vs. THERM ESTIMATE : HOE

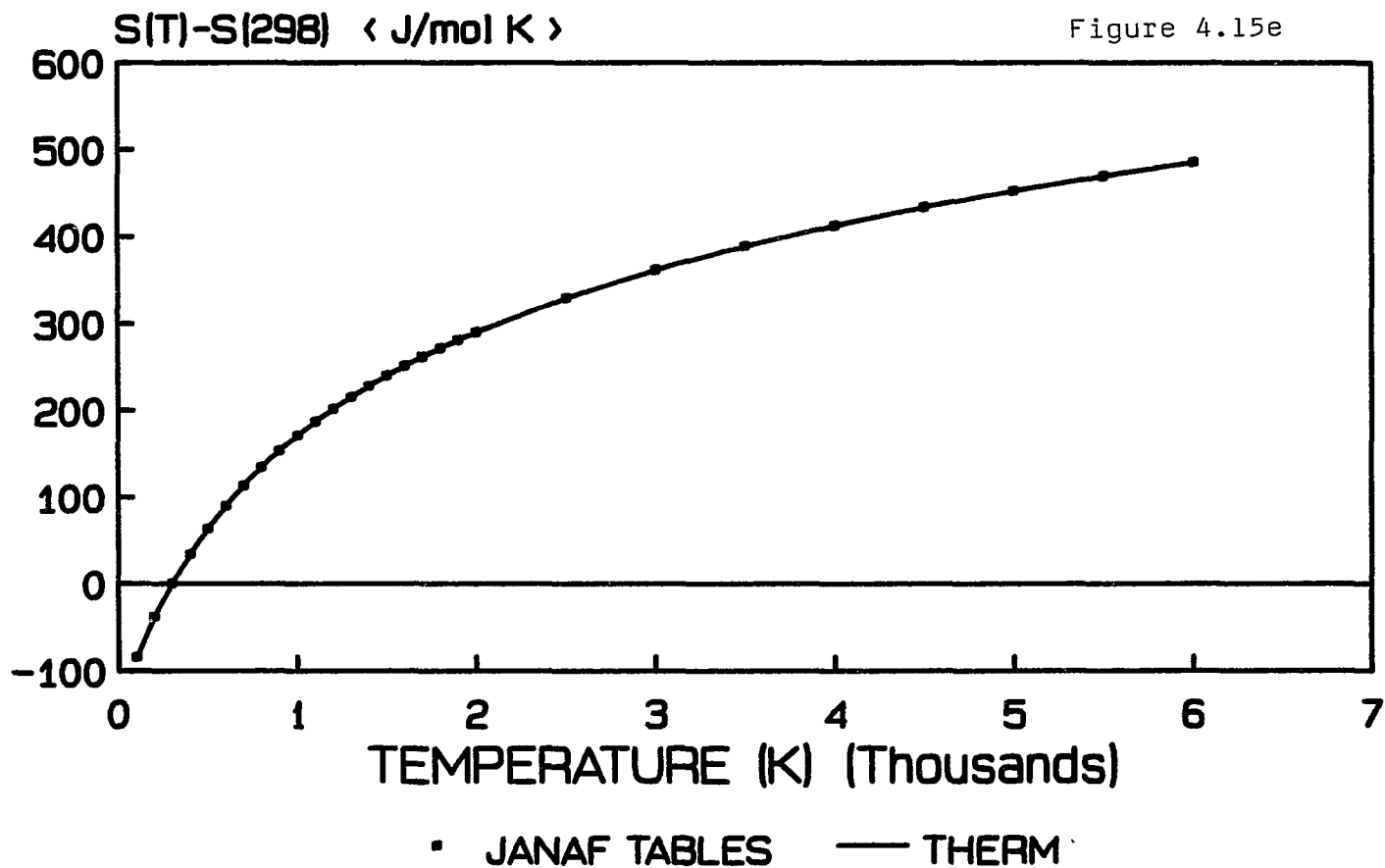


C2F6 : H(T)-H(298) : LIT & ESTIMATED
RESIDUALS : HOE FIT TO C2F6

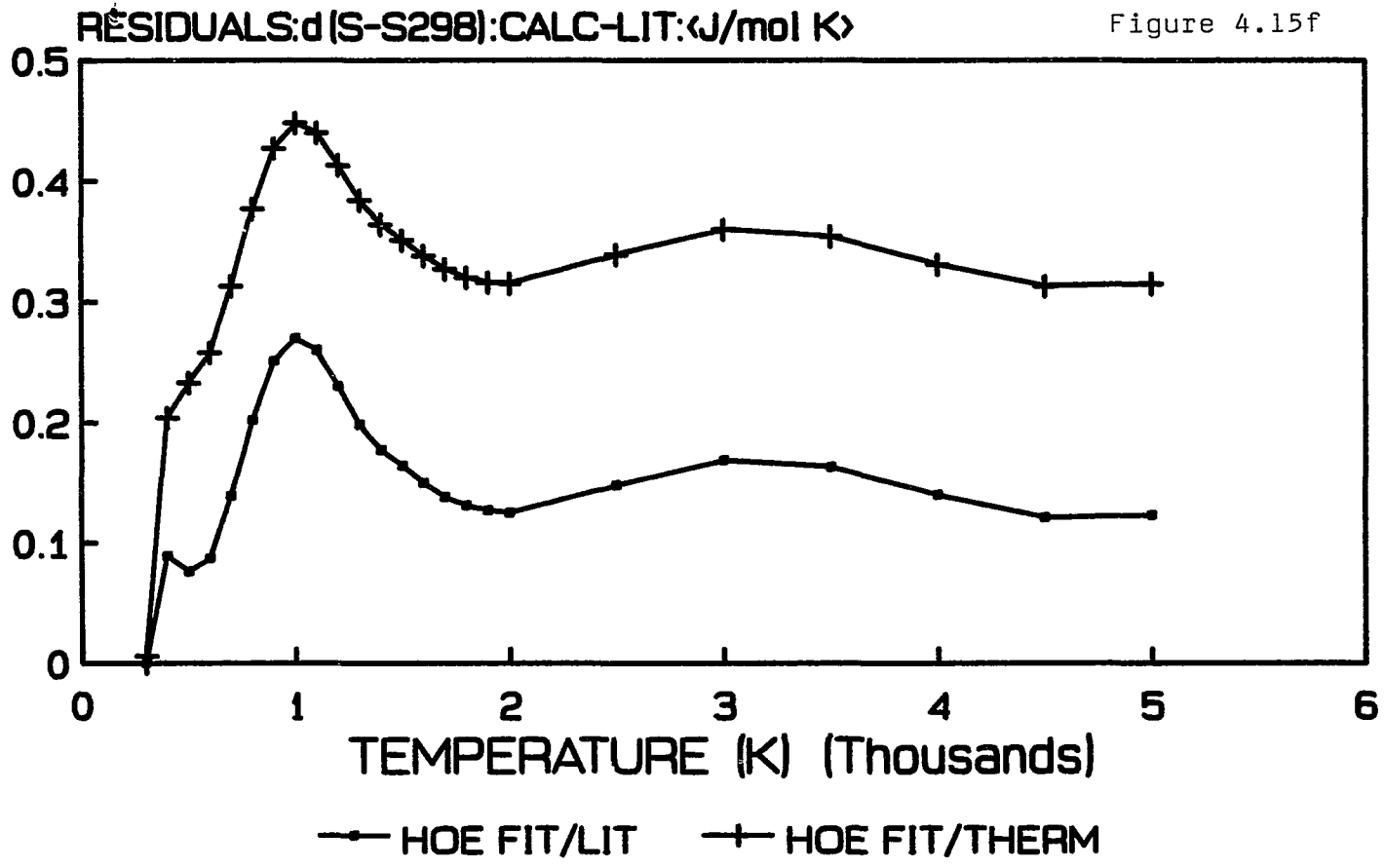
316



C2F6 : S(T)-S(298) : LIT & ESTIMATED JANAF DATA vs. THERM ESTIMATE : HOE

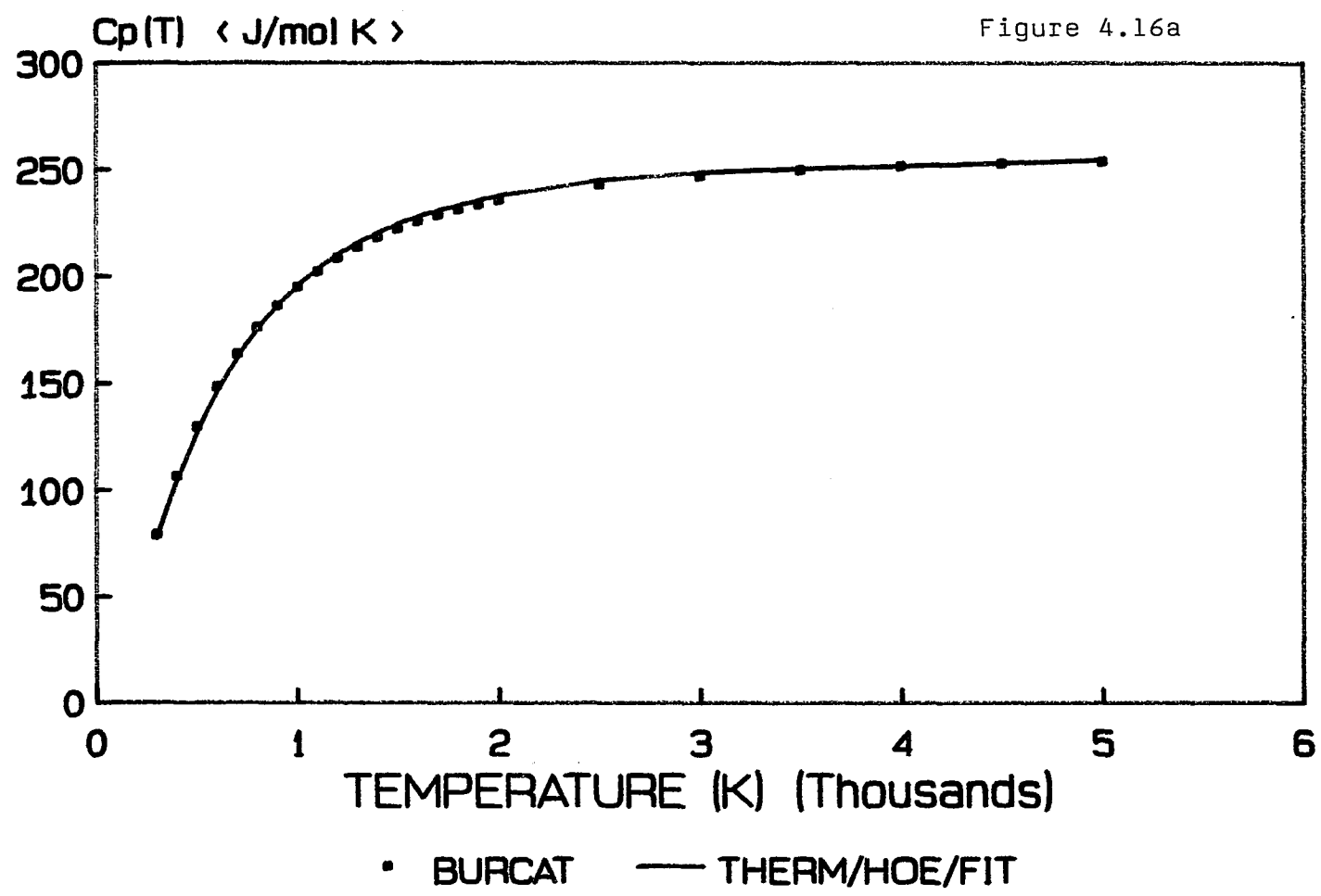


C2F6 : S(T)-S(298) : LIT & ESTIMATED RESIDUALS : HOE FIT TO C2F6

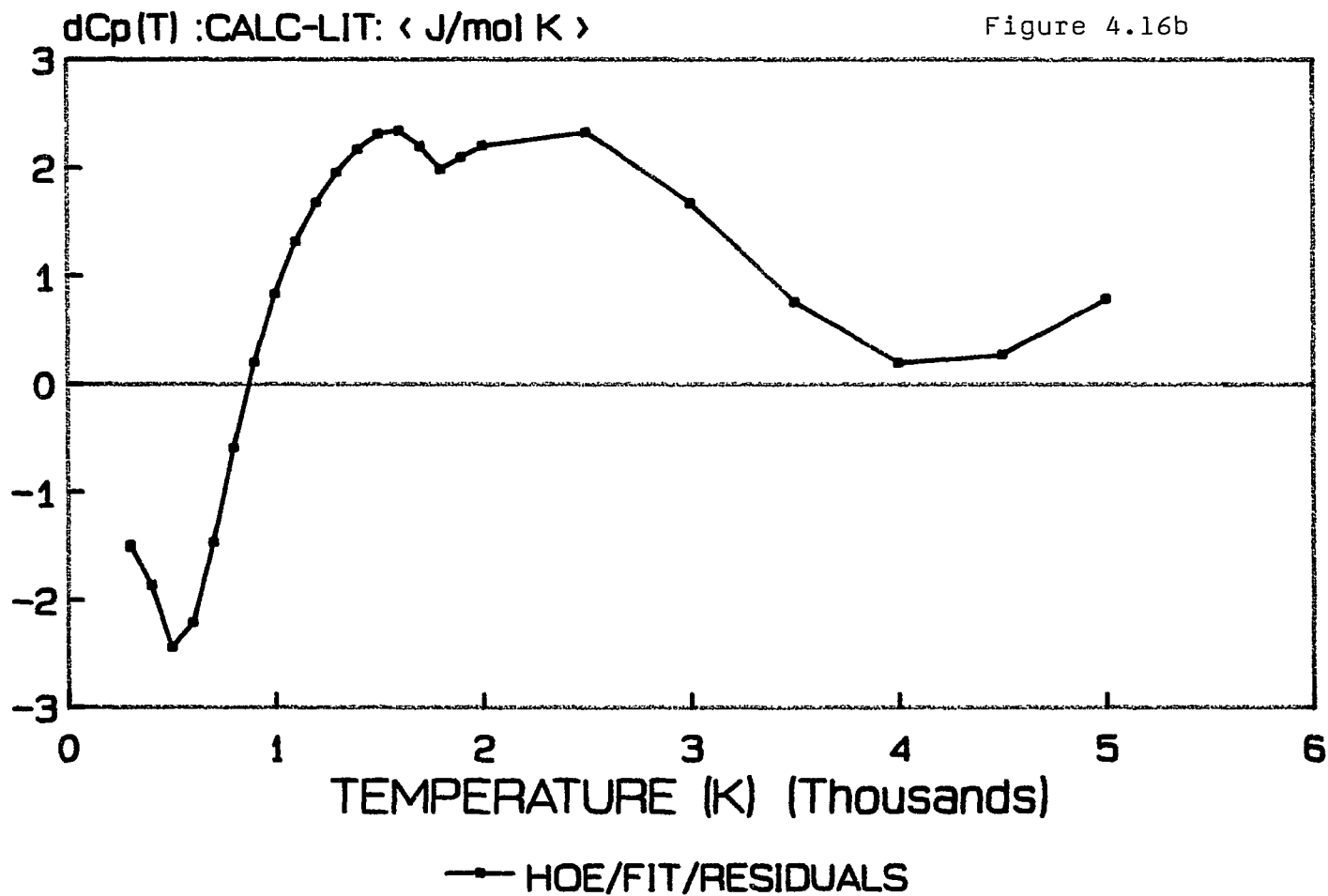


318

PHENYL : Cp (T) : FIT OF HOE

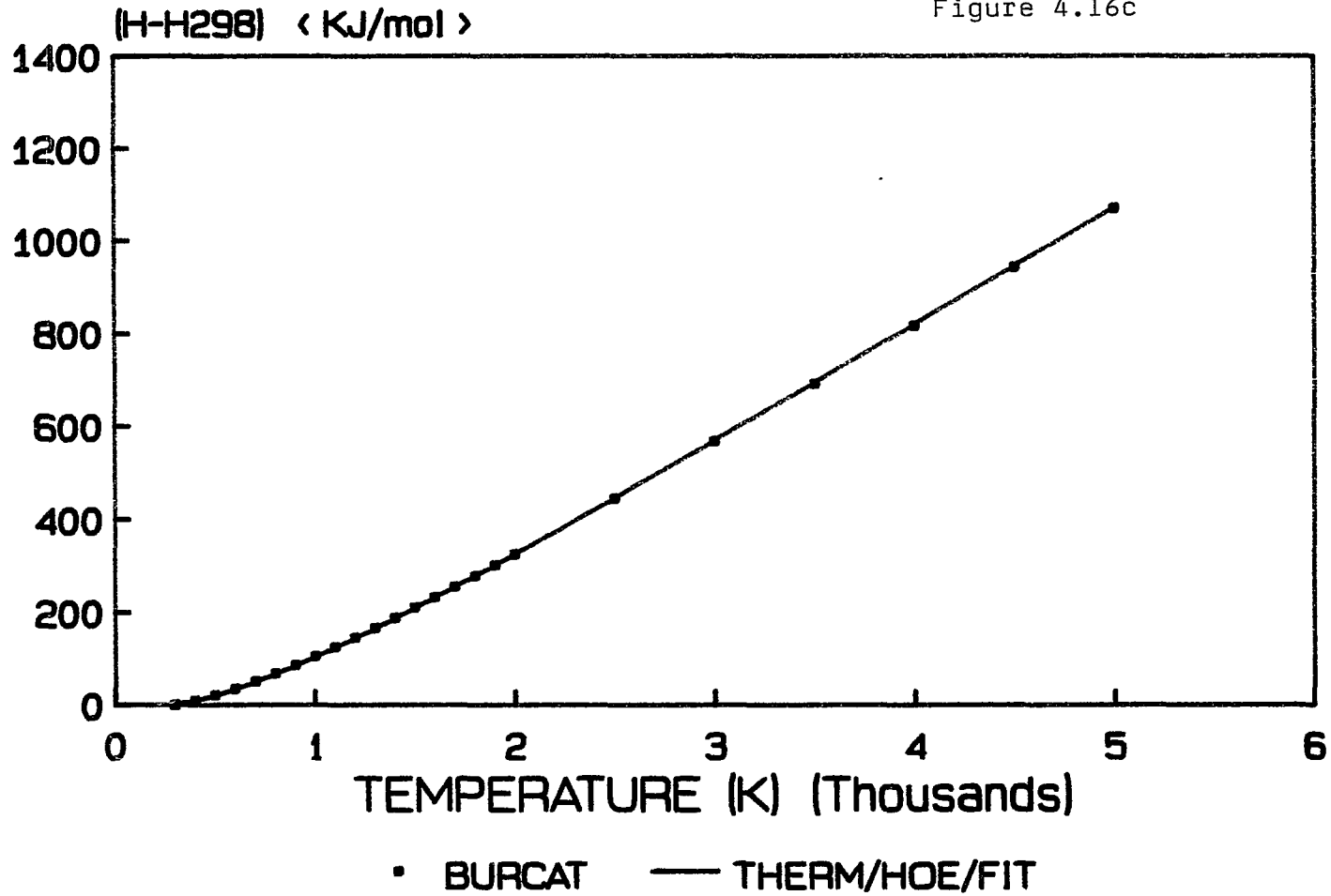


PHENYL : Cp (T) : FIT OF HOE:RESIDUALS

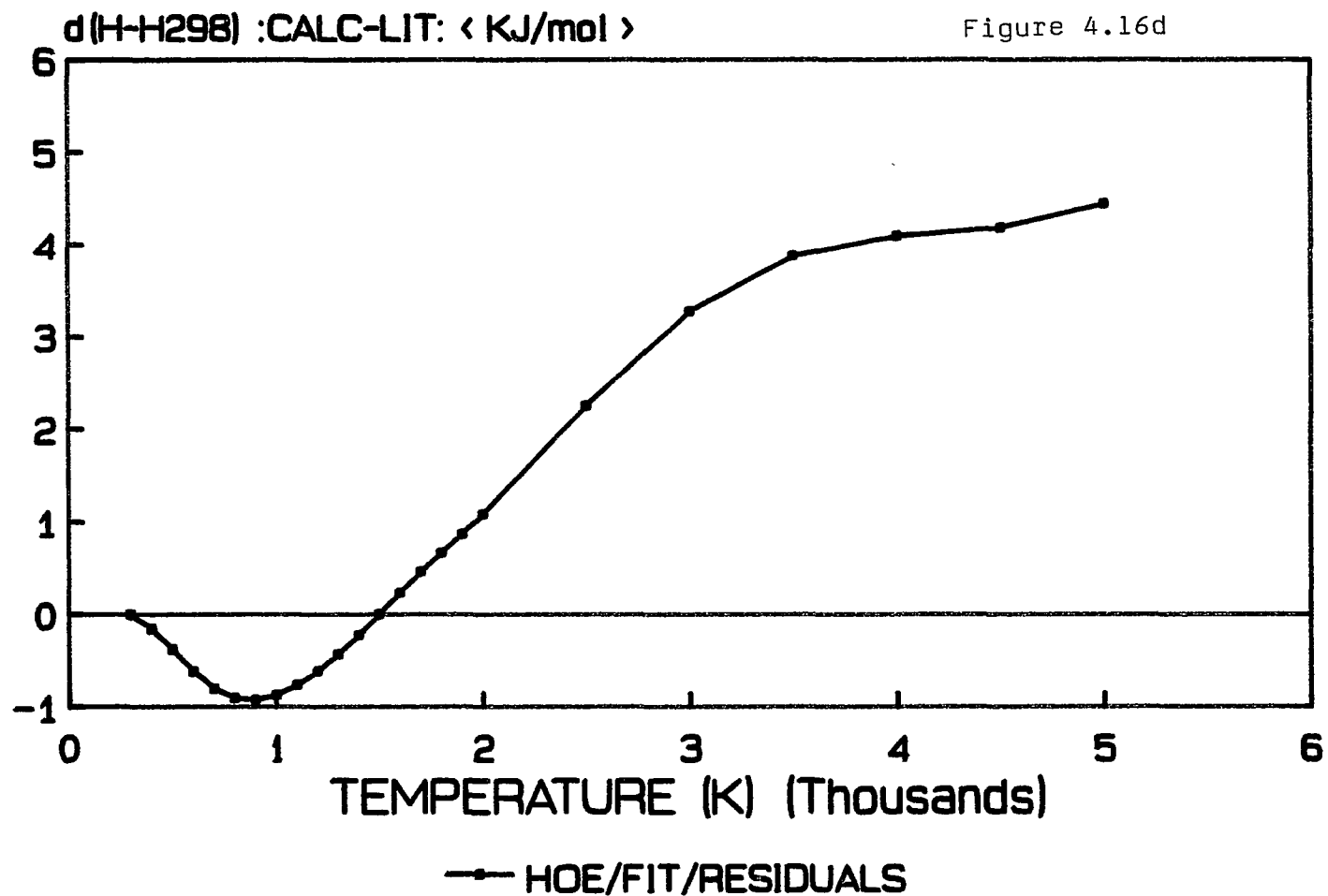


PHENYL: H-H298 : FIT OF HOE

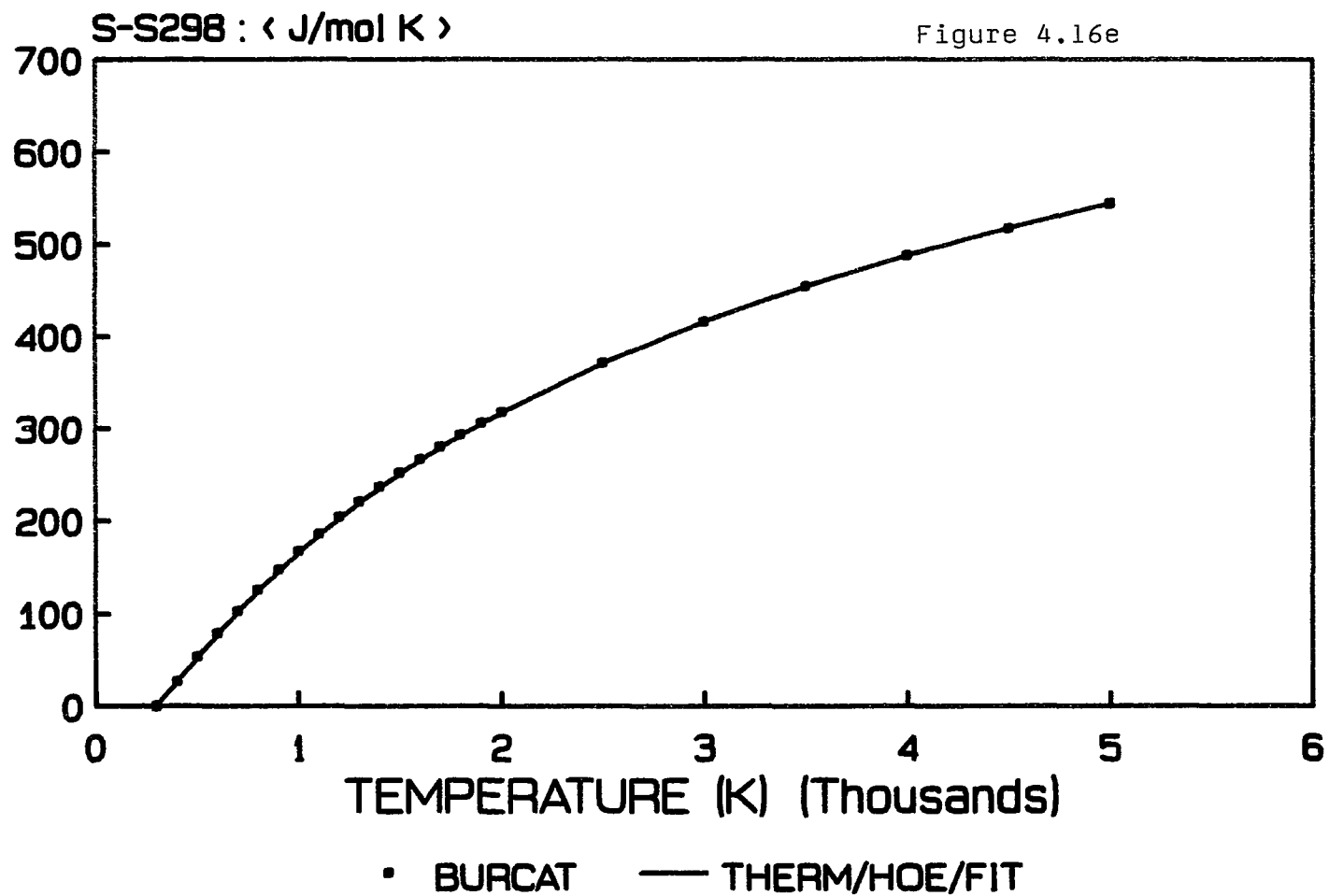
Figure 4.16c



PHENYL: H-H298 : FIT OF HOE:RESIDUALS



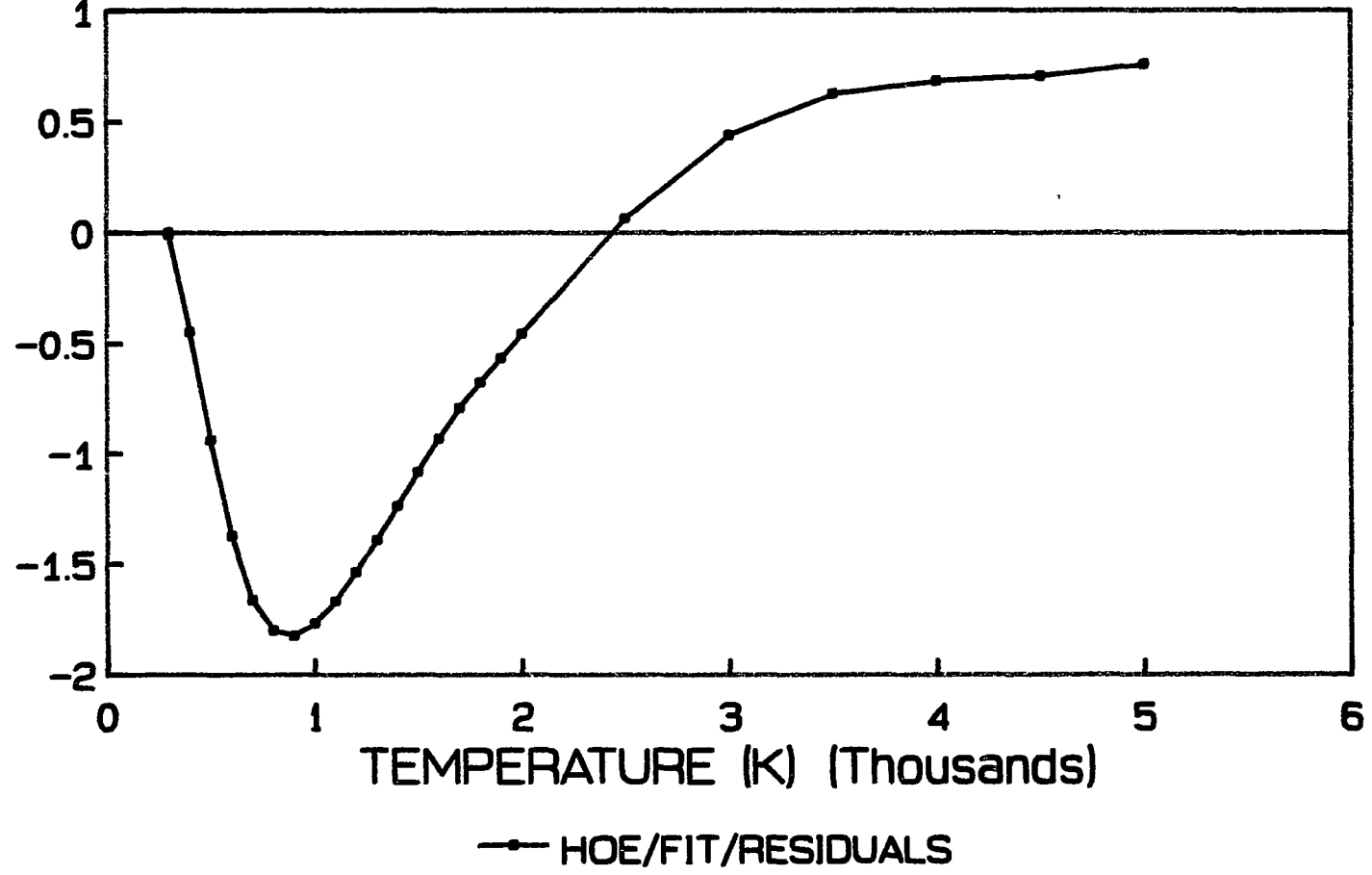
PHENYL : S-S298 : FIT OF HOE



PHENYL: S-S298 : FIT OF HOE:RESIDUALS

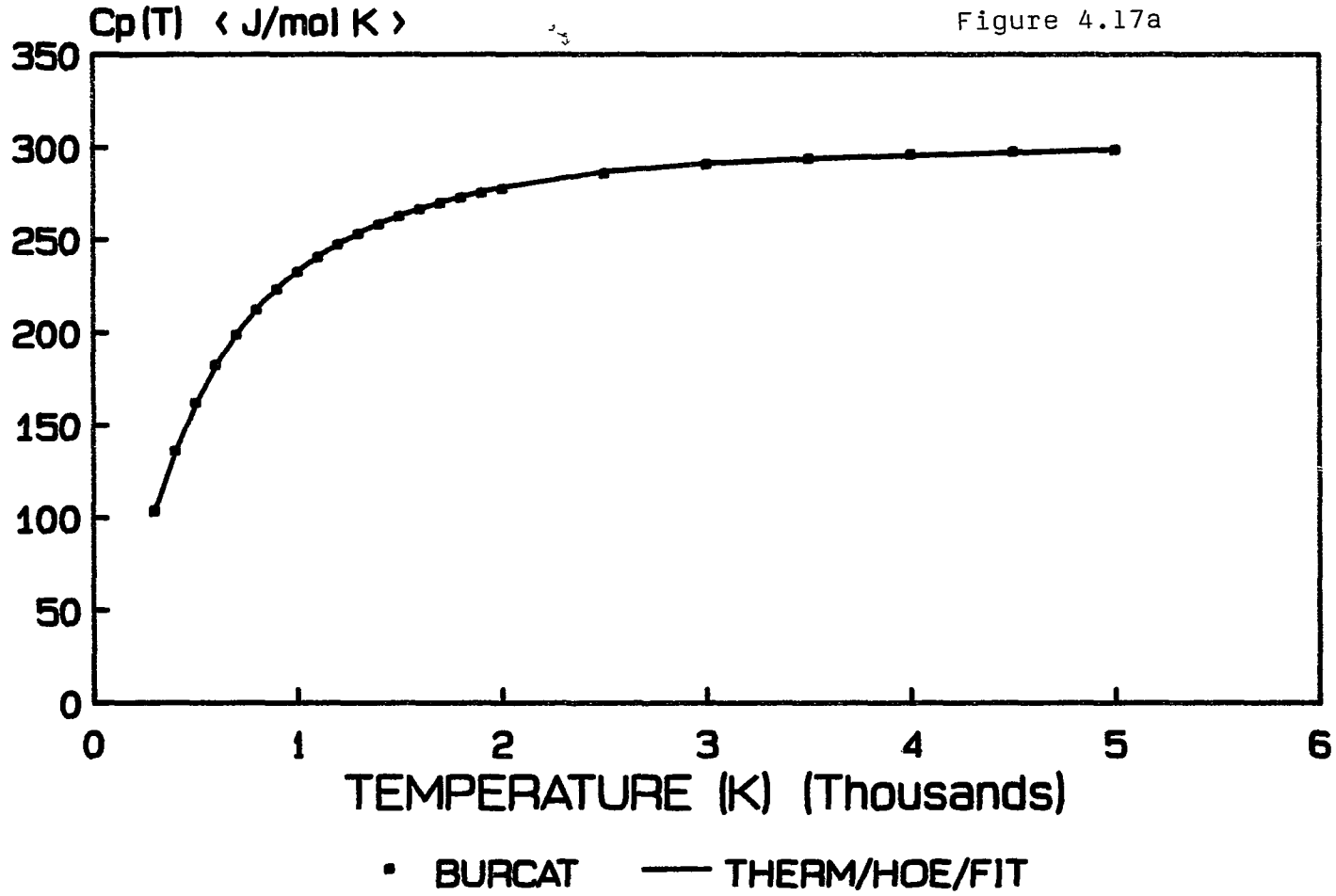
d(S-S298) :CALC-LIT: < J/mol K >

Figure 4.16f



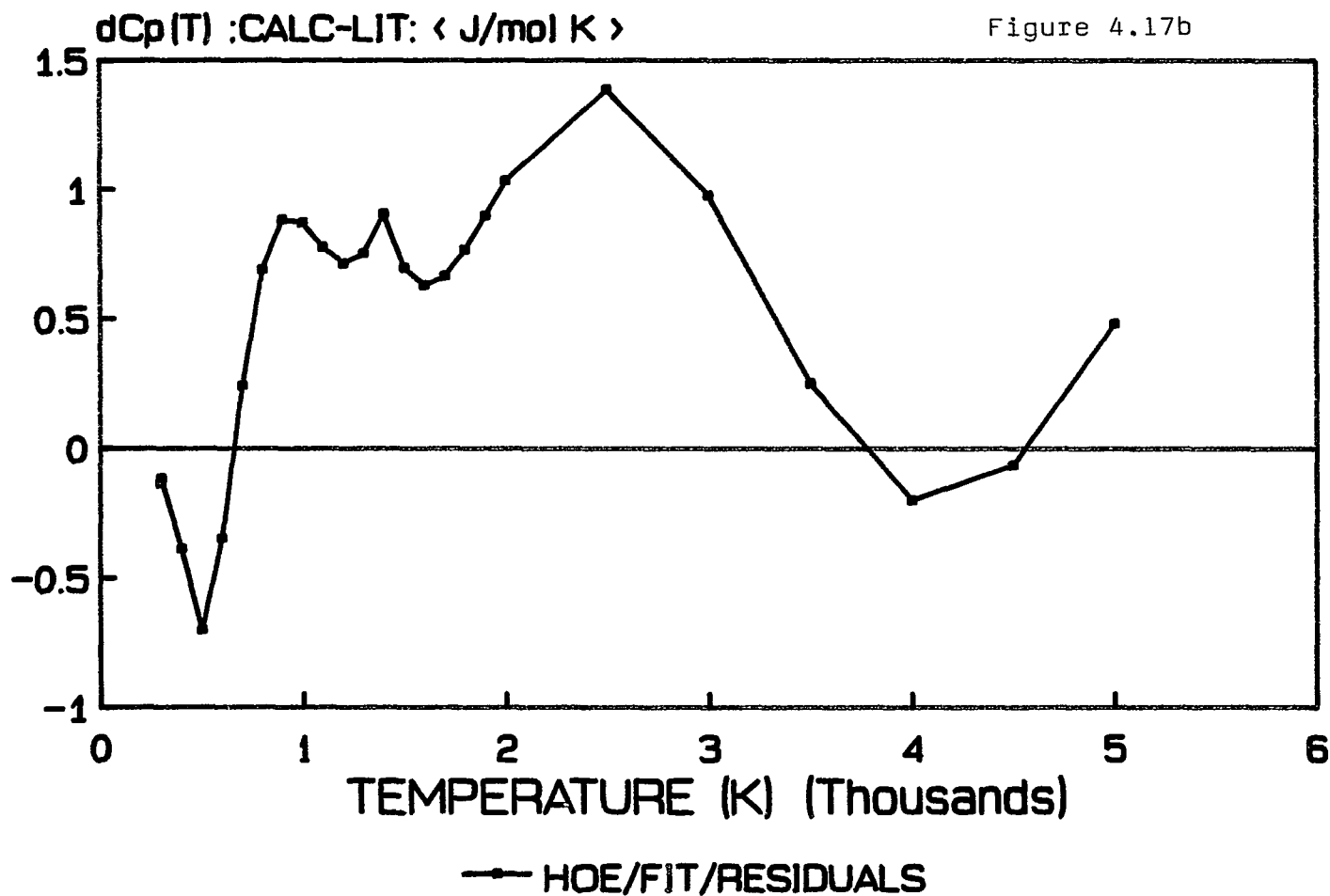
324

PHENOL : Cp (T) : FIT OF HOE

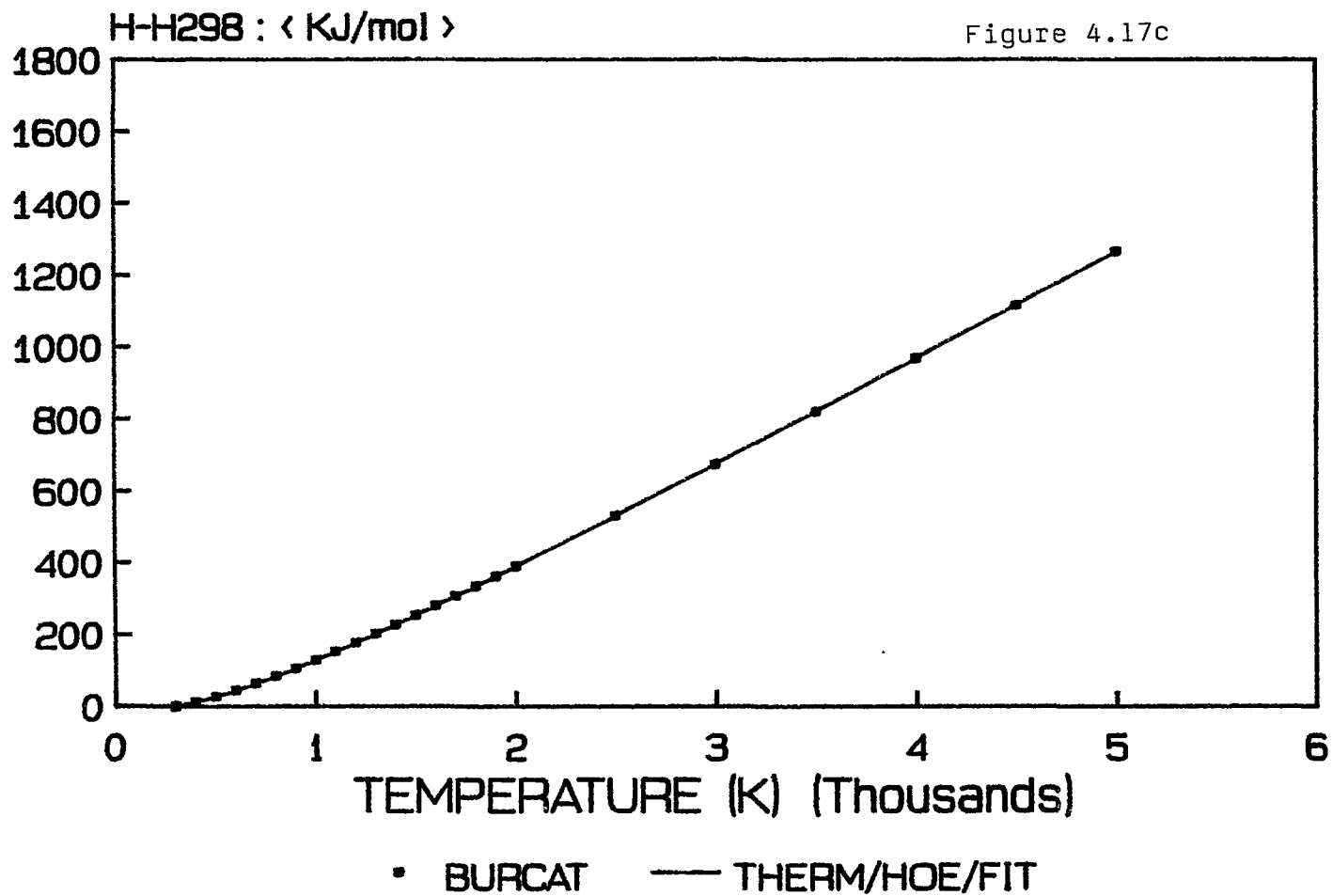


325

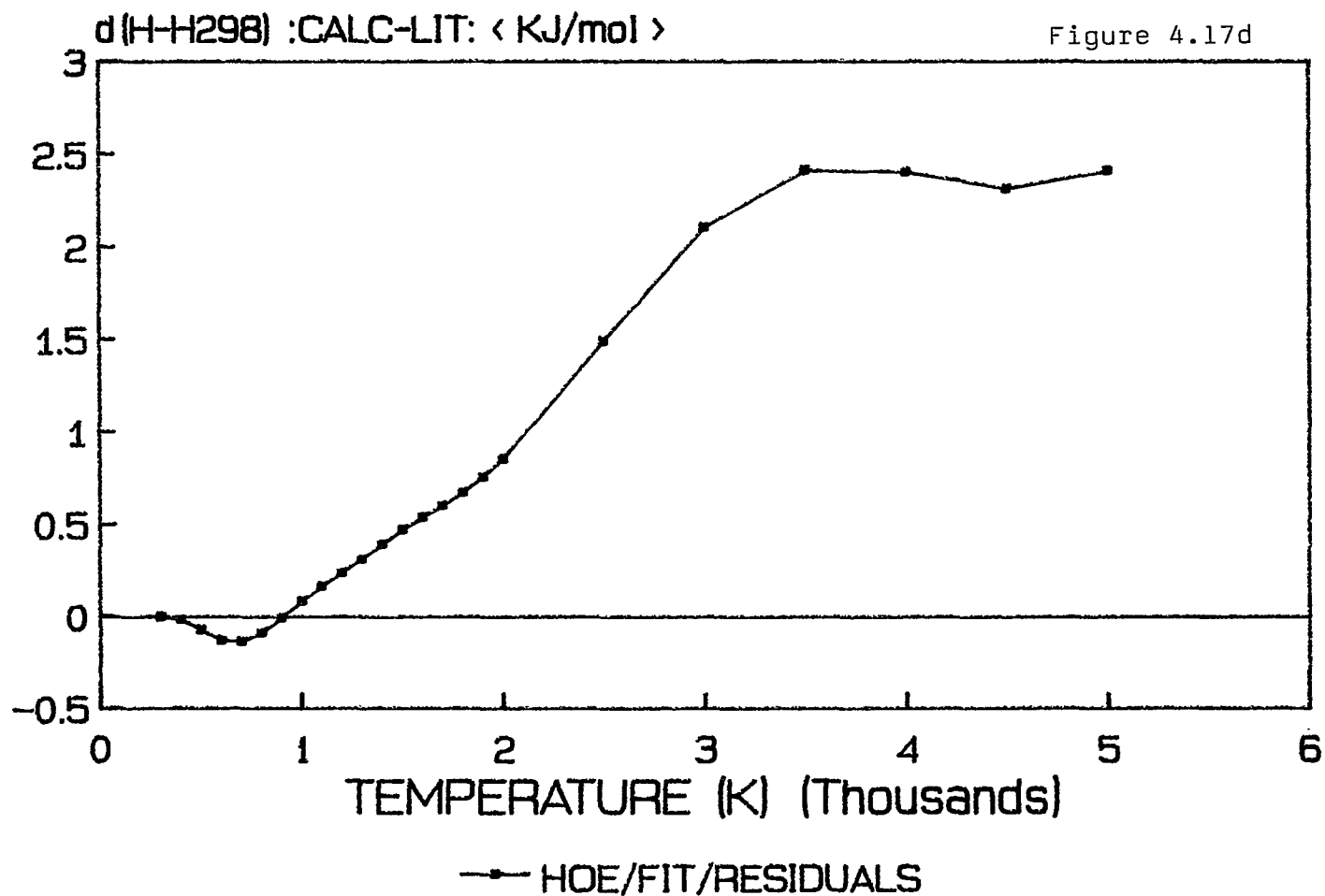
PHENOL : $C_p(T)$: FIT OF HOE:RESIDUALS



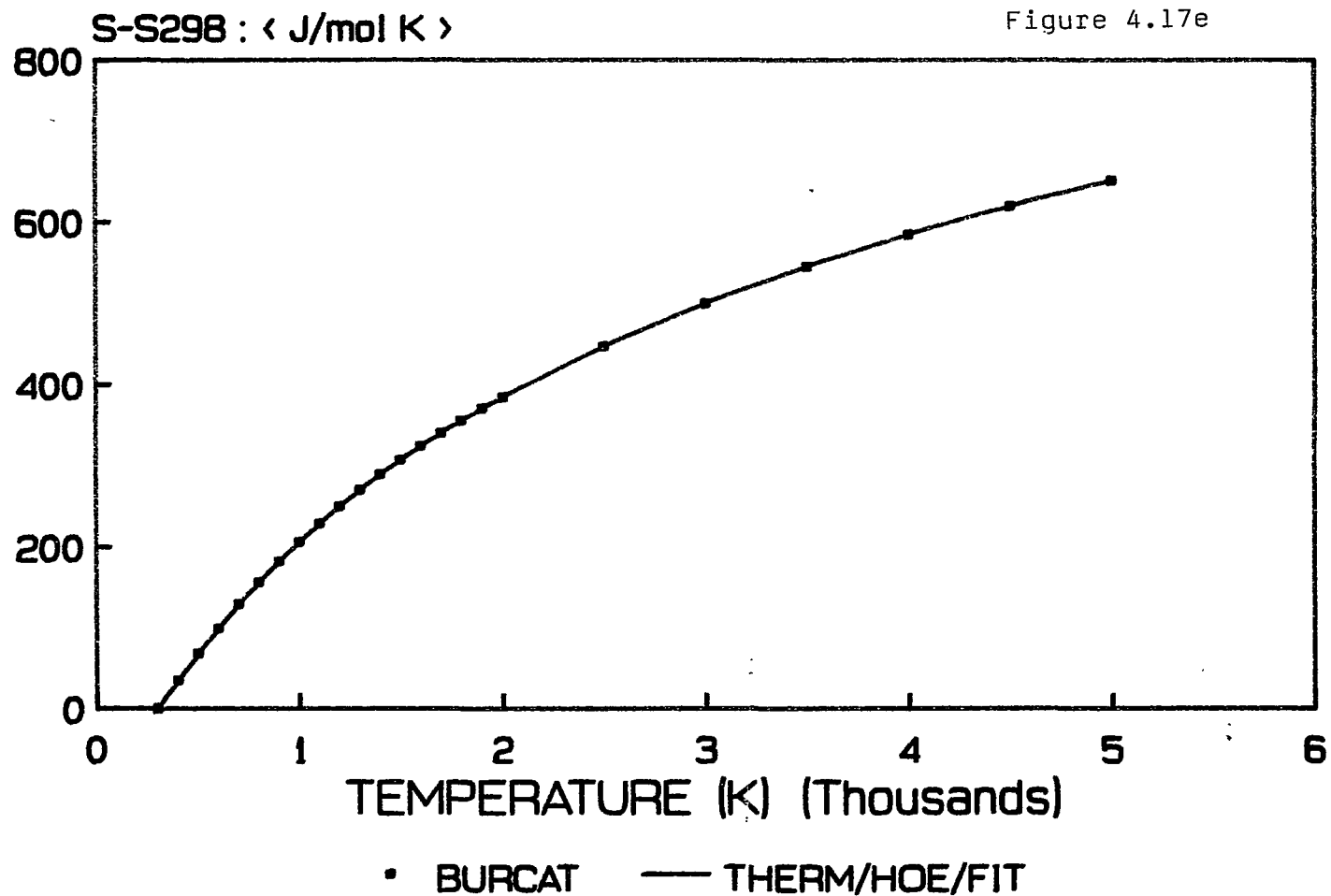
PHENOL : H-H298 : FIT OF HOE



PHENOL: H-H298 : FIT OF HOE:RESIDUALS



PHENOL : S-S298 : FIT OF HOE

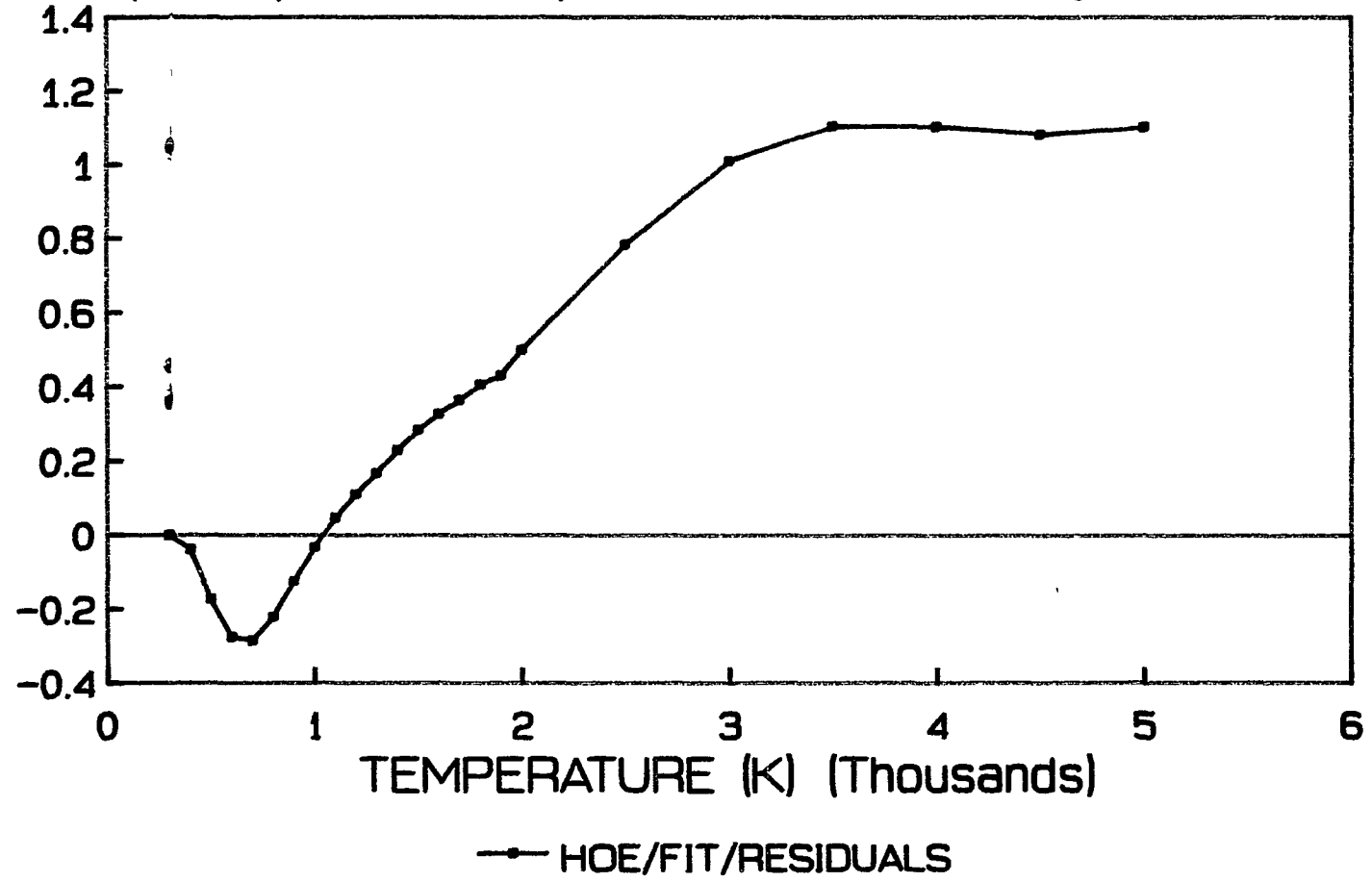


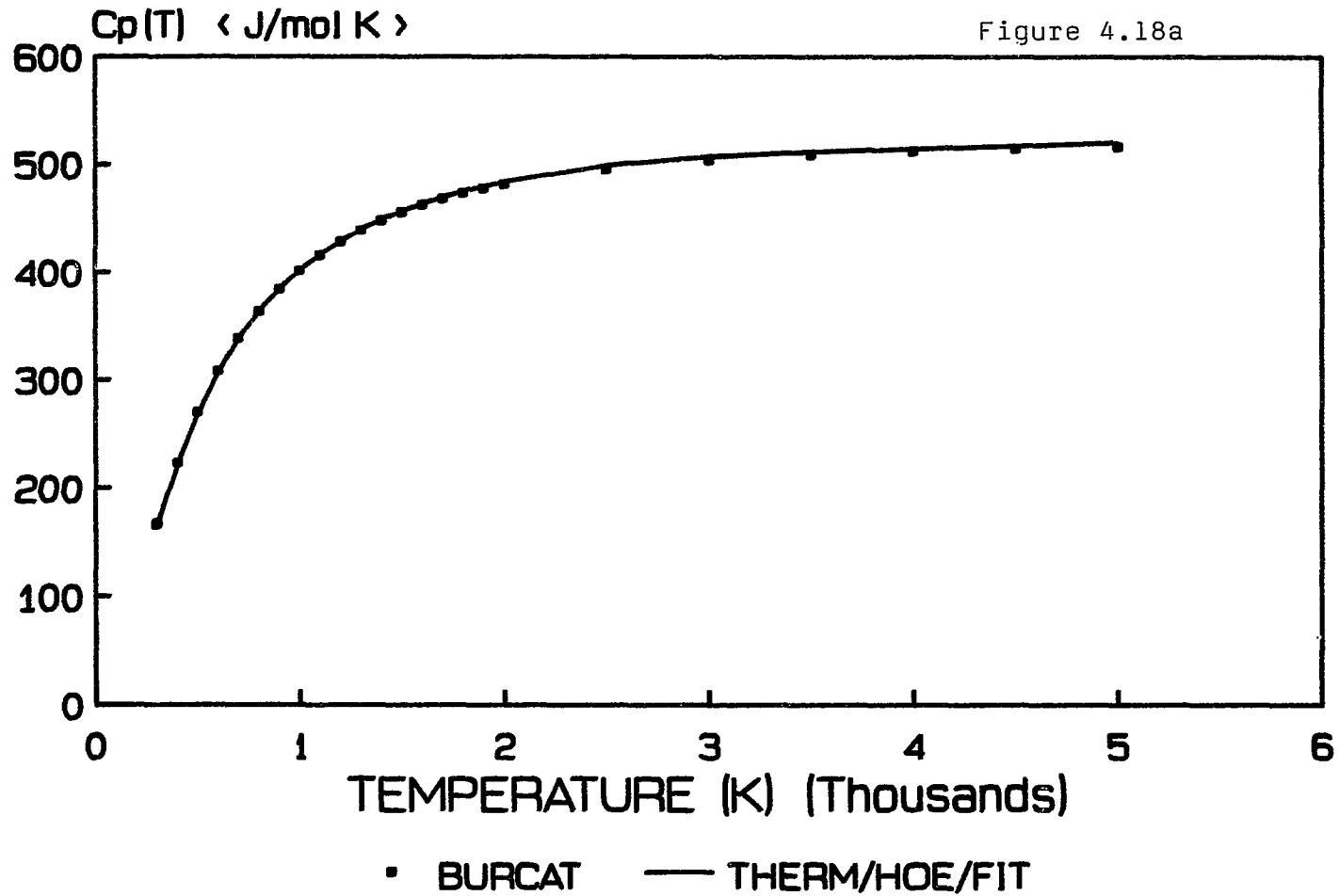
PHENOL: S-S298 : FIT OF HOE:RESIDUALS

d(S-S298) :CALC-LIT: < J/mol K >

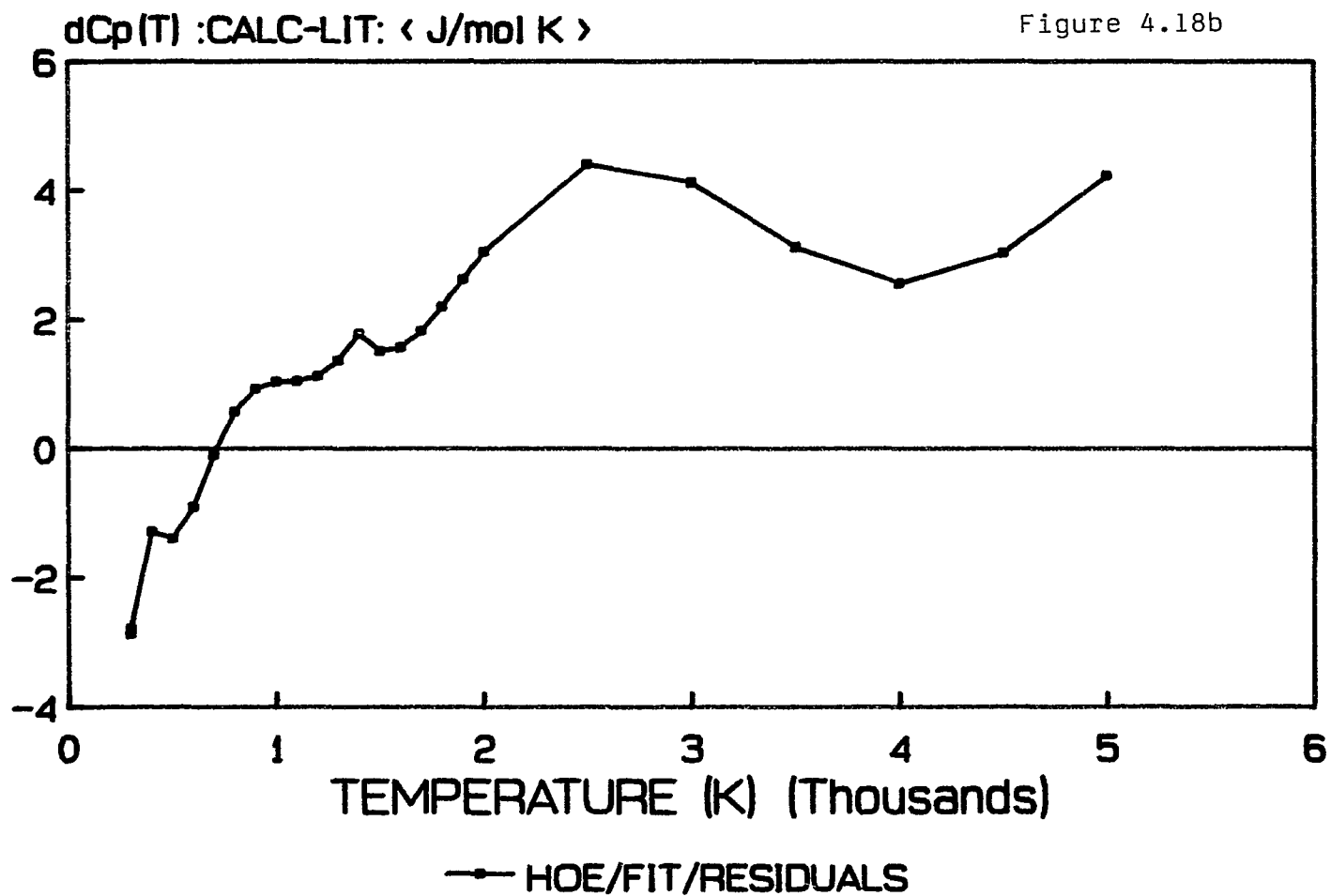
Figure 4.17f

330

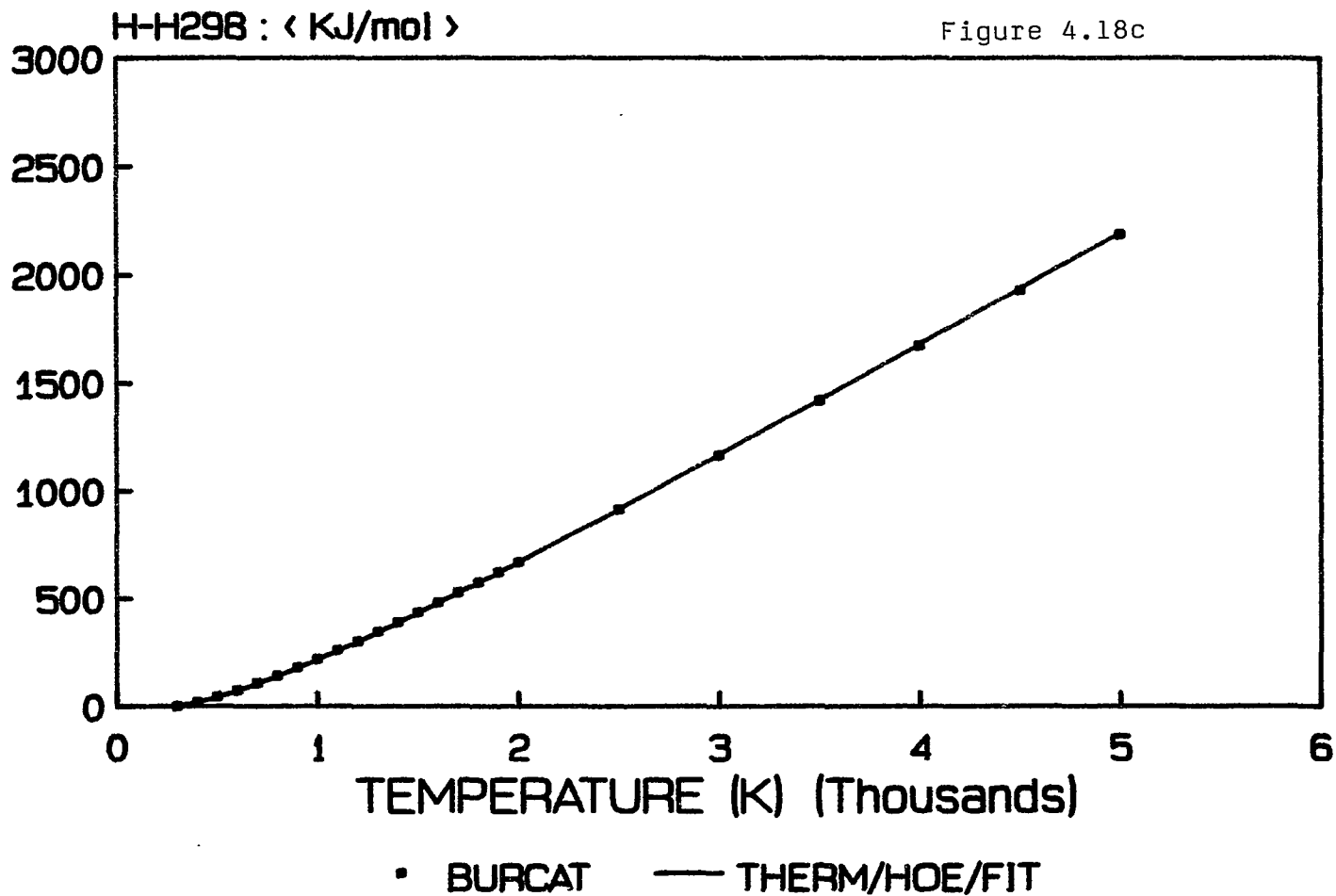


BIPHENYL : $C_p(T)$: FIT OF HOE

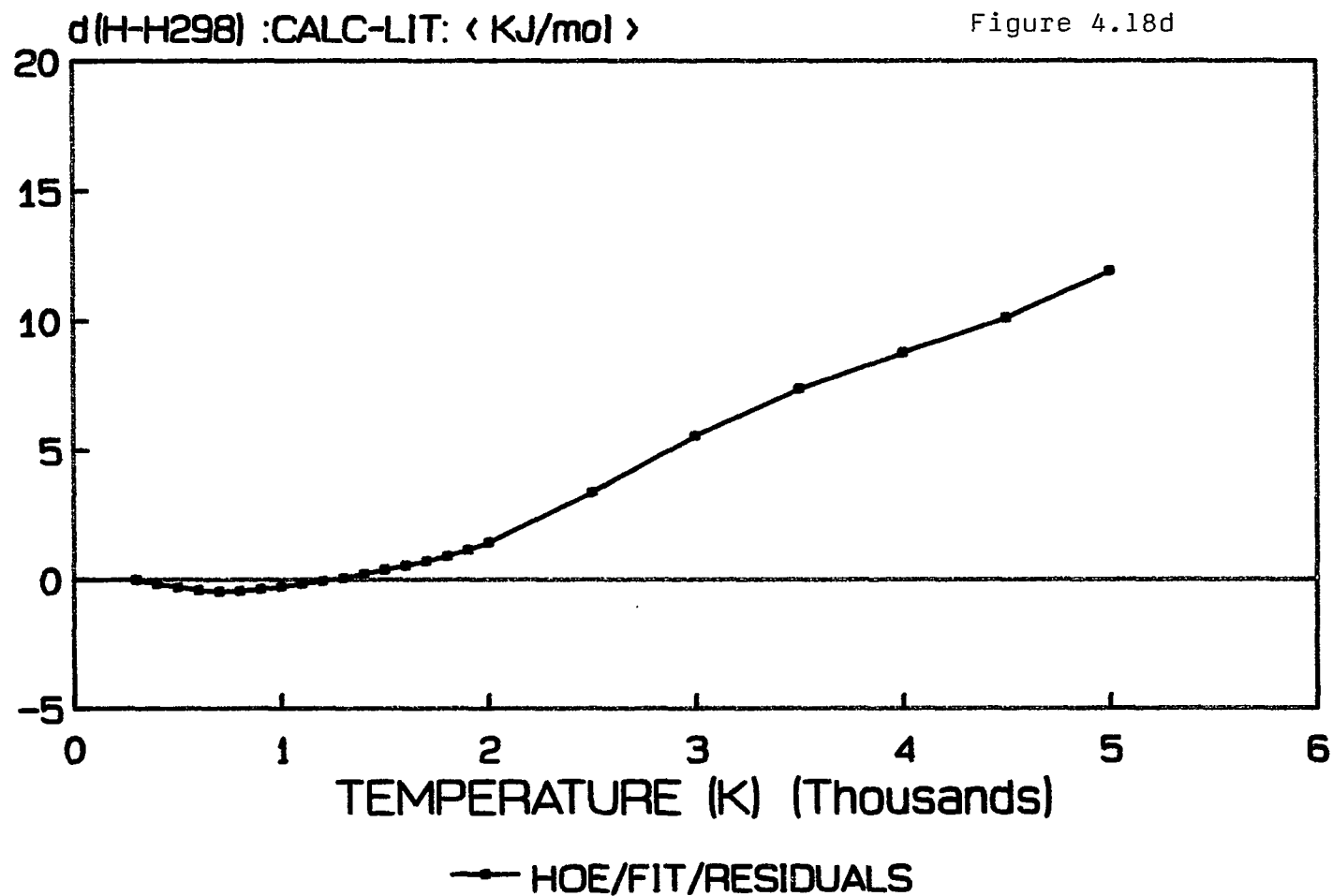
BIPHENYL : $C_p(T)$: FIT OF HOE:RESIDUALS



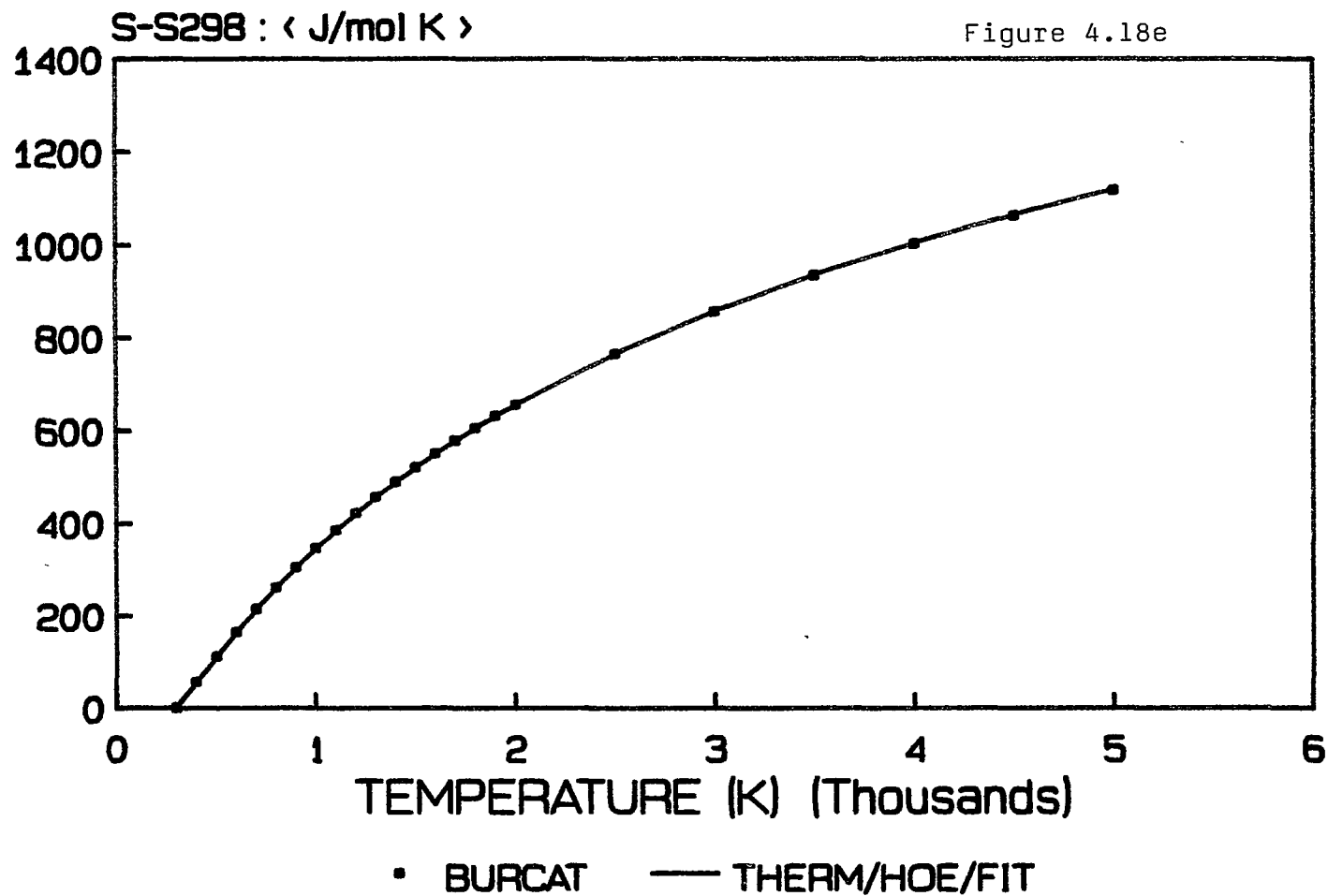
BIPHENYL : H-H298 : FIT OF HOE



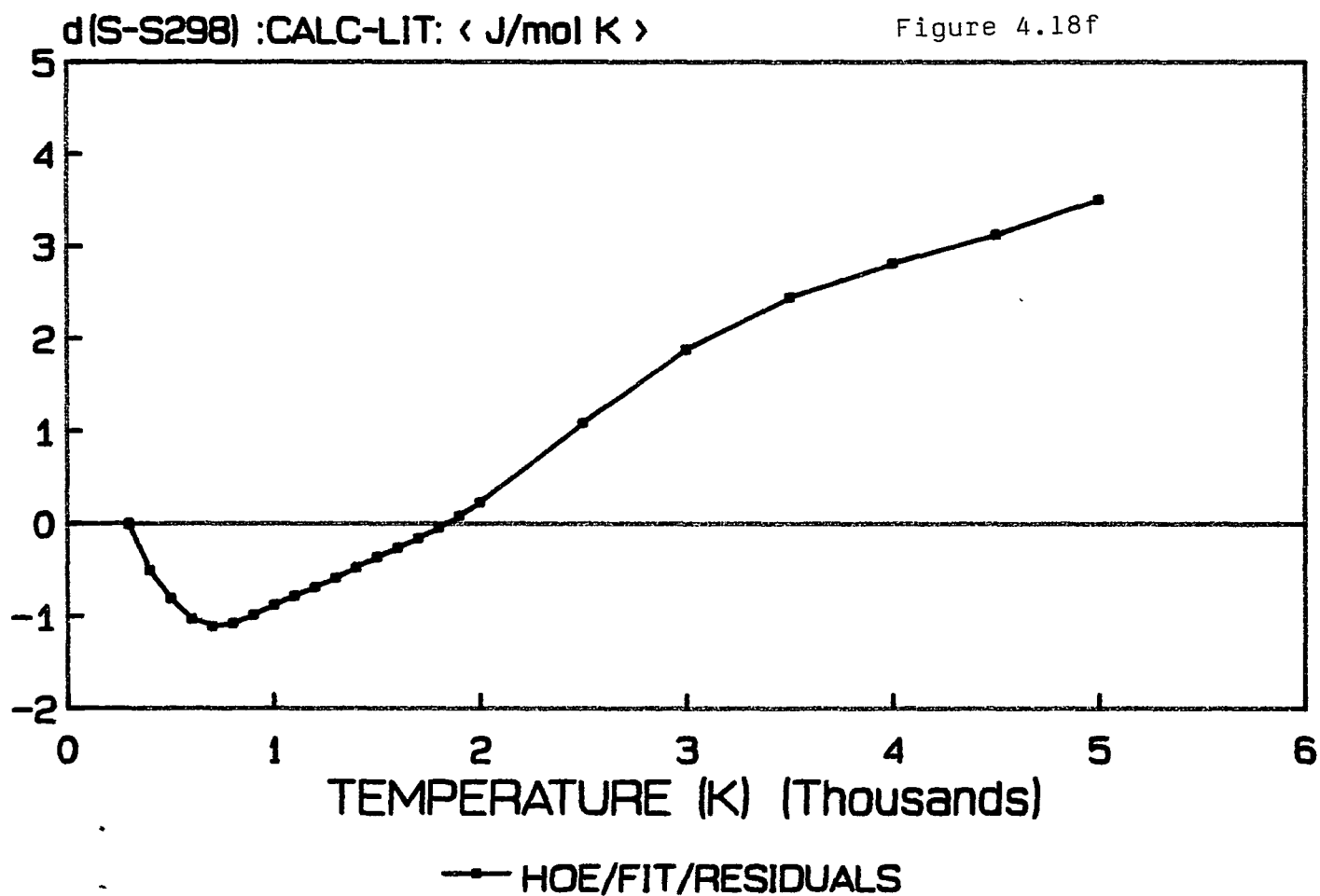
BIPHENYL: H-H298 : FIT OF HOE:RESIDUALS



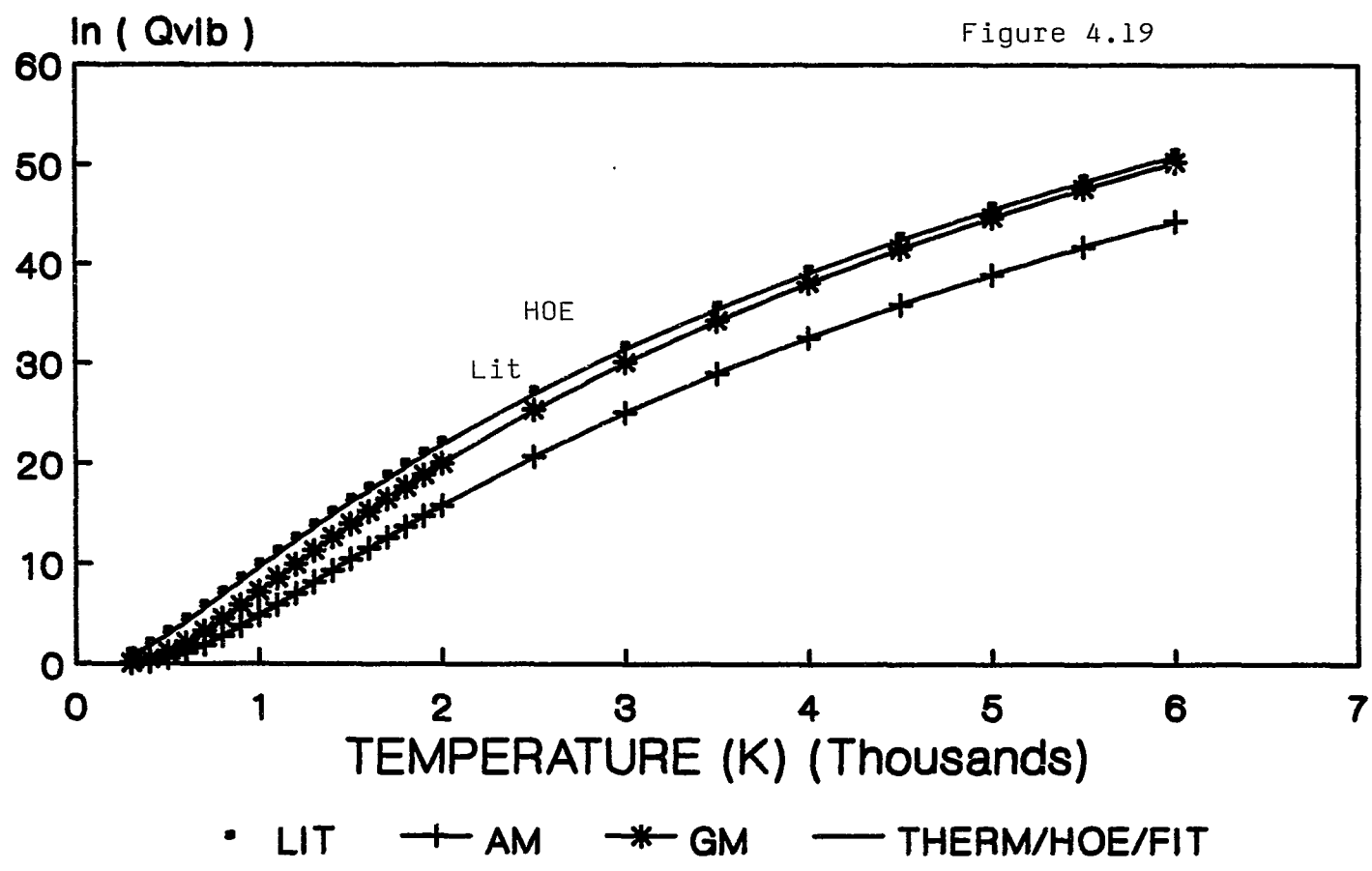
BIPHENYL : S-S298 : FIT OF HOE



BIPHENYL: S-S298 : FIT OF HOE:RESIDUALS

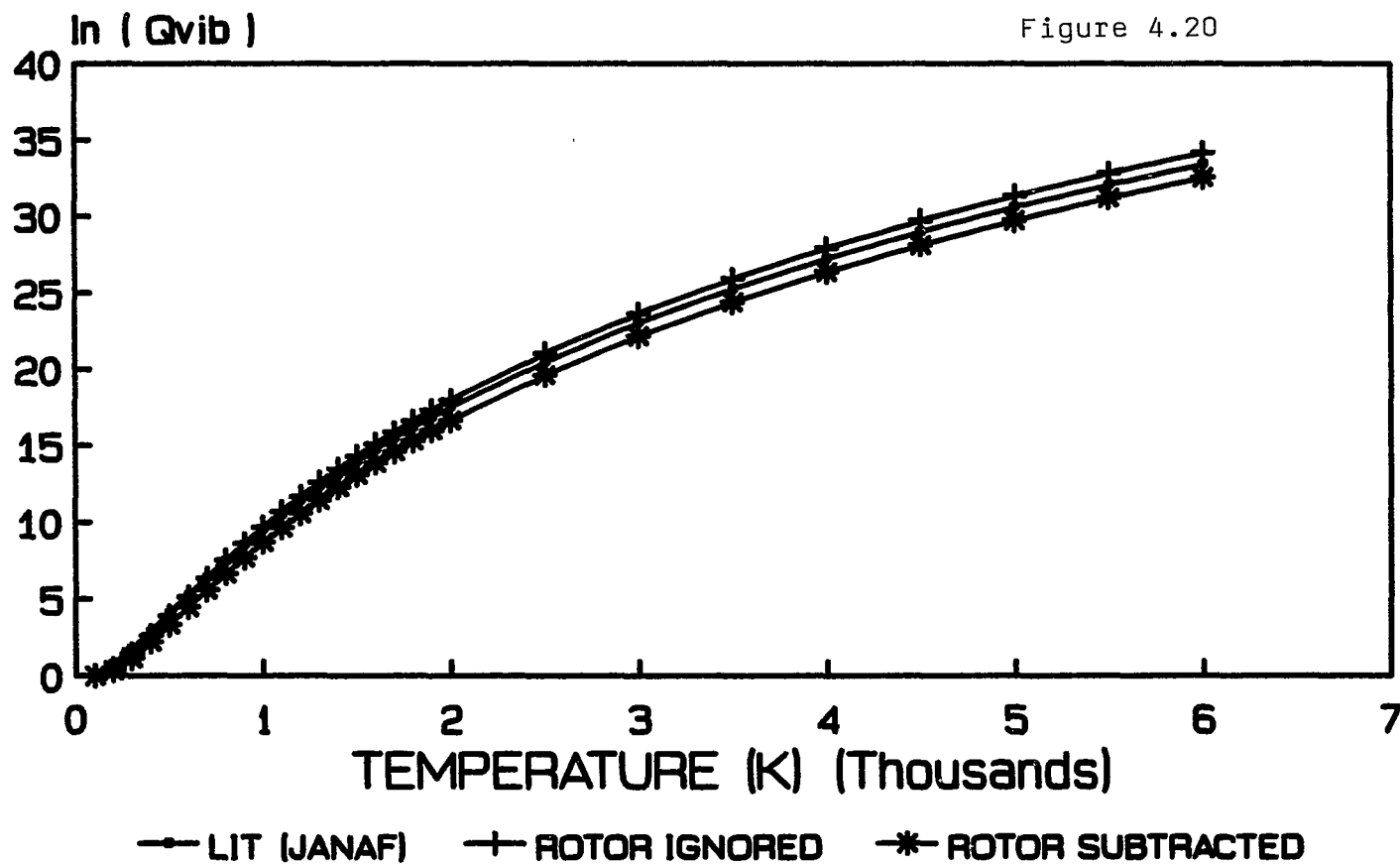


CY13HD : $\ln(Q_{vib})$: LIT VS THERM VIBRATIONAL PARTITION F'N

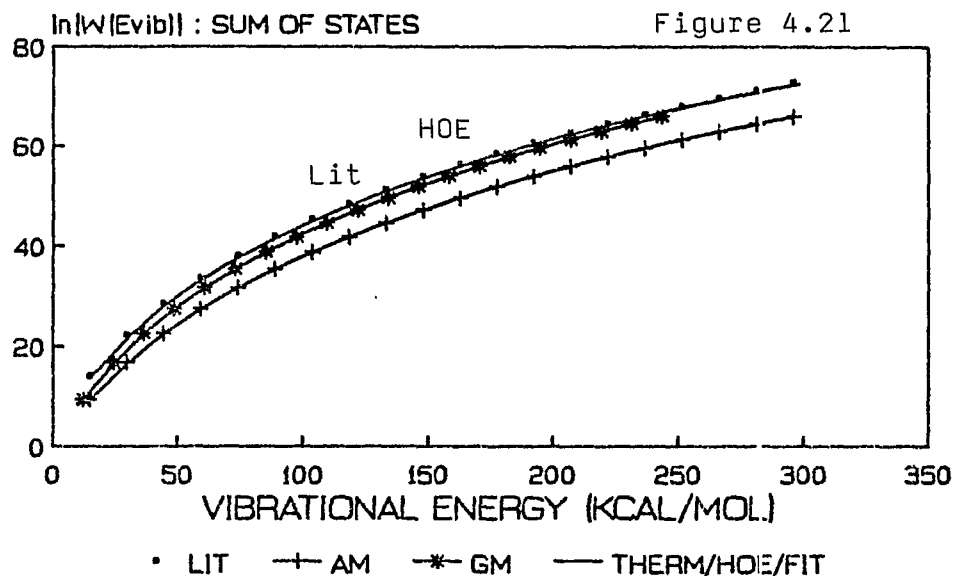


337

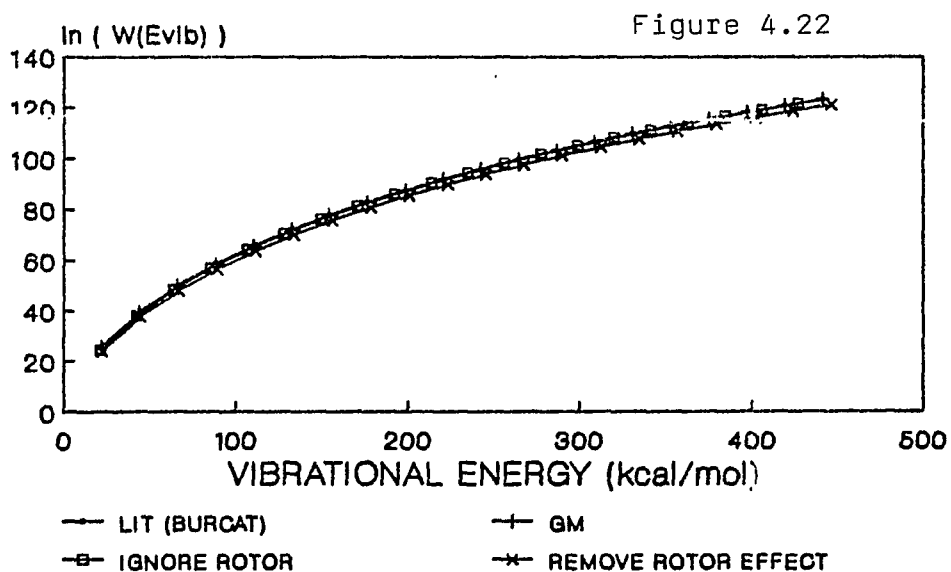
C2F6 : VIBRATIONAL PARTITION FUNCTION COMPARISON OF THERM ESTIMATE W/EXP



CHD13:SUM OF VIBRATIONAL QUANTUM STATES
COMPARISON W/R : FREQUENCIES FROM CPFIT

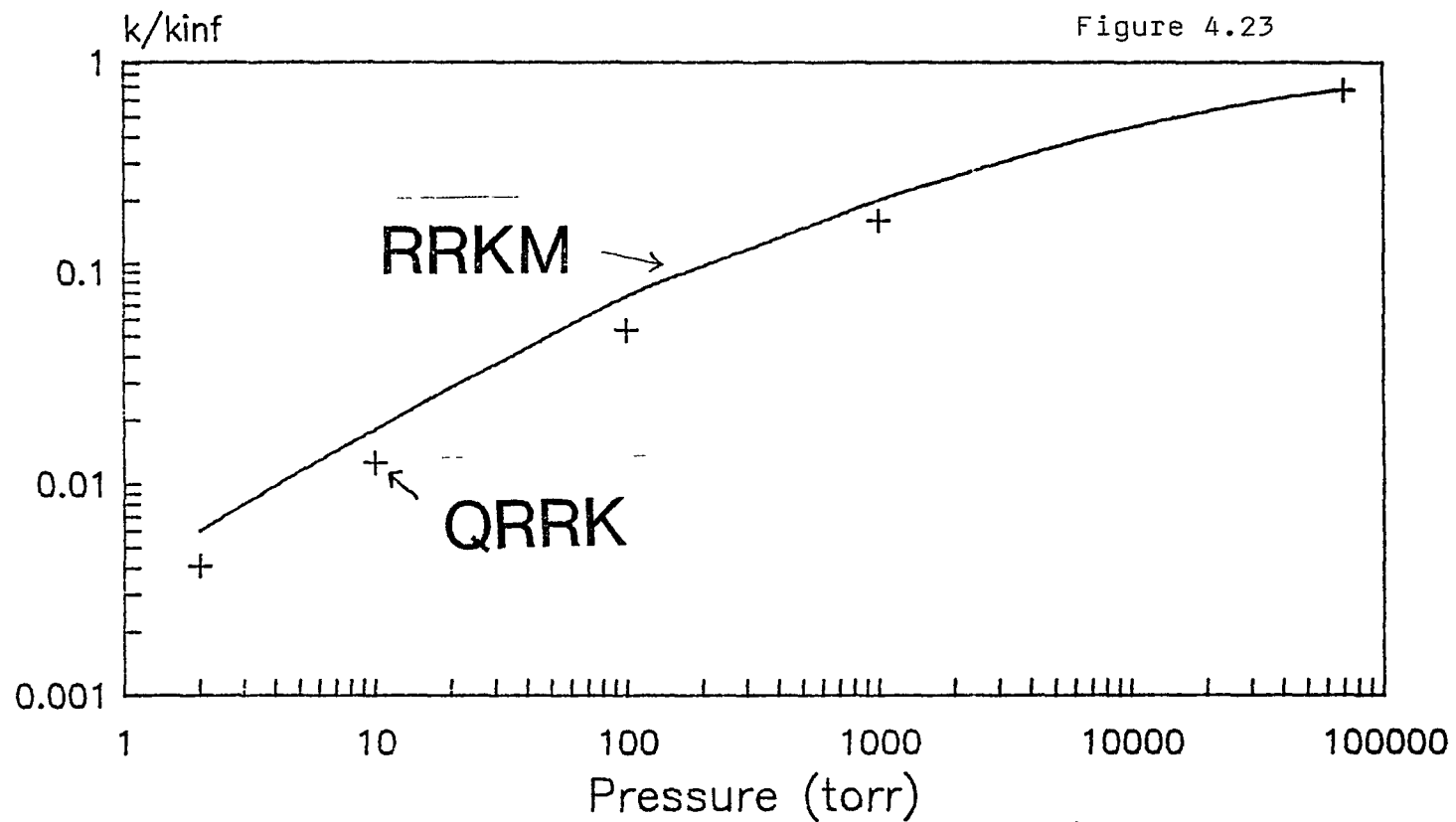


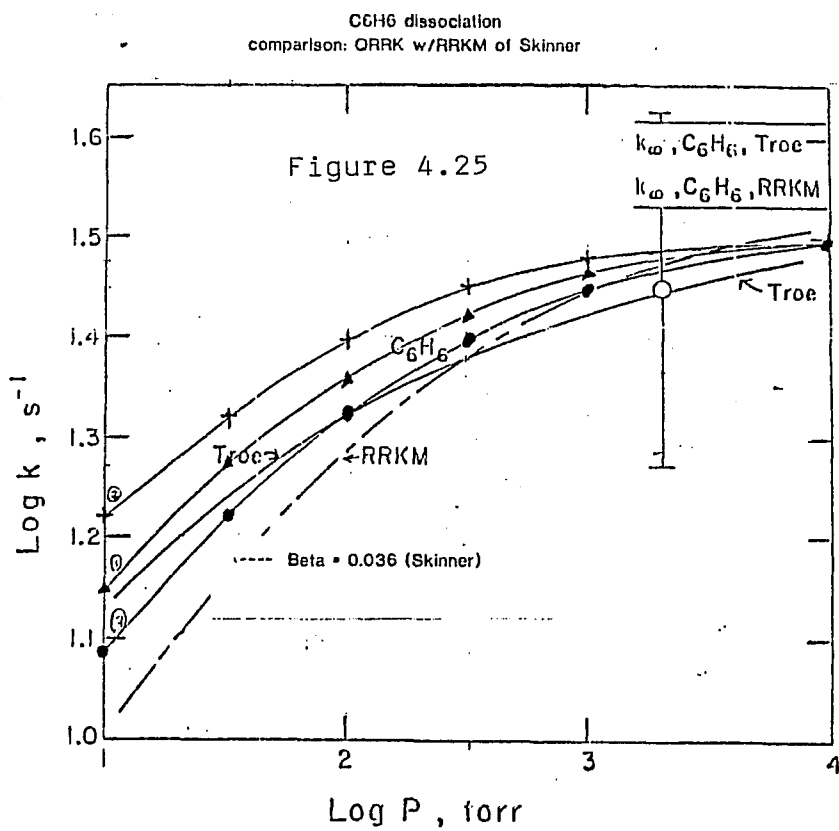
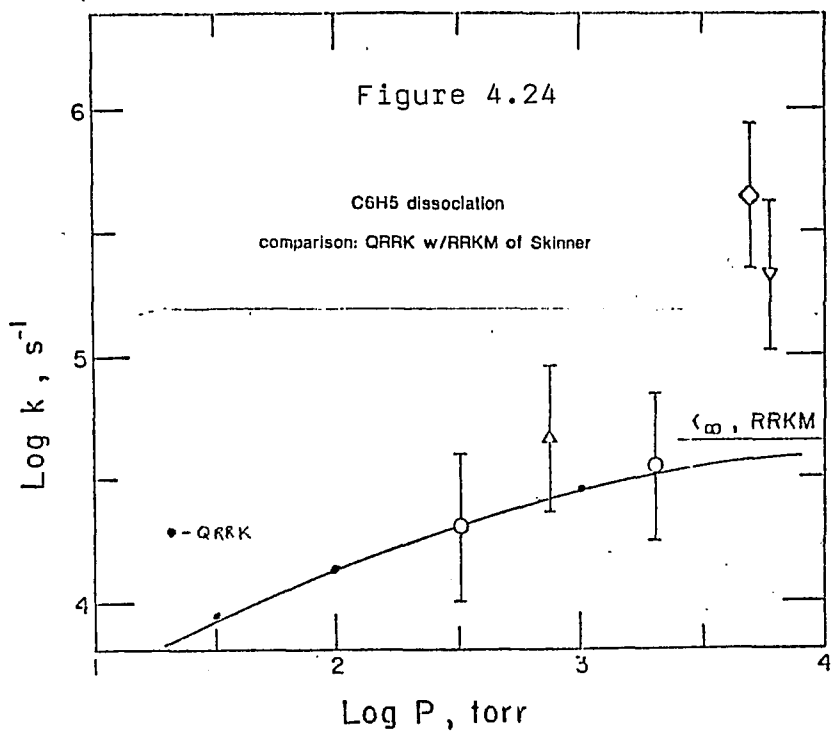
BIPHENYL : SUM OF VIBRATIONAL STATES
WHITTEN-RABINOVICH APPROXIMATION



SF6 Dissociation Comparison of QRRK w/ RRKM (Lyman)

Figure 4.23





APPENDIX IV - C

FORTRAN SOURCE CODE FOR

THERMFEX

```

PROGRAM THERMFIT
$LARGE
C*****
C      THIS PROGRAM CREATES A NASA FORMAT THERMO DATABASE FILE
C
C      TWO SETS OF COEFFICIENTS ARE GENERATED AFTER FITTING CP DATA
C      USING A MODIFIED VERSION OF THE CPFIT PROGRAM
C
C      TMP DATA FILE (UNIT 45) IS USED TO PASS FILENAMES DIRECTLY
C      TO THIS PROCEDURE FROM THERM. IF THE FILE "NASAGEN.TMP"
C      DOES NOT EXIST, THEN THE USER IS PROMPTED FOR INPUT/OUTPUT
C      FILENAMES.
C
C      INPUT FILE (UNIT 1) IS IN THERMLST FORMAT
C
C      OUTPUT FILE (UNIT 3) CONTAINS COEFFICIENTS IN NASA FORMAT
C      FOR USE WITH CHEMKIN AND OTHER PACKAGES
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION X0(2),WX(2),S(2)
      DIMENSION CPL(30),TRA(3),A(5),B(6),C(14),F(14),FS(3,14),
+TH(3),TL(3),TM(3),SSRS(3),PERMX(3)
      DIMENSION TFIT(30),CPFIT(30),PWORK(120),D(14),CONST(3)
      DIMENSION X(31,15,1),Y(31,25,1),B1(16,25,1),T(10),TEST(30),
+CPEST(30)
      REAL*8 TMID
      REAL*8 DELPCT(20)
      CHARACTER*6 TITLE(5),HEADIN(21),REF3,XNAME
      CHARACTER*1 PHASE,CFLAG
      CHARACTER*2 IE(4)
      INTEGER NE(4)
      CHARACTER*4 REF(2),INAME,IFLAG
      CHARACTER*14 FUNITS,NUL
      CHARACTER*70 FILIN,FILOUT,COMMAND,DUMMY,S1
      LOGICAL EXST,OPNED
      EXTERNAL FX
      COMMON/DATA/CPEX1,T1,IT,NT,NS
      COMMON/CONST/CONST,NTERMS
      COMMON/TOL/TOL,TSTEP
      COMMON/TEMPFIT/TFIT,F
      COMMON/FLAG/IREPEAT,DELPCT,IFLG

DATA NPTS/7/
DATA IFLAG/'END'/
DATA IC1,IC2,IC3,IC4/1,2,3,4/
      T(1)=300.0
      T(2)=400.0
      T(3)=500.0
      T(4)=600.0
      T(5)=800.0
      T(6)=1000.0
      T(7)=1500.0

```



```

TEST(1)=300.
TEST(2)=350.
TEST(3)=400.
TEST(4)=425.
TEST(5)=450.
TEST(6)=500.
TEST(7)=550.
TEST(8)=600.
TEST(9)=650.
TEST(10)=700.
T0=298.15
TLO=300.0
THI=5000.0
TMID=1500.0
TOL=1.0E-4
TSTEP=0.0
14  FORMAT(A14)

COMMAND=' '
FILIN=' '
FILOUT=' '
INQUIRE(FILE='THERMFIT.TMP',EXIST=EXST)
IF(EXST)THEN
    OPEN(45,FILE='THERMFIT.TMP',STATUS='OLD')
    READ(45,3)COMMAND
    READ(45,3)FILIN
    READ(45,3)FILOUT
    CLOSE(45,STATUS='DELETE')
    GOTO 123
ENDIF
WRITE(*,*)'ENTER FILENAME FOR INPUT (.LST)!'
3  READ(*,3)FILIN
    FORMAT(A70)
    CALL FNAME(FILIN,'LST')
    WRITE(*,*)'ENTER FILENAME FOR OUTPUT (.DAT)!'
    READ(*,3)FILOUT
    CALL FNAME(FILOUT,'DAT')
123 CONTINUE
    INQUIRE(FILE=FILIN,EXIST=EXST)
    IF(EXST)GOTO 324
    STOP 2
324 OPEN(1,FILE=FILIN,STATUS='OLD')
    OPEN(3,FILE=FILOUT,STATUS='UNKNOWN')
    IF(COMMAND.EQ.' ')THEN
        WRITE(*,*)' '
        WRITE(*,*)' '
        WRITE(*,*)' GENERATING NASA FORMAT DATABASE FROM'
        WRITE(*,*)' ',FILIN
        WRITE(*,*)' '
        WRITE(*,*)' please wait'
    ENDIF
WRITE(3,99)
WRITE(3,98)
99 FORMAT('THERMO ',73(' '))

```

```

98 FORMAT(' 300.000 1500.000 5000.000 ',49(' '))
1 ICOUNT=1
  READ(1,3)DUMMY
  CALL DBLNK(DUMMY,LEN,0)
  CONST(1)=1.0
  FUNITS='KCAL'
  IF(DUMMY(:6).EQ.'UNITS:')THEN
    IF(DUMMY(7:8).EQ.'KJ')THEN
      FUNITS='KJ'
      CONST(1)=4.184
    ENDIF
  READ(1,3)DUMMY
  ENDIF
95 FORMAT(5A6/,21A6)
  read(1,14)nul
20  CONTINUE
  DO 203 IK1=1,20
203  DELPCT(IK1)=0.0
  YERRS=1.0E+7
  IREPEAT=0
  IFLG=0
  IPOLY=0
  IPOLYC=0
  CFLAG=' '
  THI=5000.
  READ(1,'(1X,A4)',END=900)INAME
  IF(INAME.EQ.' ')THEN
    GOTO 20
  ELSE
    BACKSPACE(1)
  ENDIF
  IF(FUNITS.EQ.'KCAL')THEN
    READ(1,170,END=900)CFLAG,INAME,XNAME,HF298,S298,(CPL(I),I=1,7),
    1 (REF(I),I=1,2),REF3,(IE(I),NE(I),I=1,4),PHASE,NROT
170  FORMAT(A1,A4,A6,F7.2,2X,F7.2,3X,7(F6.2,2X),2A4,A6,
    1 3X,4(A2,I3,1X),A1,1X,I1)
    ELSE IF(FUNITS.EQ.'KJ')THEN
    READ(1,176,END=900)CFLAG,INAME,XNAME,HF298,S298,(CPL(I),I=1,7),
    1 (REF(I),I=1,2),REF3,(IE(I),NE(I),I=1,4),PHASE,NROT
176  FORMAT(A1,A4,A6,F8.2,1X,F8.2,2X,7(F7.2,1X),2A4,A6,3X,4(A2,I3,
    + 1X),A1,1X,I1)
  ENDIF
  IF(INAME(:3).EQ.'END') THEN
    WRITE(3,1012)
1012  FORMAT('END',77(' '))
1011  FORMAT(A4)
    STOP 'END OF THERMFIT'
  ENDIF
  IF(CFLAG.EQ.' ')THEN
    WRITE(*,'(1X,A4,A6)')INAME,XNAME
  ELSE
    WRITE(*,'(1X,A4,A6,2X,A1)')INAME,XNAME,CFLAG
  ENDIF
C---CONVERTING HF298 TO CAL/MOLE OR J/MOLE

```

```

      IF(FUNITS.EQ.'KCAL')THEN
        HF298=HF298*1000.
      ELSEIF(FUNITS.EQ.'KJ')THEN
        HF298=HF298*1000.0/4.184
        S298=S298/4.184
      ENDIF
    TRA(1)=300.
      NS=0
      NATOM=0
      ICARBON=0
      NCARBON=0
      DO 765 I1J=1,4
        IF(IE(I1J).EQ.'C'.OR.IE(I1J).EQ.'C')THEN
          ICARBON=1
          NCARBON=NE(I1J)
        ENDIF
765      NATOM=NATOM+NE(I1J)
986      CONTINUE
      DIF1=DABS(CPL(1)-CPL(3))
      DIF2=DABS(CPL(1)-CPL(6))
      DIFF=MAX(DIF1,DIF2)
      IF(FUNITS.EQ.'KJ')DIFF=DIFF/4.184
      IF(NATOM.NE.1.AND.DIFF.GT.0.01)THEN
        IF((ICARBON.EQ.1.AND.(NATOM-NCARBON).EQ.2).OR.NATOM.EQ.2
+)THEN
          NS=(3*NATOM)-5
          CONST(3)=1.0
          CPINFIN=1.987*(FLOAT(3*NATOM)-1.5)*CONST(1)
        ELSE
          NS=(3*NATOM)-6
          CONST(3)=0.0
          CPINFIN=1.987*(FLOAT(3*NATOM)-(2.+(FLOAT(NROT)/4.0)))
+)CONST(1)
        ENDIF
        IF(CPL(7).EQ.0.0)THEN
          CPL(7)=CPL(6)+(0.37*(CPINFIN-CPL(6)))
        ENDIF
      CPL(8)=CPL(7)+(0.37*(CPINFIN-CPL(7)))
      CPL(9)=0.99999*CPINFIN
      T(1)=300.0
      T(2)=400.0
      T(3)=500.0
      T(4)=600.0
      T(5)=800.0
      T(6)=1000.0
      T(7)=1500.0
      T(8)=2000.0
      T(9)=20000.0
      T(10)=0.0
      NT=9
      IF(CFLAG.EQ.'*')THEN
        IFLG=2
        NT=8
        GOTO 1994

```

```

                ENDIF
***** POLYNOMIAL SMOOTHING PROCEDURE *****
1994          CONTINUE
                IF(IFLG.NE.0)THEN
                    IFLG=0
                    POLYNOMIAL SMOOTHING DID NOT HELP OR USER SPECIFIES
*
*           POLYNOMIAL FIT ONLY THEN
*           DEFAULT TO SINGLE REPEATED POLYNOMIAL
*           OVER TRANGE 300 - 2000 K
                    IF(CPL(7).EQ.0.)THEN
                        CPL(7)=CPL(6)+(0.37*(CPINFIN-CPL(6)))
                    ENDIF
                    CPL(8)=CPL(7)+(0.37*(CPINFIN-CPL(7)))
                    T(8)=2000.
                    DO 61678 IK1=1,8
                    DO 61677 IK2=1,5
61677          X(IK1,IK2,1)=T(IK1)**(IK2-1)
                    CPFIT(IK1)=CPL(IK1)/1.987
                    Y(IK1,1,1)=CPFIT(IK1)
61678          CONTINUE
                    MDEG=4
                    NPTS=8
                    CALL LINLSQ(X,Y,B1,4,NPTS,1,1,SSR,AVGERR)
                    DO 61679 IK1=1,5
61679          C(IK1)=B1(IK1,1,1)
                    DO 61681 IK1=1,5
61681          F(IK1)=C(IK1)
                    F(IK1+7)=C(IK1)
                    CONTINUE

                    C6=F6(0,(HF298/1.987),T0,F)
                    C7=(S298/1.987)-F(1)*DLOG(T0)-F(2)*T0-F(3)/2.*T0**2
1          -F(4)/3.*T0**3-F(5)/4.*T0**4
                    F(6)=C6
                    F(13)=C6
                    F(7)=C7
                    F(14)=C7
                    TMID=1000.
                    THI=2000.0
                    ICOUNT=0
6545          DCPDT=DCPT(0,THI,F)
                    COMPARE=((ABS(DCPDT)*500.)/CPT(0,THI,F))*100.
                    IF(DCPDT.LT.0..AND.COMPARE.GT.10.)THEN
                        ICOUNT=ICOUNT+1
                        THI=THI-50.
                        IF(ICOUNT.LE.100)GOTO 6545
                    ENDIF
                    GOTO 12987
                ENDIF
            ENDIF
*****
            ENDIF
73590          CONTINUE
            DO 431 JK=1,2
            IF(NATOM.NE.1.AND.DIFF.GT.0.01)THEN

```

```

IF(IPOLY.EQ.1)THEN
  IF(JK.EQ.1)THEN
    TK=253.3333
    DO 1290 I8=1,15
      TK=TK+46.6667
      TFIT(I8)=TK
      TFIT(I8+15)=1000.+(71.4236*FLOAT(I8-1))
1290      CONTINUE
*      set lower temperature below room temp so that 298 is not
*      outside the range of the regression for Cp
      TFIT(1)=273.15
      ELSE
      TK=928.5764
      DO 1291 I8=1,15
        TFIT(I8)=1000.+(71.4236*FLOAT(I8-1))
        TFIT(I8+15)=2000.+(266.667*FLOAT(I8))
1291      CONTINUE
      ENDIF
      ELSEIF(IPOLY.EQ.0)THEN
      IF(JK.EQ.1)THEN
      TK=236.6667
      DO 21290 I8=1,15
        TK=TK+63.3333
        TFIT(I8)=TK
        TFIT(I8+15)=1250.+(35.714*FLOAT(I8-1))
21290      CONTINUE
*      set lower temperature below room temp so that 298 is not
*      outside the range of the regression for Cp
      TFIT(1)=273.15
      ELSE
      DO 21291 I8=1,15
        TFIT(I8)=1250.+(35.714*FLOAT(I8-1))
        TFIT(I8+15)=1700.+(283.333*FLOAT(I8))
21291      CONTINUE
      ENDIF
      ELSEIF(IPOLY.EQ.3)THEN
      IF(JK.EQ.1)THEN
      TK=263.333
      DO 22290 I8=1,15
        TK=TK+36.667
        TFIT(I8)=TK
        TFIT(I8+15)=850.+(35.714*FLOAT(I8-1))
22290      CONTINUE
*      set lower temperature below room temp so that 298 is not
*      outside the range of the regression for Cp
      TFIT(1)=273.15
      ELSE
      DO 22291 I8=1,15
        TFIT(I8)=850.+(35.714*FLOAT(I8-1))
        TFIT(I8+15)=1350.+(310.0*FLOAT(I8))
22291      CONTINUE
      ENDIF
      ELSEIF(IPOLY.EQ.2)THEN
      IF(JK.EQ.1)THEN

```

```

                TK=263.333
                DO 23290 I8=1,15
                    TK=TK+36.667
                    TFIT(I8)=TK
                    TFIT(I8+15)=850.+(21.429*FLOAT(I8-1))
23290                CONTINUE
*                   set lower temperature below room temp so that 298 is not
*                   outside the range of the regression for Cp
                    TFIT(1)=273.15
                    ELSE
                    DO 23291 I8=1,15
                        TFIT(I8)=850.+(21.429*FLOAT(I8-1))
                        TFIT(I8+15)=1150.+(323.333*FLOAT(I8))
23291                CONTINUE
                    ENDIF
                ENDIF
*   use linearized exponential function to fit cp data
*   this replaces harmonic oscillator expression.
                call cpexpoft(T,CPL,NT,TFIT,CPFIT,30,CPINFIN)
                TRA(1)=300.
                TRA(2)=1000.
                DO 30 I=1,30
                DO 31 I11=1,5
31 X(I,I11,1)=TFIT(I)**(I11-1)
                    TIN=TFIT(I)
                    Y(I,1,1)=CPFIT(I)/(1.987*CONST(1))
30 CONTINUE
                MDEG=4
                RSQ=100.
                IER=0
                NPTS=30
                CALL LINLSQ(X,Y,B1,4,NPTS,1,1,SSR,AVGERR)
                DO 32 I=1,5
32                C(I)=B1(I,1,1)

                ELSE
*                   ATOM: USE DIFFERENT METHOD FOR Cp
C   BYPASS FITTING ROUTINE IF CP <> f(T)
                    SUMCP=0.0
                    DATPNT=0.0
                    DO 1209 IJK=1,7
                        IF(CPL(IJK).NE.0.0)THEN
                            SUMCP=SUMCP+CPL(IJK)
                            DATPNT=DATPNT+1.0
                        ENDIF
1209                CONTINUE
                    C(1)=SUMCP/(1.98717*DATPNT)
*                   C(1)=CPL(1)/1.98717
                    IF(FUNITS.EQ.'KJ')C(1)=C(1)/4.184
                    DO 15 I=2,5
                    C(I)=0.0
15                CONTINUE
                    TMID=1000.
                ENDIF

```

```

                IF(JK.EQ.1)THEN
                                DO 75 I=1,5
                                F(I)=C(I)
75                                CONTINUE
                ELSEIF(JK.EQ.2)THEN
                                DO 85 J=1,5
85                                F(J+7)=C(J)
                ENDIF
431                CONTINUE
C                CALCULATE CONST C6 IN ENTHALPY EXPRESSION

*                MUST INSERT HERE CALC OF Hf & S SO THAT 1st DERIVATIVE AND
*                FUNCTION VALUES MATCH AT T BREAK POINT
*
*                TO DO THIS WE HOLD (C1-C5, C8-C12) CONSTANT AND SOLVE FOR C6,C13
*                SUCH THAT HfI(Tbp)=Hfh(Tbp)
*                MUST INTEGRATE CP BETWEEN 298 AND Tbp
*
*                WE MUST PERFORM A SIMILAR DETERMINATION FOR S TO GET C7,C14
*
*
C
                C6=F6(0,(HF298/1.987),T0,F)
C
C                CALCULATE CONST C7 FROM ENTROPY EXPRESSION
C
                C7=(S298/1.987)-F(1)*DLOG(T0)-F(2)*T0-F(3)/2.*T0**2
                1-F(4)/3.*T0**3-F(5)/4.*T0**4

*                USE F(6) TO DETERMINE HF(Tbp)
                F(6)=C6
                F(7)=C7
                H0=HF(0,T0,F)*1.987*T0
                S0=ST(0,T0,F)*1.987
**                determine break point temperature
                IF(NATOM.NE.1.AND.CFLAG.NE.'1')THEN
                                TINIT=(TFIT(1)+TFIT(15))/2.0
                                CALL TBREAK (TMID,TINIT)
                                TMID=FLOAT(INT(TMID+0.5))
                ELSE
                                TMID=1000.
                ENDIF
**                THESE MUST BE DETERMINED TO SATISFY H(Tbp)l = H(Tbp)h.
                HFTMID=HF(0,TMID,F)*1.987*TMID
                STMID=ST(0,TMID,F)*1.987
                F(13)=F6(7,(HFTMID/1.987),TMID,F)
                C14=(STMID/1.987)-F(8)*DLOG(TMID)-F(9)*TMID-F(10)/2.*TMID**2
                1-F(11)/3.*TMID**3-F(12)/4.*TMID**4
                F(14)=C14
                HCKTM=HF(7,TMID,F)*1.987*TMID
                SCKTM=ST(7,TMID,F)*1.987
                DELTACP=100.*((CPT(7,TMID,F)-CPT(0,TMID,F))/CPT(0,TMID,F))
                DDELCP=DCPT(7,TMID,F)-DCPT(0,TMID,F)
                DELTAS=100.*((ST(7,TMID,F)-ST(0,TMID,F))/ST(0,TMID,F))

```

```

DDELS=DST(7, TMID, F)-DST(0, TMID, F)
DELTAH=100.*((HF(7, TMID, F)-HF(0, TMID, F))/HF(0, TMID, F))
DDELH=DHF(7, TMID, F)-DHF(0, TMID, F)
YERR=0.0
IF(ABS(DELTAH).GT.(50.*TOL).OR.ABS(DELTAS).GT.(50.*TOL)
+.OR.ABS(DDELH).GT.(20.*TOL).OR.ABS(DDELS).GT.(20.*TOL).OR.
+ABS(DELTAHP).GT.(50.*TOL).OR.ABS(DDELCP).GT.(20.*TOL))THEN
  IF(ABS(DELTAHP).GT.(50.*TOL))THEN
    YERR=ABS(DELTAHP)
    WRITE(*,1960)ABS(DELTAHP)
1960  FORMAT(1X,'Tmid mismatch: % delta Cp(Tmid) = ',1PE10.3)
    ENDIF
    IF(ABS(DDELCP).GT.(0.005))THEN
      IF(ABS(DDELCP).GT.YERR)YERR=ABS(DDELCP)
      WRITE(*,1961)ABS(DDELCP)
1961  FORMAT(1X,'Tmid mismatch: delta dCp(Tmid) = ',1PE10.3)
    ENDIF
    IF(ABS(DELTAH).GT.(50.*TOL))THEN
      IF(ABS(DELTAH).GT.YERR)YERR=ABS(DELTAH)
      WRITE(*,1962)ABS(DELTAH)
1962  FORMAT(1X,'Tmid mismatch: % delta Hf(Tmid) = ',1PE10.3)
    ENDIF
    IF(ABS(DDELH).GT.(0.005))THEN
      IF(ABS(DDELH).GT.YERR)YERR=ABS(DDELH)
      WRITE(*,1963)ABS(DDELH)
1963  FORMAT(1X,'Tmid mismatch: delta dhf(Tmid) = ',1PE10.3)
    ENDIF
    IF(ABS(DELTAS).GT.(50.*TOL))THEN
      IF(ABS(DELTAS).GT.YERR)YERR=ABS(DELTAS)
      WRITE(*,1964)ABS(DELTAS)
1964  FORMAT(1X,'Tmid mismatch: % delta S(Tmid) = ',1PE10.3)
    ENDIF
    IF(ABS(DDELS).GT.(0.005))THEN
      IF(ABS(DDELS).GT.YERR)YERR=ABS(DDELS)
      WRITE(*,1965)ABS(DDELS)
1965  FORMAT(1X,'Tmid mismatch: delta dS(Tmid) = ',1PE10.3)
    ENDIF
    IF(IPOLY.EQ.0.AND.IPOLYC.EQ.0)THEN
      WRITE(*,*)' repeating polynomial fitting routine'
      write(*,*)' with a different overlap region'
      YERRS=YERR
      YERR1=YERR
      IPOLYC=IPOLYC+1
      IPOLY=1
      SSR(1)=SSR
      TM(1)=TMID
      DO 1357 IK1=1,14
1357  FS(1,IK1)=F(1K1)
      GOTO 73590
    ELSEIF(IPOLY.EQ.1)THEN
      WRITE(*,*)' SECOND REGRESSION FAILED TO MATCH'
      WRITE(*,*)' PROPERTY AT THE MID-POINT'
      WRITE(*,*)' MAKING A THIRD ATTEMPT TO FIT THE DATA'
      DO 13571 IK1=1,14

```



```

13571          FS(2,IK1)=F(IK1)
              IPOLY=2
              YERR2=YERR
              SSRS(2)=SSR
              TM(2)=TMID
              GOTO 73590
          ELSEIF(IPOLY.EQ.2)THEN
              WRITE(*,*)' THIRD ATTEMPT TO MATCH PROPERTIES '
              WRITE(*,*)' AT THE MIDPOINT HAS FAILED'
              WRITE(*,*)' LAST REGRESSION IN PROGRESS'
              IPOLY=3
              SSRS(3)=SSR
              YERR3=YERR
              TM(3)=TMID
              DO 13572 IK1=1,14
13572          FS(3,IK1)=F(IK1)
              GOTO 73590
          ELSEIF(IPOLY.EQ.3)THEN
              IF(YERR1.LT.YERR2)THEN
                  IF(YERR1.LT.YERR3)THEN
                      KEEP=1
                  ELSE
                      KEEP=3
                  ENDIF
              ELSE
                  IF(YERR2.LT.YERR3)THEN
                      KEEP=2
                  ELSE
                      KEEP=3
                  ENDIF
              ENDIF
              WRITE(*,*)' best regression is # ',keep
              DO 24 IK2=1,14
24          F(IK2)=FS(KEEP,IK2)
              TMID=TM(KEEP)
          ENDIF
          ENDIF
*
*      F ( 1-7 ) : LOW TEMPERATURE COEFFICIENTS
*      F ( 8-14 ) : HIGH TEMPERATURE COEFFICIENTS
*
*      REMEMBER:  NASA FORMAT  FIRST 7 COEFFICIENTS (HIGH TEMP)
*                  SECOND 7 COEFFICIENTS (LOW TEMP)
*
12987          CONTINUE

          WRITE(3,1010) INAME,XNAME,(REF(1),I=1,2),REF3,(1E(1),NE(1),I=1,
1 4),PHASE,TLO,THI,TMID,NROT,IC1
          WRITE(3,112) F(8),F(9),F(10),F(11),F(12),IC2
          WRITE(3,112)F(13),F(14),F(1),F(2),F(3),IC3
          WRITE(3,113)F(4),F(5),F(6),F(7),IC4
1010  FORMAT(A4,A6,2A4,A6,4(A2,13),A1,2F10.3,F9.3,4X,2I1)

112  FORMAT(5(1PE15.8),15)

```

```
113 FORMAT(4(1PE15.8),15X,15)
      ICOUNT=ICOUNT+1
      GO TO 20
900 WRITE(3,1012)
      CLOSE(1,STATUS='KEEP')
      CLOSE(3,STATUS='KEEP')
      STOP
      END
```

SUBROUTINE CPEXPOFT(T,CP,NTIN,T1,CP1,NTOUT,CPINF)

```

$LARGE
*****
*
*   Written by: Edward R. Ritter   2/26/89
*
*
*   This subprogram approximates the heat capacity function using
*   the following expression:
*
*       Cp (T) = Cpinf ( 1 - exp ( - (A+B*T) ) )
*
*   This is rearranged to give the following linear expression:
*
*       Y = - ln( 1 - (Cp(T)/Cpinf) ) = A + B*T
*
*   This expression is evaluated piece-wise between data points at
*   300, 400, 500, 600, 800, and 1000 K.
*
*   Cp data is then estimated at required temperatures from this eq'n
*   using the appropriate expression which covers the T range of interest*
*
*   VARIABLES:
*
*       T : vector of temperature points for which Cp is known
*       CP : vector of known Cp data points
*       NTIN : number of data points input
*       T1 : vector of Temperature for which estimates are required
*       CP1 : vector of Cp estimates evaluated at T1
*       NTOUT : number of temperatures for which Cp estimates are required
*       CPINF : the high temperature limiting heat capacity
*               CPINF = (3N-2)R    non-linear molecule
*                   = (3N-1.5)R    linear molecule
*****
      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION T(*),CP(*),T1(*),CP1(*),A(30),B(30),YEX(30)
*
*-----
*
*   determine value of Y at each T from input Cp data
*
*       Y = - LOG( 1 - (Cp(T)/CPinf) )
*
*-----
*
      DO 100 I=1,NTIN
100      YEX (I) = YEXP ( CP(I), CPINF, T(I) )
*   WRITE(*,*)' T(J)      YEX(J)      YEX(J+1)      A(I)      B(I) '
*
*-----
*
*   determine linear approximations for Y over each
*   temperature interval

```

```

*
*-----
*
      DO 300 I=1,NTIN-1
      IF(YEX(I+1).EQ.0.0.AND.I.GE.2)THEN
          A(I)=A(I-1)
          B(I)=B(I-1)
          GOTO 300
      ENDIF
      CALL LINE(T(I),T(I+1),YEX(I),YEX(I+1),A(I),B(I))
*333 WRITE(*,'(1X,F10.3,4(2X,1PE15.3))')T(I),YEX(I),YEX(I+1),A(I),B(I)
300   CONTINUE

*
*-----
*
*      now we calculate Cp at each requested output temperature
*
*-----
*
*      WRITE(*,*)' K      TJ      CP1(J)      BETA      A(K)      B(K)
*      +'
      CPS=0.0
      DO 10000 J=1,NTOUT
      TJ=T1(J)
      IF(TJ.LE.T(1))THEN
          K=1
      ELSEIF(TJ.GT.T(1).AND.TJ.LE.T(NTIN))THEN
          DO 500 I=1,NTIN-1
          IF(TJ.GT.T(I).AND.TJ.LE.T(I+1))THEN
              K=I
              GOTO 600
          ENDIF
500      CONTINUE
600      CONTINUE
      ELSE
          K=NTIN-1
      ENDIF
      IER=0
700      CONTINUE
      Y=A(K)+(B(K)*TJ)
      CP1(J)=CPOFT2(A(K),B(K),CPINF,TJ)
*      WRITE(*,'(1X,I2,2X,2F10.3,3(2X,1PE15.3))')K,TJ,CP1(J),Y,A(K),
*      +B(K)
10000  CONTINUE
      RETURN
      END

```

```

FUNCTION BETAEXP(CP,CPINF,T)
IMPLICIT REAL*8(A-H,O-Z)
Y=LOG(1.0-(CP/CPINF))
BETAEXP=Y/T
RETURN
END

```

```

FUNCTION YEXP(CP,CPINF,T)
IMPLICIT REAL*8(A-H,O-Z)
IF(CP.GE.CPINF)THEN
write(*,*)' Cp > Cpinf:   discarding this data point'
write(*,*)'   T (K)   Cp (T)   Cpinf '
write(*, '(1x,3(2x,1pe15.3))')t,cp,cpinf
      YEXP=0.0
      RETURN
ENDIF
YEXP=LOG(1.0-(CP/CPINF))
RETURN
END

```

```

FUNCTION DBDT(B1,B2,T1,T2)
IMPLICIT REAL*8(A-H,O-Z)
DBDT=(B2-B1)/(T2-T1)
RETURN
END

```

```

FUNCTION CPOFT(BETA,CPINF,T)
IMPLICIT REAL*8(A-H,O-Z)
CPOFT=CPINF*(1.0-EXP(-1.0*BETA*T))
RETURN
END

```

```

FUNCTION CPOFT2(A,B,CPINF,T)
IMPLICIT REAL*8(A-H,O-Z)
Y=A+(B*T)
CPOFT2=CPINF*(1.0-EXP(Y))
RETURN
END

```

```

FUNCTION BETA0(BETA,T,A,B)
IMPLICIT REAL*8(A-H,O-Z)
BETA0=BETA-((A*T)+((B/2.0)*T**2))
RETURN
END

```

```

FUNCTION BOFT(BETA0,A,B,T)
IMPLICIT REAL*8(A-H,O-Z)
BOFT=BETA0+(A*T)+((B/2)*T**2)
RETURN
END

```

```
SUBROUTINE LINE(X1,X2,Y1,Y2,A,B)
  IMPLICIT REAL*8 (A-H,O-Z)
  B=(Y2-Y1)/(X2-X1)
  A=Y1-(B*X1)
  RETURN
  END
```

APPENDIX IV - D

FORTRAN SOURCE CODE FOR

THERMFIT

```

PROGRAM THERMFIT
$LARGE
C*****
C   THIS PROGRAM CREATES A NASA FORMAT THERMO DATABASE FILE
C
C       TWO SETS OF COEFFICIENTS ARE GENERATED AFTER FITTING CP DATA
C       USING A MODIFIED VERSION OF THE CPFIT PROGRAM
C
C       TMP DATA FILE (UNIT 45) IS USED TO PASS FILENAMES DIRECTLY
C       TO THIS PROCEDURE FROM THERM. IF THE FILE "NASAGEN.TMP"
C       DOES NOT EXIST, THEN THE USER IS PROMPTED FOR INPUT/OUTPUT
C       FILENAMES.
C
C       INPUT FILE (UNIT 1) IS IN THERMLST FORMAT
C
C       OUTPUT FILE (UNIT 3) CONTAINS COEFFICIENTS IN NASA FORMAT
C       FOR USE WITH CHEMKIN AND OTHER PACKAGES
C*****
  IMPLICIT REAL*8 (A-H,O-Z)
    DIMENSION XO(2),WX(2),S(2)
  DIMENSION CPL(30),TRA(3),A(5),B(6),C(14),F(14),FS(3,14),
+TH(3),TL(3),TM(3),SSRS(3),PERMX(3)
  DIMENSION TFIT(30),CPFIT(30),PWORK(120),D(14),CONST(3)
  DIMENSION X(31,15,1),Y(31,25,1),B1(16,25,1),T(10),TEST(30),
+CPEST(30)
    REAL*8 TMID
    REAL*8 DELPCT(20)
  CHARACTER*6 TITLE(5),HEADIN(21),REF3,XNAME
  CHARACTER*1 PHASE,CFLAG
  CHARACTER*2 IE(4)
  INTEGER NE(4)
  CHARACTER*4 REF(2),INAME,IFLAG
    CHARACTER*14 FUNITS,NUL
    CHARACTER*70 FILIN,FILOUT,COMMAND,DUMMY,S1
    LOGICAL EXST,OPNED
    EXTERNAL FX
    COMMON/DATA/CPEX1,T1,IT,NT,NS
    COMMON/CONST/CONST,NTERMS
    COMMON/TOL/TOL,TSTEP
    COMMON/TEMPFIT/TFIT,F
    COMMON/FLAG/IREPEAT,DELPCT,IFLG
    COMMON/NROTOR/NROTOR
  DATA NPTS/7/
  DATA IFLAG/'END'/
  DATA IC1,IC2,IC3,IC4/1,2,3,4/
    T(1)=300.0
    T(2)=400.0
    T(3)=500.0
    T(4)=600.0
    T(5)=800.0
    T(6)=1000.0

```



```

T(7)=1500.0
TEST(1)=300.
TEST(2)=350.
TEST(3)=400.
TEST(4)=425.
TEST(5)=450.
TEST(6)=475.
TEST(7)=500.
TEST(8)=550.
TEST(9)=575.
TEST(10)=600.
T0=298.15
TLO=300.0
THI=5000.0
TMID=1500.0
TOL=1.0E-4
TSTEP=0.0
14  FORMAT(A14)
      COMMAND=' '
      FILIN=' '
      FILOUT=' '
      INQUIRE(FILE='THERMFIT.TMP',EXIST=EXST)
      IF(EXST)THEN
          OPEN(45,FILE='THERMFIT.TMP',STATUS='OLD')
          READ(45,3)COMMAND
          READ(45,3)FILIN
          READ(45,3)FILOUT
          CLOSE(45,STATUS='DELETE')
          GOTO 123
      ENDIF
      WRITE(*,*)'ENTER FILENAME FOR INPUT (.LST) '
      READ(*,3)FILIN
3    FORMAT(A70)
      CALL FNAME(FILIN,'LST')
      WRITE(*,*)'ENTER FILENAME FOR OUTPUT (.DAT) '
      READ(*,3)FILOUT
      CALL FNAME(FILOUT,'DAT')
123  CONTINUE
      INQUIRE(FILE=FILIN,EXIST=EXST)
      IF(EXST)GOTO 324
      STOP 2
324  OPEN(1,FILE=FILIN,STATUS='OLD')
      OPEN(3,FILE=FILOUT,STATUS='UNKNOWN')
      IF(COMMAND.EQ.' ')THEN
          WRITE(*,*)' '
          WRITE(*,*)' '
          WRITE(*,*)' GENERATING NASA FORMAT DATABASE FROM'
          WRITE(*,*)' ',FILIN
          WRITE(*,*)' '
          WRITE(*,*)'           please wait'
      ENDIF
      WRITE(3,99)
      WRITE(3,98)
99  FORMAT('THERMO ',73(' '))

```

```

98 FORMAT(' 300.000 1500.000 5000.000 ',49(' '))
1 ICOUNT=1
  READ(1,3)DUMMY
  CALL DBLNK(DUMMY,LEN,0)
  CONST(1)=1.0
  FUNITS='KCAL'
  IF(DUMMY(:6).EQ.'UNITS:')THEN
    IF(DUMMY(7:8).EQ.'KJ')THEN
      FUNITS='KJ'
      CONST(1)=4.184
    ENDIF
  READ(1,3)DUMMY
  ENDIF
95 FORMAT(5A6/,21A6)
  read(1,14)nul
20 CONTINUE
  DO 203 IK1=1,20
203 DELPCT(IK1)=0.0
  YERRS=1.0E+7
  IREPEAT=0
  IFLG=0
  IPOLY=0
  IPOLYC=0
  CFLAG=' '
  THI=5000.
  READ(1,'(1X,A4)',END=900)INAME
  IF(INAME.EQ.' ')THEN
    GOTO 20
  ELSE
    BACKSPACE(1)
  ENDIF
  IF(FUNITS.EQ.'KCAL')THEN
    READ(1,170,END=900)CFLAG,INAME,XNAME,HF298,S298,(CPL(I),I=1,7),
    1 (REF(I),I=1,2),REF3, (IE(I),NE(I),I=1,4),PHASE,NROT
170 FORMAT(A1,A4,A6,F7.2,2X,F7.2,3X,7(F6.2,2X),2A4,A6,
    1 3X,4(A2,I3,1X),A1,1X,I1)
    ELSE IF(FUNITS.EQ.'KJ')THEN
    READ(1,176,END=900)CFLAG,INAME,XNAME,HF298,S298,(CPL(I),I=1,7),
    1 (REF(I),I=1,2),REF3, (IE(I),NE(I),I=1,4),PHASE,NROT
176 FORMAT(A1,A4,A6,F8.2,1X,F8.2,2X,7(F7.2,1X),2A4,A6,3X,4(A2,I3,
    + 1X),A1,1X,I1)
  ENDIF
  IF(INAME(:3).EQ.'END') THEN
    WRITE(3,1012)
1012 FORMAT('END',77(' '))
1011 FORMAT(A4)
    STOP 'END OF THERMFIT'
  ENDIF
  IF(CFLAG.EQ.' ')THEN
    WRITE(*,'(1X,A4,A6)')INAME,XNAME
  ELSE
    WRITE(*,'(1X,A4,A6,2X,A1)')INAME,XNAME,CFLAG
  ENDIF
C---CONVERTING HF298 TO CAL/MOLE OR J/MOLE

```

```

      IF(FUNITS.EQ.'KCAL')THEN
        HF298=HF298*1000.
      ELSEIF(FUNITS.EQ.'KJ')THEN
        HF298=HF298*1000.0/4.184
        S298=S298/4.184
      ENDIF
    TRA(1)=300.
      NS=0
      NATOM=0
      ICARBON=0
      NCARBON=0
      DO 765 IIJ=1,4
        IF(IE(IIJ).EQ.'C'.OR.IE(IIJ).EQ.'C')THEN
          ICARBON=1
          NCARBON=NE(IIJ)
        ENDIF
765      NATOM=NATOM+NE(IIJ)
      *      WRITE(*,*)'NATOM= ',NATOM
986      CONTINUE
      *      BYPASS FITTING ROUTINE IF ATOM OR Cp <> F(T)
        DIF1=DABS(CPL(1)-CPL(3))
        DIF2=DABS(CPL(1)-CPL(6))
        DIFF=MAX(DIF1,DIF2)
        IF(FUNITS.EQ.'KJ')DIFF=DIFF/4.184
        IF(NATOM.NE.1.AND.DIFF.GT.0.01)THEN
          IF((ICARBON.EQ.1.AND.(NATOM-NCARBON).EQ.2).OR.NATOM.EQ.2
+)THEN
            NS=(3*NATOM)-5
            CONST(2)=FLOAT(NS)
            CONST(3)=1.0
            CPINFIN=1.987*(FLOAT(3*NATOM)-1.5)*CONST(1)
          ELSE
            NS=(3*NATOM)-6
            CONST(3)=0.0
      *      count hindered rotor as 1/2 degree of freedom
      *      CONST(2)=FLOAT(NS)-(FLOAT(NROT)/2.0)
            CONST(2)=FLOAT(NS)-(FLOAT(NROT))
            CPINFIN=1.987*(FLOAT(3*NATOM)-(2+(FLOAT(NROT)/2.0)))*
+)CONST(1)
          ENDIF
          IF(CPL(7).EQ.0.0)THEN
            NT=6
          ELSE
            NT=7
          ENDIF
          IF(CFLAG.EQ.'**')THEN
            IFLG=2
            GOTO 1994
          ENDIF
          CALL THCPFIT(NT,CPL,NATOM,B,T,CPINFIN)

```

***** POLYNOMIAL SMOOTHING PROCEDURE *****

```

      IF(IFLG.EQ.1)THEN

```

```

DO 1678 IK1=1,NT
DO 1677 IK2=1,5
1677 X(IK1,IK2,1)=T(IK1)**(IK2-1)
CPFIT(IK1)=CPL(IK1)/(1.987*CONST(1))
Y(IK1,1,1)=CPFIT(IK1)
1678 CONTINUE
MDEG=4
NPTS=NT
CALL LINLSQ(X,Y,B1,4,NPTS,1,1,SSR,AVGERR)
DO 1679 IK1=1,5
1679 C(IK1)=B1(IK1,1,1)
DO 1680 IK1=1,10
TIN=TEST(IK1)
CPEST(IK1)=CPT(0,TIN,C)*1.987*CONST(1)
1680 CONTINUE
CALL THCPFIT(10,CPEST,NATOM,B,TEST,CPINFIN)

ENDIF
1994 CONTINUE
IF(IFLG.EQ.2)THEN
IFLG=0
* POLYNOMIAL SMOOTHING DID NOT HELP OR USER SPECIFIES
* POLYNOMIAL FIT ONLY THEN
* DEFAULT TO SINGLE REPEATED POLYNOMIAL
* OVER TRANGE 300 - 2000 K
IF(CPL(7).EQ.0.)THEN
CPL(7)=CPL(6)+(0.37*(CPINFIN-CPL(6)))
ENDIF
CPL(8)=CPL(7)+(0.37*(CPINFIN-CPL(7)))
T(8)=2000.
DO 61678 IK1=1,8
DO 61677 IK2=1,5
61677 X(IK1,IK2,1)=T(IK1)**(IK2-1)
CPFIT(IK1)=CPL(IK1)/(1.987*CONST(1))
Y(IK1,1,1)=CPFIT(IK1)
61678 CONTINUE
MDEG=4
NPTS=8
CALL LINLSQ(X,Y,B1,4,NPTS,1,1,SSR,AVGERR)
DO 61679 IK1=1,5
61679 C(IK1)=B1(IK1,1,1)
DO 61681 IK1=1,5
F(IK1)=C(IK1)
F(IK1+7)=C(IK1)
61681 CONTINUE

C6=F6(0,(HF298/1.987),T0,F)
C7=(S298/1.987)-F(1)*DLOG(T0)-F(2)*T0-F(3)/2.*T0**2
1 -F(4)/3.*T0**3-F(5)/4.*T0**4
F(6)=C6
F(13)=C6
F(7)=C7
F(14)=C7
TMID=1000.
THI=2000.0

```

```

        ICOUNT=0
6545      DCPDT=DCPT(0,THI,F)
        COMPARE=((ABS(DCPDT)*500.)/CPT(0,THI,F))*100.
        IF(DCPDT.LT.0..AND.COMPARE.GT.10.)THEN
            ICOUNT=ICOUNT+1
            THI=THI-50.
            IF(ICOUNT.LE.100)GOTO 6545
        ENDIF
        GOTO 12987
    ENDIF
*****
    ENDIF
73590    CONTINUE
        DO 431 JK=1,2
        IF(NATOM.NE.1.AND.DIFF.GT.0.01)THEN
        IF(IPOLY.EQ.1)THEN
            IF(JK.EQ.1)THEN
                TK=253.3333
                DO 1290 I8=1,15
                    TK=TK+46.6667
                    TFIT(I8)=TK
                    TFIT(I8+15)=1000.+(71.4236*FLOAT(I8-1))
1290      CONTINUE
                *      set lower temperature below room temp so that 298 is not
                *      outside the range of the regression for Cp
                    TFIT(1)=273.15
                    ELSE
                    TK=928.5764
                    DO 1291 I8=1,15
                        TFIT(I8)=1000.+(71.4236*FLOAT(I8-1))
                        TFIT(I8+15)=2000.+(266.667*FLOAT(I8))
1291      CONTINUE
                    ENDIF
                ELSEIF(IPOLY.EQ.0)THEN
                    IF(JK.EQ.1)THEN
                        TK=236.6667
                        DO 21290 I8=1,15
                            TK=TK+63.3333
                            TFIT(I8)=TK
                            TFIT(I8+15)=1250.+(35.714*FLOAT(I8-1))
21290      CONTINUE
                        *      set lower temperature below room temp so that 298 is not
                        *      outside the range of the regression for Cp
                            TFIT(1)=273.15
                            ELSE
                            DO 21291 I8=1,15
                                TFIT(I8)=1250.+(35.714*FLOAT(I8-1))
                                TFIT(I8+15)=1700.+(283.333*FLOAT(I8))
21291      CONTINUE
                            ENDIF
                        ELSEIF(IPOLY.EQ.3)THEN
                            IF(JK.EQ.1)THEN
                                TK=263.333
                                DO 22290 I8=1,15

```

```

                                TK=TK+36.667
                                TFIT(18)=TK
                                TFIT(18+15)=850.+(35.714*FLOAT(18-1))
22290                                CONTINUE
*                                set lower temperature below room temp so that 298 is not
*                                outside the range of the regression for Cp
                                TFIT(1)=273.15
                                ELSE
                                DO 22291 I8=1,15
                                        TFIT(18)=850.+(35.714*FLOAT(18-1))
                                        TFIT(18+15)=1350.+(310.0*FLOAT(18))
22291                                CONTINUE
                                ENDIF
                                ELSEIF(IPOLY.EQ.2)THEN
                                IF(JK.EQ.1)THEN
                                TK=263.333
                                DO 23290 I8=1,15
                                        TK=TK+36.667
                                        TFIT(18)=TK
                                        TFIT(18+15)=850.+(21.429*FLOAT(18-1))
23290                                CONTINUE
*                                set lower temperature below room temp so that 298 is not
*                                outside the range of the regression for Cp
                                TFIT(1)=273.15
                                ELSE
                                DO 23291 I8=1,15
                                        TFIT(18)=850.+(21.429*FLOAT(18-1))
                                        TFIT(18+15)=1150.+(323.333*FLOAT(18))
23291                                CONTINUE
                                ENDIF
                                ENDIF
                                TRA(1)=300.
                                TRA(2)=1000.
                                DO 30 I=1,30
                                DO 31 I11=1,5
31 X(I,I11,1)=TFIT(1)**(I11-1)
                                TIN=TFIT(1)
                                CPFIT(1)=CPSERIES(B,TIN)
                                Y(I,1,1)=CPFIT(1)
30 CONTINUE
                                MDEG=4
                                RSQ=100.
                                IER=0
                                NPTS=30
                                CALL LINLSQ(X,Y,B1,4,NPTS,1,1,SSR,AVGERR)
                                DO 32 I=1,5
32 C(I)=B1(I,1,1)
                                ELSE
*                                ATOM: USE DIFFERENT METHOD FOR Cp
C BYPASS FITTING ROUTINE IF CP <> f(T)
                                SUMCP=0.0
                                DATPNT=0.0
                                DO 1209 IJK=1,7

```

```

                IF(CPL(IJK).NE.0.0)THEN
                    SUMCP=SUMCP+CPL(IJK)
                    DATPNT=DATPNT+1.0
                ENDIF
1209          CONTINUE
                C(1)=SUMCP/(1.98717*DATPNT)
                IF(FUNITS.EQ.'KJ')C(1)=C(1)/4.184
                DO 15 I=2,5
                    C(I)=0.0
15          CONTINUE
                TMID=1000.
        ENDIF
                IF(JK.EQ.1)THEN
                    DO 75 I=1,5
                        F(I)=C(I)
75          CONTINUE
                ELSEIF(JK.EQ.2)THEN
                    DO 85 J=1,5
85          F(J+7)=C(J)
                ENDIF
431          CONTINUE
C          CALCULATE CONST C6 IN ENTHALPY EXPRESSION

*          MUST INSERT HERE CALC OF Hf & S SO THAT 1st DERIVATIVE AND
*          FUNCTION VALUES MATCH AT T BREAK POINT
*
*          TO DO THIS WE HOLD (C1-C5, C8-C12) CONSTANT AND SOLVE FOR C6,C13
*          SUCH THAT Hf1(Tbp)=Hfh(Tbp)
*          MUST INTEGRATE CP BETWEEN 298 AND Tbp
*
*          WE MUST PERFORM A SIMILAR DETERMINATION FOR S TO GET C7,C14
*
C
                C6=F6(0,(HF298/1.987),T0,F)
C
C          CALCULATE CONST C7 FROM ENTROPY EXPRESSION
C
                C7=(S298/1.987)-F(1)*DLOG(T0)-F(2)*T0-F(3)/2.*T0**2
                1-F(4)/3.*T0**3-F(5)/4.*T0**4

*          USE F(6) TO DETERMINE HF(Tbp)
                F(6)=C6
                F(7)=C7
                H0=HF(0,T0,F)*1.987*T0
                S0=ST(0,T0,F)*1.987
**          determine break point temperature
                IF(NATOM.NE.1.AND.CFLAG.NE.'**')THEN
                    TINIT=(TFIT(1)+TFIT(15))/2.0
                    CALL TBREAK (TMID,TINIT)
                    TMID=FLOAT(INT(TMID+0.5))
                ELSE
                    TMID=1000.
                ENDIF

```

```

**      THESE MUST BE DETERMINED TO SATISFY  $H(T_{bp})_l = H(T_{bp})_h$ .
      HFTMID=HF(0,TMID,F)*1.987*TMID
      STMID=ST(0,TMID,F)*1.987
      F(13)=F6(7,(HFTMID/1.987),TMID,F)
      C14=(STMID/1.987)-F(8)*DLOG(TMID)-F(9)*TMID-F(10)/2.*TMID**2
      1-F(11)/3.*TMID**3-F(12)/4.*TMID**4
      F(14)=C14
      HCKTM=HF(7,TMID,F)*1.987*TMID
      SCKTM=ST(7,TMID,F)*1.987
      DELTACP=100.*((CPT(7,TMID,F)-CPT(0,TMID,F))/CPT(0,TMID,F))
      DDELCP=DCPT(7,TMID,F)-DCPT(0,TMID,F)
      DELTAS=100.*((ST(7,TMID,F)-ST(0,TMID,F))/ST(0,TMID,F))
      DDELS=DST(7,TMID,F)-DST(0,TMID,F)
      DELTAH=100.*((HF(7,TMID,F)-HF(0,TMID,F))/HF(0,TMID,F))
      DDELH=DHF(7,TMID,F)-DHF(0,TMID,F)
      YERR=0.0
      IF(ABS(DELTAS).GT.(50.*TOL).OR.ABS(DELTAC).GT.(50.*TOL)
+.OR.ABS(DDELH).GT.(20.*TOL).OR.ABS(DDELS).GT.(20.*TOL).OR
+ABS(DELTACP).GT.(50.*TOL).OR.ABS(DDELCP).GT.(20.*TOL))THEN
      IF(ABS(DELTAC).GT.(50.*TOL))THEN
          YERR=ABS(DELTAC)
          WRITE(*,1960)ABS(DELTAC)
1960      FORMAT(1X,'Tmid mismatch: % delta Cp(Tmid) = ',1PE10.3)
      ENDIF
      IF(ABS(DDELCP).GT.(20.*TOL))THEN
          IF(ABS(DDELCP).GT.YERR)YERR=ABS(DDELCP)
          WRITE(*,1961)ABS(DDELCP)
1961      FORMAT(1X,'Tmid mismatch: delta dCp(Tmid) = ',1PE10.3)
      ENDIF
      IF(ABS(DELTAS).GT.(50.*TOL))THEN
          IF(ABS(DELTAS).GT.YERR)YERR=ABS(DELTAS)
          WRITE(*,1962)ABS(DELTAS)
1962      FORMAT(1X,'Tmid mismatch: % delta Hf(Tmid) = ',1PE10.3)
      ENDIF
      IF(ABS(DDELH).GT.(20.*TOL))THEN
          IF(ABS(DDELH).GT.YERR)YERR=ABS(DDELH)
          WRITE(*,1963)ABS(DDELH)
1963      FORMAT(1X,'Tmid mismatch: delta dhf(Tmid) = ',1PE10.3)
      ENDIF
      IF(ABS(DELTAC).GT.(50.*TOL))THEN
          IF(ABS(DELTAC).GT.YERR)YERR=ABS(DELTAC)
          WRITE(*,1964)ABS(DELTAC)
1964      FORMAT(1X,'Tmid mismatch: % delta S(Tmid) = ',1PE10.3)
      ENDIF
      IF(ABS(DDELS).GT.(20.*TOL))THEN
          IF(ABS(DDELS).GT.YERR)YERR=ABS(DDELS)
          WRITE(*,1965)ABS(DDELS)
1965      FORMAT(1X,'Tmid mismatch: delta dS(Tmid) = ',1PE10.3)
      ENDIF
      IF(IPOLY.EQ.0.AND.IPOLYC.EQ.0)THEN
          WRITE(*,*)' repeating polynomial fitting routine'
          write(*,*)' with a different overlap region'
          YERRS=YERR
          YERR1=YERR

```



```

IPOLYC=IPOLYC+1
IPOLY=1
SSRS(1)=SSR
TM(1)=TMID
DO 1357 IK1=1,14
1357 FS(1,IK1)=F(IK1)
GOTO 73590
ELSEIF(IPOLY.EQ.1)THEN
WRITE(*,*)' SECOND REGRESSION FAILED TO MATCH'
WRITE(*,*)' PROPERTY AT THE MID-POINT'
WRITE(*,*)' MAKING A THIRD ATTEMPT TO FIT THE DATA'
DO 13571 IK1=1,14
13571 FS(2,IK1)=F(IK1)
IPOLY=2
YERR2=YERR
SSRS(2)=SSR
TM(2)=TMID
GOTO 73590
ELSEIF(IPOLY.EQ.2)THEN
WRITE(*,*)' THIRD ATTEMPT TO MATCH PROPERTIES '
WRITE(*,*)' AT THE MIDPOINT HAS FAILED'
WRITE(*,*)' LAST REGRESSION IN PROGRESS'
IPOLY=3
SSRS(3)=SSR
YERR3=YERR
TM(3)=TMID
DO 13572 IK1=1,14
13572 FS(3,IK1)=F(IK1)
GOTO 73590
ELSEIF(IPOLY.EQ.3)THEN
IF(YERR1.LT.YERR2)THEN
IF(YERR1.LT.YERR3)THEN
KEEP=1
ELSE
KEEP=3
ENDIF
ELSE
IF(YERR2.LT.YERR3)THEN
KEEP=2
ELSE
KEEP=3
ENDIF
ENDIF
WRITE(*,*)' best regression is # ',keep
DO 24 IK2=1,14
24 F(IK2)=FS(KEEP,IK2)
TMID=TM(KEEP)
ENDIF
ENDIF

```

```

*
* F ( 1-7 ) : LOW TEMPERATURE COEFFICIENTS
* F ( 8-14 ) : HIGH TEMPERATURE COEFFICIENTS
*
* REMEMBER: NASA FORMAT FIRST 7 COEFFICIENTS (HIGH TEMP)

```

```

*                               SECOND 7 COEFFICIENTS (LOW TEMP)
*
12987      CONTINUE
          WRITE(3,1010) INAME,XNAME,(REF(I),I=1,2),REF3,(IE(I),NE(I),I=1,
1 4),PHASE,TLO,THI,TMID,NROT,IC1
          WRITE(3,112) F(8),F(9),F(10),F(11),F(12),IC2
          WRITE(3,112)F(13),F(14),F(1),F(2),F(3),IC3
          WRITE(3,113)F(4),F(5),F(6),F(7),IC4
1010  FORMAT(A4,A6,2A4,A6,4(A2,I3),A1,2F10.3,F9.3,4X,2I1)
112  FORMAT(5(1PE15.8),I5)
113  FORMAT(4(1PE15.8),15X,I5)
          ICOUNT=ICOUNT+1
          GO TO 20
900  WRITE(3,1012)
          CLOSE(1,STATUS='KEEP')
          CLOSE(3,STATUS='KEEP')

          STOP
          END

```

SUBROUTINE THCPFIT(NT,CP,NATOM,A1,TEMPIN,CPINF)

\$LARGE

C

IMPLICIT REAL*8(A-H,O-Z)

```

CHARACTER*8 FMT1
CHARACTER*39 FMT2
CHARACTER*33 FMT3A(5)
CHARACTER*44 FMT3B
CHARACTER*21 FMT4A(5)
CHARACTER*13 FMT4B
CHARACTER*1 PLTCHR,DIGIT(10)
CHARACTER*72 TITLE(20),TEXT
CHARACTER*4 BLANK,TEST
CHARACTER*72 FIN, FOUT
LOGICAL DONE, NEG
REAL*8 NORML, MEAN
DIMENSION B(6),BMIN(6),BMAX(6),Y(20),Z(20),PDERIV(6,20),
@      BI(6),ZI(20),CONV(5),X(1,20),NORMAL(7,7),WORK(7),
@      SCALE(6),GRAD(6),DIAG(7),CONST(3),VAR(6),STD(6),
@      IPIVOT(6), COVAR(6,6), NORML(7,7), DIAG2(6),
@      IX(120), XTEMP(120),CP(30),A1(6),DELPCT(20),BS(5),
@      BSMIN(5),BSMAX(5),TEMPIN(*)
DOUBLE PRECISION SUMSQ,B,BMIN,BMAX,BI,NORMAL,GRAD,WORK,DIAG,CONST
@,SCALE,BTEMP,MLARGE,PLARGE,AVG,COEF2,COEF3,A1,CP,BS,BSMIN,BSMAX,
@BTMP,TEMPIN
INTEGER PARM,DATA,ERROR,ERROR2,INPUT,OUTPUT,
%      OPTION,FREQ,MAXPAR,MAXIND,
%      MAXDAT,NTITLE,MAXIT,NIND,OPT2,INTMSK,
%      PRTOPT,PLTOPT,MAXCON,NT,BFLAG
EQUIVALENCE (IPIVOT(1), SCALE(1)), (COVAR(1,1), PDERIV(1,1)),
@      (NORML(1,1), NORMAL(1,1)), (DIAG2(1), DIAG(1)),
@      (IOVER1, OVERF1), (IOVER2, OVERF2),
@      (IX(1), PDERIV(1,1)), (XTEMP(1), PDERIV(1,1))
COMMON /DINFO/ IPARM1, IDATA, IPARM, INDPT
COMMON /CONST/ CONST,NTERMS
COMMON /PDV/ PDERIV
COMMON/FLAG/IREPEAT,DELPCT,IFLAG
      SAVE BSMAX,BSMIN,BS
DATA INPUT/5/,OUTPUT/6/,BLANK/' ',MAXPAR/20/,MAXIND/10/
DATA MAXDAT/400/,MAXCON/40/
DATA MLARGE/-1.6D308/,PLARGE/1.6D308/
DATA FMT1/'(8F10.5)'/,DONE/.TRUE./
DATA FMT2/'(3X /(9H      B(,12,4H) =,1PE16.7))'/
DATA FMT3A/'(3X /8H      ,1(1HX,11,12X))\)',
&      '(3X /8H      ,2(1HX,11,12X))\)',
&      '(3X /8H      ,3(1HX,11,12X))\)',
&      '(3X /8H      ,4(1HX,11,12X))\)',
&      '(3X /8H      ,5(1HX,11,12X))\)'
DATA FMT3B/'(2HX,13X,2HY,13X,2HYC,11X,4HYC-Y,10X,3HPCT//) '/
DATA FMT4A/'(5H      ,4(1PE14.5))\)','(5H      ,5(1PE14.5))\)',
&      '(5H      ,6(1PE14.5))\)','(5H      ,7(1PE14.5))\)',
&      '(5H      ,8(1PE14.5))\)', FMT4B/'(1H ,OPF10.2)'/
DATA DIGIT/'0','1','2','3','4','5','6','7','8','9',PLTCHR/'0'/

```

```

      CALL RESET
      IPARM = MAXPAR
      IDATA = MAXDAT
      IPARM1 = MAXPAR + 1
      INDPT = MAXIND
100  NTITLE = 1
110  CONTINUE
1   FORMAT(A72)
120  CONTINUE
      FREQ=1000
      MAXIT=65
      CONV(1)=1.0E-2
      CONV(2)=1.0E-2
      CONV(3)=0.0
      CONV(3)=0.0
      CONV(4)=0.0
      CONV(5)=0.0
*   DEFINE DEFAULTS
      IREPEAT=0
      IREPNUM=0
      option=1
      opt2=1
      nprt=1
      prtopt=1
      pltopt=1
      icall=0
      parm=5
      nterms=3
      nind=1
      ISTART=1
8   FORMAT(3D10.8)
      iconst=3
      fvalue=0.
      tvalue=0.
32  FORMAT(7E10.0,8X,I2)
11  FORMAT(8D10.0)
*   CONST(1): GAS CONSTANT CONVERSION FACTOR;  CONST(1)=1.0 (CAL)
*   CONST(1)=4.184 (J)
*   CONST(2) = TOTAL NUMBER OF VIBRATIONAL DEGREES OF FREEDOM
*
*   CONST(3) = 0., IF NON-LINEAR MOLECULE; = 1., IF LINEAR
170 NIND1 = NIND + 1
C
C   FILL DATA POINT ARRAY WITH CP VALUES.
C
180 CONTINUE
      DO 190 IK1=1,NT
      Y(IK1)=CP(IK1)
      X(1,IK1)=TEMPIN(IK1)
190 CONTINUE
      DATA=NT+1
195 CONTINUE

```

```

*   DETERMINE TYPE OF MOLECULE:  LOW, MID, HIGH FREQUENCY
*   FROM CP(300)/CONST(2) :  HEAT CAPACITY PER OSCILLATOR
*       FIRST DATA POINT MUST BE CP(300)

**                               set last data point equal to cpinf
**                               at last temperature = 99999. K
**

                                Y(DATA)=CPINF

**                               continue test for frequency range
*
*       CPRATIO=Y(1)/CPINF

*   SET DEFAULT STARTING POINT TO MID FREQUENCY WEIGHTING
        CPRATIO=0.5
        IREPEAT=0
        IREPNUM=0
        IF(IFLAG.EQ.1)THEN
                DO 7634 IK1=1,5
                B(IK1)=BS(IK1)
                BMAX(IK1)=BSMAX(IK1)
                BMIN(IK1)=BSMIN(IK1)
7634         CONTINUE
        GOTO 9865
        ENDIF
9268     CONTINUE
        IF(IREPEAT.NE.0)THEN
                IREPNUM=IREPNUM+1
                IREPEAT=0
                IF(IREPNUM.GE.7)THEN
                        WRITE(*,*) ' CpFIT FAILURE '
                        IF(IFLAG.EQ.0)THEN
                                WRITE(*,*) ' POLYNOMIAL SMOOTHING OF DATA IN PROGRESS'
                                IFLAG=1
                        ELSE
                                WRITE(*,*) ' TEMPERATURE RANGE DEFAULTING TO 300 - 2000 K'
                                IFLAG=2
                        ENDIF
                        RETURN
                ENDIF
                IF(IREPNUM.GT.1)THEN
                        IBS=0
                        DO 9655 I=1,5
                        DELTAB=(ABS(BS(I)-B(I))/BS(I))
                        IF(DELTAB.GT.0.01)IBS=1
9655         CONTINUE
                        IF(IBS.EQ.0)THEN
                                IREPNUM=NREPEAT
                                IREPEAT=2
                                GOTO 600
                        ENDIF
                ENDIF
        IF(DELPCT(1).LE.0.0.AND.IREPNUM.EQ.1)THEN
                CPRATIO=0.75

```

```

DO 9651 I=1,5
BS(I)=B(I)
BSMIN(I)=BMIN(I)
BSMAX(I)=BMAX(I)
CONTINUE
BFLAG=0
ELSE IF(DELPCT(1).GT.0.0.AND.IREPNUM.EQ.1)THEN
CPRATIO=0.25
DO 9652 I=1,5
BS(I)=B(I)
BSMIN(I)=BMIN(I)
BSMAX(I)=BMAX(I)
CONTINUE
BFLAG=1
ELSEIF((DELPCT(1).LT.0.0.AND.DE LPCT(2).LT.0.0)
.AND.IREPNUM.GT.1)THEN
IF(ABS(B(3)-BMIN(3)).LE.0.1)THEN
BMIN(3)=BMIN(3)-50.
ELSE
IF(BFLAG.EQ.1)THEN
DO 9653 I=1,5
BTMP=B(I)
B(I)=(B(I)+BS(I))/2.0
BS(I)=BTMP
IF(BMAX(I).LT.BSMAX(I))BMAX(I)=BSMAX(I)
IF(BMIN(I).GT.BSMIN(I))BMIN(I)=BSMIN(I)
CONTINUE
ENDIF
ENDIF
BFLAG=0
GOTO 9865
ELSEIF((DELPCT(1).GT.0.0.AND.DE LPCT(2).GT.0.0)
.AND.IREPNUM.GT.1)THEN
IF(ABS(B(3)-BMIN(3)).LE.0.1)THEN
BMIN(3)=BMIN(3)+50.
B(3)=BMIN(3)+50.
ELSE
IF(BFLAG.EQ.0)THEN
DO 9654 I=1,5
BTMP=B(I)
B(I)=(B(I)+BS(I))/2.0
BS(I)=BTMP
IF(BMAX(I).LT.BSMAX(I))BMAX(I)=BSMAX(I)
IF(BMIN(I).GT.BSMIN(I))BMIN(I)=BSMIN(I)
CONTINUE
BLFAG=1
ELSE
BMIN(1)=0.
BMIN(2)=0.
BMIN(3)=100.
BMIN(4)=300.
BMIN(5)=700.
BMAX(1)=CONST(2)
BMAX(2)=CONST(2)

```

BMAX(3)=999.
BMAX(4)=1999.
BMAX(5)=3600.

ENDIF

ENDIF
GOTO 9865

ENDIF

ENDIF

```
* set initial parameter values, max & min
* RANGE DETERMINED BY CPRATIO
*   CPRATIO < 0.4 : VERY HIGH FREQUENCY WEIGHTED
*   0.4 < CPRATIO < 0.65 : MID FREQUENCY WEIGHTED
*   CPRATIO > 0.65 : LOW FREQUENCY WEIGHTED
* IF(CPRATIO.LT.0.4)THEN
*   starting point : high frequency weighted
*   B(1)=0.2*CONST(2)
*   B(2)=0.5*CONST(2)
*   B(3)=600.
*   B(4)=1500.
*   B(5)=3000.
*   BMIN(1)=0.
*   BMIN(2)=0.
*   BMIN(3)=350.
*   BMIN(4)=900.
*   BMIN(5)=1500.
*   BMAX(1)=0.6*CONST(2)
*   BMAX(2)=CONST(2)
*   BMAX(3)=1500.
*   BMAX(4)=2500.
*   BMAX(5)=3600.
*   IF(IREPNUM.NE.1)THEN
911     DO 911 IKJ=1,5
*       BS(IKJ)=B(IKJ)
*   ENDIF
* ELSE IF(CPRATIO.GE.0.4.AND.CPRATIO.LE.0.63)THEN
*   starting point : spread over range
*   B(1)=0.3*CONST(2)
*   B(2)=0.3*CONST(2)
*   B(3)=600.
*   B(4)=1200.
*   B(5)=2400.
*   BMIN(1)=0.
*   BMIN(2)=0.
*   BMIN(3)=250.
*   BMIN(4)=800.
*   BMIN(5)=900.
*   BMAX(1)=CONST(2)
*   BMAX(2)=CONST(2)
*   BMAX(3)=1500.
*   BMAX(4)=2500.
*   BMAX(5)=4000.
*   IF(IREPNUM.NE.1)THEN
```

```

DO 9121 IKJ=1,5
9121      BS(IKJ)=B(IKJ)
          ENDIF
          ELSE IF(CPRATIO.GT.0.63)THEN
*          starting point: low frequency weighted
*          parameters are constrained to low frequencies;
*          with lower minimum frequencies acceptable.
          B(1)=0.5*CONST(2)
          B(2)=0.4*CONST(2)
          B(3)=300.
          B(4)=500.
          B(5)=700.
          BMIN(1)=CONST(2)/10.
          BMIN(2)=CONST(2)/10.
          BMIN(3)=100.
          BMIN(4)=401.
          BMIN(5)=601.
          BMAX(1)=CONST(2)
          BMAX(2)=CONST(2)
          BMAX(3)=450.
          BMAX(4)=1000.
          BMAX(5)=2000.
          IF(IREPNUM.NE.1)THEN
DO 913 IKJ=1,5
913      BS(IKJ)=B(IKJ)
          ENDIF
          ENDIF
          GOTO 9865
13      FORMAT (/,10(' ',A72/))
23      FORMAT (/ ' ',15X,'INPUT DATA'// ' '   FORMAT FOR DATA POINTS'
*          ,5X,A8)
14      FORMAT (' NUMBER OF PARAMETERS',10X,I4/
#          ' MAXIMUM NO. OF ITERATIONS',5X,I4/
#          ' NUMBER OF DATA POINTS',9X,I4/
#          ' FREQUENCY OF PRINTING',9X,I4// ' COEFFICIENT',
#          6X,'STARTING',9X,'LOWER',11X,'UPPER'/' NUMBER',
#          10X,'VALUE',2(11X,'LIMIT')//30(17,7X,3(1PE16.8)/))
9865      ioutlim=0
9866      continue
          IREDUCE=0
          DO 200 ITER = ISTART,MAXIT

* SUBROUTINE SOLVE IS A CANNED MARQUARDT'S METHOD SUBROUTINE
* PROVIDED BY Dr. Dana Knox OF NJIT Chem.Eng. DEPT
* A LISTING OF THIS CODE IS NOT PROVIDED IN THIS THESIS

          CALL SOLVE (PARM,DATA,ERROR,ERROR2,B,BMIN,BMAX,Y,Z,
&          SUMSQ,CONV,NORMAL,SCALE,
&          WORK,GRAD,BI,ZI,DIAG,X )
          IF(SUMSQ.LT.CONV(1)) GOTO 600

C
C          CHECK FOR TERMINAL ERROR CODES FROM SUBROUTINE
C          SOLVE.
C

```



```

IF (ERROR .EQ. -1) GO TO 900
IF (ERROR .EQ. -2) GO TO 900
IF (ERROR .EQ. -3) then
    if(ioutlim.eq.1)goto 900
    ioutlim=1
    BMIN(1)=0.
    BMIN(2)=0.
    BMIN(3)=75.
    BMIN(4)=150.
    BMIN(5)=300.
    BMAX(1)=CONST(2)
    BMAX(2)=CONST(2)
    BMAX(3)=1500.
    BMAX(4)=3500.
    BMAX(5)=4500.
    GOTO 9866
endif
IF (ERROR .EQ. 0) GO TO 600
IF (ITER/FREQ*FREQ .NE. ITER) GO TO 20001
WRITE (OUTPUT,18) ITER,SUMSQ
18 FORMAT('0/' ITERATION',I4/'OSUM OF SQUARES',1PE17.8)
20001 continue
200 CONTINUE
WRITE (OUTPUT,19)
19 FORMAT ('/ MAXIMUM NUMBER OF ITERATIONS EXCEEDED')
ITER=MAXIT
600 CONTINUE
AI(1)=B(1)
AI(2)=B(2)
AI(3)=CONST(2)-(B(1)+B(2))
AI(4)=B(3)
AI(5)=B(4)
AI(6)=B(5)
20 FORMAT (' F I N A L R E S U L T S',I8,' ITERATIONS PERFORMED')
45 FORMAT ('/ SUM OF SQUARES = ',1PE17.8)
8764 FORMAT(1X,/,5X,'Cv vib: sum of ',i2,' terms!/)
8763 format(1x,'coef: A(i) exp: A(i+n)')
8765 format(1x,/,1PE10.3,' ',1PE10.3)
8990 FORMAT(1X,/, ' Cp = 4.0 + C vib (non-linear molecule)'
+ /)
8991 format(1x,/, ' Cp = 7/2 + C vib ( linear molecule)'
+ /)
* format(/, ' C vib =
8992 format(1x, ' n')
8993 format(1x, ' _____')
8994 format(1x, ' \ _____')
8995 format(1x, ' \ _____ 2 ex
+p(A(i+n)*(hc/kT))')
8996 format(1x, ' C vib = / A(i)*[A(i+n)*(hc/kT)] . _____
_____')
8997 format(1x, ' /_____
+ 2')
8998 format(1x,24x,'i',24x,'[1 - exp(A(i+n)*hc/kT)]'//)

```

```

        IF (NPRT .LT. NIND) NPRT = NIND
        IF (NPRT .GT. 5)      NPRT = 5
9987  FORMAT(1X, 'X', 13X, 'Y', 13X, 'YC', 11X, 'YC-Y', 10X, 'PCT', //)
        SUMP = 0.0
        DO 630 I = 1, DATA
            ZI(I) = Z(I) - Y(I)
            IF (Y(I) .EQ. 0.0) GO TO 620
            PCT = 100.0 * ZI(I) / Y(I)
            GO TO 625
620    PCT = 0.0
625    CONTINUE
            IF (ABS(PCT) .GT. 4.5 .AND. IREPEAT .NE. 2) THEN
                IREPEAT = 1
                DELPCT(I) = PCT
            ELSEIF (ABS(PCT) .GT. 5.5 .AND. IREPEAT .EQ. 2) THEN
                IREPEAT = 1
                IREPNUM = 7
                GOTO 9268
            ENDIF
            SUMP = SUMP + ABS(PCT)
630    CONTINUE
        SUMSQ = SUMSQ
        FDATA = DATA
        FPARM = PARM
        SEE = SQRT (SUMSQ / FDATA)
        AVP = SUMP / FDATA
        IRDF = DATA - PARM
        RDF = IRDF
        RMS = SUMSQ / RDF
        RRMS = SQRT(RMS)
22    FORMAT('O  CONSTANTS : ', 1P8D12.5/)
21    FORMAT ('/ STANDARD ERROR OF ESTIMATE =', 1PE15.6/
@      ' ABSOLUTE AVERAGE PERCENT ERROR = ', 0PF7.2/
@      ' RESIDUAL DEGREES OF FREEDOM =', I4/
@      ' RESIDUAL MEAN SQUARE =', 1PE15.6/
@      ' RESIDUAL ROOT MEAN SQUARE =', E15.6)
        IF (IREPEAT .NE. 0) THEN
            CALL RESET
            GOTO 9268
        ENDIF
        RETURN
900    WRITE(*,*) ' ERROR ENCOUNTERED IN SUBROUTINE CPFIT'
        WRITE(*,*) ' ERROR CODE = ', ERROR
        WRITE(*,*) '   B(I)   BMIN(I)   BMAX(I)'
        DO 912 IK1 = 1, 5
912    WRITE(*, '(1X, 3(F10.3, 1X))') B(IK1), BMIN(IK1), BMAX(IK1)
        STOP ' CPFIT TERMINATED DUE TO ERROR'
END

```

APPENDIX IV - E

CALCULATION OF HEAT CAPACITY
AND EFFECT OF HINDERED INTERNAL ROTATION

JANAF : HEXAFLUOROETHANE : C2F6

NON - LINEAR MOLECULE

Cp_{inf} (cal/mol K) = 37.75

NUMBER OF OSCILLATORS = 17

Arithmetic mean frequency = 745.765 (1/cm)

Geometric mean frequency = 637.699 (1/cm)

Root Mean Square frequency = 838.446 (1/cm)

Mean Square frequency = 7.030E+05 (1/cm²)

Square of Mean frequency = 5.562E+05 (1/cm²)

modified frequency dispersion parameter = 1.190E+00

TEMP(K)	Cp(cal/mol K)	Cp(J/mol K)	1/Qf	V/RT	Cp		Cp JANAF
					Cp _{ir} (J/mol K)	Cp _t (J/mol K)	
100.00	10.812	45.236					
200.00	17.588	73.589					
298.15	23.160	96.900					
300.00	23.253	97.289	0.0725	6.643	9.414	106.703	106.809
400.00	27.660	115.729	0.0628	4.982	9.76	125.49	125.545
500.00	30.954	129.510	0.0561	3.986	9.506	139.01	139.139
600.00	33.356	139.561	0.0521	3.322	9.109	148.67	148.708
700.00	35.105	146.879					
800.00	36.393	152.268	0.0444	2.49	8.03	160.3	160.31
900.00	37.357	156.302					
1000.00	38.092	159.377	0.0397	1.993	7.037	166.414	166.486
1100.00	38.662	161.761					
1200.00	39.111	163.641					
1300.00	39.471	165.145					
1400.00	39.762	166.365					
1500.00	40.002	167.368	0.0324	1.33	5.742	173.110	173.114
1600.00	40.201	168.200					
1700.00	40.368	168.898					
1800.00	40.509	169.489					
1900.00	40.629	169.994					
2000.00	40.733	170.427	0.028	0.996	5.104	175.53	175.548
2500.00	41.084	171.894					
3000.00	41.278	172.705					
3500.00	41.396	173.199					
4000.00	41.473	173.521					
4500.00	41.526	173.743					
5000.00	41.564	173.903	0.0178	0.3986	4.322	178.22	178.155
5500.00	41.592	174.021					
6000.00	41.613	174.111					

BIPHENYL: BURCAT, ZELEZNIK, McBride: NASA TECH MEMO# 83800: JAN 1985.

NON - LINEAR MOLECULE

Cp_{inf} (Kcal/mol) = 121.207

NUMBER OF OSCILLATORS = 59

Arithmetic mean frequency = 1308.508 (1/cm)

Geometric mean frequency = 1038.418 (1/cm)

Root Mean Square frequency = 1575.540 (1/cm)

Mean Square frequency = 2.482E+06 (1/cm²)

Square of Mean frequency = 1.712E+06 (1/cm²)

modified frequency dispersion parameter = 1.425E+00

TEMP(K)	Cp(cal/mol K)	Cp(J/mol K)	1/Qf	V/RT	Cp _{ig} (J/mol K)	Cp _t (J/mol K)
100.00	12.869	53.843				
200.00	24.017	100.489				
298.15	37.752	157.953				
300.00	38.016	159.059	0.0488	2.516	8.02	167.08
400.00	51.612	215.944	0.0423	1.887	6.85	222.79
500.00	63.049	263.799	0.038	1.51	6.067	269.87
600.00	72.232	302.220	0.0345	1.258	5.012	307.23
700.00	79.608	333.079				
800.00	85.622	358.241	0.0299	0.944	4.725	362.97
900.00	90.602	379.078				
1000.00	94.776	396.542	0.0267	0.755	4.72	401.26
1100.00	98.305	411.308				
1200.00	101.308	423.874				
1300.00	103.878	434.627				
1400.00	106.088	443.873				
1500.00	107.997	451.859	0.0218	0.503	4.42	456.28
1600.00	109.653	458.787				
1700.00	111.095	464.823				
1800.00	112.357	470.104				
1900.00	113.466	474.743				
2000.00	114.444	478.834	0.0189	0.377	4.286	483.12
2500.00	117.932	493.427				
3000.00	119.991	502.042				
3500.00	121.295	507.498				
4000.00	122.168	511.153				
4500.00	122.780	513.711				
5000.00	123.224	515.569	0.012	0.151	4.088	519.66
5500.00	123.556	516.958				
6000.00	123.811	518.024				

PROGRAM CPIDEAL

* THIS PROGRAM CALCULATES THE VIBRATIONAL CONTRIBUTION TO Cp *
 * GIVEN VIBRATIONAL FREQUENCIES FOR EACH OSCILATOR *
 *
 * WRITTEN BY: EDWARD RITTER 11/26/88 *

```

    IMPLICIT REAL*8 (A-H,O-Z)
    INTEGER NS, ND
    DIMENSION FREQ(100),T(30),CVI(100),THETA(100),GI(100)
    REAL*8 CP,CVV,MS,RMS,SMS
    nrot=0
    T(1)=100.
    T(2)=200.
    T(3)=298.15
    T(4)=300.0
    T(5)=400.0
    T(6)=500.0
    T(7)=600.
    T(8)=700.
    T(9)=800.0
    T(10)=900.
    T(11)=1000.0
    T(12)=1100.
    T(13)=1200.
    T(14)=1300.
    T(15)=1400.
    T(16)=1500.0
    T(17)=1600.
    T(18)=1700.
    T(19)=1800.
    T(20)=1900.
    T(21)=2000.0
    T(22)=2500.
    T(23)=3000.0
    T(24)=3500.
    T(25)=4000.
    T(26)=4500.
    T(27)=5000.
    T(28)=5500.
    T(29)=6000.0
    CALL INPUT(NS,ND,GI,FREQ)
    CALL CLS
    WRITE(*,*)' enter : 0 - non-linear molecule'
    write(*,*)'          1 - linear molecule'
    read(*,*)lin
    call lines(30,2)
    if(lin.eq.0)then
        write(30,*)' NON - LINEAR MOLECULE '
    else
        WRITE(30,*)'          LINEAR MOLECULE'
    endif
    IF(LIN.EQ.0)THEN
        write(*,*)' enter # of free rotors in this molecule '

```

```

        read(*,*)nrot
        NAT=(NS+6+nrot)/3
        CPINF=(3.0*FLOAT(NAT)-(2.0+(nrot/2.))*1.987
ELSE
        NAT=(NS+5)/3
        CPINF=(3.0*FLOAT(NAT)-(3./2.))*1.987
ENDIF
WRITE(30,*)' Cpinf (Kcal/mol) = ',CPINF
FARM=0.0
FGM=0.0
SS=0.0
SQM=0.0
DO 1999 I1=1,ND
SS=SS+(GI(I1)*(FREQ(I1)**2))
FGM=FGM+(GI(I1)*LOG(FREQ(I1)))
FARM=FARM+(GI(I1)*FREQ(I1))
1999 CONTINUE
MS=SS/FLOAT(NS)
FARM=FARM/FLOAT(NS)
FARMSQ=FARM**2
BETA=(FLOAT(NS-1)/FLOAT(NS))*(MS/FARMSQ)
FGM=EXP(FGM/FLOAT(NS))
RMS=MS**0.5
WRITE(30,*)' NUMBER OF OSCILLATORS = ',NS
WRITE(30,17000)FARM
17000 FORMAT(1X,5X,'Arithmetic mean frequency = ',f10.3,' ( 1/cm )')
WRITE(30,17001)FGM
17001 format(1x,5x,'Geometric mean frequency = ',f10.3,' ( 1/cm )')
WRITE(30,17004)RMS
17004 FORMAT(6X,'Root Mean Square frequency = ',f10.3,' ( 1/cm )')
WRITE(30,17002)MS
17002 format(6x,'Mean Square frequency = ',1pe15.3,' ( 1/cm^2 )')
WRITE(30,17003)FARMSQ
17003 format(6x,'Squre of Mean frequency = ',1pe15.3,' ( 1/cm^2 )')
WRITE(30,17005)BETA
17005 format(6x,'modified frequency dispersion parameter = ', 1pe15.3)
WRITE(*,17000)FARM
WRITE(*,17001)FGM
WRITE(*,17004)RMS
WRITE(*,17002)MS
WRITE(*,17003)FARMSQ
WRITE(*,17005)BETA
WRITE(30,7003)
10 CONTINUE

call lines(30,1)
call cls
WRITE(*,*)' enter : 1 - default temp range ( 300 - infin K)'
write(*,*)'          2 - enter a specific temperature'
write(*,*)'          3 - end program'
read(*,*)iop
if(iop.eq.1)then
        it=1
        nt=29

```

```

elseif(iop.eq.2)then
    call cls
    write(*,*)' enter Temperature (K)'
    read(*,*)T(1)
    it=1
    nt=1
else
    goto 301
endif
DO 300 J=IT,NT
CVV=0.0
CP=0.0
CPCAL=0.0
CPJ=0.0
CALL LINES(20,3)
WRITE(20,7000)T(J)
WRITE(20,7001)
DO 100 I=1,ND
CALL CVVIB(FREQ(I),T(J),CVI(I),THETA(I))
CVCONT=(CVI(I)*GI(I))
CVV=CVV+CVCONT
WRITE(20,7002)I,FREQ(I),THETA(I),GI(I),CVCONT
100 CONTINUE
WRITE(20,7005)T(J),CVV
if(lin.eq.0)then
    CP=CVV+4.0+(nrot/2.)
else
    CP=CVV+(7./2.)
endif
CPCAL=CP*1.987
CPJ=CPCAL*4.184
if(lin.eq.0)then
    WRITE(20,7007)
else
    write(20,7008)
endif
WRITE(20,7006)CP
WRITE(30,7004)T(J),CPCAL,CPJ
300 CONTINUE
WRITE(30,7004)99999.,CPINF,CPINF*4.184
if(iop.eq.2)goto 10
301 continue
CLOSE(20,STATUS='KEEP')
CLOSE(30,STATUS='KEEP')
WRITE(*,17000)FARM
WRITE(*,17001)FGM
WRITE(*,*)' NUMBER OF OSCILLATORS = ',NS
STOP ' have a nice day !'
7000 FORMAT(1X,' VIBRATIONAL CONTRIBUTION TO Cv AT ',F7.1,' deg K')
7001 FORMAT(1X,' i v (1/cm) THETAi gi Cv,vib i ')
7002 FORMAT(1X,13,5X,F8.3,5X,F8.2,5X,F6.2,5X,F8.3)
7003 FORMAT(1X,' TEMP(K) Cp(cal/mol K) Cp(J/mol K)')

```



```

7004 FORMAT(2X,F8.2,5X,F8.3,6X,F8.3)
7005     FORMAT(1X,9X,' T = ',F8.2,' K',3X,'Cv,vib = ',F5.2,' * R')
7006 FORMAT(1X,28X,'Cp,tot = ',F5.2,' * R')
7007     FORMAT(3X,'Trans and rot + convert Cv-> Cp = 4.00 * R')
7008 FORMAT(3X,'Trans and rot + convert Cv-> Cp = 7/2 * R')
      END

```

```

      SUBROUTINE INPUT(NS,ND,GI,FREQ)
      IMPLICIT REAL*8(A-H,O-Z)
      INTEGER NS,ND
      CHARACTER*70 SPEC, FN, FIN, FOUT, FTBL, spec2
      DIMENSION FREQ(100), GI(100)
      CALL CLS
      WRITE(*,*)'ENTER INPUT FILENAME'
      READ(*,70)FN
70     FORMAT(A70)
71     FORMAT(1X,A70)
      FIN=FN
      FOUT=FN
      FTBL=FN
      CALL FNAME(FIN,'INP')
      CALL FNAME(FOUT,'OUT')
      CALL FNAME(FTBL,'TBL')
      OPEN(10,FILE=FIN,STATUS='OLD')
      read(10,70)spec2
      if(spec2(:5).eq.'SHORT')FOUT='NUL'
      OPEN(20,FILE=FOUT,STATUS='UNKNOWN')
      OPEN(30,FILE=FTBL,STATUS='UNKNOWN')
      READ(10,70)SPEC
      WRITE(20,71)SPEC
      WRITE(30,71)SPEC
      CALL LINES(20,3)

      I=0
      S=0.
      NS=0
      ND=0
100    CONTINUE
      READ(10,*,END=200)FNUIN,DEGEN
      I=I+1
      FREQ(I)=FNUIN
      GI(I)=DEGEN
      S=S+DEGEN
      ND=I
      GOTO 100
200    CONTINUE
      NS=IDINT(S+.1)
      write(20,7001)
7001   format(5x,' FREQ(i)',3x,'gi')
      DO 300 I=1,ND
      WRITE(20,7000)FREQ(I),GI(I)
7000   FORMAT(5X,F8.3,2X,'(',F8.3,')')

```

```

300      CONTINUE
        CALL LINES(20,2)
        WRITE(20,7002)NS
7002    FORMAT(1X,' number of vibrational modes = ',I3)
        call lines(20,2)
        WRITE(30,*)NS
        CALL LINES(30,3)
        return
        end

```

```

SUBROUTINE CVVIB(FREQ,T,CV,THETA)
IMPLICIT REAL*8(A-H,O-Z)
REAL*8 HP,KB,C,NAVAG
HP=6.6256E-34
KB=1.3805E-23
C=3.0E+10
NAVAG=6.023E+23

```

*

```

THETA=((HP*C)/KB)*FREQ
X=THETA/T
TOP=EXP(X)
BOTTOM=(EXP(X)-1)**2
CV=(X**2)*(TOP/BOTTOM)
RETURN
END

```

APPENDIX IV - F

FORTRAN SOURCE CODE LISTING FOR

CPFIT

EXAMPLE INPUT FILE FOR CPFIT

.
. .
. C2H4O : DATA FROM THERM
. .
. REGRESSION OF Cp DATA vs. T TO A 5 PARAMETER HARMONIC OSCILLATOR
. .
. SERIES (3 TERMS) : C2H4O
. .

REPORT EVERY # ITER: MAX-ITER: CONV(1 - 5)
100, 75, 1.0E-3, 1.0E-3, 0.05, 0.0, 0.0
R CONVERSION: # VIB MODES: GEOMETRY 0.(NON-LIN) 1.(LIN)
4.184 15. 0.
300.00 48.45
400.00 64.14
500.00 75.56
600.00 85.10
800.00 102.09
1000.00 114.47

EXAMPLE OUTPUT FILE FROM CPFIT

.
 .
 . C2H4O : DATA FROM THERM
 .
 . REGRESSION OF Cp DATA vs. T TO A 5 PARAMETER HARMONIC OSCILLATOR
 . SERIES (3 TERMS) : C2H4O
 .

NUMBER OF PARAMETERS 5
 MAXIMUM NO. OF ITERATIONS 75
 NUMBER OF DATA POINTS 7
 FREQUENCY OF PRINTING 100

COEFFICIENT NUMBER	STARTING VALUE	LOWER LIMIT	UPPER LIMIT
1	4.50000018E+00	0.00000000E+00	1.50000000E+01
2	6.00000009E+00	0.00000000E+00	1.50000000E+01
3	6.00000000E+02	3.50000000E+02	9.99000000E+02
4	1.20000000E+03	9.00000000E+02	1.99900000E+03
5	2.40000000E+03	1.50000000E+03	3.60000000E+03

.
 .
 . C2H4O : DATA FROM THERM
 .
 . REGRESSION OF Cp DATA vs. T TO A 5 PARAMETER HARMONIC OSCILLATOR
 . SERIES (3 TERMS) : C2H4O
 .

F I N A L R E S U L T S 8 ITERATIONS PERFORMED

SUM OF SQUARES = 1.47886716E+00

B(1) = 4.5332389E+00
 B(2) = 4.5309800E+00
 B(3) = 9.7201365E+02
 B(4) = 9.7201365E+02
 B(5) = 2.6244423E+03

Cp = 4.0 + c vib (non-linear molecule)

$$c \text{ vib} = \sum_{i=1}^n \frac{A(i) \cdot [A(i+n) \cdot (hc/kT)]^2 \cdot \exp(A(i+n) \cdot (hc/kT))}{[1 - \exp(A(i+n) \cdot (hc/kT))]^2}$$

Cvvib: sum of 3 terms

coef: A(i)		exp: A(i+n)		
4.533E+00		9.720E+02		
4.531E+00		9.720E+02		
5.936E+00		2.624E+03		
X	Y	YC	YC-Y	PCT
3.000E+02	4.845E+01	4.905E+01	6.008E-01	1.240
4.000E+02	6.414E+01	6.329E+01	-8.469E-01	-1.320
5.000E+02	7.556E+01	7.551E+01	-5.066E-02	-.067
6.000E+02	8.510E+01	8.571E+01	6.087E-01	.715
8.000E+02	1.021E+02	1.020E+02	-8.404E-02	-.082
1.000E+03	1.145E+02	1.143E+02	-1.433E-01	-.125
1.000E+05	1.580E+02	1.580E+02	-7.092E-03	-.004
0	CONSTANTS : 4.18400D+00 1.50000D+01 0.00000D+00			

STANDARD ERROR OF ESTIMATE = 4.596376E-01
ABSOLUTE AVERAGE PERCENT ERROR = .51
RESIDUAL DEGREES OF FREEDOM = 2
RESIDUAL MEAN SQUARE = 7.394336E-01
RESIDUAL ROOT MEAN SQUARE = 8.599032E-01
NUMBER OF OSCILLATORS = 15.00000000000000

ESTIMATED ARITHMETIC MEAN FREQUENCY
1625.911

ESTIMATED GEOMETRIC MEAN FREQUENCY
1440.030

Root Mean Square frequency = 1815.633 (1/cm)
Mean Square frequency = 3.297E+06 (1/cm²)
Square of Mean frequency = 2.644E+06 (1/cm²)
modified frequency dispersion parameter = 1.164E+00

```

PROGRAM CPFIT
$LARGE
      IMPLICIT REAL*8(A-H,O-Z)
CHARACTER*8 FMT1
CHARACTER*39 FMT2
CHARACTER*33 FMT3A(5)
CHARACTER*44 FMT3B
CHARACTER*21 FMT4A(5)
CHARACTER*13 FMT4B
CHARACTER*1 PLTCHR,DIGIT(10)
CHARACTER*72 TITLE(20),TEXT
CHARACTER*4 BLANK,TEST
CHARACTER*72 FIN,FOUT
LOGICAL DONE,NEG
REAL*8 NORML,MEAN
DIMENSION B(20),BMIN(20),BMAX(20),Y(400),Z(400),PDERIV(20,400),
@      BI(20),ZI(400),CONV(5),X(10,400),NORMAL(21,21),WORK(21),
@      SCALE(20),GRAD(20),DIAG(21),CONST(40),VAR(6),STD(6),
@      IPIVOT(20),COVAR(20,20),NORML(21,21),DIAG2(20),
@      IX(800),XTEMP(8000),DELPCT(20),BS(20),BSMIN(20),
@      BSMAX(20)
DOUBLE PRECISION SUMSQ,B,BMIN,BMAX,BI,NORMAL,GRAD,WORK,DIAG,CONST
@      ,SCALE,BTEMP,MLARGE,PLARGE,AVG,COEF2,COEF3,
@      BS,BSMIN,BSMAX,BTMP
INTEGER PARM,DATA,ERROR,ERROR2,INPUT,OUTPUT,
%      OPTION,FREQ,MAXPAR,MAXIND,
%      MAXDAT,NTITLE,MAXIT,NIND,OPT2,INTMSK,
%      PRTOPT,PLTOPT,MAXCON,BFLAG
EQUIVALENCE (IPIVOT(1),SCALE(1)),(COVAR(1,1),PDERIV(1,1)),
@      (NORML(1,1),NORMAL(1,1)),(DIAG2(1),DIAG(1)),
@      (IOVER1,OVERF1),(IOVER2,OVERF2),
@      (IX(1),PDERIV(1,1)),(XTEMP(1),PDERIV(1,1))
COMMON /DINFO/ IPARM1, IDATA, IPARM, INDPT
COMMON /CONST/ CONST, NTERMS, NROT
COMMON /PDV/ PDERIV
DATA INPUT/5/,OUTPUT/6/,BLANK/'  ',MAXPAR/20/,MAXIND/10/
DATA MAXDAT/400/,MAXCON/40/
DATA MLARGE/-1.6D308/,PLARGE/1.6D308/
DATA FMT1/'(8F10.5)'/,DONE/.TRUE./
DATA FMT2/'(3X /8H      B(,12,4H) =,1PE16.7))'/
DATA FMT3A/'(3X /8H      ,1(1HX,11,12X)\)\',
&      '(3X /8H      ,2(1HX,11,12X)\)\',
&      '(3X /8H      ,3(1HX,11,12X)\)\',
&      '(3X /8H      ,4(1HX,11,12X)\)\',
&      '(3X /8H      ,5(1HX,11,12X)\)\'/
DATA FMT3B/'(2HX,13X,2HY,13X,2HYC,11X,4HYC-Y,10X,3HPCT//) '/
DATA FMT4A/'(5H      ,4(1PE14.5)\)\', '(5H      ,5(1PE14.5)\)\',
&      '(5H      ,6(1PE14.5)\)\', '(5H      ,7(1PE14.5)\)\',
&      '(5H      ,8(1PE14.5)\)\', FMT4B/'(1H ,OPF10.2)'/
DATA DIGIT/'0','1','2','3','4','5','6','7','8','9'/,PLTCHR/'O'/
WRITE(*,693)
READ(*,1) FIN
OPEN(5,FILE=FIN,STATUS='OLD')
WRITE(*,694)

```

```

      READ(*,1) FOUT
      OPEN(6,FILE=FOUT,STATUS='UNKNOWN')
693 FORMAT(' Enter the filename for the data points      :')
694 FORMAT(' Enter the filename for the output          :')
      WRITE(*,*)'ENTER # OF HIGH TEMP FREE ROTORS'
      READ(*,*)NROT
      NREPEAT=10
      RMXPCT=3.75
695 FORMAT(A10)
      CALL RESET
      IPARM = MAXPAR
      IDATA = MAXDAT
      IPARM1 = MAXPAR + 1
      INDPT = MAXIND
100  NTITLE = 1
110  READ (INPUT,1,END=900) TITLE(NTITLE)
1    FORMAT(A72)
      IF (TITLE(NTITLE).EQ.' ') GO TO 120
      IF (NTITLE .EQ. 9) GO TO 500
      NTITLE = NTITLE + 1
      GO TO 110
120  CONTINUE
      READ(INPUT,1,END=900)TEXT
      READ(INPUT,*)FREQ,MAXIT,CONV(1),CONV(2),CONV(3),CONV(4),CONV(5)
*    DEFINE DEFAULTS
      IREPNUM=0
      IREPEAT=0
      option=1
      opt2=1
      nprt=1
      prtopt=1
      pltopt=1
      icall=0
      parm=5
      nterms=3
      nind=1
      ISTART=1
8    FORMAT(3D10.8)
      iconst=3
      fvalue=0.
      tvalue=0.
32   FORMAT(7E10.0,8X,12)
11   FORMAT(8D10.0)
      READ(INPUT,1,END=900)TEXT
      READ (INPUT,*) (CONST(I), I = 1, ICONST)
*     CONST(1): GAS CONSTANT CONVERSION FACTOR;  CONST(1)=1.0 (CAL)
*                                           CONST(1)=4.184 (J)
*     CONST(2) = TOTAL NUMBER OF VIBRATIONAL DEGREES OF FREEDOM
*
*     CONST(3) = 0., IF NON-LINEAR MOLECULE; = 1., IF LINEAR
*
170  NIND1 = NIND + 1
C

```



```

C          READ IN THE DATA POINTS.
C
DATA = 1
180 READ (INPUT,*,END=190) X(1,DATA),Y(DATA)
DATA = DATA + 1
IF (DATA .GT. MAXDAT) GO TO 565
GO TO 180
190 CONTINUE
195 IF (FREQ .LE. 0)      FREQ = 1
IF (MAXIT .LE. 0)      GO TO 530
IF (PARM .LE. 0)       GO TO 520
IF (NIND .LE. 0)       GO TO 540
IF (PARM .GT. MAXPAR)  GO TO 550
IF (NIND .GT. MAXIND)  GO TO 560
*
* DETERMINE TYPE OF MOLECULE: LOW, MID, HIGH FREQUENCY
* FROM CP(300)/CONST(2) : HEAT CAPACITY PER OSCILLATOR
* FIRST DATA POINT MUST BE CP(300)
IF(CONST(3).EQ.0.)THEN
*
* non-linear molecule
*
RNATOM=((CONST(2)+6.0)/3.0)
CPINF=(3.0*RNATOM-(2.+(NROT/4.)))*1.987*CONST(1)
* empirically determined correction for # of rotors.
* theory gives nrot/2 but nrot/4 works better.
* CPINF=( 3.0 * NATOM - (2.0+(NROT/2.)))*1.987*CONST(1)*
* CONST(2)=CONST(2)-float(NROT/2.)
ELSE
* linear molecule
* NATOM=IDINT((CONST(2)+5.)/3.)
* CPINF=(3.0* NATOM - (3./2.))*1.987*CONST(1)
ENDIF
**
** set last data point equal to cpinf
** at last temperature = 99999. K
**
X(1,DATA)=99999.
Y(DATA)=CPINF
** continue test for frequency range
*
BFLAG=0
* CPRATIO=Y(1)/CPINF
CPRATIO=0.5
9268 CONTINUE
IF(IREPEAT.EQ.1)THEN
IREPNUM=IREPNUM+1
IREPEAT=0
IF(IREPNUM.GE.NREPEAT)THEN
STOP ' FIT PROCEDURE FAILED '
ENDIF
IF(IREPNUM.GT.1)THEN
IBS=0
DO 9655 I=1,5
if(bs(i).EQ.0.0)goto 9655

```

```

                                DELTAB=(ABS(BS(I)-B(I)))/BS(I)
                                IF(DELTAB.GT.0.01)IBS=1
9655                                CONTINUE
                                IF(IBS.EQ.0)THEN
                                        IREPNUM=NREPEAT
                                        IREPEAT=2
                                        GOTO 600
                                ENDIF
                                ENDIF
                                IF(DELPCT(1).LT.0.0.AND.IREPNUM.EQ.1)THEN
                                        CPRATIO=0.75
                                        DO 9651 I=1,5
9651                                BS(I)=B(I)
                                        BSMIN(I)=BMIN(I)
                                        BSMAX(I)=BMAX(I)
                                        CONTINUE
                                        BFLAG=0
                                ELSE IF(DELPCT(1).GT.0.0.AND.IREPNUM.EQ.1)THEN
                                        CPRATIO=0.25
                                        DO 9652 I=1,5
9652                                BS(I)=B(I)
                                        BSMIN(I)=BMIN(I)
                                        BSMAX(I)=BMAX(I)
                                        CONTINUE
                                        BFLAG=1
                                ELSEIF((DELPCT(1).LT.0.0.AND.DEHPCT(2).LT.0.0)
+                                .AND.IREPNUM.GT.1)THEN
                                        IF(ABS(B(3)-BMIN(3)).LE.0.1)THEN
                                                BMIN(3)=BMIN(3)-50.
                                        ELSE
9653                                IF(BFLAG.EQ.1)THEN
                                        DO 9653 I=1,5
                                                BTMP=B(I)
                                                B(I)=(B(I)+BS(I))/2.0
                                                BS(I)=BTMP
                                        IF(BMAX(I).LT.BSMAX(I))BMAX(I)=BSMAX(I)
                                        IF(BMIN(I).GT.BSMIN(I))BMIN(I)=BSMIN(I)
                                        CONTINUE
                                        ENDIF
                                ENDIF
                                        BFLAG=0
                                        GOTO 9238
                                ELSEIF((DEHPCT(1).GT.0.0.AND.DEHPCT(2).GT.0.0)
+                                .AND.IREPNUM.GT.1)THEN
                                        IF(ABS(B(3)-BMIN(3)).LE.0.1)THEN
                                                BMIN(3)=BMIN(3)+50.
                                                B(3)=BMIN(3)+50.
                                        ELSE
9653                                IF(BFLAG.EQ.0)THEN
                                        DO 9654 I=1,5
                                                BTMP=B(I)
                                                B(I)=(B(I)+BS(I))/2.0
                                                BS(I)=BTMP
                                        IF(BMAX(I).LT.BSMAX(I))BMAX(I)=BSMAX(I)

```

9654

```
IF(BMIN(1).GT.BSMIN(1))BMIN(1)=BSMIN(1)
CONTINUE
BLFAG=1
ELSE
    BMIN(1)=0.
    BMIN(2)=0.
    BMIN(3)=100.
    BMIN(4)=300.
    BMIN(5)=700.
    BMAX(1)=CONST(2)
    BMAX(2)=CONST(2)
    BMAX(3)=999.
    BMAX(4)=1999.
    BMAX(5)=3600.
ENDIF
```

```
ENDIF
GOTO 9238
```

```
ENDIF
```

```
ENDIF
```

```
* set initial parameter values, max & min
* RANGE DETERMINED BY CPRATIO
*     CPRATIO < 0.4 : VERY HIGH FREQUENCY WEIGHTED
*     0.4 < CPRATIO < 0.65 : MID FREQUENCY WEIGHTED
*     CPRATIO > 0.65 : LOW FREQUENCY WEIGHTED
* IF(CPRATIO.LT.0.4)THEN
*     starting point : high frequency weighted
*     B(1)=0.2*CONST(2)
*     B(2)=0.5*CONST(2)
*     B(3)=600.
*     B(4)=1500.
*     B(5)=3000.
*     BMIN(1)=0.
*     BMIN(2)=0.
*     BMIN(3)=350.
*     BMIN(4)=900.
*     BMIN(5)=1500.
*     BMAX(1)=0.6*CONST(2)
*     BMAX(2)=CONST(2)
*     BMAX(3)=1500.
*     BMAX(4)=2500.
*     BMAX(5)=3600.
* ELSE IF(CPRATIO.GE.0.4.AND.CPRATIO.LE.0.63)THEN
*     starting point : spread over range
*     B(1)=0.3*CONST(2)
*     B(2)=0.4*CONST(2)
*     B(3)=600.
*     B(4)=1200.
*     B(5)=2400.
*     BMIN(1)=0.
*     BMIN(2)=0.
*     BMIN(3)=350.
*     BMIN(4)=900.
```

```

          BMIN(5)=1500.
          BMAX(1)=CONST(2)
          BMAX(2)=CONST(2)
          BMAX(3)=999.
          BMAX(4)=1999.
          BMAX(5)=3600.
      ELSE IF(CPRATIO.GT.0.63)THEN
*           starting point: low frequency weighted
*           parameters are constrained to low frequencies;
*           with lower minimum frequencies acceptable.
          B(1)=0.5*CONST(2)
          B(2)=0.4*CONST(2)
          B(3)=300.
          B(4)=500.
          B(5)=700.
          BMIN(1)=CONST(2)/10.
          BMIN(2)=CONST(2)/10.
          BMIN(3)=100.
          BMIN(4)=401.
          BMIN(5)=601.
          BMAX(1)=CONST(2)
          BMAX(2)=CONST(2)
          BMAX(3)=450.
          BMAX(4)=1000.
          BMAX(5)=2000.
      ENDIF
9238      CONTINUE

      WRITE (OUTPUT,13) (TITLE(J),J=1,NTITLE)
*       WRITE (OUTPUT,23) FMT1
      WRITE (OUTPUT,14) PARM,MAXIT,DATA,FREQ,(J,B(J),BMIN(J),BMAX(J),
?           J=1,PARM )
13      FORMAT (/,10(' ',A72/))
23      FORMAT (/ ' ',15X,'INPUT DATA'// ' '   FORMAT FOR DATA POINTS'
*           ,5X,A8)
14      FORMAT (' NUMBER OF PARAMETERS',10X,14/
#           ' MAXIMUM NO. OF ITERATIONS',5X,14/
#           ' NUMBER OF DATA POINTS',9X,14/
#           ' FREQUENCY OF PRINTING',9X,14// ' COEFFICIENT',
#           6X,'STARTING',9X,'LOWER',11X,'UPPER'/' NUMBER',
#           10X,'VALUE',2(11X,'LIMIT')//30(17,7X,3(1PE16.8)/))
9865      continue
          IREDUCE=0
      DO 200 ITER = ISTART,MAXIT
          CALL SOLVE (PARM,DATA,ERROR,ERROR2,B,BMIN,BMAX,Y,Z,
&           SUMSQ,CONV,NORMAL,SCALE,
&           WORK,GRAD,BI,ZI,DIAG,X )
          IF(SUMSQ.LT.CONV(1)) GOTO 600
C
C           CHECK FOR TERMINAL ERROR CODES FROM SUBROUTINE
C           SOLVE.
C
          IF (ERROR .EQ. -1) GO TO 570
          IF (ERROR .EQ. -2) GO TO 590

```

```

        IF (ERROR .EQ. -3) GO TO 580
        IF (ERROR .EQ. 0) GO TO 600
        IF (ITER/FREQ*FREQ .NE. ITER) GO TO 20001
        WRITE (OUTPUT,18) ITER,SUMSQ
18      FORMAT('0'/' ITERATION',I4/'OSUM OF SQUARES',1PE17.8)
        WRITE (OUTPUT,FMT2) (J,B(J),J=1,PARM)

*
*      CHECK TO SEE IF TWO FREQUENCIES ARE APPROACHING ONE ANOTHER.
*

20001      continue

200      CONTINUE
        WRITE (OUTPUT,19)
19      FORMAT (/ ' MAXIMUM NUMBER OF ITERATIONS EXCEEDED' )
        ITER=MAXIT
        GO TO 600

C
C      ERROR GENERATION
C
500      WRITE (OUTPUT,2)
2        FORMAT(/ ' MAXIMUM NUMBER OF TITLE CARDS EXCEEDED, ONLY ',
$          'THE FIRST TEN WILL BE RETAINED' )
510     READ (INPUT,3) TEST
3        FORMAT (72X,A4)
        IF (TEST .EQ. BLANK) GO TO 510
        GO TO 120

515     WRITE(OUTPUT,49) MAXCON
49      FORMAT(/ ' NUMBER OF CONSTANTS SPECIFIED EXCEEDS MAXIMUM (',
&        '4,') ALLOWED. ' )
520     WRITE (OUTPUT,5)
5        FORMAT(/ ' NUMBER OF PARAMETERS SPECIFIED LESS THAN OR ',
$          'EQUAL TO ZERO' )
        GO TO 900

530     WRITE (OUTPUT,6)
6        FORMAT (/ ' MAXIMUM NUMBER OF ITERATIONS SPECIFIED LESS ',
%          'THAN OR EQUAL TO 0' )
        GO TO 900

540     WRITE (OUTPUT,7)
7        FORMAT (/ ' NUMBER OF INDEPENDENT VARIABLES SPECIFIED ',
*          'IS LESS THAN OR EQUAL TO 0' )
        GO TO 900

550     WRITE (OUTPUT,9)
9        FORMAT (/ ' NUMBER OF PARAMETERS EXCEEDS MAXIMUM' )
        GO TO 900

560     WRITE (OUTPUT,10)
10      FORMAT (/ ' NUMBER OF INDEPENDENT VARIABLES EXCEEDS MAXIMUM' )
        GO TO 900

565     WRITE (OUTPUT,24)
24      FORMAT(/ ' MAXIMUM NUMBER OF DATA POINTS EXCEEDED' )
        GO TO 900

570     WRITE (OUTPUT,15)
15      FORMAT(/ ' NUMBER OF PARAMETERS EXCEEDS NUMBER OF DATA POINTS' )

```

```

      GO TO 700
580  WRITE (OUTPUT,16)
16   FORMAT (/ ' INITIAL B VALUES NOT BETWEEN BMIN AND BMAX' )
      GO TO 700
590  WRITE (OUTPUT,17) ERROR2
17   FORMAT (/ ' SINGULAR MATRIX ENCOUNTERED IN SUBROUTINE SOLVE, ',
%      'DIAGONAL ELEMENT ',13)
      GO TO 700
C
C      SOLUTION FOUND
C
600  CONTINUE
      WRITE (OUTPUT,13) (TITLE(J),J=1,NTITLE)
      WRITE (OUTPUT,20) ITER
20   FORMAT (' F I N A L R E S U L T S',I8,' ITERATIONS PERFORMED' )
      WRITE (OUTPUT, 45) SUMSQ
45   FORMAT (/ ' SUM OF SQUARES = ',1PE17.8)
      WRITE (OUTPUT,FMT2) (J,B(J),J=1,PARM)
          IF(CONST(3).EQ.0)THEN
              write(output,8990)
          ELSE
              write(output,8991)
          ENDIF
          write(output,8992)
          write(output,8993)
          write(output,8994)
          write(output,8995)
          write(output,8996)
          write(output,8997)
          write(output,8998)
          WRITE(OUTPUT,*)' '
          WRITE(OUTPUT,8764)NTERMS
8764  FORMAT(1X,/,5X,'Cv vib: sum of ',i2,' terms'//)
          WRITE(OUTPUT,*)' '
          write(output,8763)
          IF(NTERMS.EQ.1)THEN
              WRITE(OUTPUT,8765)B(1),B(2)
          ELSE IF(NTERMS.EQ.2)THEN
              COEF2=CONST(2)-B(1)
              WRITE(OUTPUT,8765)B(1),B(2)
              WRITE(OUTPUT,8765)COEF2,B(3)
          ELSE IF(NTERMS.EQ.3)THEN
              COEF3=CONST(2)-(B(1)+B(2))
              WRITE(OUTPUT,8765)B(1),B(3)
              WRITE(OUTPUT,8765)B(2),B(4)
              WRITE(OUTPUT,8765)COEF3,B(5)
          ENDIF
8763  format(1x,'coef: A(i)          exp:  A(i+n)')
8765  format(1x,/,1PE10.3,'          ',1PE10.3)
8990  FORMAT(1X,/,',          Cp = 4.0 + C vib   (non-linear molecule)'
+//)
8991  format(1x,/,',          Cp = 7/2 + C vib   (   linear molecule)'
+//)
8992  format(1x,'          n')

```

```

8993 format(1x,'          _____')
8994 format(1x,'          \      ')
8995 format(1x,'          \      2      ex
+p(A(i+n)*(hc/KT))')
8996 format(1x,'          C vib = /      A(i)*[A(i+n)*(hc/KT)] . _____
          _____')
8997 format(1x,'          /_____
+          2')
8998 format(1x,24x,'i',24x,'[1 - exp(A(i+n)*hc/kT)]'//)
      IF (NPRT .LT. NIND) NPRT = NIND
      IF (NPRT .GT. 5)      NPRT = 5
      WRITE (OUTPUT,9987)
9987 FORMAT(1X,'X',13X,'Y',13X,'YC',11X,'YC-Y',10X,'PCT',//)
      SUMP = 0.0
      DO 630 I = 1,DATA
          ZI(I) = Z(I) - Y(I)
          IF (Y(I) .EQ. 0.0) GO TO 620
          PCT = 100.0 * ZI(I) / Y(I)
          GO TO 625
620      PCT = 0.0
625      CONTINUE
          IF(ABS(PCT).GT.3.75.AND.IREPEAT.NE.2)THEN
              IREPEAT=1
              DELPCT(I)=PCT
          ENDIF
          SUMP = SUMP + ABS(PCT)
          WRITE (OUTPUT,'(1X,4(1PE10.3,3X),OPF9.3)')
+ X(1,I),Y(I),Z(I),ZI(I),PCT
630      CONTINUE
          SUMSQ = SUMSQ
          FDATA = DATA
          FPARM = PARM
          SEE = SQRT (SUMSQ/ FDATA)
          AVP = SUMP / FDATA
          IRDF = DATA - PARM
          RDF = IRDF
          RMS = SUMSQ / RDF
          RRMS = SQRT(RMS)
          IF (ICONST .LE. 0) GO TO 632
          WRITE (OUTPUT,22) (CONST(I), I = 1, ICONST)
22      FORMAT('0  CONSTANTS : ',1P8D12.5/)
632      WRITE (OUTPUT,21) SEE,AVP,IRDF,RMS,RRMS
21      FORMAT ('/ STANDARD ERROR OF ESTIMATE =',1PE15.6/
@          ' ABSOLUTE AVERAGE PERCENT ERROR = ',OPF7.2/
@          ' RESIDUAL DEGREES OF FREEDOM =',I4/
@          ' RESIDUAL MEAN SQUARE =',1PE15.6/
@          ' RESIDUAL ROOT MEAN SQUARE =',E15.6)
          IF(IREPEAT.EQ.1)THEN
              CALL RESET
              WRITE(OUTPUT,*)' '
              WRITE(OUTPUT,*)' ***** REPEAT REGRESSION *****'
              WRITE(OUTPUT,*)' REPEAT # ',IREPNUM+1
              WRITE(OUTPUT,*)' '
              GOTO 9268

```

```

ENDIF
IF(NTERMS.EQ.3)THEN
GM=((B(1)*LOG(B(3)))+(B(2)*LOG(B(4)))+(COEF3*LOG(B(5))))/CONST(2)
AM=((B(1)*B(3))+(B(2)*B(4))+(COEF3*B(5)))/CONST(2)
SS=((B(1)*(B(3)**2))+(B(2)*(B(4)**2))+(COEF3*(B(5)**2)))
ELSEIF(NTERMS.EQ.2)THEN
GM=((B(1)*LOG(B(2)))+(COEF2*LOG(B(3))))/CONST(2)
AM=((B(1)*B(2))+(COEF2*B(3)))/CONST(2)
SS=((B(1)*(B(2)**2))+(COEF2*(B(3)**2)))
ELSE
GM=LOG(B(2))
AM=B(2)
SS=B(2)**2
ENDIF
GM=EXP(GM)
*****

SMS=SS/CONST(2)
FARMSQ=AM**2
BETA=((CONST(2)-1)/CONST(2))*(SMS/FARMSQ)
RMS=SMS**0.5
WRITE(OUTPUT,*)' NUMBER OF OSCILLATORS = ',CONST(2)
WRITE(OUTPUT,*)' '
WRITE(OUTPUT,*)' ESTIMATED ARITHMETIC MEAN FREQUENCY'
WRITE(OUTPUT,'(5X,F10.3)')AM
WRITE(OUTPUT,*)' '
WRITE(*,*)' '
WRITE(*,*)' ESTIMATED ARITHMETIC MEAN FREQUENCY'
WRITE(*,'(5X,F10.3)')AM
WRITE(*,*)' '
WRITE(OUTPUT,*)' '
WRITE(OUTPUT,*)' ESTIMATED GEOMETRIC MEAN FREQUENCY'
WRITE(OUTPUT,'(5X,F10.3)')GM
WRITE(OUTPUT,*)' '
WRITE(*,*)' '
WRITE(*,*)' ESTIMATED GEOMETRIC MEAN FREQUENCY'
WRITE(*,'(5X,F10.3)')GM
WRITE(*,*)' '

WRITE(OUTPUT,17004)RMS
17004 FORMAT(6X,'Root Mean Square frequency = ',f10.3,' ( 1/cm )')
WRITE(OUTPUT,17002)SMS
17002 format(6X,'Mean Square frequency = ',1pe15.3,' ( 1/cm^2 )')
WRITE(OUTPUT,17003)FARMSQ
17003 format(6X,'Square of Mean frequency = ',1pe15.3,' ( 1/cm^2 )')
WRITE(OUTPUT,17005)BETA
17005 format(6X,'modified frequency dispersion parameter = ', 1pe15.3)
WRITE(*,17004)RMS
WRITE(*,17002)SMS
WRITE(*,17003)FARMSQ
WRITE(*,17005)BETA
CALL SIGMACP(B)
STOP ' END OF Cp FIT'

```



```

FUNCTION AVG(A,B)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(1),B(1)
AVG=(A(1)+B(1))/2.0
RETURN
END

```

```

SUBROUTINE FOFX(I,X,B,Y,Z)
$LARGE
    IMPLICIT REAL*8(A-H,O-Z)
    DOUBLE PRECISION B,CONST,XIN,THETA,CV,TERM(3),SUM
    DIMENSION X(1),B(1),CONST(40)
    COMMON /CONST/ CONST,NTERMS,NROT
    XIN=X(1)
*   write(*,*)x(1),y
    Z=0.0
    DO 100 II=1,NTERMS
    THETA=0.0
    IF(NTERMS.EQ.1)THEN
        CALL CVVIB(B(2),XIN,CV,THETA)
    ELSE
        CALL CVVIB(B(NTERMS+II-1),XIN,CV,THETA)
    ENDIF
    IF(II.NE.NTERMS.OR.NTERMS.EQ.1)THEN
        TERM(II)=B(II)*CV
    ELSE IF(II.EQ.NTERMS.AND.NTERMS.GT.1)THEN
        SUM=0.0
234      DO 234 IK=1,NTERMS-1
        SUM=SUM+B(IK)
        TERM(II)=(CONST(2)-SUM)*CV
    ENDIF
    Z=Z+TERM(II)
100    CONTINUE
    IF(CONST(3).EQ.0.)THEN
*       non-linear molecule
*       Z=(Z+4.0+(NROT/2.))*1.987*CONST(1)
*   theory tells us to add (nrot/2) to Cp/R, but fits better
*   if we ignore this.
*       Z=(Z+4.0)*1.987*CONST(1)
*       Z=(Z+4.0)*1.987*CONST(1)
    ELSE
*       linear molecule
*       Z=(Z+(7./2.))*1.987*CONST(1)
    ENDIF
*   write(*,*)'xin ',xin,' z= ',z
*   write(*,*)'theta= ',theta
    RETURN
    END

```

\$LARGE

```
SUBROUTINE CVVIB(FREQ,T,CV,THETA)
  IMPLICIT REAL*8(A-H,O-Z)
  REAL*8 HP,KB,C,X,THETA,TEST
  HP=6.62517E-34
  KB=1.3804E-23
  C=2.998E+10
  IF(FREQ.GT.25000.0.OR.FREQ.LT.1.)THEN
    CV=1000.
    RETURN
  ENDIF
  IF(FREQ.NE.0.0)THEN
    THETA=((HP*C)/KB)*FREQ
  ELSE
    IF(THETA.EQ.0.)THEN
      CV=1000.
      RETURN
    ENDIF
  ENDIF
  X=THETA/T
  IF(X.GT.230.)THEN
    CV=1000.
    RETURN
  ENDIF
  TEST=DEXP(X)
  IF(TEST-1.0.LT.10.0E-6)THEN
    CV=100.
    RETURN
  ENDIF
  TOP=EXP(X)
  BOTTOM=(TOP-1.0)**2
  CV=(X**2)*(TOP/BOTTOM)
  RETURN
END
```

70

```
SUBROUTINE SIGMACP(B)
  IMPLICIT REAL*8(A-H,O-Z)
  CHARACTER*70 FILPRN
  DIMENSION B(1),CONST(40),T(30)
  COMMON/CONST/CONST,NTERMS,NROT
  WRITE(*,*)'ENTER PRN FILENAME'
  READ(*,70)FILPRN
  FORMAT(A70)
  OPEN(12,FILE=FILPRN,STATUS='UNKNOWN')
  WRITE(12,'(1X,A70)')FILPRN
  T(1)=100.
  T(2)=200.
  T(3)=298.15
  T(4)=300.0
  T(5)=400.0
  T(6)=500.0
  T(7)=600.
  T(8)=700.
  T(9)=800.0
  T(10)=900.
  T(11)=1000.0
  T(12)=1100.
  T(13)=1200.
  T(14)=1300.
  T(15)=1400.
  T(16)=1500.0
  T(17)=1600.
  T(18)=1700.
  T(19)=1800.
  T(20)=1900.
  T(21)=2000.0
  T(22)=2500.
  T(23)=3000.0
  T(24)=3500.
  T(25)=4000.
  T(26)=4500.
  T(27)=5000.
  T(28)=5500.
  T(29)=6000.0
  DO 100 I=1,29
  CP=0.
  DO 200 J=1,NTERMS
  THETA=0.0
  IF(NTERMS.EQ.1)THEN
      CALL CVVIB(B(2),T(I),CV,THETA)
  ELSE
      CALL CVVIB(B(NTERMS+J-1),T(I),CV,THETA)
  ENDIF
  IF(J.NE.NTERMS.OR.NTERMS.EQ.1)THEN
      TERM=B(J)*CV
  ELSE IF(J.EQ.NTERMS.AND.NTERMS.NE.1)THEN
      SUM=0.0
      DO 234 IK=1,NTERMS-1
      SUM=SUM+B(IK)
```

234

```
                TERM=(CONST(2)-SUM)*CV
ENDIF
CP=CP+TERM
200 CONTINUE
CP=(CP+4.0)*1.987*CONST(1)
WRITE(12, '(1X,2(F10.3,2X))' )T(1),CP
100 CONTINUE
CLOSE(12,STATUS='KEEP')
RETURN
END
```

```

SUBROUTINE PD(NDATA,X,NPARM,B,Y,ZZ,Z,PDERIV,NORMAL,WORK,POIN01)
$LARGE
      IMPLICIT REAL*8(A-H,O-Z)
      DOUBLE PRECISION NORMAL(21,21),WORK(21),B(20),DEL,POIN01,
+CONST(40),U,U1,DU,DU1,V,V1,DV,DV1,ALPHA,PRD,TERM1,TERM2,TERM3,
+TERM4,HP,KB,C
      DIMENSION X(10,400),Y(400),PDERIV(20,400),Z(400)
      INTEGER NDATA,NPARM
      COMMON/CONST/CONST,NTERMS,NROT
      HP=6.62517E-34
      KB=1.3804E-23
      C=2.998E+10

C      INITIALIZE NORMAL TO 0.0, ONLY THE PART OF
C      THE ARRAY THAT WILL BE USED
C
      DO 101 I = 1,NPARM+1
      DO 100 J = I,NPARM+1
      NORMAL(J,I) = 0.0
100      CONTINUE
101      CONTINUE
*****
*      REPLACE THIS SECTION WITH EXPLICIT JACOBIAN
*
C
C      CALCULATE THE PARTIAL DERIVATIVES OF THE FUNCTION
C      VALUES WITH RESPECT TO THE PARAMETER VALUES FOR
C      EACH SET OF DATA POINTS. THESE DERIVATIVES WILL BE
C      STORED IN PDERIV.
C
      DO 200 J = 1,NDATA
      ALPHA=(HP*C)/(KB*X(1,J))
      U2=EXP(ALPHA*B(5))
      TERM3=(ALPHA*B(5))**2
      TERM4=(U2/((U2-1.0)**2))
      PRD=TERM3*TERM4
      DO 150 I=1,2
      U1=EXP(ALPHA*B(I+2))
      TERM1=(ALPHA*B(I+2))**2
      TERM2=(U1/((U1-1.0)**2))
      PDERIV(I,J)=(TERM1*TERM2-PRD)*1.987*CONST(1)
150      CONTINUE
      DO 1000 I=3,5
      U=(ALPHA*B(I))**2
      DU=2.0*(ALPHA**2)*B(I)
      U1=EXP(ALPHA*B(I))
      DU1=ALPHA*U1
      V1=(U1-1.0)**2
      DV1=(2.0*(U1-1.0)*DU1)
      V=U1/V1
      DV=((1.0/V1)*DU1)-((U1/(V1**2))*DV1)
      PDERIV(I,J)=(U*DV)+(V*DU)
      IF(I.LT.5)THEN
          PDERIV(I,J)=PDERIV(I,J)*B(I-2)*1.987*CONST(1)

```

```

                ELSE
                    PDERIV(I,J)=PDERIV(I,J)*(CONST(2)-(B(1)+B(2)))*1.987*
+CONST(1)
                ENDIF
1000            CONTINUE

*                PDERIV(J,I) = (ZZ - Z(I)) / DEL
200            CONTINUE
*
*
*****
C
C                COMPUTE THE NORMAL EQUATIONS
C
DO 240 J1 = 1,NDATA
DO 230 J2 = 1,NPARM
230            WORK(J2) = PDERIV(J2,J1)
                WORK(NPARM+1) = Y(J1) - Z(J1)
DO 240 J3 = 1,NPARM+1
DO 240 J4 = J3,NPARM+1
240            NORMAL(J4,J3) = NORMAL(J4,J3) + WORK(J3) * WORK(J4)
                RETURN
                END

```

APPENDIX V

SOURCE CODE LISTING

THERM COMPUTER PACKAGE

APPENDIX V-A

FORTRAN SOURCE CODE FOR

THERM MAIN PROGRAM


```

$LARGE
C
C      PROGRAM THERM
C*****
C*                                     *
C*                                     *
C*      THERMODYNAMIC PROPERTY ESTIMATION BY BENSON'S      *
C*                                     *
C*      GROUP ADDITIVITY METHOD                               *
C*                                     *
C*      program developed at:                               *
C*                                     *
C*      NEW JERSEY INSTITUTE of TECHNOLOGY                  *
C*                                     *
C*      KINETICS RESEARCH LABORATORY                       *
C*                                     *
C*      Under the direction of Dr. Joseph W. Bozzelli      *
C*                                     *
C*                                     *
C*                                     *
C*      VERSION : 4.0                                       *
C*      DATE : 4/22/89                                       *
C*                                     *
C*                                     *
C*      WRITTEN BY : EDWARD R. RITTER                       *
C*                                     *
C*                                     *
C*      OTHER CONTRIBUTORS:                                  *
C*      S. C. CHUANG (PC BASIC VERSION 1)                   *
C*      J. W. BOZZELLI (PC BASIC VERSION 2)                 *
C*                                     *
C*                                     *
C*****
$INCLUDE: 'forexec.inc'
      INTEGER*2 SYSTEM, SPAWN, MODE
      CHARACTER STRING
      INTEGER IX(50), E(50), N, NGRPT, Q,E1,FIL,Z1,I9(50),NSAVE,
+I1CH(50),I2CH(35),INDX(70),GRTOT,NLROT(400)
      INTEGER FLAG, BFLAG, SYMM,SYMS, SYMR, CTRL, Z, NGRP, NATOM,
+NED,ISORT(500),KEY(10),I3(25)
      INTEGER IG, Y, NG, P, X, O, D,NE(4),NE1(4,400),FLG,IFIRST(25),
+ILAST(25),EP(50),NATOMP,NP(4),IOP,IDOC(500),NSPEC,KDOCT,ITMP(25),
+IGRL2(400)
      INTEGER*2 IMON,IDAY,IYR
      REAL A(400,9),S(400,9),SCOR, CPINF, CP2K,DELTA(9)
      REAL*4 B(2,9),BSAVE(9),BO(9)
      CHARACTER*70 TEXT(50),TEXTS(50),EXEFIL,NUMIN1,GRDOC(400),
+GRLIN2(100)
      CHARACTER*14 DOC(400)
      CHARACTER*70 OPTION,KS(25),NASAFI,NASAFO,FILNM
      CHARACTER*70 DS1,DUMMY,FORM,FORMP,S1,S2,HLP(10)
      CHARACTER*14 AS(400),SS(400),NUMIN,TSS,SPECP,FS2,THERMFIL,SPECL

```

```

CHARACTER*14 CS(2,60), WS(5) , LS, RS,CP, TS, FS,DS
      CHARACTER*2 ELEM(50),DRIVE1,DRIVE2,DRIVE3,ERRORCK
CHARACTER ES, ANSS,PHASE,PHSE(400),TITLE*30,HEADIN*126
CHARACTER*14 NUL,NUL1(2,50),DOCFIL,RS22,DOCTYPE,COMMAND,OUTPUT,
+UNITS,GRUNITS,FOUNITS,FIUNITS
CHARACTER*4 IE(4),IP(4),IE1(4,400),REF(2),REF1(2,400)
CHARACTER*6 REF3,REF2(400)
      LOGICAL EXST,OPNED
      COMMON/CONTRL/FIL
      COMMON/CTRL2/COMMAND,OUTPUT
      COMMON/DELETE/NDEL, IDEL(500)
      COMMON/NASANM/NASAFI, NASAFO
      COMMON/CONFIG1/ELEM
      COMMON/CONFIG2/NELEM,N1CH,N2CH, I1CH, I2CH
      COMMON/CONFIG3/HLP
      COMMON/CONFIG4/DRIVE1,DRIVE2,DRIVE3
      COMMON/CONFIG5/NKEYS
      COMMON/CONFIG6/UNITS
      COMMON/CONFIG7/ERRORCK
      COMMON/GRFNM1/NFILES, I3
      COMMON/GRFNM2/KS
      COMMON/UNITSET/FOUNITS,FIUNITS
      COMMON/ELEM1/NE1
      COMMON/ELEM2/IE1
      COMMON/FILEFLG/NCALL
      COMMON/GROUPD/GRDOC,GRLIN2
      COMMON/GROUP1/IGRL2
      COMMON/DATE/IMON, IDAY, IYR
      COMMON/NROTOR/NROT, NROTS
      COMMON/NROTLST/NLROT
*
      SET CREATION DATE
      CALL GETDAT(IYR,IMON, IDAY)
      IF(INT(IYR/100).EQ.19)THEN
          IYR=IYR-1900
      ELSE
          IYR=IYR-2000
      ENDIF
*
      IXFER=0
      ERRORCK=' '
      GRUNITS='KCAL'
      FOUNITS='KCAL'
      FIUNITS='KCAL'
591      CONTINUE
      CALL CLS
      DO 6677 I=1,9
      KEY(I)=0
      BSAVE(I)=0.0
6677      DELTA(I)=0.0
      ICNT=0
      NED=0
      RXFIL=0
      FILNM=' '
      WRITE (*,6645)

```

```

6645 FORMAT('0',7X,'                                THERM')
      CALL LINES(0,1)
      WRITE(*,6646)
6646 FORMAT('0',18X,'Thermo Estimation for Radicals & Molecules')
      CALL LINES(0,2)
      WRITE(*,666)
666  FORMAT('0', 32X,'written by')
      write(*,667)
667  format('0',7X,'                                E. R. Ritter & J. W. Bozzelli ')
      write(*,668)
668  format(' ',15x,'Department of Chemical Engineering and Chemistry')
      write(*,669)
669  format(' ',21x,'New Jersey Institute of Technology')
      CALL LINES(0,2)
      WRITE(*,6647)
6647  FORMAT('0',7X,'                                revision 4.0 : 4/22/89')
      INQUIRE(FILE='THERM.CFG',EXIST=EXST)
      IF(EXST)GOTO 670
680  continue
      STOP '"THERM.CFG" is missing'

670  CONTINUE
      CALL LINES(0,2)
      write(*,671)
671  FORMAT('+',20(' '), ' **** Loading Configuration File ****')

      CALL CONFIG(ELEM,NFILES,KS,ISTAT,OUTPUT)
      IF(ISTAT.NE.0)GOTO 680
C    WRITE(*,*)' '
91827 CONTINUE
      NGRPT = 0
      D = 0
      DO 8 I1 = 1, NFILES
*-----*
*    inquire if group data file specified in THERM.CFG exists *
*-----*
92827  continue
1    FORMAT(A14)
      INQUIRE(FILE=KS(I1),EXIST=EXST)
      IF(EXST)GOTO 88
      CALL CLS
      WRITE(*,*)' CANNOT FIND GROUP DATA FILE'
      WRITE(*,*)'           ',KS(I1)
      CALL LINES(0,2)
      WRITE(*,*)' enter a new path and filename ( "Q" to quit )'

      READ(*,'(A)')DUMMY
      CALL READCHAR(DUMMY)
      IF(dummy.EQ.'Q')STOP 'THERM4 aborted by user'
      KS(I1)=DUMMY
      GOTO 92827
*-----*
*    end inquire file block *
*-----*

```

```

88      CONTINUE
        OPEN(I1,FILE=KS(I1),STATUS='OLD')
        READ(I1,52)DUMMY
        CALL LRDCHAR(DUMMY)
        IF(DUMMY.EQ.'BOND DISSOCIATION')I3(4)=I1
        IF(DUMMY.EQ.'RADICAL_GROUPS')I3(3)=I1

        CLOSE(I1,STATUS='KEEP')
8      CONTINUE
        IF(I3(4).EQ.0)THEN
            IFIRST(4)=0
            ILAST(4)=0
        ENDIF
        IF(I3(3).EQ.0)THEN
            IFIRST(3)=0
            ILAST(3)=0
        ENDIF
        I=0
        DO 33650 I2=1,NFILES-2
33651    I=I+1
            IF(I.EQ.I3(3).OR.I.EQ.I3(4))GOTO 33651
            ITMP(I2)=I
33650    CONTINUE
            I3(1)=ITMP(1)
            I3(2)=ITMP(2)
            DO 511 I=5,NFILES
511      I3(I)=ITMP(I-2)
            WRITE(*,33652)
33652  FORMAT('+',22(' '), '***** LOADING GROUP DATAFILES *****',5(' '))
            N2LIN=0
            DO 300 I1=1,NFILES
                grunits='KCAL'
                IF(I3(I1).EQ.0)GOTO 300
                OPEN(I1,FILE=KS(I3(I1)),STATUS='OLD')
                IF(I1.EQ.3.OR.I1.EQ.4)READ(I1,52)DUMMY
*      determine units for group data
                read(i1,52)dummy
                call lrdchar(dummy)
                call deblnk(dummy,s1,len1,0)
                if(dummy(:6).eq.'UNITS:')then
                    if(dummy(7:8).eq.'KJ')grunits='KJ'
                else if(dummy(:6).ne.'UNITS:')then
                    backspace(i1)
                endif
*
            READ (I1,*) Q
            IFIRST(I1)=NGRPT+1
            ILAST(I1)=NGRPT+Q
            DO 400 J = 1, Q
                D = D + 1
                GRDOC(D)=' '
                GRLIN2(N2LIN+1)=' '
                if(grunits.ne.'KJ')grunits='KCAL'
                if(grunits.eq.'KCAL')then

```

```

      READ(11, 2) AS(D), (A(D, ID9), ID9=1, 9), GRDOC(D), DUMMY
2     FORMAT(A, 9F7.2, 2A70)
      else if(grunits.eq.'KJ')then
      READ(11, 39) AS(D), (A(D, ID9), ID9=1, 9), GRDOC(D), DUMMY
39     FORMAT(A, 9F8.2, 2A70)
      endif
      IF(DUMMY.NE.' ')THEN
          N2LIN=N2LIN+1
*          A(D, 9)=FLOAT(N2LIN)
          IGRL2(D)=FLOAT(N2LIN)
          GRLIN2(N2LIN)=DUMMY
      ELSE
          IGRL2(D)=0
      ENDIF
*     convert units to kcal if necessary
      if(grunits.eq.'KJ')then
          do 445 j1=1, 9
445         a(d, j1)=a(d, j1)/4.184
      endif
*
      IN3=1
C     CHANGE COMMA AT END OF GROUP NAME TO A BLANK
398    IF(AS(D)(IN3:IN3).EQ.',')THEN
          AS(D)(IN3:14)=' '
          GOTO 399
      ENDIF
      IN3=IN3+1
      IF(IN3.GT.14)GOTO 399
      GOTO 398
399    CONTINUE
400    CONTINUE
      NGRPT = NGRPT + Q
      CLOSE(11)
300    CONTINUE
      write(*, 909)ngrpt
909    FORMAT('+', 27X, I3, ' Groups in the dataBase.      ')
      WRITE(*, *)' '
      WRITE(*, *)'           ( hit return to continue )'
      read(*, 3)NUMIN
      call readchar(numin)
C
C
***** END OF GROUP DB INPUT *****
C
C
      IF(NUMIN.EQ.' ' .OR.NUMIN.EQ.'1' .OR.NUMIN.EQ.'L')THEN
          IHELP=1
          GOTO 27
      ENDIF
      IOP=0
      IF(NUMIN.EQ.'0' .OR.NUMIN.EQ.'S')THEN
          IHELP=0
          GOTO 27
      ENDIF

```

```

C
C*****
C***** THERM MAIN MENU*****
C*****
C
27  CALL CLS
      COMMAND=' '
C  RESET ALL APPROPRIATE FLAGS HERE
C
      SPECL=' '
      IIICT=0
      ISOURCE=0
      BLFAG=0
      BLFLAG=0
      FLAG=0
      NROT=0
      NROTS=0
      BD=0.0
      DELB=0.0
      DO 28 I=1,9
28  DELTA(I)=0.0
      DOCTYPE=' '
      KDOCT=0
      NED=0
C
      WRITE(*,4300)
4300 FORMAT(1X,30X,'THERM MAIN MENU')
      CALL LINES(0,1)
      if(units.ne.'KJ')units='KCAL'
      if(units.eq.'KCAL')then
          write(*,98256)IMON,IDAY,IYR
98256 FORMAT(6X,' Units: Kcal/mol ( cal/mol K )',19X,12,2('/',12))
          else if(units.eq.'KJ')then
          write(*,98257)IMON,IDAY,IYR
98257 FORMAT(6X,' Units: KJ/mol (J/mol K)',25X,12,2('/',12))
          endif
      WRITE(*,4310)
4310 FORMAT(1X,5X,75(' '))
      CALL LINES(0,1)
      WRITE(*,4320)
C
      column 72 1

4320 FORMAT(6X,'1 - ENTER/ESTIMATE SPECIES',5X,'5 - REVIEW (LST FORMAT
+FILE)')
      WRITE(*,4330)
4330 FORMAT(6X,'2 - VIEW GROUPS',16X,'6 - GET SPECIES FROM FILE (*.DOC)
+')
      IF(IHELP.EQ.1)WRITE(*,4335)'SHORT'
      IF(IHELP.EQ.0)WRITE(*,4335)'LONG'
4335 FORMAT(6X,'3 - SELECT ',A5,' MENU',10X,'7 - ReWrite THERMO FILES (
+*.DOC, *.LST)')
      WRITE(*,4337)
4337 FORMAT(6X,'4 - SELECT LIST FILE (*.LST)',3X,'8 - RUN THERMFI crea

```

```

+te NASA (*.DAT)')
  WRITE(*,4437)
4437 FORMAT(1X,16X,'9 - RUN THERMRXN (calculate dU, dH, dS, dG for reac
+tion)')
  WRITE(*,4438)
4438 FORMAT(1X,15X,'10 - Sort & ReWrite THERMO FILES ( *.DOC, *.LST )')
  WRITE(*,4439)
4439 FORMAT(16X,'11 - Sort/Write "LST" file or Write w/ new Units )')
  WRITE(*,44391)
44391 FORMAT(1X,15X,'          ( no "DOC" format file is needed )')
  write(*,4444)
4444 format(1x,15x,'12 - RUN THERMLST (LIST NASA FORMAT FILE) /create *
+.LST')
  WRITE(*,4440)
4440 FORMAT(1X,15X,'13 - DOS utilities')
  if(units.eq.'KCAL')then
    write(*,4840)
4840    format(1x,16x,'U - CHANGE CURRENT UNITS TO : KJ/mol (J/mol K)')
  else if(units.eq.'KJ')then
    write(*,4841)
4841    format(1x,16x,'U - CHANGE CURRENT UNITS TO : Kcal/mol (cal/mol
+K)')
  endif
c    CALL LINES(0,1)
  WRITE(*,4843)
4843    FORMAT(1X,25X,'* - CLOSE ALL OPENED FILES')
*    write(*,4842)
*4842 format(1x,25x,'C - review / set configuration')
  WRITE(*,4336)
4336 FORMAT(1X,25X,'X - EXIT PROGRAM ')
  WRITE(*,4342)
4342    FORMAT(1X,25X,'? - HELP')
  CALL LINES(0,1)
321  CONTINUE
  WRITE(*,4341)
4341  FORMAT(1X,27X,'enter option : { 1 }')
  READ(*,3) NUMIN
  CALL READCHAR(NUMIN)
69696  CONTINUE
      IF(NUMIN(:1).EQ.'*')THEN
          NCALL = 0
          FIL=0
          IOP=0
          ICNT=0
          INQUIRE(7,OPENED=OPNED)
          IF(OPNED)THEN
              ENDFILE(7)
              CLOSE(7)
          ENDFIL
          INQUIRE(25,OPENED=OPNED)
          IF(OPNED)CLOSE(25)
          INQUIRE(41,OPENED=OPNED)
          IF(OPNED)THEN
              ENDFILE(41)

```

```

                                CLOSE(41)
                                ENDIF
                                INQUIRE(52,OPENED=OPNED)
                                IF(OPNED)THEN
69992                                read(52,51,end=69993)nul
                                goto 69992
69993                                BACKSPACE(52)
                                NUL=' '
                                WRITE(52,'(A70)')NUL
                                WRITE(52,'(A70)')NUL
                                ENDFILE(52)
                                CLOSE(52)

                                ENDIF
                                GOTO 27

                                ENDIF
                                if(numin(:1).eq.'U')then
                                    if(units.eq.'KCAL')then
                                        units='KJ'
                                        goto 27
                                    else if(units.eq.'KJ')then
                                        units='KCAL'
                                        goto 27
                                    endif
                                goto 27
                                endif
                                IF(NUMIN.EQ.'?')THEN
4343                                WRITE(*,4343)
                                FORMAT('+',10X,' HELP ON WHICH OPTION ?')
                                READ(*,52)OPTION
                                CALL READCHAR(OPTION)
                                IF(OPTION.EQ.' ' .OR. OPTION.EQ.'Q')GOTO 27
                                IF(OPTION.EQ.'1' .OR. OPTION.EQ.'2' .OR. OPTION.EQ.'3' .OR. OPTION.EQ.
+ '4' .OR. OPTION.EQ.'5' .OR. OPTION.EQ.'6' .OR. OPTION.EQ.'7')THEN
                                    CALL HELP(HLP(1),OPTION)
                                    GOTO 27
                                ELSE IF(OPTION.EQ.'8' .OR. OPTION.EQ.'9' .OR. OPTION.EQ.'10' .OR.
+ OPTION.EQ.'11' .OR. OPTION.EQ.'12' .OR. OPTION.EQ.'13' .OR.
+ OPTION(:1).EQ.'X' .OR. OPTION(:1).EQ.'*' .OR. OPTION(:1).EQ.'U')THEN
                                    CALL HELP(HLP(2),OPTION)
                                    GOTO 27
                                ENDIF
                                ENDIF

                                IF(NUMIN.EQ.'7' .OR. NUMIN.EQ.'10' .OR. NUMIN.EQ.'11')THEN
FIL=0
                                INQUIRE(52,OPENED=OPNED)
                                IF(OPNED)THEN
                                    CLOSE(52,STATUS='KEEP')
                                ENDIF
                                CLOSE(7,STATUS='KEEP')
                                IOP=0
                                IF(NUMIN(:2).EQ.'10' .OR. NUMIN(:1).EQ.'7')GOTO 2109
                                ENDIF

```



```

IF(NUMIN(:1).EQ.'Q')THEN
  CALL CLS
  WRITE(*,*)'      TYPE "X" TO EXIT THERM '
  WRITE(*,*)'      or hit RETURN to return to main menu'
  read(*,3)NUMIN
  CALL READCHAR(NUMIN)
  IF(NUMIN(:1).NE.'X')GOTO 27
ENDIF

IF(NUMIN(:1).EQ.'X') THEN
  CALL CLS
  GOTO 9200
ENDIF
516 IF(NUMIN(:2).EQ.'12')THEN
  CONTINUE
  EXEFIL=' '
  EXEFIL(:2)=DRIVE2
  EXEFIL(3:15)='THERMLST.EXE'
  INQUIRE(FILE=EXEFIL,EXIST=EXST)
  IF(EXST)GOTO 517
  CALL CLS
  WRITE(*,*)'CANNOT FIND:'
  WRITE(*,*)EXEFIL
  WRITE(*,*)'NASA to "LST" CONVERSION PROCEDURE'
  CALL LINES(0,2)
  WRITE(*,*)'CURRENT DRIVE AND DIRECTORY :'
  I = SYSTEM('cd'C)
  PAUSE 'change directory or drive specification'
  CALL CLS
  WRITE(*,*)'CURRENT DRIVE AND DIRECTORY :'
  I = SYSTEM('cd'C)
  WRITE(*,*)'(hit return to continue or "Q" to main menu )'
  read(*,1)NUMIN
  CALL READCHAR(NUMIN)
  IF(NUMIN(:1).EQ.'Q')GOTO 27
  GOTO 516
517 CONTINUE
  OPEN(13,FILE='THUNITS.TMP',STATUS='UNKNOWN')
  WRITE(13,1)UNITS
  CLOSE(13,STATUS='KEEP')
  IF(DRIVE2.EQ.'A:')THEN
    I = SPAWN(0,LOC('a:thermlst'C),INT4(0))
  ELSE IF(DRIVE2.EQ.'B:')THEN
    I = SPAWN(0,LOC('b:thermlst'C),INT4(0))
  ELSE IF(DRIVE2.EQ.'C:')THEN
    I = SPAWN(0,LOC('c:thermlst'C),INT4(0))
  ELSE IF(DRIVE2.EQ.'D:')THEN
    I = SPAWN(0,LOC('d:thermlst'C),INT4(0))
  ELSE IF(DRIVE2.EQ.' ')THEN
    I = SPAWN(0,LOC('thermlst'C),INT4(0))
  ENDF

```

```

IF(I.NE.0)THEN
    CALL CLS
    WRITE(*,*)' ERROR ENCOUNTERED IN NASALST'
    WRITE(*,*)' NASA to "LST" CONVERSION PROCEDURE'
    CALL LINES(0,2)
    WRITE(*,*)' ERROR CODE RETURNED = ',I
    CALL LINES(0,2)
IF(I.EQ.-1)THEN
    WRITE(*,*)' insufficient memory available to spawn'
    write(*,*)'      this procedure.'
    write(*,*)' use a system w/ 640K RAM or run this'
    write(*,*)' procedure off line (from DOS directly)'
    call lines(0,1)
endif
    WRITE(*,*)' { hit return to continue }'
    read(*,3)numin
ENDIF
GOTO 27
ENDIF

18455     IF(NUMIN(:2).EQ.'13')THEN
CONTINUE
KE=KE
KF=0
10371     IF(KF.EQ.0)THEN
*         DOS OPTION MENU
            CALL CLS
            WRITE(*,7300)
7300     FORMAT(1X,30X,' DOS UTILITIES MENU')
            WRITE(*,7301)
7301     FORMAT(1X,25X,40('_'))
            CALL LINES(0,1)
            WRITE(*,7302)
7302     FORMAT(1X,25X,' 1 - SHELL TO DOS { COMMAND.COM }')
            WRITE(*,7303)
7303     FORMAT(1X,25X,' 2 - CHANGE DEFAULT:  DISK DRIVE')
            WRITE(*,7304)
7304     FORMAT(1X,25X,' 3 -                      DIRECTORY')
            write(*,7305)
7305     FORMAT(1X,25X,' 4 -                      PATH')
            WRITE(*,7306)
7306     FORMAT(1X,25X,' 5 - DIRECTORY:      { *.LST } FILES')
            WRITE(*,7307)
7307     FORMAT(1X,25X,' 6 -                      { *.DOC } FILES')
            WRITE(*,7308)
7308     FORMAT(1X,25X,' 7 -                      { *.DAT } FILES')
            WRITE(*,7309)
7309     FORMAT(1X,25X,' 8 - ISSUE ANOTHER DOS COMMAND')
            CALL LINES(0,2)
            WRITE(*,7350)
7350     FORMAT(1X,25X,' enter option (return to previous menu)')
            read(*,83)numin
83       format(a14)
            call readchar(numin)

```

```

CALL CLS
ENDIF
c
if(numin.eq.'1'.or.kf.eq.1)then

CALL LINES(0,2)
WRITE(*,*)' THERM3....type EXIT to return to THERM3'
call lines(0,1)
I = SPAWN(0,LOC('\command'C),INT4(0))
if(i.ne.0.OR.ke.ne.0)GOTO 27
if(ke.eq.0)then
kf=ke
goto 10371
endif

CALL CLS
KF=0
GOTO 10371
endif
c
if(numin.eq.'2'.or.kf.eq.2)then
WRITE(*,*)'current disk'
WRITE(*,*)'and directory:'
CALL LINES(0,1)
I = SYSTEM('cd'C)
CALL LINES(0,1)
PAUSE 'enter new drive ( ex. "A:" )'
IF(KE.NE.0)GOTO 27
goto 10371
endif
c
if(numin.eq.'3'.or.kf.eq.3)then
WRITE(*,*)'current disk'
WRITE(*,*)'and directory:'
CALL LINES(0,1)
I = SYSTEM('cd'C)
CALL LINES(0,1)
PAUSE 'enter new directory ( ex. "cd\" )'
IF(KE.NE.0)GOTO 27
goto 10371
endif
c
if(numin.eq.'4'.or.kf.eq.4)then
WRITE(*,*)'current path'
CALL LINES(0,1)
I = SYSTEM('path'C)
CALL LINES(0,1)
PAUSE 'enter new path ( ex. "path=\; \dos; \therm" )'
IF(KE.NE.0)GOTO 27
goto 10371
endif
c
if(numin.eq.'5'.or.kf.eq.5)then
I = SYSTEM('dir *.lst'C)
call lines(0,1)

```

```

        PAUSE ' ( hit RETURN to continue )'
        IF(KE.NE.0)GOTO 27
        goto 10371
    endif
c
    if(numin.eq.'6'.or.kf.eq.6)then
        I = SYSTEM('dir *.doc'C)
        call lines(0,1)
        PAUSE ' ( hit RETURN to continue )'
        IF(KE.NE.0)GOTO 27
        goto 10371
    endif
c
    if(numin.eq.'7'.or.kf.eq.7)then
        I = SYSTEM('dir *.dat'C)
        call lines(0,1)
        PAUSE ' ( hit RETURN to continue )'
        IF(KE.NE.0)GOTO 27
        goto 10371
    endif
c
    if(numin.eq.'8'.or.kf.eq.8)then
        CALL LINES(0,1)
        PAUSE
        PAUSE ' ( hit return to continue )'
        IF(KE.NE.0)GOTO 27
        goto 10371
    endif
    NUMIN='Q'

        IF(NUMIN.eq.'q'.OR.NUMIN.EQ.'Q')GOTO 27
        GOTO 18455
    ENDIF

124   IF((NUMIN(:2).EQ.'10'.AND.NSPEC.NE.0)
      +.OR.(NUMIN(:2).EQ.'11'.AND.ICNT.NE.0))THEN

      DO 7856 LOOP=1,ICNT
7856   ISORT(LOOP)=LOOP
      DO 125 IH=1,10
125   KEY(IH)=0
12512  CALL CLS
        write(*,*)' Sort database (Y/N/Q)? : (Y)'
        read(*,'(a70)')numin1
        call readchar(numin1)
        if(numin1(:1).eq.'Q')goto 27
        if(numin1(:1).eq.'N')goto 12312
        if(numin1(:1).eq.'?')then
            OPTION='SORT/Y/N/Q'
            CALL HELP(HLP(2),OPTION)
            GOTO 12512
        endif
        CALL CLS

```

```

WRITE(*,*)'   SORTING DATABASE BY COMPOSITION'
WRITE(*,*)'           PLEASE WAIT'
      IF(NUMIN(:2).EQ.'10')ICNT=NSPEC
CALL ATMSORT(ISORT,NE1,IE1,ICNT,KEY)
CALL CLS
IPG=0
DO 123 KJI=1,ICNT
IPG=IPG+1
IF(IPG.GT.20)THEN
WRITE(*,*)' { PRESS RETURN TO CONTINUE }'
READ(*,3)NUL
IF(NUL(:1).EQ.'q')GOTO 786
IPG=0
ENDIF
CALL DELCHK(ISORT(KJI),ID)
IF(ID.EQ.1.or.ss(isort(kji)).eq.' ')GOTO 123
IF(NUMIN(:2).EQ.'10')THEN
WRITE(*,876)DOC(ISORT(KJI))(:14),(IE1(KJ,ISORT(KJI)),
+NE1(KJ,ISORT(KJI)),KJ=1,4)
ELSE IF(NUMIN(:2).NE.'10')THEN
WRITE(*,876)SS(ISORT(KJI)),(IE1(KJ,ISORT(KJI)),NE1(KJ,ISORT
+(KJI)),KJ=1,4)
ENDIF
123  CONTINUE
12312 CONTINUE
      IF(NUMIN(:2).EQ.'10')THEN
          ICNT=0
          GOTO 9786
      ENDIF
876  FORMAT(1X,A14,2X,4(2X,A4,13))

      IF(NUMIN1(:1).NE.'N')THEN
          WRITE(*,*)' { press return to continue }'
          READ(*,3)NUL
      ENDIF
      IF(NUL(:1).EQ.'q'.OR.NUL(:1).EQ.'q')GOTO 27
786  CONTINUE
      IF(NUMIN(:2).EQ.'11')THEN
          FIL=2
          IQR=0
          DO 23987 JN=1,ICNT
C      IGNORE SPECIES ON THE DELETED LIST
          DO 44441 IHJ=1,NDEL
44441  IF(ISORT(JN).EQ.IDEL(IHJ))GOTO 23987
          bflag=0
          blflag=0
          NROT=NLROT(ISORT(JN))
          NROTS=NROT
          LS=SS(ISORT(JN))
          DO 23997 JM=1,9
23997  B(1,JM)=S(ISORT(JN),JM)
          CP2K=B(1,8)
          DO 23999 JM=1,4
          NE(JM)=NE1(JM,ISORT(JN))

```

```

23999  IE(JM)=IE1(JM,ISORT(JN))
      REF(1)=REF1(1,ISORT(JN))
      REF(2)=REF1(2,ISORT(JN))
      REF3=REF2(ISORT(JN))
      COMMAND='AUTO_RECALC'
      IF(NUMIN(:2).EQ.'11')DOCTYPE='NOCALC'
      CALL FILE(LS,RS,B,CP2K,REF,REF3,IE,NE,CS,IX,MM1,E,FLAG,BFLAG
+,TEXT,BLFLAG,FORM,FORMP,SPECP,RS22,CPINF,SYMR,SYMS,SYMM,BD,TS,FIL
+,N,KOUNT,LENF,LENFP,DELB,DOCTYPE,KDOCT,DELTA,IOP)
      IF(FIL.EQ.-10)THEN
          FIL=0
          GOTO 27
      ENDIF
      COMMAND=' '
      DOCTYPE=' '
      IF(IQR.EQ.0)THEN
          WRITE(*,*)' ReWriting Database. Please Wait'
          IQR=1
      ENDIF
23987  CONTINUE
      NUMIN(:1)='*'
      GOTO 69696
*
      GOTO 27
      ENDIF
      GOTO 2109
      ENDIF
      IF(NUMIN(:2).EQ.'11'.AND.ICNT.EQ.0)GOTO 2108
      IF((NUMIN(:1).EQ.'1').OR.(NUMIN(:1).EQ.'E')) GOTO 10000
      IF((NUMIN(:1).EQ.'2').OR.(NUMIN(:1).EQ.'V')) THEN
          IENTRY=0
          CALL LISTGR(AS,A,NGRPT,IFIRST,ILAST,IENTRY,IHELP,NE1,IE1)
          GOTO 27
      ENDIF
      IF(NUMIN(:1).EQ.'3'.OR.NUMIN(:1).EQ.'M'.OR.NUMIN(:1)
+.EQ.'?')THEN
          IF(IHELP.EQ.0)THEN
              IHELP=1
              GOTO 27
          ENDIF
          IF(IHELP.EQ.1)THEN
              IHELP=0
              GOTO 27
          ENDIF
      ENDIF

```

```

c
2108  CONTINUE
      IF(NUMIN(:1).EQ.'D'.OR.NUMIN(:1).EQ.'4'.OR.NUMIN(:1).EQ.'L'
+.OR.((NUMIN(:1).EQ.'5'.OR.NUMIN(:2).EQ.'11').AND.ICNT.EQ.0))THEN
          ICNT=0
          NDEL=0
          CALL READSP(S,SS,ICNT,IE1,NE1,REF1,REF2,PHSE,IENTRY,IHELP)

```

```

        IF(ICNT.EQ.0)GOTO 27
    IF(NUMIN(:1).EQ.'8'.OR.NUMIN(:1).EQ.'9')GOTO 87
    IF(NUMIN(:2).EQ.'11')GOTO 124
        GOTO 27
    ENDIF

87    CONTINUE
    IF(NUMIN(:1).EQ.'8')THEN
        IF(IIICT.EQ.0)THEN
            CALL CLS
            WRITE(*,*)' ENTER (*.LST) FILENAME FOR INPUT TO'
            WRITE(*,*)'     THERMFIT NASA TYPE POLYNOMIAL PROCEDURE '
            read(*,52)NASAFI
            CALL LRDCHAR(NASAFI)
            IF(NASAFI.EQ.' ' .OR.NASAFI.EQ.'Q'.OR.NASAFI.EQ.'q')GOTO 27
            call fname(nasafi,'lst')
            INQUIRE(FILE=NASAFI,EXIST=EXST,ERR=27)
            IF(EXST)GOTO 193
            CALL CLS
            WRITE(*,*)NASAFI, 'DOES NOT EXIST'
            CALL LINES(0,2)
            WRITE(*,*)' { hit RETURN to continue }'
            read(*,3) numin
            goto 27
193    CALL CLS
            WRITE(*,*)' ENTER (*.DAT) OUTPUT FILENAME'
            WRITE(*,*)'     FOR NASA FORMAT COEFFICIENTS'
            read(*,52)NASAFO
            CALL LRDCHAR(NASAFO)
            call fname(nasafo,'dat')
            IF(NASAFO.EQ.' ' .OR.NASAFO.EQ.'Q'.OR.NASAFO.EQ.'q')GOTO 27
            ENDIF
            CLOSE(7,STATUS='KEEP')

            INQUIRE(52,OPENED=OPNED)
            IF(OPNED)THEN
                DUMMY=' '
                WRITE(52,'(A70)')DUMMY
                WRITE(52,'(A70)')DUMMY
                ENDFILE(52)
                CLOSE(52,STATUS='KEEP')
            ENDIF

            CLOSE(34,STATUS='KEEP')
            FIL=0
            IOP=0
            ICNT=0
802    CONTINUE
            EXEFIL=' '
            EXEFIL(:2)=DRIVE1
            EXEFIL(3:15)='THERMFIT.EXE'
            INQUIRE(FILE=EXEFIL,EXIST=EXST)

```

```

IF(EXST)GOTO 801
CALL CLS
WRITE(*,*)' CANNOT FIND:'
WRITE(*,*)EXEFIL
CALL LINES(0,2)
WRITE(*,*)' CURRENT DEFAULT DISK AND DIRECTORY:'
CALL LINES(0,1)
I = SYSTEM('cd'C)
CALL LINES(0,2)
PAUSE ' enter new drive specification or change directory "cd\""'
CALL CLS
WRITE(*,*)' NEW DEFAULT DISK AND DIRECTORY:'
CALL LINES(0,1)
I = SYSTEM('cd'C)
CALL LINES(0,2)
WRITE(*,*)' { hit RETURN to continue or Q return to main menu }'
READ(*,3)NUMIN
CALL READCHAR(NUMIN)
IF(NUMIN.EQ.'Q')GOTO 27
GOTO 802
801 CONTINUE
OPEN(45,FILE='THERMFIT.TMP',STATUS='UNKNOWN')
WRITE(45,*)' '
WRITE(45,52)NASAFI
WRITE(45,52)NASAF0
64 FORMAT(1X,A14)
CLOSE(45,STATUS='KEEP')
IF(DRIVE1.EQ.'A:')THEN
I = SPAWN(0,LOC('a:thermfit'C),INT4(0))
ELSE IF(DRIVE1.EQ.'B:')THEN
I = SPAWN(0,LOC('b:thermfit'C),INT4(0))
ELSE IF(DRIVE1.EQ.'C:')THEN
I = SPAWN(0,LOC('c:thermfit'C),INT4(0))
ELSE IF(DRIVE1.EQ.'D:')THEN
I = SPAWN(0,LOC('d:thermfit'C),INT4(0))
ELSE IF(DRIVE1.EQ.' ')THEN
I = SPAWN(0,LOC('thermfit'C),INT4(0))
ENDIF
IF(I.NE.0)THEN
CALL CLS
WRITE(*,*)' ERROR ENCOUNTERED IN NASA FORMAT'
WRITE(*,*)' DATABASE GENERATION PROCEDURE'
CALL LINES(0,2)
WRITE(*,*)' ERROR CODE RETURNED = ',I
CALL LINES(0,2)
if(i.eq.2)then
write(*,*)' INPUT FILES NOT FOUND'
ENDIF
IF(I.EQ.-1)THEN
WRITE(*,*)' insufficient memory available to spawn'
write(*,*)' this procedure.'
write(*,*)' use a system w/ 640K RAM or run this'
write(*,*)' procedure off line (from DOS directly)'
call lines(0,1)

```



```

endif
WRITE(*,*)' { hit return to continue }'
read(*,3)numin
ENDIF
GOTO 27
ENDIF

316 IF(NUMIN(:1).EQ.'9')THEN
continue
CLOSE(7,STATUS='KEEP')
EXEFIL=' '
EXEFIL(:2)=DRIVE3
EXEFIL(3:15)='THERMRXN.EXE'
INQUIRE(FILE=EXEFIL,EXIST=EXST)
IF(EXST)GOTO 317
CALL CLS
WRITE(*,*)'CANNOT FIND:'
WRITE(*,*)EXEFIL
WRITE(*,*)'REACTION ANALYSIS PROCEDURE'
CALL LINES(0,2)
WRITE(*,*)'CURRENT DRIVE AND DIRECTORY :'
I = SYSTEM('cd'C)
PAUSE 'change directory or drive specification'
CALL CLS
WRITE(*,*)'CURRENT DRIVE AND DIRECTORY :'
I = SYSTEM('cd'C)
WRITE(*,*)'(hit return to continue or "Q" to main menu )'
read(*,1)NUMIN
CALL READCHAR(NUMIN)
IF(NUMIN(:1).EQ.'Q')GOTO 27
GOTO 316

317 CONTINUE
OPEN(13,FILE='THUNITS.TMP',STATUS='UNKNOWN')
WRITE(13,1)UNITS
CLOSE(13,STATUS='KEEP')
IF(DRIVE3.EQ.'A:')THEN
I = SPAWN(0,LOC('a:thermrxn'C),INT4(0))
ELSE IF(DRIVE3.EQ.'B:')THEN
I = SPAWN(0,LOC('b:thermrxn'C),INT4(0))
ELSE IF(DRIVE3.EQ.'C:')THEN
I = SPAWN(0,LOC('c:thermrxn'C),INT4(0))
ELSE IF(DRIVE3.EQ.'D:')THEN
I = SPAWN(0,LOC('d:thermrxn'C),INT4(0))
ELSE IF(DRIVE3.EQ.' ')THEN
I = SPAWN(0,LOC('thermrxn'C),INT4(0))
ENDIF
INQUIRE(13,EXIST=EXST)
IF(EXST)THEN
OPEN(13,FILE='THUNITS.TMP',STATUS='OLD')
READ(13,1)UNITS
CLOSE(13,STATUS='DELETE')
ENDIF
ENDIF

```

```

IF(I.NE.0)THEN
    CALL CLS
    WRITE(*,*)' ERROR ENCOUNTERED IN THERMRXN'
    WRITE(*,*)' REACTION ANALYSIS PROCEDURE'
    CALL LINES(0,2)
    WRITE(*,*)' ERROR CODE RETURNED = ',I
    CALL LINES(0,2)
IF(I.EQ.-1)THEN
    WRITE(*,*)' insufficient memory available to spawn'
    write(*,*)'      this procedure.'
write(*,*)' use a system w/ 640K RAM or run "THERMRXN.EXE"'
    write(*,*)'      from DOS directly'
    call lines(0,1)
endif
    WRITE(*,*)' { hit return to continue }'
    read(*,3)numin
ENDIF
GOTO 27
ENDIF

```

```

IF(NUMIN(:1).EQ.'5'.OR.NUMIN(:1).EQ.'T')THEN
CALL LISTGR(SS,S,ICNT,IFIRST,ILAST,8,IHELP,NE1,IE1)
    NUMIN=' '
    GOTO 27
ENDIF

```

```

2109 IF(NUMIN(:1).EQ.'6'.OR.NUMIN(:1).EQ.'S'.OR.((NUMIN(:1).EQ.'7'.OR.
+NUMIN(:2).EQ.'10').AND.IOP.EQ.0))THEN

```

```

** FOR OPTION 10 AND 7 THIS BLOCK INITIALIZES BOTH LOADSP AND FILE

```

```

IENTER=0
REF(1)=' '
REF(2)=' '
REF3=' '
SYMS=0
SYMM=0
SYMR=0
FORM=' '
FORMP=' '
N=0
NSAVE=0
LS=' '
RS=' '
SPEC=' '
SPECP=' '
NATOM=0
NATOMP=0
FLAG=0
FLG=0
BFLAG=0
BLFLAG=0

```

```

SCOR=0.0
SCORP=0.0
BD=0.0
DELB=0.0
DO 32 I=1,60
  CS(1,I)=' '
32  CS(2,I)=' '
  DO 33 I=1,50
    E(I)=0
33  IX(I)=0
    DO 34 I=1,4
      IE(I)=' '
34  NE(I)=0
    KNT=0
    IF(NUMIN(:1).EQ.'7'.OR.NUMIN(:2).EQ.'10')THEN
      IENTER=3
      NCALL=0
    ENDIF
    CALL LOADSP(AS,A,IFIRST,ILAST,NGRPT,CS,B,N,NSAVE,SYMM,SYMS,
+SYMR,SCOR,SCORP,FORM,FORMP,SPECP,IE,NE,NATOM,FLAG,BFLAG,FLG,LS,RS,
+RS22,FILST,DOCFIL,IX,E,LENF,EP,FILNM,DOC,NDOC,TEXT,TEXTS,KOUNT,
+IOP,IDOC,NSPEC,BD,LENFP,IENTER,JC,DELB,DOCTYPE,KDOCT,DELTA)
    IF(NUMIN(:1).EQ.'7'.OR.NUMIN(:2).EQ.'10')THEN
      IOP=1
      IENTER=2
      IF(NUMIN(:2).EQ.'10')GOTO 124
      GOTO 9786
    ENDIF
    IF(FLG.EQ.1)GOTO 27
    CALL FORMINT(FORMP,LENFP,IP,NP,NATOMP,1)
    ISOURCE=1
    GOTO 8990
  ENDIF

9786  IF((NUMIN(:1).EQ.'7'.OR.NUMIN(:2).EQ.'10').AND.IOP.NE.0)THEN
  IQR=0
  DO 45632 JC=1,NSPEC
  IENTER=2
    IF(NUMIN(:1).EQ.'7')THEN
      CALL DELCHK(JC,ID)
      IF(ID.EQ.1)GOTO 45632
    ELSE IF(NUMIN(:2).EQ.'10')THEN
      CALL DELCHK(ISORT(JC),ID)
      IF(ID.EQ.1)GOTO 45632
    ENDIF
  SYMS=0
  SYMM=0
  SYMR=0
  FORM=' '
  FORMP=' '
  N=0
  NSAVE=0

```

```

LS=' '
RS=' '
SPEC=' '
SPECP=' '
NATOM=0
NATOMP=0
FLAG=0
FLG=0
BFLAG=0
BLFLAG=0
SCOR=0.0
SCORP=0.0
BD=0.0
DELB=0.0
KNT=0
DO 69 I=1,60
  CS(1,I)=' '
69  CS(2,I)=' '
  DO 73 I=1,50
    E(I)=0
73  IX(I)=0
    DO 71 I=1,4
      IE(I)=' '
71  NE(I)=0
  IF(NUMIN(:2).EQ.'10')THEN
    IF(ISORT(JC).EQ.0)THEN
      C   ON SORT ERROR RETURN TO MAIN MENU
          WRITE(*,*)'SORT ERROR ON SPECIES# ',JC
          WRITE(*,*)' AUTO_RECALC ABORTED'
          PAUSE' hit return to continue'
          GOTO 27
    ENDIF
    JL=ISORT(JC)
  ENDIF
  IF(NUMIN(:1).EQ.'7')JL=JC
  COMMAND='AUTO_RECALC'
  CALL LOADSP(AS,A,IFIRST,ILAST,NGRPT,CS,B,N,NSAVE,SYMM,SYMS,
+SYMR,SCOR,SCORP,FORM,FORMP,SPECP,IE,NE,NATOM,FLAG,BFLAG,FLG,LS,RS,
+RS22,FILST,DOCFIL,IX,E,LENF,EP,FILNM,DOC,NDOC,TEXT,TEXTS,KOUNT,
+IOP,IDOC,NSPEC,BD,LENFP,IENTER,JL,DELB,DOCTYPE,KDOCT,DELTA)
  COMMAND=' '
  IF(FLG.EQ.1)GOTO 27
  C   CALL FORMINT(FORMP,LENFP,IP,NP,NATOMP,1)
  PHASE='G'
  REF(1)=' '
  REF(2)=' '
  REF3=' '
  DO 45631 JCOUNT=1,N
  IF((IX(JCOUNT).GE.IFIRST(4)).AND.(IX(JCOUNT).LE.ILAST(4)))THEN
    BFLAG=1
    KNT=KNT+1
    IF(KNT.EQ.2)BFLAG=2
    GOTO 45631
  ENDIF

```

```

        IF((IX(JCOUNT).GE.IFIRST(3)).AND.(IX(JCOUNT).LE.ILAST(3)))THEN
            FLAG=1
            GOTO 45631
        ENDIF
        IF(FLAG.EQ.1)GOTO 45631
        FLAG=0
45631 CONTINUE
        ISOURCE=1
        CPINF = ((3*NATOM) - (2.+(FLOAT(NROT)/2.)))*1.987
        CP2K = B(1,9) + .37*(CPINF - B(1, 9))
        COMMAND='AUTO_RECALC'
        CALL FILE(LS,RS,B,CP2K,REF,REF3,IE,NE,CS,IX,MM1,E,FLAG,BFLAG
+,TEXT,BLFLAG,FORM,FORMP,SPECP,RS22,CPINF,SYMR,SYMS,SYMM,BD,TS,FIL
+,N,KOUNT,LENF,LENFP,DELB,DOCTYPE,KDOCT,DELTA,IOP)
            IF(FIL.EQ.-10)THEN
                FIL=0
                GOTO 27
            ENDIF
            COMMAND=' '
        IF(IQR.EQ.0)THEN
            WRITE(*,*)'ReGenerating Database Files. Please Wait'
            IQR=1
        ENDIF
45632 CONTINUE
            IIICT=1
            NUMIN='8'
            GOTO 87
c      GOTO 27
        ENDIF

```

```

C
C***** ENTER A NEW SPECIES *****
C
10000 FLAG = 0
        NTEMPS=7
        DO 29 I=1,9
29      DELTA(I)=0.0
        NED=0
        BFLAG = 0
        SCORP=0
        BLFLAG=0
        SYMS=0
        SCOR = 0
        SYMM = 0
        SYMR = 0
        GRTOT=0
        IERR=0
        ISOURCE=0

```

```

      BD=0.0
      DELB=0.0
      DOCTYPE=' '
      KDOCT=0
      DO 543 IZ1=1,10
      TEXTS(IZ1)=' '
543  TEXT(IZ1)=' '
      KOUNT=0
      KOUNTS=0
      DO 502 Z1=1,3
      DO 500 Z = 1, 9
         B(Z1,Z) = 0.0
500  CONTINUE
502  CONTINUE
501  CALL CLS
      WRITE(*,*) '   Enter species name (ID)'
      WRITE(*,*) '       9 characters maximum'
      WRITE(*,*) '{ "Q" return to opening menu }'
      READ(*,3) LS
3     FORMAT(A14)
      CALL READCHAR(LS)
      IF((LS(:1).EQ.'Q').AND.(LS(2:2).EQ.' '))GOTO 27
         IF(LS(:1).EQ.'?')THEN
            OPTION='ENTERSPEC'
            CALL HELP(HLP(3),OPTION)
            GOTO 502
         ENDIF

      SPECP(:14)=LS(:14)
      M = 1

8803  CALL CLS
      write(*,*)' '
      WRITE(*,*)'enter the elemental formula for this species '
      write(*,*)'{ example: for PHENOL enter " C6H5OH " }'
      WRITE(*,*)'{           for TOLUENE enter " C6H5CH3 " }'
      WRITE(*,*)'{           for CHLOROPHENOL enter " C6H4CLOH " }'
      CALL LINES(0,2)
      WRITE(*,*)'       4 ELEMENTS MAXIMUM : 70 CHARACTERS MAX'
      CALL LINES(0,1)
      IF(IHELP.EQ.1)THEN
         WRITE(*,*)' THE FOLLOWING ELEMENTS ARE DEFINED:'
         IF(NELEM.GT.10)THEN
            ISTOP=10
         ELSE IF(NELEM.LE.10)THEN
            ISTOP=NELEM
         ENDIF
         WRITE(*,1832)(ELEM(15),15=1,ISTOP)
1832  FORMAT(' ',10(2X,A2))
         IF(NELEM.LE.20.AND.NELEM.GT.10)WRITE(*,1832)(ELEM(15),15=11,
+NELEM)
         IF(NELEM.GT.20)THEN
            WRITE(*,*)' MORE THAN 20 ELEMENTS ARE DEFINED'
            WRITE(*,*)' NOT ALL ARE SHOWN'

```

```

        ENDIF
        CALL LINES(0,1)
        WRITE(*,*)' ALL OTHER ELEMENTS OR NON-NUMERIC CHARACTERS'
        WRITE(*,*)'           WILL BE IGNORED !'
        CALL LINES(0,1)
        WRITE(*,*)' enter formula here: {Q=QUIT}'
        ENDIF
52  read(*,52) FORM
        FORMAT(A70)
        CALL LRDCHAR(FORM)
        IF(FORM.EQ.' '.OR.FORM.EQ.'Q')GOTO 10000
        IF(FORM(:1).EQ.'?')THEN
                OPTION='FORM'
                CALL HELP(HLP(3),OPTION)
                CALL CLS
                GOTO 8803
        ENDIF

        CALL DEBLNK(FORM,DUMMY,LENF,0)
51  FORMAT(A14)
        CALL CLS
        IF(ERRORCK.EQ.' ')THEN
                iform=0
        ELSE
                IFORM=1
        ENDIF
        CALL FORMINT(FORM,LENF,IE,NE,NATOM,iform)
        if(iform.lt.0)goto 8803
        FORMP(:LENF)=FORM(:LENF)
        LENFP=LENF
        DO 568 KJ=1,4
                IP(KJ)=IE(KJ)
568         NP(KJ)=NE(KJ)
        NATOMP=NATOM
25001  CONTINUE
        IF(ERRORCK.EQ.' ')THEN
                CALL LINES(0,2)
                WRITE(*,*) ' number of Atoms for This Species =' ,NATOM
                WRITE(*,*)' '
                WRITE(*,*)'   IF THIS IS INCORRECT ENTER " Q "'
                WRITE(*,*)'           TO BEGIN AGAIN'
                WRITE(*,*)' OTHERWISE HIT RETURN TO CONTINUE'
                READ(*,3) FS
                CALL READCHAR(FS)
                IF (FS(1:1) .EQ. 'Q' ) GOTO 8803

2500  IF(IHELP.EQ.1)THEN
        CALL CLS
        WRITE(*,*)' Radicals are estimated either by entering a'
        write(*,*)' radical {CDOT} group such as " CB/. " on this'
        write(*,*)' screen; or by first estimating the properties'
        write(*,*)' for the stable molecule here { ex: benzene } and'
        write(*,*)' then applying a bond increment {BD} group to '
        write(*,*)' account for loss of H atom from the molecule.'

```

```

      call lines(0,1)
      write(*,*)' Bond increments cannot be entered here. They'
      write(*,*)' are entered at the RADICAL menu { available'
      write(*,*)' after the molecule's properties are estimated }.'
      call lines(0,1)
      write(*,*)' You must be sure that groups you enter adequately'
      write(*,*)' define a molecule (no unbonded electrons).'

```

 call lines(0,2)
ENDIF

WRITE(*,*) ' Enter the Number of Groups in this species'
WRITE(*,*)' (each Central Atom or Ring Correction counts as 1 grou
+p)'
```



```

 ELSE
WRITE(*,*)' Enter 0 for literature data input or RETURN to enter g
+roups'
```



```

 ENDIF
READ(*,3) NUMIN
CALL READCHAR(NUMIN)
IF(NUMIN(1:1).EQ.'Q')GOTO 10000
 IF(NUMIN.EQ.'0')THEN
* transfer to literature data input block
 DOCTYPE='NOCALC'
 GOTO 1277
 ENDIF
 IF(NUMIN(:3).EQ.'REF'.OR.NUMIN(:3).EQ.'LIT')THEN
 DOCTYPE='NOCALC'
 IF(NUMIN(:3).EQ.'REF'.OR.NUMIN(:3).EQ.'LIT')THEN
 call cls
 WRITE(*,*)' enter literature data: record groups'
 write(*,*)'enter total number of groups: { Q=QUIT }'
 read(*,3)numin
 call readchar(numin)
 if(numin.eq.' '.or.numin.eq.'Q')goto 10000
 call readnum(numin,rnum,ngrp,flg)
 if (flg.eq.1)then
 flg=0
 goto 10000
 endif
 goto 8802
 ENDIF
 IF(NUMIN.EQ.'0')THEN
 N=0
 NSAVE=0
 NGRP=0
 ENDIF
 IF(NUMIN.EQ.' '.AND.ERRORCK.NE.' ')THEN
 N=100
 NSAVE=100
 NGRP=100
 ENDIF
ENDIF

```


```



```

                                GOTO 8802
ENDIF
IF(NUMIN(:1).EQ.'?' .AND. IHHELP.NE.1 .AND. .ERRORCK.EQ.' ')THEN
    IHHELP=1
    GOTO 2500
ELSE IF (NUMIN(:1).EQ.'?' .AND. IHHELP.EQ.1 .AND. ERRORCK.EQ.' ')THEN
    OPTION='NGROUPS'
    CALL HELP(HLP(3),OPTION)
    CALL CLS
    GOTO 2500
ELSE IF(NUMIN(:1).EQ.'?' .AND. ERRORCK.NE.' ')THEN
    OPTION='LIT/REF'
    CALL HELP(HLP(3),OPTION)
    CALL CLS
    GOTO 25001
ENDIF
CALL READNUM(NUMIN,RNUM,NGRP,FLG)
IF(FLG.EQ.1)THEN
    FLG=0
    GOTO 10000
ENDIF
8802 CONTINUE
    IF(NGRP.NE.0 .AND. ERRORCK.EQ.' ')THEN
WRITE(*,*) ' '
WRITE(*,*) 'How many different groups are to be entered?'
READ(*,3) NUMIN
CALL READCHAR(NUMIN)

IF(NUMIN(1:1).EQ.'Q')GOTO 10000
    IF(NUMIN(:1).EQ.'?')THEN
        OPTION='DGROUPS'
        CALL HELP(HLP(3),OPTION)
        CALL CLS
        GOTO 8802
    ENDIF
    IF(NUMIN.EQ.' ' .OR. NUMIN.EQ.'0')THEN
        N=0
        NSAVE=0
        DOCTYPE='NOCALC'
        GOTO 459
    ENDIF
CALL READNUM(NUMIN,RNUM,N,FLG)
IF (FLG.EQ.1)THEN
    FLG=0
    GOTO 10000
ENDIF
NSAVE=N
ENDIF
459 CONTINUE
*----- NUMBER FREE ROTORS ( AT 5000 K )-----
22501 CALL CLS
WRITE(*,*) ' how many rotors in this species { 0 }'
read(*,'(a)')numin

```

```

        call readchar(numin)
        call dblnk(numin,lnum,0)
        if(numin.eq.'Q')goto 22501
        if(numin.eq.'?')then
            option='NROTOR'
            CALL HELP(HLP(3),OPTION)
            GOTO 22501
        ENDIF
        if(numin.eq.' '.or.numin.eq.'0')then
            nrot=0
        else
            call readnum(numin,rnum,NROT,kflg)
            if(kflg.ne.0)goto 22501
        endif
        nrots=nrot

```

*-----

```

45    CALL CLS
        IF((NGRP.NE.0.AND.N.NE.0).OR.(ERRORCK.NE.' '))THEN
            write(*,*)ngrpt,' groups in the database'
            WRITE(*,*)' '
            IF(ERRORCK.EQ.' ')WRITE(*,50)N
50    FORMAT(1X,'You must enter a total of ',I3,' different groups')
            WRITE(*,*)' {enter " D " to re-enter the last group}'
            WRITE(*,*)' {enter " Q " to start a new species}'
            WRITE(*,*)' {enter " L " to list group database}'
            IF(ERRORCK.EQ.'NO')THEN
                WRITE(*,*)' {enter " " ( blank ) when finished}'
            ENDIF
            CALL LINES(0,2)
            WRITE(*,*)' ENTER: "GROUP ID,QUANTITY"'
            IF(IACT.EQ.3)THEN
                IACT=0
                IGM1=IG-1
                CALL LINES(0,2)
                IF(ERRORCK.EQ.' ')WRITE(*,1812)IGM1,N
1812  FORMAT('0',10X,I3,' out of ',I3,' groups have been entered')
                IF(IGM1.LE.0)GOTO 1778
                CALL WRITEGR(1,IGM1,CS,E,IG,6,LS)
                CALL LINES(0,2)
1778  IACT=0
                GOTO 3010
            ENDIF
            GRTOT=0
            IG=0
600  IG = IG+1
            IF(ERRORCK.EQ.' ')THEN
                IACT=1
            ELSE
                IACT=0
            ENDIF
            IF(IG.GT.N.AND.ERRORCK.EQ.' ')GOTO 601
3010  CALL READGR(IG,CS,EI,IACT,MM1)
            E(IG)=EI

```

```

        IF(IACT.EQ.-10)THEN
            IG=IG-1
            N=IG
            NSAVE=N
            GOTO 601

        ENDIF
        IF((IACT.EQ.1).AND.(IG.GE.2))IG=IG-2
        IF (IACT.EQ.1)GOTO 600
        IF(IACT.EQ.2) GOTO 10000
        IF(E(IG).EQ.0)E(IG)=1
        IF(IACT.EQ.3)THEN
            IENTRY=0
        CALL LISTGR(AS,A,NGRPT,IFIRST,ILAST,IENTRY,IHELP,NE1,IE1)
            GOTO 45
        ENDIF
        IF(IACT.EQ.4)GOTO 45
        CALL FINDGR(AS,NGRPT,CS,IX,IG,ISTAT,MM1)
        IF(ISTAT.EQ.1)THEN
            ISTAT=0
            GOTO 3010
        ENDIF
        IF((IX(IG).LE.ILAST(3)).AND.(IX(IG).GE.IFIRST(3)))FLAG=1
        IF((IX(IG).LE.ILAST(4)).AND.(IX(IG).GE.IFIRST(4))
        +.AND.(ERRORCK.EQ.' '))THEN
            CALL CLS
            WRITE(*,*)'          ERROR : YOU CANNOT ENTER'
            WRITE(*,*)'          BOND DISSOCIATION GROUPS'
            WRITE(*,*)'          ON THIS SCREEN'
            CALL LINES(0,3)
            WRITE(*,*)'          { hit return to continue }'
            call lines(0,3)
            READ(*,3)NUL
            IACT=3
            GOTO 45
        ENDIF
        GOTO 600
601  CONTINUE
            IF(N.NE.0)THEN

                DO 700 Y = 1, 9
                DO 800 NG = 1, N
                    IF(A(IX(NG),9).EQ.0.0.AND.A(IX(NG),8).NE.0.)NTEMPS=6
                    B(1, Y) = E(NG) * A(IX(NG), Y) + B(1,Y)
                    B(2,Y) = E(NG)*A(IX(NG),Y)+B(2,Y)
                    EP(NG)=E(NG)
                    CS(2,NG)=CS(1,NG)
                800  CONTINUE
                700  CONTINUE
                    GRTOT=0
                    DO 7801 Y=1,N
                7801  GRTOT=E(Y)+GRTOT
                    IF(GRTOT.NE.NGRP.AND.ERRORCK.EQ.' ' )THEN
                        CALL CLS
                        WRITE(*,*)' WARNING! You said there were ',NGRP,' total'

```

```

WRITE(*,*)'          but 'GRTOT,' groups were identified'
      CALL LINES (0,2)
WRITE(*,*)' hit RETURN to continue or enter "Q" to begin again'
      read(*,1)nul
      call readchar(nul)
      if(nul.eq.'Q')goto 10000

      ENDIF
      ENDIF
8804  CONTINUE
      ENDIF
IF (FLAG .EQ. 0) THEN
  WRITE(*,*) '    Enter symmetry # for molecule'
  READ(*,3) NUMIN
  CALL READCHAR(NUMIN)
  IF(NUMIN(1:1).EQ.'Q')GOTO 45
  IF(numin(:1).EQ.'?')THEN
    OPTION='SYMMETRY'
    CALL HELP(HLP(3),OPTION)
    CALL CLS
    GOTO 8804
  ENDIF
  CALL READNUM(NUMIN,RNUM,SYMM,FLG)
  SYMS=SYMM
C    WE SAVE PARENTS SYMMETRY NUMBER FOR LATER PROCESSING
  IF(FLG.EQ.1)THEN
    FLG=0
    GOTO 45
  ENDIF
ENDIF
IF (FLAG .EQ. 1) THEN
  WRITE(*,*) '    Enter symmetry # for radical'
  READ(*,3) NUMIN
  CALL READCHAR(NUMIN)
  IF(NUMIN(1:1).EQ.'Q')GOTO 45
  IF(numin(:1).EQ.'?')THEN
    OPTION='SYMMETRY'
    CALL HELP(HLP(3),OPTION)
    CALL CLS
    GOTO 8804
  ENDIF
  CALL READNUM(NUMIN,RNUM,SYMM,FLG)
  IF(FLG.EQ.1)THEN
    FLG=0
    GOTO 45
  ENDIF
ENDIF
IF (FLAG .EQ. 1) THEN
  SYMR = SYMM
ENDIF
  IF(DOCTYPE.NE.'NOCALC')THEN
    REF3(:6)=' THERM'
  SCOR = 1.98717 * ALOG(SYMM*1.0)
  B(1, 2) = B(1, 2) - SCOR
  SCORP=SCOR

```

```

P = NGRP
      ENDIF

***** LITERATURE INPUT FOLLOWS *****
1277  CONTINUE
      IF(DOCTYPE.EQ.'NOCALC')THEN
19991  fiunits='KCAL'
      CALL CLS
      WRITE(*,*)'enter literature data ( Q=QUIT )'
      call lines(0,1)
      write(*,*)'species: ',LS
      write(*,*)'form
      call lines(0,2)
      write(*,*)'input: Hf, S, Cp300, Cp400, Cp500, Cp600, Cp800, Cp100
+0, (Cp1500)'
      write(*,*)'      separate numbers with commas or blanks'
      read(*,52)numin1
      do 9765 ij9=1,70
9765  if(numin1(ij9:ij9).eq.',')numin1(ij9:ij9)=' '
      call deblnk(numin1,s2,len,1)
      if(numin1.eq.' '.or.numin1.eq.'q'.or.numin1.eq.'Q'.OR.
+len.eq.0)goto 10000
      IF(NUMIN1(:1).EQ.'?')THEN
          OPTION='LIT/INPUT'
          CALL HELP(HLP(3),OPTION)
          GOTO 1277

      ENDIF
97651  CALL LINES(0,1)
      write(*,*)' enter units: 1- Kcal/mol (cal/mol K)'
      write(*,*)'          2- KJ/mol (J/mol K)'
      CALL LINES(0,1)
      write(*,*)'      enter choice ( 1 )'
      read(*,3)nul
      IF(NUL(:1).EQ.'?')THEN
          OPTION='LIT/UNITS'
          CALL HELP(HLP(3),OPTION)
          GOTO 97651

      ENDIF
      if(nul(:1).eq.'2')fiunits='KJ'
      call indxst(numin1,' ',noccur,indx,len,1,flg)
      NUMIN=numin1(:indx(1)-1)
      call readnum(NUMIN,rnum,num,flg)
      if(fiunits.eq.'KJ')rnum=rnum/4.184
      B(1,1)=rnum
      b(2,1)=rnum
      do 9766 ij9=2,noccur
      NUMIN=numin1(indx(ij9-1)+1:indx(ij9)-1)
      call readnum(NUMIN,rnum,num,flg)
      if(fiunits.eq.'KJ')rnum=rnum/4.184
      b(1,ij9)=rnum
      b(2,ij9)=rnum
9766  continue
      NUMIN=numin1(indx(noccur)+1:len)
      call readnum(NUMIN,rnum,num,flg)

```

```

        if(fiunits.eq.'KJ')rnum=rnum/4.184
        b(1,noccur+1)=rnum
        b(2,noccur+1)=rnum
        if(units.eq.'KJ')then
            do 446 j1=1,9
                bo(j1)=b(1,j1)*4.184
                write(*,11)(bo(j1),j1=1,9)
            446
        else if(units.eq.'KCAL')then
            write(*,10)(b(1,ij9),ij9=1,9)
        endif
*----- NUMBER FREE ROTORS ( AT 5000 K )-----

62501      CONTINUE
        WRITE(*,*)' how many rotors in this species { 0 }'
        read(*,'(a)')numin
        call readchar(numin)
        call dblnk(numin,lnum,0)
        if(numin.eq.'Q')goto 62501
        if(numin.eq.'?')then
            option='NROTOR'
            CALL HELP(HLP(3),OPTION)
            CALL CLS
            GOTO 62501
        ENDIF
        if(numin.eq.' ' .or. numin.eq.'0')then
            nrot=0
        else
            call readnum(numin,rnum,NROT,kflg)
            if(kflg.ne.0)THEN
                CALL CLS
                goto 62501
            ENDIF
        endif
        nrots=nrot

*-----
4661      call lines(0,2)
        write(*,*)'enter text for reference { journal name, date, etc }'
        write(*,*)'      blank line or "Q" end text input'
        kount=0
9768      read(*,52)dummy
        IF(DUMMY(:1).EQ.'?')THEN
            OPTION='TEXT'
            CALL HELP(HLP(3),OPTION)
            GOTO 4661
        ENDIF
        if(dummy.ne.' ' .and. dummy.ne.'q' .and. dummy.ne.'Q')then
            kount=kount+1
            text(kount)=dummy
            IF(KOUNT.LE.50)goto 9768
        endif
        IF(KOUNT.EQ.1.AND.TEXT(KOUNT).EQ.' ')KOUNT=0
        call lines(0,2)
46619     symm=1

```

```

syms=1
write(*,*)' enter symmetry # ( not used for calculation )'
read(*,'(a)')numin
call readchar(numin)
if(numin.eq.'?')then
    OPTION='SYMMETRYL'
    CALL HELP(HLP(3),OPTION)
    CALL CLS
    GOTO 46619
elseif(numin.eq.' ' .or. numin.eq.'Q')THEN
    goto 80009
else
    call readnum(numin,rnum,SYMM,kflg)
    if(kflg.ne.0)goto 46619
    syms=symm
endif
80009 CALL CLS
write(*,*)'enter reference string { "Q" or " " = no string }'
write(*,*)'          14 characters max'
read(*,'(a14)')numin
IF(numin.EQ.'?')THEN
    OPTION='REF/STR'
    CALL HELP(HLP(3),OPTION)
    GOTO 80009
ENDIF
if (numin.eq.'Q'.or.numin.eq.' ' .or.numin.eq.'q')then
    REF(1)=' '
    REF(2)=' '
    REF3=' '
else
    ref(1)(:4)=numin(:4)
    ref(2)(:4)=numin(5:8)
    ref3(:6)=numin(9:14)
endif
goto 8990
ENDIF
***** END OF LITERATURE INPUT *****
C
C
C***** SPECIES SCREEN *****
8990 CALL CLS
    X=1
    KNT=0
    DO 8991 JCOUNT=1,N
c
column 72 ]

IF(NTEMPS.EQ.6)THEN
    B(1,9)=0.0
    B(2,9)=0.0
ENDIF
IF((IX(JCOUNT).GE.IFIRST(4)).AND.(IX(JCOUNT).LE.ILAST(4)))THEN
    BFLAG=1
    KNT=KNT+1
    IF(KNT.EQ.2)BFLAG=2

```

```

      GOTO 8991
ENDIF
IF((IX(JCOUNT).GE.IFIRST(3)).AND.(IX(JCOUNT).LE.ILAST(3)))THEN
  FLAG=1
  GOTO 8991
ENDIF
IF(FLAG.EQ.1)GOTO 8991
FLAG=0
8991 CONTINUE
  IF(DOCTYPE.EQ.'NOCALC')THEN
    WRITE(*,*)'Thermo Data Entered:'
  ELSE IF(BFLAG.GE.2)THEN
    WRITE(*,*)'Thermo estimation for diradical'
  ELSE IF (FLAG .EQ. 1 .OR. BFLAG .EQ. 1 ) THEN
    WRITE(*,*) 'Thermo estimation for radical'
  ELSE IF (FLAG .EQ. 0 .AND. BFLAG .EQ. 0 ) THEN
    WRITE(*,*) 'Thermo estimation for molecule'
  ENDIF
  IF (BLFLAG .EQ. 1) THEN
    WRITE(*,22) RS22,FORM(:LENF)
22   FORMAT(1X,A14,3X,A50)
23   FORMAT(1X,'RADICAL BASED UPON PARENT ',A14,3X,A70)
    GOTO 9003
  ENDIF
  IF (BFLAG.GE.1) THEN
    WRITE (*,22)RS,FORM(:LENF)
    WRITE(*,23)SPECP,FORMP(:LENFP)
  ENDIF
  IF (BFLAG.EQ.0) WRITE(*,22) LS,FORM(:LENF)
  IF(BFLAG.GE.1)WRITE(*,*)'PARENT SYMMETRY',SYMS
  CALL LINES(0,1)
9003  CALL WRITEGR(1,N,CS,E,IG,6,LS)
  CALL LINES(0,1)
  if(units.eq.'KCAL')then
    WRITE(*,*)'UNITS: Hf(Kcal/mol) S & Cp (cal/mol K)'
    WRITE(*,*) ' Hf      S      Cp 300  400    500    600      8
+00  1000  1500'
  else if(units.eq.'KJ')then
    WRITE(*,*)'UNITS: Hf(KJ/mol) S & Cp {J/mol K}'
    WRITE(*,*) ' Hf      S      Cp 300  400    500    600
+   800  1000  1500'
  endif
  CPINF = (3.0*FLOAT(NATOM)-(2.0+FLOAT(NROT/2.0)))*1.987
  if(units.eq.'KCAL')then
    IF(B(1,9).NE.0.)WRITE(*,10) (B(X,ID9),ID9=1,9)
    IF(B(1,9).EQ.0.)WRITE(*,10) (B(X,ID9),ID9=1,8)
10   FORMAT(9F8.2)
11   format(1x,F8.2,8(1x,F8.2))
    WRITE(*,665) CPINF
665  FORMAT(' ',5X,'CPINF',2X,F7.2)
    else if(units.eq.'KJ')then
      do 659 j1=1,9
659  bo(j1)=b(x,j1)*4.184

```



```

IF(BO(9).NE.0.)write(*,11)(bo(j1),j1=1,9)
IF(BO(9).EQ.0.)write(*,11)(bo(j1),j1=1,8)
cpio=cpinf*4.184
write(*,665)cpio

endif
IF (BFLAG .GE. 1) THEN
WRITE(*,*)'Symmetry number used to correct S value is ',SYMR
WRITE(*,*) 'R ln(2) has been added to S to account for unpaired
+d electron'
IF((TS(:1).EQ.'Q').OR.(TS(:1).EQ.' ').OR.(TS(:1).EQ.'O'))
+TS(:14)=TSS(:14)
IF(UNITS.EQ.'KCAL')THEN
WRITE(*,84848)BD
84848 FORMAT(5X,'bond dissociation energy used = ',f10.2)
ELSE IF(UNITS.EQ.'KJ')THEN
BDO=BD*4.184
WRITE(*,84848)BDO
ENDIF
ENDIF
IF (BFLAG .GE. 1 ) GOTO 900
WRITE(*,*) 'Symmetry number used to correct S value is', SYMM
900 CONTINUE
IF(KOUNT.GE.1)THEN
WRITE(*,*)' Notes : '
DO 933 IZ1=1,KOUNT
IF((BFLAG.EQ.0).OR.(FLAG.EQ.1)) TEXTS(IZ1)=TEXT(IZ1)
933 WRITE(*,74)TEXT(IZ1)
IF((BFLAG.EQ.0).OR.(FLAG.EQ.1)) KOUNTS=KOUNT
74 FORMAT(1x,A70)
CALL LINES(0,1)
ENDIF
9192 WRITE(*,*)' EDIT THESE RESULTS? "Y" OR {"N"}'
READ(*,3) DS
CALL READCHAR(DS)
IF(DS(:1).EQ.'?')THEN
OPTION='EDIT'
CALL HELP(HLP(3),OPTION)
CALL CLS
GOTO 8990
ENDIF

if(ds(:1).eq.'U')then
if(units.eq.'KCAL')then
units='KJ'
goto 8990
else if(units.eq.'KJ')then
units='KCAL'
goto 8990
endif
goto 8990
endif

IF(DS(1:1).EQ.'Y')THEN

```

```

CALL EDIT(CS,E,B,AS,A,N,RS22,LS,RS,TEXT,BD,TS,IX,FORM,FORMP,
+ CPINF,SYMM,SYMR,BFLAG,FLAG,BLFLAG,SCOR,SCORP,NSAVE,IG,NE,
+ IE,NGRPT,IFIRST,ILAST,NATOM,KOUNT,SYMS,TEXTS,KOUNTS,SPECP,
+ IHELP,LENF,LENFP,EP,NATOMP,IP,NP,ISOURCE,DELB,DOCTYPE,KDOCT,
+ DELTA,NED,BSAVE,DOCFIL,FILNM,DOC)
GOTO 8990

```

```
ENDIF
```

```
C*****
```

```
C
```

```
C SPECIES MENU OPTIONS
```

```
55 CALL CLS
```

```
IF(IHELP.EQ.0.AND.BFLAG.EQ.0)THEN
```

```
WRITE(*,*)'SPECIES OPTIONS MENU: R, F, P, L, H, Q, X, S, U'
```

```
GOTO 56
```

```
ENDIF
```

```
IF(IHELP.EQ.0.AND.BFLAG.NE.0)THEN
```

```
WRITE(*,*)'SPECIES OPTIONS MENU: R, F, M, P, L, H, Q, X, S, U'
```

```
goto 56
```

```
endif
```

```
WRITE(*,*)' SPECIES ESTIMATION OPTIONS MENU'
```

```
if(units.eq.'KCAL')then
```

```
write(*,*)' Units: Kcal/mol ( cal/mol K )'
```

```
else if(units.eq.'KJ')then
```

```
write(*,*)' Units: KJ/mol (J/mol K)'
```

```
endif
```

```
WRITE(*,*)'
```

```
+ _____'
```

```
write(*,*)' '
```

```
WRITE(*,*)'
```

```
R - CALCULATE RADICAL BASED UPON PREV
```

```
+IOUS SPECIES'
```

```
WRITE(*,*)'
```

```
F - ADD CURRENT SPECIES TO OUTPUT FIL
```

```
+E'
```

```
WRITE(*,*)'
```

```
H - TOGGLE (SHORT/LONG) MENU'
```

```
WRITE(*,*)'
```

```
P - RETURN TO PREVIOUS SPECIES SCREEN
```

```
+'
```

```
IF(BFLAG.NE.0)THEN
```

```
WRITE(*,*)'
```

```
M - RETURN TO PREVIOUS PARENT MOLECUL
```

```
+E'
```

```
ENDIF
```

```
WRITE(*,*)'
```

```
RETURN - ENTER A NEW SPECIES'
```

```
WRITE(*,*)'
```

```
L - LIST GROUPS'
```

```
WRITE(*,*)'
```

```
Q - RETURN TO MAIN MENU {choose "F" '
```

```
WRITE(*,*)'
```

```
first; current species is discard
```

```
+ed'
```

```
write(*,*)'
```

```
when you return to MAIN menu)'
```

```
WRITE(*,*)'
```

```
X - EXIT PROGRAM'
```

```
WRITE(*,*)'
```

```
S - GET SPECIES FROM { *.DOC } FILE'
```

```
WRITE(*,*)'
```

```
? - HELP '
```

```

        if(units.eq.'KCAL')then
            write(*,4940)
4940 format(1x,12x,'U',6x,'- CHANGE CURRENT UNITS TO : KJ/mol (J/mol
+K)')
            else if(units.eq.'KJ')then
                write(*,4941)
4941 format(1x,12x,'U',6x,'- CHANGE CURRENT UNITS TO : Kcal/mol (cal/
+mol K)')
            endif
        CALL LINES(0,1)

56        CONTINUE
        INQUIRE(7,OPENED=OPNED)
        IF(OPNED)THEN
            CALL LINES(0,1)
            BACKSPACE(7)
            READ(7,82)SPECL
82        FORMAT(A10)
            WRITE(*,*)' LAST SPECIES FILED: ',SPECL
            CALL LINES(0,1)
        ENDIF
        WRITE(*,*)'          enter option : { ENTER NEW SPECIES }'
        READ(*,3) DS
        CALL READCHAR(DS)
        CALL DEBLNK(DS,NUL,LEN,0)

* change units
        if(ds(:1).eq.'U')then
            if(units.eq.'KCAL!')then
                units='KJ'
                goto 55
            else if(units.eq.'KJ')then
                units='KCAL'
                goto 55
            endif
        goto 55
    endif

C*****
        IF(DS.EQ.' ' .OR.DS.EQ.'NEW')GOTO 10000
C*****
***** HELP *****
        IF(DS.EQ.'?')THEN
            WRITE(*,4343)
            READ(*,52)OPTION
            CALL LRDCHAR(OPTION)
            IF(OPTION.EQ.' ' .OR.OPTION.EQ.'Q')GOTO 55
            IF(OPTION(:1).EQ.'R' .OR.OPTION.EQ.'F' .OR.OPTION.EQ.'H' .OR.OPTION
+.EQ.'P' .OR.OPTION.EQ.'M')THEN
                CALL HELP(HLP(4),OPTION)
                GOTO 55
            ELSE IF(OPTION.EQ.'L' .OR.OPTION.EQ.'Q' .OR.OPTION.EQ.'X' .OR.

```

```

+OPTION.EQ.'S'.OR.OPTION.EQ.'O'.OR.OPTION.EQ.'?')THEN
      CALL HELP(HLP(5),OPTION)
      GOTO 55
    ENDIF
    GOTO 55
  ENDIF

*****
  IF(DS.EQ.'S')THEN
    NUMIN(:1)='6'
    GOTO 87
  ENDIF
  IF(DS.EQ.'Q')THEN
    GOTO 27
  ENDIF

C*****
  IF(DS.EQ.'H')THEN
    IF(IHELP.EQ.0)THEN
      IHELP=1
      GOTO 55
    ENDIF
    IF(IHELP.EQ.1)THEN
      IHELP=0
      GOTO 55
    ENDIF
  ENDIF

C*****
  IF (DS.EQ.'P') GOTO 8990
  IENTRY=0
  IF (DS.EQ.'L') CALL LISTGR(AS,A,NGRPT,IFIRST,ILAST,IENTRY,IHELP,
+NE1,IE1)
  IF (DS.EQ.'L')GOTO 55
  IF (DS .EQ. 'X' .OR. DS .EQ. 'EXIT') GOTO 9200
C*****
C
C***** M - RESET TO PARENT MOLECULE *****
C
4567 CONTINUE
  IF ((DS .EQ. 'M').AND.(BFLAG.NE.0))THEN
    IF(ISOURCE.EQ.0)THEN
      NROT=NROTS
      N=NSAVE
      BFLAG=0
      DO 857 NG=1,N
        CS(1,NG)=CS(2,NG)
857      E(NG)=EP(NG)
      DO 866 Y=1,9
866      B(1,Y)=B(2,Y)
      SYMM=SYMS
      SCOR=SCORP
      B(1,2)=B(1,2)-SCOR
      KOUNT=KOUNTS
      DO 867 IZ1=1,KOUNT

```

```

867      TEXT(IZ1)=TEXTS(IZ1)
        FORM=FORMP
        LENF=LENFP
        NATOM=NATOMP
            DO 548 KJ=1,4
            IE(KJ)=IP(KJ)
548      NE(KJ)=NP(KJ)
        GOTO 8990
ENDIF
IF(ISOURCE.EQ.1)THEN
IENTER=1
SYMS=0
SYMM=0
SYMR=0
FORM=' '
FORMP=' '
N=0
NSAVE=0
LS=' '
RS=' '
SPEC=' '
NATOM=0
NATOMP=0
FLAG=0
FLG=0
BFLAG=0
BLFLAG=0
SCOR=0.0
SCORP=0.0
BD=0.0
DELB=0.0
DO 869 I=1,60
CS(1,I)=' '
869    CS(2,I)=' '
DO 873 I=1,50
E(I)=0
873    IX(I)=0
DO 871 I=1,4
IE(I)=' '
871    NE(I)=0
        COMMAND=' '
CALL LOADSP(AS,A,IFIRST,ILAST,NGRPT,CS,B,N,NSAVE,SYMM,SYMS,
+SYMR,SCOR,SCORP,FORM,FORMP,SPEC,IE,NE,NATOM,FLAG,BFLAG,FLG,LS,RS,
+RS22,FILST,DOCFIL,IX,E,LENF,EP,FILNM,DOC,NDOC,TEXT,TEXTS,KOUNT,
+IOP,IDOC,NSPEC,BD,LENFP,IENTER,JC,DELB,DOCTYPE,KDOCT,DELTA)
        IF(FLG.EQ.1)GOTO 55
DO 54631 JCOUNT=1,N
IF((IX(JCOUNT).GE.IFIRST(4)).AND.(IX(JCOUNT).LE.ILAST(4)))THEN
        BFLAG=1
        GOTO 54631
ENDIF
IF((IX(JCOUNT).GE.IFIRST(3)).AND.(IX(JCOUNT).LE.ILAST(3)))THEN
        FLAG=1
        GOTO 54631

```

```

ENDIF
IF(FLAG.EQ.1)GOTO 54631
FLAG=0
54631 CONTINUE
ISOURCE=1
CPINF = ((3.0*NATOM) - (2.+(FLOAT(NROT)/2.0)))*1.987
CP2K = B(1,7) + .37*(CPINF - B(1, 7))
GOTO 8990
ENDIF
ENDIF
C***** END OF M BLOCK*****
C
C***** F - FILE BLOCK *****
IF (DS .EQ. 'F'.OR. DS .EQ. 'FILE') THEN
19020 X=1
PHASE='G'
COMMAND=' '
CALL FILE(LS,RS,B,CP2K,REF,REF3,IE,NE,CS,IX,MM1,E,FLAG,BFLAG
+,TEXT,BLFLAG,FORM,FORMP,SPECP,RS22,CPINF,SYMR,SYMS,SYMM,BD,TS,FIL
+,N,KOUNT,LENF,LENFP,DELB,DOCTYPE,KDOCT,DELTA,IOP)
ENDIF
IF (DS(1:1) .EQ. 'F' .OR. DS .EQ. 'FILE') GOTO 55
C***** END OF F - FILE BLOCK *****
C
C
C*****
IF(DS.EQ.' '.OR.DS.EQ.'NEW')GOTO 10000
C
C***** BEGIN R - CALCULATE RADICAL BLOCK *****
656 NUM=0
IF((DS.EQ.'R'.AND.BFLAG.GE.1).OR.(DS.EQ.'R'.AND.FLAG.EQ.1))THEN
CALL CLS
IF(IHELP.EQ.0.AND.FLAG.EQ.0)THEN
WRITE(*,*)'RADICAL OPTIONS: 1 - DIRADICAL, 2 - NEW RADICAL'
GOTO 456
ENDIF
IF(IHELP.EQ.0.AND.FLAG.EQ.1)THEN
WRITE(*,*)'RADICAL OPTIONS: 1 - DIRADICAL'
GOTO 456
ENDIF
WRITE(*,2525)
2525 FORMAT(35X,'RADICAL OPTIONS')
WRITE(*,2526)
2526 FORMAT('0',30X,30(' '))
WRITE(*,2527)
2527 FORMAT('0',30X,'1 - CALCULATE DIRADICAL FROM LAST RADICAL')
IF(FLAG.NE.1)THEN
WRITE(*,2528)
ENDIF
2528 FORMAT('0',30X,'2 - CALCULATE DIFFERENT RADICAL FROM PARENT')
WRITE(*,2529)
2529 FORMAT('0',30X,'Q - QUIT { RETURN TO PREVIOUS MENU }')
WRITE(*,*)' ? - HELP'
```

```

CALL LINES(0,3)
WRITE(*,*)'                               enter option : { Q }'
456   READ(*,51)NUMIN
CALL READCHAR(NUMIN)
IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 55
***** HELP *****
IF(NUMIN.EQ.'?')THEN
WRITE(*,4343)
READ(*,52)OPTION
CALL LRDCCHAR(OPTION)
IF(OPTION.EQ.' '.OR.OPTION.EQ.'Q')GOTO 55
CALL HELP(HLP(6),OPTION)
GOTO 656
ENDIF

*****
CALL READNUM(NUMIN,RNUM,NUM,FLG)
IF(FLAG.EQ.1.AND.NUM.EQ.2)FLG=1
IF(FLG.EQ.1)THEN
FLG=0
GOTO 55
ENDIF
c                               column 72 ]

IF((NUM.EQ.1.AND.BFLAG.GE.2).OR.(NUM.EQ.1.AND.FLAG.EQ.1.AND.
+BFLAG.NE.0).AND.ERRORCK.EQ.' '))THEN
CALL CLS
WRITE(*,*)' YOU CANNOT CALCULATE A TRIRADICAL'
CALL LINES(0,5)
WRITE(*,*)' { hit return to continue }'
read(*,51)nul
goto 55
endif
IF(NUM.EQ.1)THEN
BFLAG=2
GOTO 72
ENDIF
IF(NUM.EQ.2)THEN
BFLAG=1
DO 865 Y=1,9
865 B(1,Y)=B(2,Y)
SYMM=SYMS
SCOR=SCORP
GOTO 72
ENDIF
IF ((NUM.GE.3).OR.(NUM.LE.0))GOTO 55
ENDIF
72 IF (DS .NE. 'R') GOTO 55
CALL CLS
IF(IHELP.EQ.0)THEN
WRITE(*,*)'RADICAL MENU OPTIONS:'
GOTO 10100
ENDIF

```

C ***** RADICAL MENU OPTIONS *****

```

WRITE(*,*) '                RADICAL CALCULATION MENU '
WRITE(*,*) '                {radical by loss of H from parent}
+1
WRITE(*,*)'
+_____ '
CALL LINES(0,1)

WRITE(*,*)'                Q      -  RETURN TO PREVIOUS MENU'
WRITE(*,*)'                ?      -  HELP'
WRITE(*,*)' '
10100  continue
        IENTRY=4
CALL LISTGR(AS,A,NGRPT,IFIRST,ILAST,IENTRY,IHELP,NE1,IE1)
write(*,*)' '
write(*,*)'  ENTER BOND INCREMENT NAME ONLY'
WRITE(*,*)'                enter option : { Q }'
READ(*,3) TS
CALL READCHAR(TS)

```

C***** END OF RADICAL BD MENU *****

C*

***** HELP *****

```

IF(TS.EQ.'?')THEN
WRITE(*,4343)
READ(*,52)OPTION
CALL LRDCHAR(OPTION)
IF(OPTION.EQ.' '.OR.OPTION.EQ.'Q')GOTO 72
CALL HELP(HLP(6),OPTION)
DS='R'
GOTO 72

```

ENDIF

C***** Q - QUIT OPTION RETURN TO PREVIOUS MENU *****

```

IF((TS(:1).EQ.'Q').OR.(TS(:1).EQ.' '))GOTO 55

```

C***** BEGIN OTHER INPUT *****

```

IF (TS. EQ. 'O' .OR. TS .EQ. 'o') THEN
WRITE(*,*)'OPTION NOT YET AVAILABLE'
WRITE(*,*)' HIT RETURN TO CONTINUE'
READ (*,3)NUMIN
GOTO 10301

```

ENDIF

C***** END OTHER INPUT *****

C***** BEGIN SEARCH DATABASE FOR BOND DISSOCIATION GROUP **

```

ISTAT=0
MM1=14
NUL1(1,1)(:MM1)=TS(:MM1)
CALL FINDGR(AS,NGRPT,NUL1,19,1,ISTAT,MM1)
IF(ISTAT.EQ.1)THEN
ISTAT=0
GOTO 10100
ENDIF

```



```

IF((I9(1).GT.ILAST(4)).OR.(I9(1).LT.IFIRST(4)))THEN
  CALL CLS
  WRITE(*,*)'          ERROR : ENTER ONLY'
  WRITE(*,*)'          BOND DISSOCIATION GROUPS'
  WRITE(*,*)'          ON THIS SCREEN'
  CALL LINES(0,3)
  WRITE(*,*)'          { hit return to continue }'
  call lines(0,3)
  READ(*,3)NUL
  DS='R'
  GOTO 72
ENDIF
IF(NUM.EQ.2)THEN
  N=NSAVE+1
  GOTO 365
ENDIF
N=N+1
365 CS(1,N)=AS(I9(1))
E(N)=1
BD=A(I9(1),1)

      DO 1300 K = 2,9
      B(1,K)=B(1,K)+A(I9(1),K)
      IF(A(I9(1),9).EQ.0.0.AND.A(I9(1),8).NE.0.0)THEN
        B(1,9)=0.0
      ENDIF
1300 CONTINUE

C***** ESTIMATE PROPERTIES FOR THE RADICAL *****
10300 CONTINUE
      B(1,1)=B(1,1)+BD-52.1
      CALL CLS
10302 WRITE(*,*)'PARENT = ',FORMP(:LENFP)
      WRITE(*,*)' '
      WRITE(*,*)'BOND TYPE = ',TS
      WRITE(*,*)' '
10301 WRITE(*,*)'enter the symmetry number for the radical'
      READ(*,3) NUMIN
      CALL READCHAR(NUMIN)
      IF(NUMIN(1:1).EQ.'Q')THEN
        DS='M'
        GOTO 4567
      ENDIF
      IF(NUMIN(:1).EQ.'?')THEN
        OPTION='SYMMETRY'
        CALL HELP(HLP(3),OPTION)
        CALL CLS
        GOTO 10302
      ENDIF
      CALL READNUM(NUMIN,RNUM,SYMR,FLG)
      IF(FLG.EQ.1)THEN
        FLG=0
        DS='M'
        GOTO 4567

```

```

ENDIF
B(1,2)=B(1,2)+SCOR
SCOR=1.987*ALOG(SYMR*1.0)
10333 B(1,2)=B(1,2)-SCOR
IF(FLAG.EQ.0.AND.BFLAG.EQ.0)THEN
    BFLAG=1
    GOTO 2345
ENDIF
IF(FLAG.EQ.1.AND.BFLAG.EQ.0)THEN
    BFLAG=2
    GOTO 2345
ENDIF
IF(BFLAG.LE.1)THEN
    BFLAG=1
    GOTO 2345
ENDIF
2345 CONTINUE
IF (DS(1:1) .EQ. 'R' .AND. FLAG .EQ. 0) THEN
    WRITE(*,*)' '
    WRITE(*,*) 'Enter radical name(ID)'
    READ(*,3) RS
    CALL READCHAR(RS)
    IF(RS.EQ.'Q'.OR.RS.EQ.'QUIT')THEN
        DS='M'
        GOTO 4567
    ENDIF
    IF(RS(:1).EQ.'?')THEN
        OPTION='ENTERSPEC'
        CALL HELP(HLP(3),OPTION)
        CALL CLS
        GOTO 2345
    ENDIF
ENDIF
IF (DS(1:1) .EQ. 'R' .AND. FLAG .EQ. 1) THEN
    WRITE(*,*)' '
    WRITE(*,*) 'Enter diradical name(ID)'
    READ(*,3) RS22
    CALL READCHAR(RS22)
    IF(RS22.EQ.'Q'.OR.RS22.EQ.'QUIT')THEN
        DS='M'
        GOTO 4567
    ENDIF
    IF(RS22(:1).EQ.'?')THEN
        OPTION='ENTERSPEC'
        CALL HELP(HLP(3),OPTION)
        CALL CLS
        GOTO 2345
    ENDIF
ENDIF
2346 CONTINUE
write(*,*)' '
WRITE(*,*)'enter the elemental formula for this radical'
write(*,*)'({ example: for PHENYL enter " C6H5 " })'
WRITE(*,*)'({           for BENZYL enter " C6H5CH2 " })'

```

```

WRITE(*,*)'(          FOR VINYL enter " C2H3 " )'
CALL LINES(0,2)
WRITE(*,*)'          4 ELEMENTS MAXIMUM'
CALL LINES(0,2)
read(*,52)FORM
CALL LRDCHAR(FORM)
      IF(FORM(:1).EQ.'?')THEN
            OPTION='FORM'
            CALL HELP(HLP(3),OPTION)
            CALL CLS
            GOTO 2346
      ENDIF
CALL DEBLNK(FORM,DUMMY,LENF,0)
IF(FORM.EQ.' ' .OR.FORM(:1).EQ.'Q')THEN
      DS='M'
      GOTO 4567
ENDIF
      IF(ERRORCK.EQ.' ')THEN
            iform=0
      ELSE
            IFORM=1
      ENDIF
CALL FORMINT(FORM,LENF,IE,NE,NATOM,iform)
if(iform.lt.0)goto 2346
IF(ERRORCK.NE.' ')THEN
22601 CALL CLS
WRITE(*,*)' how many rotors in this species ( 0 )'
read(*,'(a)')numin
call readchar(numin)
call dblnk(numin,lnum,0)
if(numin.eq.'Q')goto 22601
if(numin.eq.'?')then
      option='NROTOR'
      CALL HELP(HLP(3),OPTION)
      GOTO 22601
ENDIF
if(numin.eq.' ' .or.numin.eq.'0')then
      nrot=0
else
      call readnum(numin,rnum,NROT,kflg)
      if(kflg.ne.0)goto 22601
endif
ENDIF
      IF(ERRORCK.EQ.' ')THEN
CALL LINES(0,2)
WRITE(*,*)' number of Atoms for This Species =' ,NATOM
WRITE(*,*)' '
WRITE(*,*)' IF THIS IS INCORRECT ENTER " Q "'
WRITE(*,*)' TO BEGIN AGAIN'
WRITE(*,*)' OTHERWISE HIT RETURN TO CONTINUE'
READ(*,3) FS
CALL READCHAR(FS)

```

```

        IF (FS(1:1) .EQ. 'Q' )THEN
            DS='M'
            GOTO 4567
        ENDIF

22602    CALL CLS
        WRITE(*,*)' how many rotors in this species { 0 }'
        read(*,'(a)')numin
        call readchar(numin)
        call dblnk(numin,lnum,0)
        if(numin.eq.'Q')goto 22602
        if(numin.eq.'?')then
            option='NROTOR'
            CALL HELP(HLP(3),OPTION)
            GOTO 22602
        ENDIF
        if(numin.eq.' ' .or. numin.eq.'0')then
            nrot=0
        else
            call readnum(numin,rnum,NROT,kflg)
            if(kflg.ne.0)goto 22602
        endif
    ENDIF
    IF (DS .EQ. 'R' .AND. FLAG .EQ. 0 )GOTO 8990
C*****END RADICAL ESTIMATION BLOCK*****
C*
C***** IF RETURN IS SELECTED : NEW SPECIES*****
    GOTO 10000
C***** GOTO 10000 :ENTER NEW SPECIES *****
C*
C***** IF X - EXIT WAS SELECTED, FILES ARE CLOSED ****
C***** AND THE PROGRAM TERMINATES *****
99999 CONTINUE
9200 CONTINUE

        INQUIRE(7,OPENED=OPNED)
        IF(OPNED)THEN
            ENDFILE(7)
            CLOSE(7)
        ENDIF

        INQUIRE(25,OPENED=OPNED)
        IF(OPNED)CLOSE(25)

        INQUIRE(41,OPENED=OPNED)
        IF(OPNED)THEN
            ENDFILE(41)
            CLOSE(41)
        ENDIF

        INQUIRE(52,OPENED=OPNED)
        IF(OPNED)THEN
19992    read(52,51,end=19993)nul
            goto 19992
        ENDIF

```

```
19993      BACKSPACE(52)
           NUL=' '
           WRITE(52,'(A70)')NUL
           WRITE(52,'(A70)')NUL
           ENDFILE(52)
           CLOSE(52)

           ENDIF

STOP ' '
END
```

APPENDIX V-B

FORTRAN SOURCE CODE FOR

THERMLST

```

PROGRAM THERMLST
C
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION TRA(3),F(14),CPL(50)
CHARACTER*1 PHASE
CHARACTER*2 IE(4), BLK1
CHARACTER*3 BLK2
      INTEGER NE(4)
CHARACTER*4 IFLAG,INAME,ID(10),REF(2)
CHARACTER*6 REF3
      CHARACTER*6 XNAME
      CHARACTER*1 CFLAG,CNROT
      CHARACTER*70 FILIN,FILOUT,DUMMY,S1,title
      character*14 nul,UNITS,FUNITS,FORM
      LOGICAL EXST1,EXST2,EXST
      COMMON/UNIT/UNITS,FORM,CFLAG
DATA IFLAG,BLK1,BLK2/'END ',' ',' ' /

C *****
C THE INPUT IS TAKEN DIRECTLY FROM THE THERMO DATA USED FOR
C CHEMKIN
C
C
C NPTS= NUMBER OF TEMPERATURE POINTS FOR A GIVEN SET
C INAME= NAME OF SPECIES (FIRST 4 LETTERS)
C XNAME= NAME OF SPECIES (NEXT 6 LETTERS)
C GMW= GRAM MOLECULAR WEIGHT OF SPECIES
C HF298= HEAT OF FORMATION AT 298 K (KCAL/MOLE) (JANAF INPUT)
C T (I) = TEMP IN DEGREE K
C CPL(I) = HEAT CAPACITY
C
C
C FILE ASSIGNMENTS ARE
C FILE 1 - INPUT DATA FITTED IN NASAFIT FORMAT FOR
C CHECKING 9SAME FORMAT AS USED FOR INTERPRETER)
C FILE 3 - OUTPUT LISTING H AND S 298 K AND CP'S OVER TEMP
C RANGES
C
C
C*****
C
C
* DEFINE DEFAULT UNITS
      FUNITS='KCAL'
      UNITS='KCAL'
      FORM='LONG'
      INQUIRE (FILE='THUNITS.TMP',EXIST=EXST)
      IF(EXST)THEN
            OPEN(13,FILE='THUNITS.TMP',STATUS='OLD')
            READ(13,70)DUMMY
            CALL DEBLNK(DUMMY,S1,LEN,0)
            UNITS='KCAL'

```

```

          IF(DUMMY(:2).EQ.'KJ')UNITS='KJ'
          READ(13,70,END=987)DUMMY
          CALL DEBLNK(DUMMY,S1,LEN,0)
          IF(DUMMY(:5).EQ.'SHORT')THEN
              FORM='SHORT'
          ENDIF
987      CLOSE(13,STATUS='DELETE')
      ENDIF

110      CONTINUE
      DO 111 I=1,30
111      WRITE(*,*)' '
          WRITE(*,*)'ENTER INPUT FILENAME (.DAT) '
          READ(*,70)FILIN
          CALL FNAME(FILIN,'DAT')
          INQUIRE(FILE=FILIN,EXIST=EXST1)
          if(exst1)then
              OPEN(1,FILE=FILIN,STATUS='OLD')
              goto 120
          endif
          write(*,*)' cannot find input file:'
          write(*,*)filin
          write(*,*)' hit return to continue or "Q" to abort'
          read(*,3)nul
          if(nul.eq.'q'.or.nul.eq.'Q')stop 2
          goto 110

120      WRITE(*,*)'ENTER OUTPUT FILNAME (.LST) '
          READ(*,70)FILOUT
          CALL FNAME(FILOUT,'LST')
          INQUIRE(FILE=FILOUT,EXIST=EXST2)
          ktrl=0
          IF(EXST2)THEN
              WRITE(*,*)'FILE ALREADY EXISTS'
              WRITE(*,70)FILOUT
              WRITE(*,*)' '
              WRITE(*,*)' 1 - OVERWRITE'
              WRITE(*,*)' 2 - APPEND'
              WRITE(*,*)' 3 - ENTER DIFFERENT FILENAME'
              WRITE(*,*)' '
              WRITE(*,*)'   enter option { 1 }'
              read(*,3) nul
              if(nul.eq.'2')ktrl=1
              if(nul.eq.'3')goto 120
          ENDIF

          if(units.ne.'KJ')units='KCAL'
          if(ktrl.eq.0)THEN
              CALL CLS
              WRITE(*,*)' what units do you want for output'
              write(*,*)' 1- Kcal/mol  or 2- KJ/mol'
              write(*,*)'   enter option: {1}'
              read(*,70)dummy
              call lrdchar(dummy)

```



```

        call dblnk(dummy, len, 0)
        if(dummy(:2).eq.'KJ'.or(dummy(:1).eq.'2')units='KJ'
OPEN(3, FILE=FILOUT, STATUS='UNKNOWN')
        if(units.eq.'KCAL')THEN
            write(3,*)'UNITS:KCAL'
        else if(units.eq.'KJ')then
            write(3,*)'UNITS:KJ'
        endif

    else if(ktrl.eq.1)then
        open(3, file=filout, status='old')
        UNITS='KCAL'
        READ(3,3,END=140)NUL
            IF(NUL(:8).EQ.'UNITS:KJ'.or.NUL(:9).eq.
+          ' UNITS:KJ')UNITS='KJ'
130         read(3,3, end=140)nul
            goto 130
140         backspace(3)
            backspace(3)

        endif

3         FORMAT(A14)
70        FORMAT(A70)

        CALL CLS
        write(*,*)' which table format do yo prefer?'
        write(*,*)' 1 - LONG format: Cp 300 - 5000 K'
        write(*,*)' 2 - SHORT format: Cp 300 - 1500 K'
        write(*,*)' enter option: {1}'
        read(*,70)dummy
        call lrdchar(dummy)
        call dblnk(dummy, len, 0)
        if(dummy(:5).eq.'SHORT'.or(dummy(:1).eq.'2')THEN
            FORM='SHORT'
        ELSE
            FORM='LONG'
        ENDF

10 READ (1,71) INAME
12 READ (1,71) TNAME

C
C

C ** READ DATA IN FROM FILES USED BY CHEMKIN, NOT JANAFIT.**
C   OR THERCOEF

C   GET ID FOR PRINTOUT

        WRITE(*,100)
100 FORMAT(1X,'enter a title line for the output file (blank = no
+ title)')
        READ(*,70) TITLE
101 FORMAT(15A4)
650 ICOUNT=1

```

```

WRITE(3,'(1X,A70)') TITLE
102  FORMAT (1H1,15A4)
WRITE(3,119)
119  FORMAT (1X,'SPECIES',4X,'HF(298)',2X,'S(298)',5X,'CP300',3X,
+ 'CP400',3X,'CP500',3X,'CP600',3X,'CP800',3X,'CP1000',2X,'CP1500',
+ 2X,'DATE REF ',8X,'ELEMENTS ')
IF(FORM.EQ.'LONG')WRITE(3,187)
187  FORMAT (1X,31X,'CP2000 CP2500 CP3000 CP3500 CP4000 CP5000 ')
655  CONTINUE
CFLAG=' '
READ(1,1010,END=900) INAME, XNAME, (REF(I),I=1,2),REF3,
1 (IE(I),NE(I),I=1,4),PHASE,TRA(1),TRA(3),TRA(2),CNROT
*   TRA(2)=1500.0
NROT=0
IF(CNROT.EQ.'1')NROT=1
IF(CNROT.EQ.'2')NROT=2
IF(CNROT.EQ.'3')NROT=3
IF(CNROT.EQ.'4')NROT=4
IF(CNROT.EQ.'5')NROT=5
IF(CNROT.EQ.'6')NROT=6
IF(CNROT.EQ.'7')NROT=7
IF(CNROT.EQ.'8')NROT=8
IF(CNROT.EQ.'9')NROT=9
IF (INAME.EQ.IFLAG) GOTO 900
DO 658 J = 1,4
IF (NE(J).EQ.0) IE(J) = BLK1
658  CONTINUE
C   TRA(1)=LOW TWMP   TRA(2)=MID-TEMP   TRA(3)=HIGH TEMP
660  READ(1,1020,END=900) (F(I),I=1,14)
ISAME=1
DO 1959 KI=1,7
IF(F(KI).NE.F(KI+7))ISAME=0
1959  CONTINUE
IF(ISAME.EQ.1)CFLAG='*'
C   F(8)-F(14) ARE LOW TEMP COEFFICIENTS
C   F(1)-F(7) ARE HIGH TEMP COEFFICIENTS
CALL CHECK(INAME,XNAME,IE,NE,REF,REF3,PHASE,F,TRA,NROT)
ICOUNT=ICOUNT+1
C   IF(ICOUNT.GE.55) GO TO 650
GO TO 655

71  FORMAT(A4)
1010 FORMAT(A4,A6,2A4,A6,4(A2,I3),A1,2F10.3,1X,F8.0,4X,A1)
1020 FORMAT(5E15.8,/,5E15.8,/,4E15.8)
900  CONTINUE
CLOSE(1,STATUS='KEEP')
CLOSE(3,STATUS='KEEP')
STOP
END
C

```

```

SUBROUTINE CHECK (INAME,XNAME,IE,NE,REF,REF3,PHASE,F,TRA,NROT)
  IMPLICIT REAL *8 (A-H,O-Z)
  DIMENSION TRA(3),F(14),CPL(50),CPJ(50),T1(20)
  CHARACTER*1 PHASE,CFLAG
  CHARACTER*2 IE(4)
  INTEGER NE(4)
  CHARACTER*4 REF(2),INAME
  CHARACTER*6 REF3
    CHARACTER*6 XNAME
    CHARACTER*14 UNITS,FORM
    COMMON/UNIT/UNITS,FORM,CFLAG
    T1(1)=300.
    T1(2)=400.
    T1(3)=500.
    T1(4)=600.
    T1(5)=800.
    T1(6)=1000.
    T1(7)=1500.
    T1(8)=2000.
    T1(9)=2500.
    T1(10)=3000.
    T1(11)=3500.
    T1(12)=4000.
    T1(13)=5000.
    NATOM=0
    ICARBON=0
    NCARBON=0

```

C

C-----FIRST COMPUTING HF298 AND S298 FROM THE INPUT PARAMETERS

C---- WANT TO COMPUTE H AND S AT 298 WITH THE LOW TEMP PARAMETERS

```

7  T=298.16
  H=1.98717*T*(((F(12)*T/5.+F(11)/4.)*T+F(10)/3.)*T+F(9)/2.)*
1  T+F(8)+F(13)/T
  HF298=H/1000.
  S=1.98717*(((F(12)*T/4.+F(11)/3.)*T+F(10)/2.)*T +F(9))*T
1  +F(8)*DLOG(T)+F(14))
  S298 = S
  ICP = 1

```

C

C

```

DO 40 J= 1,13
  T = T1(J)
  IF(T.GT.TRA(3))THEN
    CPL(J)=0.0
    GOTO 40
  ENDF
  TMID = TRA(2)
  IF(T.LE.TMID)THEN
    CPL(J)=CPT(7,T1(J),F)*1.987
  ELSE
    CPL(J)=CPT(0,T1(J),F)*1.987
  ENDF
40  CONTINUE

```

40

```

C
      IF(UNITS.EQ.'KJ')THEN
          HF298=HF298*4.184
          S298=S298*4.184
          DO 87665 IK1=1,13
87665      CPL(IK1)=CPL(IK1)*4.184
          ENDIF
      WRITE(3,165)CFLAG,INAME,XNAME,HF298,S298,(CPL(IJ),IJ=1,7),
1 (REF(I),I=1,2),REF3,(IE(I),NE(I),I =1,4),PHASE,NROT
C
165  FORMAT (A1,A4,A6,F8.2,1X,F8.2,2X,7(F7.2,1X),2A4,A6,
1 3X,4(A2,I3,1X),A1,1X,I1)
      IF(FORM.EQ.'LONG')WRITE(3,167)(CPL(IJ),IJ=8,13)
167  FORMAT(30X,6(F7.2,1X))
50  RETURN
END

```

APPENDIX V-C

FORTRAN SOURCE CODE FOR

THERMRXN

PROGRAM THERMRXN

\$LARGE

* WRITTEN BY: ED RITTER

*

* THERM REACTION INTERPRETER

*

* CALCULATES THERMODYNAMIC PROPERTY CHANGES FOR REACTION

IMPLICIT REAL*8(A-H,O-Z)

REAL*8 DELH,DELS,DELG,SHJ(10),SSJ(10),KEQ(20),DNUM

REAL*4 RNUM

INTEGER NE1(4,400),LX(10),RX(10),IHELP,ICNT,

+NLHS,NRHS,IERR,IND(70),JIND(70),RXFIL,FLG,NX(400)

integer inlp(132),inbl(132),INEQ(132)

DIMENSION ST1(20),STOT(20),HT1(20),HTOT(20),UTOT(20),T1(20),

+RH298(10),SH298(10),RS298(10),SS298(10),AFAR(20),GORT(20),SOR(20),

+COEF(10)

CHARACTER*4 IE1(4,400)

CHARACTER*14 RHS(10),LHS(10),SS(400),S(10),S3,OUTPUT

CHARACTER*70 S1,S2,NUL,NUL2,NUL1,FILIN,FLNAME,DUMMY,KS(25),

+CKFILE

CHARACTER*127 S132

CHARACTER PHSE(400)

CHARACTER*4 REF1(2,400),S4(10)

CHARACTER*6 REF2(400)

CHARACTER*14 UNITS,NUMIN

CHARACTER*2 ELEM(50)

LOGICAL EXST, EXST1,OPNED,OPNED2,EXST2

COMMON/CONFIG6/UNITS

COMMON/DELETE/NDEL,IDEL(500)

COMMON/RTEMP/ST1,HT1,T1,NT

COMMON/CONFIG1/ELEM

CALL CONFIG(ELEM,NFILES,KS,ISTAT,OUTPUT)

1023

RXFIL=0

ICHEMKIN=0

NCALL =0

ICNT=0

RC=1.987

RJ=8.31361

*

DEFINE DEFAULT VECTOR OF TEMPERATURES

T1(1)=298.15

T1(2)=300.

T1(3)=400.

T1(4)=500.

T1(5)=600.

T1(6)=800.

T1(7)=1000.

T1(8)=1200.

T1(9)=1500.

```

      T1(10)=2000.
      NT=10

C

      FLNAME=' '
      UNITS='KCAL'
      INQUIRE(FILE='THUNITS.TMP',EXIST=EXST1)
      IF(EXST1)THEN
          OPEN(13,FILE='THUNITS.TMP',STATUS='OLD')
          READ(13,14)UNITS
14          format(a14)
          CLOSE(13,STATUS='DELETE')

      ENDIF
      IHELP=1
      if(units.ne.'KJ')units='KCAL'
      CALL CLS
WRITE(*,*)'      Thermodynamic Property Analysis for Reactions'
      call lines(0,3)
      CALL NASAINIT(SS,NX,IE1,NE1,ICNT,FLNAME)
99      CALL CLS
          IF(ICNT.EQ.0)THEN
              OPEN(13,FILE='THUNITS.TMP',STATUS='UNKNOWN')
              WRITE(13,14)UNITS
              CLOSE(13,STATUS='KEEP')
              STOP 'NO INPUT FILE SPECIFIED'

          ENDIF
100      CONTINUE
          ICHEMKIN=0
          ICR=0
          call cls
          do 7790 i1=1,10
7790      coef(i1)=1.0
          ITR=0
      IF(IHELP.EQ.0)WRITE(*,*)' enter Reaction expression: { "?" for hel
+p }'
          IF(IHELP.EQ.1)THEN
              if(units.eq.'KCAL')then
                  write(*,*)' current units: Kcal/mol (cal/mol K)'
                  WRITE(*,*)' _____'
              else if(units.eq.'KJ')then
                  write(*,*)' current units: KJ/mol (J/mol K)'
                  WRITE(*,*)' _____'
              endif

          CALL LINES(0,1)
      write(*,*)'      To Calculate Property Change of Reaction for'
      write(*,*)'      enthalpy (del H), entropy (del S), and '
      write(*,*)'      gibbs free energy (del G) '
      WRITE(*,*)'      enter a Reaction expression as follows:'
      call lines(0,1)
      write(*,*)'      " A+B=C+D " or " A+B=C " or " A=B+C "'
      write(*,*)'      (ad'n/abstr) (ad'n/recomb) (dissoc)'
      write(*,*)'      where A, B, C, etc. are species defined '
      write(*,*)'      in the current Thermo D Base (*.DAT) file'

```

```

write(*,*)' EXAMPLE:   C6H5CL=CYC6H5+ CL (blanks are ignored)'
call lines(0,1)
write(*,*)'   NOTE:   Reaction expression MUST BALANCE'
write(*,*)'           no quote marks are needed'
call lines(0,1)
write(*,*)'   enter " L " to list defined species'
WRITE(*,*)'           " C " to process a "CHEMKIN" input file'
write(*,*)'           " Q " to return to the MAIN MENU'
WRITE(*,*)'           " ? " to supress this information'
      if(units.eq.'KJ')then
write(*,*)'           " U " change units to KJ/mol (J/mol K)'
      else if(units.eq.'KCAL')then
write(*,*)'           " U " change units to Kcal/mol (cal/mol K)'
      endif
write(*,*)'           or enter Reaction expression here:'
ENDIF
READ(*,3)S1
3  FORMAT(A70)
CALL READCHAR(S1)
CALL SLEN(S1,LEN)
CALL SUBSTIT(S1,CHAR(39),CHAR(32),LEN,1)
CALL SUBSTIT(S1,CHAR(34),CHAR(32),LEN,1)
CALL DBLNK(S1,LEN,0)
IF(S1.EQ.' '.OR.S1.EQ.'Q')THEN
      OPEN(13,FILE='THUNITS.TMP',STATUS='UNKNOWN')
      WRITE(13,14)UNITS
      CLOSE(13,STATUS='KEEP')
      CLOSE(41)
      STOP' '
ENDIF
IF(S1.EQ.'N')THEN
      CLOSE(54)
      GOTO 1023
ENDIF
if(S1.EQ.'?')THEN
      IF(IHELP.EQ.0)THEN
            IHELP=1
            GOTO 99
      ENDIF
      IF(IHELP.EQ.1)THEN
            IHELP=0
            GOTO 99
      ENDIF
ENDIF
IF(S1.EQ.'U')THEN
      IF(UNITS.EQ.'KJ')THEN
            UNITS='KCAL'
            CALL CLS
            GOTO 100
      ELSE IF(UNITS.EQ.'KCAL')THEN
            UNITS='KJ'
            CALL CLS
            GOTO 100
      ENDIF
ENDIF

```



```

        ENDIF
    IF(S1.EQ.'L')THEN
        CALL CLS
        iline=0
        DO 2093 I=1,ICNT,3
            iline=iline+1
            WRITE(*,'(3(5X,A10))')(SS(I+K-1),K=1,3)
            if(iline.ge.21)then
                iline=0
                write(*,*)' '
                pause '          { hit return to continue }'
            endif
2093      CONTINUE
            PAUSE 'hit return to continue!'
            GOTO 100
        ENDIF
    IF(S1.EQ.'C')THEN
        CALL CLS
        WRITE(*,*)' enter name of CHEMKIN format mechanism'
        read(*,'(A70)')CKFILE
        INQUIRE(FILE=CKFILE,EXIST=EXST2,OPENED=OPNED2)
        IF(OPNED2)THEN
            PAUSE ' error : file is opened! : hit return to continue!'
            goto 100
        ENDIF
        if(exst2)then
            open(87,file=ckfile,status='old')
123      read(87,'(a70)',end=1324)nul
            if(nul(:5).ne.'REACT')goto 123
            ichemkin=1
            goto 10999
1324      continue
            close(87)
            pause 'file error: "REACTIONS" not found: hit return to continue!'
            goto 100
10999     IF(RXFIL.EQ.0)THEN
            CALL CLS
            WRITE(*,*)' ENTER FILENAME FOR REACTION ANALYSIS OUTPUT'
            READ(*,3)NUL1
            IF(NUL1.EQ.' ' .OR. NUL1.EQ.'q' .OR. NUL1.EQ.'q')THEN
                IU=0
                GOTO 100
            ENDIF
            INQUIRE(FILE=NUL1,EXIST=EXST,OPENED=OPNED)
            RXFIL=1
            IF(EXST)THEN
                WRITE(*,4)NUL1
                WRITE(*,*)'ALREADY EXISTS'
                CALL LINES(0,1)
                WRITE(*,*)' 1 - OVERWRITE'
                WRITE(*,*)' 2 - APPEND'
                WRITE(*,*)' 3 - ABORT'
                CALL LINES(0,1)
                WRITE(*,*)' enter choice { 1 }'

```

```

READ(*,3)NUL2
CALL READCHAR(NUL2)
      IF(NUL2.EQ.' ' .OR. NUL2.EQ.'1')THEN
        OPEN(41,FILE=NUL1,STATUS='UNKNOWN')
      ELSEIF (NUL2.EQ.'2')THEN
        OPEN(41,FILE=NUL1,STATUS='OLD')
        IHJ=0
        CONTINUE
        IHJ=IHJ+1
        READ(41,3,END=14591)NUL2
        GOTO 23451
23451
14591          RXFIL=1
                BACKSPACE(41)
      ELSE
        IU=0
        GOTO 100
      ENDIF
    ELSE
      OPEN(41,FILE=NUL1,STATUS='UNKNOWN')
      ENDIF
      RXFIL=1
      GOTO 10000
    ENDIF
  else
    PAUSE ' file does not exist: hit return to continue'
    goto 100
  endif
  ENDIF
  ICR=0
10000 CONTINUE
*
*
*   PROCESS A CHEMKIN INPUT FILE
*
*
      IF(ICHEMKIN.EQ.1)THEN
        ICR=ICR+1

        READ(87,'(A)',END=10001)S132
        call readchar(s132)
        CALL DBLNK(S132,L132,1)
        IF(S132(:1).EQ.'/')GOTO 10000
        IF (S132(:3).EQ.'END')THEN
          CLOSE(87,STATUS='KEEP')
          CLOSE(41,STATUS='KEEP')
          RXFIL=0
          ICHEMKIN=0
          CALL CLS
          WRITE(*,*)' CHEMKIN input file processing completed'
          WRITE(*,*)ICR,' reactions processed'
          PAUSE ' { hit return to continue }'
          GOTO 100
        ENDIF
        CALL INDXST(S132,'(',NLP,INLP,L132,1,FLG)

```

```

CALL INDXST(S132,CHAR(32),NBL,INBL,L132,1,FLG)
S1=' '
IF(NLP.EQ.1)THEN
    S1(:INLP(1)-1)=S132(:INLP(1)-1)
ELSE
    S1(:INBL(NBL-2))=S132(:INBL(NBL-2))
ENDIF
CALL DBLNK(S1,LS1,0)
WRITE(*,*) ' processing reaction # ',ICR
WRITE(*,'(1X,A)')S1(:LS1)
CALL SUBSTIT(S1,'-', '=',LS1,1)
CALL INDXST(S1,'=',NEQ,INEQ,LS1,1,FLG)
IF(NEQ.NE.1)THEN
    CALL CLS
    WRITE(*,'(1X,A)')S1(:LS1)
    write(*,*) ' invalid reaction expression'
    WRITE(*,*)
    ' { hit return to continue or " Q " to quit }'
    read(*,'(a)')nul
    call readchar(nul)
    call dblnk(nul,lnul,0)
    if(nul.eq.'Q')then
        rxfil=0
        ichemkin=0
        close(41,status='keep')
        close(87,status='keep')
        goto 100
    else
        goto 10000
    endif
ENDIF
*
INITIALIZE STOICHIOMETRIC COEFFICIENT ARRAY
do 97790 i1=1,10
97790 coef(i1)=1.0
GOTO 10002
10001 CALL CLS
ICHEMKIN=0
RXFIL=0
CLOSE(41,STATUS='KEEP')
CLOSE(87,STATUS='KEEP')
WRITE(*,*) ' WARNING : " END " CARD MISSING'
WRITE(*,*) ' "END" CARD IS REQUIRED FOR CHEMKIN'
CALL LINES(0,2)
WRITE(*,*)ICR,' reactions processed'
PAUSE '{ hit return to continue }'
GOTO 100

ENDIF
*
-----
*
10002 IKTL=0
CALL DBLNK(S1,LEN,0)
CALL INDXST(S1,'-',NOCCUR,IND,LEN,1,FLG)
IF(NOCCUR.NE.0)THEN
    CALL CLS

```

```

        WRITE(*,4)S1
        WRITE(*,*)'   CONTAINS INVALID OPERATION "=" '
        WRITE(*,*)'   (hit return to continue)!'
        read(*,3)nul
        GOTO 99
    ENDIF
    CALL INDXST(S1,'=',NOCCUR,IND,LEN,1,FLG)
    IF(NOCCUR.NE.1)THEN
        CALL CLS
        WRITE(*,4)S1
4        FORMAT(1X,A)
        WRITE(*,*)'   CONTAINS INVALID NUMBER OF "=" '
        WRITE(*,*)'   (hit return to continue)!'
        read(*,3)nul
        GOTO 99
    ENDIF
    CALL INDXST(S1,'+',NOCR,JIND,LEN,1,FLG)
    NRHS=1
    NLHS=1
    DO 700 K=1,NOCR
        IF(JIND(K).LT.IND(1))NLHS=NLHS+1
        IF(JIND(K).GT.IND(1))NRHS=NRHS+1
700    CONTINUE
    IF(NLHS.GT.3)THEN
        WRITE(*,*)' TOO MANY REACTANTS : RE-ENTER REACTION!'
        WRITE(*,*)' (hit return to continue)!'
        READ(*,3)NUL
        GOTO 99
    ENDIF
    IF(NRHS.GT.3)THEN
        WRITE(*,*)' TOO MANY PRODUCTS : RE-ENTER REACTION!'
        WRITE(*,*)' (hit return to continue)!'
        READ(*,3)NUL
        GOTO 99
    ENDIF

C
C*****
C          FIND LEFT HAND SIDE (LHS) SPECIES
C*****
C
    IF(NLHS.EQ.1)LHS(1)=S1(:IND(1)-1)
    IF(NLHS.GE.2)THEN
        LHS(1)=S1(:JIND(1)-1)
        LHS(2)=S1(JIND(1)+1:IND(1)-1)
    ENDIF
    IF(NLHS.EQ.3)THEN
        LHS(2)=S1(JIND(1)+1:JIND(2)-1)
        LHS(3)=S1(JIND(2)+1:IND(1)-1)
    ENDIF
    IF(NLHS.GE.4)THEN
        LHS(3)=S1(JIND(2)+1:JIND(3)-1)
        LHS(4)=S1(JIND(3)+1:IND(1)-1)
    ENDIF

```

```

      IF(NLHS.EQ.5)THEN
        LHS(4)=S1(JIND(3)+1:JIND(4)-1)
        LHS(5)=S1(JIND(4)+1:IND(1)-1)
      ENDIF
C
C*****
C      FIND RIGHT HAND SPECIES (RHS)
C*****
C
      IF(NRHS.EQ.1)RHS(1)=S1(IND(1)+1:LEN)
      IF(NRHS.GE.2)THEN
        RHS(1)=S1(IND(1)+1:JIND(NLHS)-1)
        RHS(2)=S1(JIND(NLHS)+1:LEN)
      ENDIF
      IF(NRHS.EQ.3)THEN
        RHS(2)=S1(JIND(NLHS)+1:JIND(NLHS+1)-1)
        RHS(3)=S1(JIND(NLHS+1)+1:LEN)
      ENDIF
      IF(NRHS.GE.4)THEN
        RHS(3)=S1(JIND(NLHS+1)+1:JIND(NLHS+2)-1)
        RHS(4)=S1(JIND(NLHS+2)+1:LEN)
      ENDIF
      IF(NRHS.EQ.5)THEN
        RHS(4)=S1(JIND(NLHS+2)+1:JIND(NLHS+3)-1)
        RHS(5)=S1(JIND(NLHS+3)+1:LEN)
      ENDIF
C
C*****
C
***** DETERMINE COEFFICIENTS IF ANY *****
      DO 800 K=1,NLHS
        S(K)=' '
        S(K)=LHS(K)
        CALL INQNUM(S(K), IANS, NUMLEN, LSTR, 0)
        IF(IANS.EQ.1.OR.IANS.EQ.2)THEN
          NUMIN=' '
          NUMIN(:LSTR)=S(K)(:LSTR)
          CALL READNUM(NUMIN, RNUM, NUMM, IFLG)
          IF(IFLG.NE.0)THEN
            WRITE(*,*)NUMIN
            STOP 'ILLEGAL STRING'
          ENDIF
          COEF(K)=COEF(K)*RNUM
        ELSEIF(IANS.EQ.3.OR.IANS.EQ.4)THEN
          NUMIN=' '
          NUMIN(:NUMLEN)=S(K)(:NUMLEN)
          CALL READNUM(NUMIN, RNUM, NUMM, IFLG)
          IF(IFLG.NE.0)THEN
            STOP 'ILLEGAL STRING'
          ENDIF
          COEF(K)=COEF(K)*DBLE(RNUM)
          DUMMY=' '
          DUMMY(:LSTR)=S(K)(:LSTR)
          S(K)=' '

```

```

                LEN10=LSTR-NUMLN
                S(K)(:LEN10)=DUMMY(NUMLN+1:LSTR)
ENDIF
800 CONTINUE
DO 801 K=1,NRHS
S(K+NLHS)=' '
S(K+NLHS)=RHS(K)
CALL INQNUM(S(K+NLHS), IANS, NUMLEN, LSTR, 0)
IF(IANS.EQ.1.OR.IANS.EQ.2)THEN
    NUMIN=' '
    NUMIN(:LSTR)=S(K+NLHS)(:LSTR)
    CALL READNUM(NUMIN, RNUM, NUMM, IFLG)
    IF(IFLG.NE.0)THEN
        STOP 'ILLEGAL STRING'
    ENDIF
    COEF(K+NLHS)=COEF(K+NLHS)*DBLE(RNUM)
ELSEIF(IANS.EQ.3.OR.IANS.EQ.4)THEN
    NUMIN=' '
    NUMIN(:NUMLEN)=S(K+NLHS)(:NUMLEN)
    CALL READNUM(NUMIN, RNUM, NUMM, IFLG)
    IF(IFLG.NE.0)THEN
        STOP 'ILLEGAL STRING'
    ENDIF
    COEF(K+NLHS)=COEF(K+NLHS)*RNUM
    DUMMY=' '
    DUMMY(:LSTR)=S(K+NLHS)(:LSTR)
    S(K+NLHS)=' '
    LEN10=LSTR-NUMLN
    S(K+NLHS)(:LEN10)=DUMMY(NUMLN+1:LSTR)
ENDIF
801 CONTINUE
*****
***** REMOVE STRINGS WHICH APPEAR ON BOTH *****
***** SIDES OF THE EQUAL SIGN *****
DO 850 I1=1,NLHS
DO 851 I2=1,NRHS
IF(S(I1)(:10).EQ.S(I2+NLHS)(:10).AND.COEF(I1).EQ.COEF(I2+NLHS))
+THEN
    S(I1)=' '
    S(I2+NLHS)=' '
    LHS(I1)=' '
    RHS(I2)=' '
    COEF(I1)=0.0
    COEF(I2+NLHS)=0.0
ELSEIF(S(I1)(:10).EQ.S(I2+NLHS)(:10).AND.COEF(I1).NE.
+COEF(I2+NLHS))THEN
    DEL=COEF(I1)-COEF(I2+NLHS)
    IF(DEL.GT.0.0)THEN
        COEF(I1)=DEL
        S(I2+NLHS)=' '
        RHS(I2)=' '
        COEF(I2+NLHS)=0.0
    ELSE
        COEF(I2+NLHS)=-1.0*DEL

```

```

S(I1)=' '
LHS(I1)=' '
COEF(I1)=0.0
ENDIF
ENDIF
851 CONTINUE
850 CONTINUE
NSTR=NLHS+NRHS
NCOEF=NSTR
CALL DCREAL(COEF,NCOEF)
CALL CSTRING(S,NSTR)
CALL CSTRING(LHS,NLHS)
CALL CSTRING(RHS,NRHS)

*****
***** CHECK TO SEE IF ALL SPECIES IN THE REACTION ARE DEFINED *****
DO 701 K=1,NLHS
CALL DBLNK(S(K),LEN,0)
J=0
750 J=J+1
IF(J.GT.ICNT)THEN
WRITE(*,*)'SPECIES NOT FOUND: ',LHS(K)
WRITE(*,*)' {HIT RETURN TO CONTINUE}'
READ(*,3)NUL
GOTO 99
ENDIF
CALL DBLNK(SS(J),LEN2,0)
IF(S(K)(:10).EQ.SS(J)(:10))THEN
LX(K)=J
GOTO 701
ENDIF
GOTO 750
701 CONTINUE
DO 702 K=1,NRHS
CALL DBLNK(S(K+NLHS),LEN,0)
J=0
760 J=J+1
IF(J.GT.ICNT)THEN
WRITE(*,*)'SPECIES NOT FOUND: ',RHS(K)
WRITE(*,*)' {HIT RETURN TO CONTINUE}'
READ(*,3)NUL
GOTO 99
ENDIF
CALL DBLNK(SS(J),LEN2,0)
IF(S(K+NLHS)(:10).EQ.SS(J)(:10))THEN
RX(K)=J
GOTO 702
ENDIF
GOTO 760
702 CONTINUE
IERR=0
CALL MATBAL(NLHS,LX,NRHS,RX,IE1,NE1,COEF,IERR)
IF(IERR.EQ.1)THEN

```

```

WRITE(*,4)S1
WRITE(*,*)' HIT RETURN TO RE-ENTER EXPRESSION OR "Q" TO QUIT'
READ(*,3)NUL
CALL READCHAR(NUL)
      IF(NUL.EQ.' '.AND.ICHEMKIN.EQ.1)THEN
          GOTO 10000
      ELSEIF(NUL.EQ.'Q'.AND.ICHEMKIN.EQ.1)THEN
          CLOSE(87,STATUS='KEEP')
          CLOSE(41,STATUS='KEEP')
          RXFIL=0
          ICHEMKIN=0
          GOTO 100
      ELSEIF(NUL.EQ.'Q')THEN
          OPEN(13,FILE='THUNITS.TMP',STATUS='UNKNOWN')
          WRITE(13,14)UNITS
          CLOSE(13,STATUS='KEEP')
          STOP' '
      ENDIF
      GOTO 99
ENDIF
C
C*****
C CALCULATE PROPERTY CHANGE OF REACTION
C*****
C
8876 CONTINUE
      SMOLE=0.0
      RMOLE=0.0
      DO 7309 I1=1,NLHS
7309      SMOLE=SMOLE+COEF(I1)
      DO 7310 I1=1,NRHS
7310      RMOLE=RMOLE+COEF(I1+NLHS)
      DELTAN= RMOLE-SMOLE
      IF(ICHEMKIN.NE.1)THEN
          CALL CLS
      ENDIF
      DO 101 J=1,NT
      ST1(J)=0.
      STOT(J)=0.
      HT1(J)=0.
      HTOT(J)=0.
      UTOT(J)=0.
101 CONTINUE
* REMEMBER HT1(I1) = (Hf(T1(I1))*T1(I1))/(1000.*R)
      DO 904 J=1,NLHS
      CALL READNASA(S(J),NX(LX(J)),FLNAME,IFLG)
      IF(IFLG.NE.0)THEN
          WRITE(*,*)S(J),' NOT FOUND'
          WRITE(*,*)' IN NASA FORMAT FILE'
          PAUSE '{ hit return to continue }'
          goto 99
      ENDIF
* SAVING 1st TEMP'S PROPERTIES FOR ALL LHS SPECIES

```



```

SH298(J)=HT1(1)*COEF(J)
SS298(J)=ST1(1)*COEF(J)
DO 905 J1=1,NT
* REM SUBTRACT LEFT HAND SIDE FROM RIGHT ( PROD - REACT )
* REM : HTOT = H/RT
* UTOT = U/RT
* STOT = S/R
HTOT(J1)=HTOT(J1)-(COEF(J)*HT1(J1))
STOT(J1)=STOT(J1)-(COEF(J)*ST1(J1))
905 CONTINUE
904 CONTINUE

DO 902 J=1,NRHS
CALL READNASA(S(J+NLHS),NX(RX(J)),FLNAME,IFLG)
IF(IFLG.NE.0)THEN
WRITE(*,*)S(J+NLHS),' NOT FOUND'
WRITE(*,*)' IN NASA FORMAT FILE'
PAUSE '{ hit return to continue }'
goto 99
ENDIF

RH298(J)=HT1(1)*COEF(J+NLHS)
RS298(J)=ST1(1)*COEF(J+NLHS)

DO 903 J1=1,NT
HTOT(J1)=HTOT(J1)+(COEF(J+NLHS)*HT1(J1))
STOT(J1)=STOT(J1)+(COEF(J+NLHS)*ST1(J1))
903 CONTINUE
902 CONTINUE

* CONVERT DELTA H TO DELTA U : dU = dH - dn(RT)
DO 9905 J1=1,NT
9905 UTOT(J1)=HTOT(J1)-(DELTAN*T1(J1)/1000.0)
IF(ICHEMKIN.EQ.1)THEN
IU=41
ELSE
IU=0
ENDIF

***** OUTPUT TO TERMINAL : IU = 0 *****
***** OR FILE : IU =41 *****

5762 CONTINUE
IF(IU.EQ.0)THEN
CALL CLS
ELSE
CALL LINES(IU,2)
ENDIF
WRITE(IU,*)' THERMODYNAMIC ANALYSIS for REACTION'
IF(NLHS.EQ.1.AND.NRHS.EQ.1)WRITE(IU,620)LHS(1),RHS(1)
IF(NLHS.EQ.1.AND.NRHS.EQ.2)WRITE(IU,621)LHS(1),
+(RHS(12),I2=1,NRHS)
IF(NLHS.EQ.1.AND.NRHS.EQ.3)WRITE(IU,622)LHS(1),
+(RHS(12),I2=1,NRHS)
IF(NLHS.EQ.2.AND.NRHS.EQ.1)WRITE(IU,630)(LHS(I1),I1=1,NLHS),
+RHS(1)
IF(NLHS.EQ.2.AND.NRHS.EQ.2)WRITE(IU,631)(LHS(I1),I1=1,NLHS),
+(RHS(12),I2=1,NRHS)
IF(NLHS.EQ.2.AND.NRHS.EQ.3)WRITE(IU,632)(LHS(I1),I1=1,NLHS),

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```

+(RHS(I2), I2=1, NRHS)
      IF(NLHS.EQ.3.AND.NRHS.EQ.1)WRITE(IU,640)(LHS(I1), I1=1, NLHS),
+(RX(I2), I2=1, NRHS)
      IF(NLHS.EQ.3.AND.NRHS.EQ.2)WRITE(IU,641)(LHS(I1), I1=1, NLHS),
+(RHS(I2), I2=1, NRHS)
      IF(NLHS.EQ.3.AND.NRHS.EQ.3)WRITE(IU,642)(LHS(I1), I1=1, NLHS),
+(RHS(I2), I2=1, NRHS)
      IF(UNITS.EQ.'KCAL')THEN
WRITE(IU,654)(SH298(I1)*RC, I1=1, NLHS), (RH298(I2)*RC, I2=1, NRHS)
WRITE(IU,656)(SS298(I1)*RC, I1=1, NLHS), (RS298(I2)*RC, I2=1, NRHS)
      ELSE IF(UNITS.EQ.'KJ')THEN
          DO 1126 I1=1, NLHS
              SHJ(I1)=SH298(I1)*RJ
              SSJ(I1)=SS298(I1)*RJ
1126          CONTINUE
          DO 1127 I1=1, NRHS
              SHJ(NLHS+I1)=RH298(I1)*RJ
              SSJ(NLHS+I1)=RS298(I1)*RJ
1127          CONTINUE
WRITE(IU,6542)(SHJ(I1), I1=1, NLHS), (SHJ(I2), I2=NLHS+1, NLHS+NRHS)
WRITE(IU,6562)(SSJ(I1), I1=1, NLHS), (SSJ(I2), I2=NLHS+1, NLHS+NRHS)
      ENDIF
      DO 9977 I=1, NT
          SOR(I)=STOT(I)
          GORT(I)=(HTOT(I))-(STOT(I)*T1(I)/1000.0)
          AFAR(I)=EXP(STOT(I)-(DELTAN*LOG(EXP(1.0)*82.05*T1(I))))
9977          CONTINUE
      CALL LINES(IU, 1)
      IF(UNITS.EQ.'KCAL')THEN
          WRITE(IU,500)HTOT(1)*RC
          WRITE(IU,504)UTOT(1)*RC
          WRITE(IU,501)SOR(1)*RC
          WRITE(IU,502)GORT(1)*RC
      ELSE
          WRITE(IU,5001)HTOT(1)*RJ
          WRITE(IU,505)UTOT(1)*RJ
          WRITE(IU,5011)SOR(1)*RJ
          WRITE(IU,5021)GORT(1)*RJ
      ENDIF
      WRITE(IU,503)AFAR(1)
      CALL LINES(IU, 1)
      IF(UNITS.EQ.'KCAL')THEN
          WRITE(IU,67000)
      ELSE IF(UNITS.EQ.'KJ')THEN
          WRITE(IU,67800)
      ENDIF
      DO 29977 I=2, NT
          IF(UNITS.EQ.'KCAL')THEN
              WRITE(IU,67001)T1(I), HTOT(I)*RC, UTOT(I)*RC, SOR(I)*RC,
+AFAR(I), GORT(I)*RC
          ELSE IF (UNITS.EQ.'KJ')THEN
              WRITE(IU,67001)T1(I), HTOT(I)*RJ, UTOT(I)*RJ, SOR(I)*RJ,
+AFAR(I), GORT(I)*RJ
          ENDIF

```

```

29977      CONTINUE
          CALL LINES(0,1)
          IF(IU.NE.0.AND.ICHEMKIN.EQ.0)THEN
              IU=0
              GOTO 5762
          ELSEIF(ICHEMKIN.EQ.1)THEN
              GOTO 10000
          ENDIF
*****
***** OPTIONS HERE *****
          IF(RXFIL.EQ.0)THEN
              write(*,8208)
          else
              WRITE(*,8209)
          endif
          write(*,8300)
          READ(*,3)NUL
          CALL READCHAR(NUL)
          IF(NUL.EQ.' ')then
              call cls
              GOTO 100
          ELSEIF(NUL.EQ.'Q')THEN
              CLOSE(41)
              OPEN(13,FILE='THUNITS.TMP',STATUS='UNKNOWN')
              WRITE(13,14)UNITS
              CLOSE(13,STATUS='KEEP')
              STOP ' '
          ELSEIF(NUL.EQ.'U')THEN
              IF(UNITS.EQ.'KJ')THEN
                  UNITS='KCAL'
                  IU=0
                  GOTO 5762
              ELSE IF(UNITS.EQ.'KCAL')THEN
                  UNITS='KJ'
                  IU=0
                  GOTO 5762
              ENDIF
          ELSEIF(NUL.EQ.'N')THEN
              CLOSE(54)
              GOTO 1023
          ELSEIF(NUL.EQ.'*')THEN
              RXFIL=0
              CLOSE(41)
              NUL='F'
          ENDIF
          IF(NUL.EQ.'F'.AND.RXFIL.EQ.0)THEN
              CALL CLS
              WRITE(*,*)' ENTER FILENAME FOR REACTION ANALYSIS OUTPUT'
              READ(*,3)NUL1
              IF(NUL1.EQ.' '.OR.NUL1.EQ.'Q'.OR.NUL1.EQ.'q')THEN
                  IU=0
                  GOTO 5762
              ENDIF
              INQUIRE(FILE=NUL1,EXIST=EXST,OPENED=OPNED)
              RXFIL=1

```

```

IF(EXST)THEN
WRITE(*,4)NUL1
WRITE(*,*)'ALREADY EXISTS'
CALL LINES(0,1)
WRITE(*,*)' 1 - OVERWRITE'
WRITE(*,*)' 2 - APPEND'
WRITE(*,*)' 3 - ABORT'
CALL LINES(0,1)
WRITE(*,*)'      enter choice { 1 }'
READ(*,3)NUL2
CALL READCHAR(NUL2)
IF(NUL2.EQ.'1'.OR.NUL2.EQ.'1')THEN
OPEN(41,FILE=NUL1,STATUS='UNKNOWN')
ELSEIF (NUL2.EQ.'2')THEN
OPEN(41,FILE=NUL1,STATUS='OLD')
IHJ=0
12345 CONTINUE
IHJ=IHJ+1
READ(41,3,END=4591)NUL2
GOTO 12345
4591 RXFIL=1
BACKSPACE(41)
ELSE
IU=0
GOTO 5762
ENDIF
ELSE
OPEN(41,FILE=NUL1,STATUS='UNKNOWN')
ENDIF
ENDIF
IF(NUL.EQ.'F')THEN
IU=41
GOTO 5762
8877 CONTINUE
ENDIF
GOTO 5762
STOP
***** FORMAT BLOCK *****
620 FORMAT(1X,'Rx',1,6X,A10,1X,'=',1X,A10)
621 FORMAT(1X,'Rx',1,6X,A10,1X,'=',1X,A10,1X,'+',1X,A10)
622 FORMAT(1X,'Rx',1,6X,A10,1X,'=',1X,A10,2(1X,'+',1X,A10,1X))
630 FORMAT(1X,'Rx',1,6X,A10,1X,'+',1X,A10,1X,'=',1X,A10)
631 FORMAT(1X,'Rx',1,6X,A10,1X,'+',1X,A10,1X,'=',1X,A10,1X,'+',
+,1X,A10)
632 FORMAT(1X,'Rx',1,6X,A10,1X,'+',1X,A10,1X,'=',1X,A10,2(1X,'+',
+,1X,A10,1X))
640 FORMAT(1X,'Rx',1,6X,A10,2(1X,'+',1X,A10,1X),'=',1X,A10)
641 FORMAT(1X,'Rx',1,6X,A10,2(1X,'+',1X,A10,1X),'=',1X,A10,
+1X,'+',1X,A10)
642 FORMAT(1X,'Rx',1,6X,A10,2(1X,'+',1X,A10,1X),'=',1X,A10,
+2(1X,'+',1X,A10,1X))
654 FORMAT(1X,'Hf (Kcal/mol)',1X,6(F8.3,3X))

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```

656   FORMAT(1X,'S (cal/mol K)',1X,6(F8.3,3X))
6542  FORMAT(1X,'Hf (KJ/mol) ',1X,6(F8.3,3X))
6562  FORMAT(1X,'S (J/mol K) ',1X,6(F8.3,3X))
500   FORMAT(1X,' dHr (298K) = ',1X,F10.3,1X,' Kcal/mol')
5001  FORMAT(1X,' dHr (298K) = ',1X,F10.3,1X,' KJ/mol')
501   FORMAT(1X,' dSr ( " ) = ',1X,F10.3,1X,' cal/mol K')
5011  FORMAT(1X,' dSr ( " ) = ',1X,F10.3,1X,' J/mol K')
502   FORMAT(1X,' dGr ( " ) = ',1X,F10.3,1X,' Kcal/mol')
5021  FORMAT(1X,' dGr ( " ) = ',1X,F10.3,1X,' KJ/mol')
503   FORMAT(1X,' Af/Ar ( " ) = ',1X,1P,E10.3)
504   FORMAT(1X,'dU (dE) ( " ) = ',1X,F10.3,1X,' Kcal/mol')
505   FORMAT(1X,'dU (dE) ( " ) = ',1X,F10.3,1X,' KJ/mol')
8208  format(1x,'Q (quit)',3x,'F (file)',3x,'N (new input file)',3x,
+'U (change units)')
8209  format(1x,'Q (quit)',2x,'F (file)',2x,'N (new input file)',2x,
+'U (change units)',2x,'* (new output file)')
8300  format(1x,' enter option { enter new reaction }')
67000 FORMAT(6X,'T (K)',2X,'dH(Kcal/mol)',2x,'dU(Kcal/mol)',1X,
+'dS(cal/mol K)',3X,'(Af/Ar)',1X,'dG(Kcal/mol)')
67800 FORMAT(6X,'T (K)',3X,'dH(KJ/mol)',3x,'dU(KJ/mol)',3X,
+'dS(J/mol K)',4X,'(Af/Ar)',5X,'dG(KJ/mol)')
67001 FORMAT(1X,F10.3,5(3X,1P,E10.3))
*****
      END

```

```

SUBROUTINE NASAINIT(SS,NX,IE1,NE1,ICNT,THERMFIL)
  IMPLICIT REAL*8(A-H,O-Z)
  INTEGER IG, Y, NG, P, X, O, D,NE(4),NE1(4,400),FLG,IFIRST(7),
+ILAST(7),U,NX(400)
  REAL*8 TRA(3),F(14)
  LOGICAL EXST,OPNED
  CHARACTER*14 SS(400)
    CHARACTER*70 THERMFIL,s1
    CHARACTER*80 DUMMY
  CHARACTER*14 NUL,NUL1(2,50),funits
    CHARACTER*4 IE1(4,400),REF(2)
    CHARACTER*6 REF3
    CHARACTER PHASE
  * THIS SUBROUTINE INITIALIZES A NASA FORMAT DATABASE FILE (*.DAT)
  * AS A DIRECT ACCESS FILE FOR USE ELSEWHERE
  * RETURNS A VECTORS OF SPECIES NAMES AND LINE# IN FILE
  *     SS(400) : SPECIES NAMES (UP TO 400 SPECIES SUPPORTED)
  *     NX(400) : THE LINE NUMBER IN THE NASA FILE WHICH STARTS SS(I)
  *     ICNT   : TOTAL NUMBER OF ENTRIES IN NASA FILE
  *     THERMFIL: NASA FORMAT FILENAME

70     FORMAT(A70)
14     FORMAT(A14)
10000  WRITE(*,*)'   ENTER FILENAME FOR NASA FORMAT COEFFICIENTS
+ ( *.DAT )'
    CALL LINES(0,4)
    READ(*,70)THERMFIL
897    FORMAT(A14)
    CALL LRDCCHAR(THERMFIL)
    IF(THERMFIL.EQ.' '.OR.THERMFIL.EQ.'Q')RETURN
    IIH=0
956    IIH=IIH+1
    IF (THERMFIL(IIH:IIH).EQ.' '.OR.THERMFIL(IIH:IIH).EQ.' ')THEN
      LEN=IIH-1
      GOTO 987
    ENDIF
    GOTO 956
987    CONTINUE
    THERMFIL(LEN+1:LEN+4)='.DAT'
    INQUIRE(FILE=THERMFIL,EXIST=EXST,OPENED=OPNED)
    IF(EXST)GOTO 10002
    CALL CLS
    WRITE(*,7000)THERMFIL
7000  FORMAT(' ',5X,A70)
    WRITE(*,*)'           does not exist'
    CALL LINES(0,2)
    WRITE(*,7001)
7001  FORMAT(' ',20X,'please try again')
    goto 10000
10002  CONTINUE
    OPEN(54,FILE=THERMFIL,ACCESS='DIRECT',RECL=80,FORM='FORMATTED'
+,STATUS='OLD')

```

```

**      INITIALIZE NASA FORMAT FILE
*      FIRST SPECIES NAME APPEARS ON LINE 3 OF NASA FORMAT FILE
*      SUBSEQUENT NAMES APPEAR EVERY 4 th LINE : FILE IS TERMINATED
*      BY THE WORD "END"
*      SET INITIAL VALUES
      READ(54,'(A)',REC=1)DUMMY
      READ(54,'(A)',REC=2)DUMMY
      ICNT=0
      J=3
1      CONTINUE
      IF(ICNT.NE.0)J=J+4
      ICNT=ICNT+1
      SS(ICNT)=' '
      READ(54,1010,REC=J,END=99999)SS(ICNT),(REF(I),I=1,2),REF3,
+(IE1(I,ICNT),NE1(I,ICNT),I=1,4),PHASE,TRA(1),TRA(3),TRA(2)
      IF(SS(ICNT)(:3).NE.'END'.AND.SS(ICNT)(:3).NE.'end')THEN
      NX(ICNT)=J
          GOTO 1
      ELSE
          ICNT=ICNT-1
          RETURN
      ENDIF
1010  FORMAT(A10,2A4,A6,4(A2,I3),A1,2F10.3,1X,F8.0)
1020  FORMAT(5E15.8,/,5E15.8,/,4E15.8)
99999  ICNT=ICNT-1
      CALL CLS
      WRITE(*,*)' WARNING ! "END" card is missing'
      write(*,*)' the last line in a NASA format file'
      write(*,*)' MUST have END starting in column 1'
      call lines (0,1)
      write(*,*)' an end of file was encountered'
      pause ' hit return to continue'
      return
98989  call cls
      write(*,*)' I/O ERROR encountered'
      pause ' hit return to continue'
      CLOSE(54)
      return
      end

```

```

        SUBROUTINE READNASA(SPEC,IADD,FILIN,IFLG)
        IMPLICIT REAL*8(A-H,O-Z)
        DIMENSION TRA(3),F(14),ST1(20),HT1(20),T1(20)
        CHARACTER*10 NNAME
        CHARACTER*14 SPEC
        CHARACTER*1 PHASE
        CHARACTER*2 IE(4), BLK1
        CHARACTER*3 BLK2,NE(4)
        CHARACTER*4 IFLAG,INAME,ID(10),REF(2)
        CHARACTER*6 XNAME,REF3
        CHARACTER*14 UNITS
        CHARACTER*70 FILIN
        LOGICAL EXST,OPNED
        COMMON/RTEMP/ST1,HT1,T1,NT
        COMMON/CONFIG6/UNITS
110  DATA IFLAG,BLK1,BLK2/'END ',' ',' '/
        CONTINUE
        IFLG=0
102  FORMAT(A70)
3    FORMAT(A14)
        INQUIRE(FILE=FILIN,OPENED=OPNED,EXIST=EXST,ERR=101)
        IF(OPNED)GOTO 100
        IF(EXST)THEN
                WRITE(*,*)' FILE NOT OPENED ERROR'
                PAUSE' hit return to continue'
                IFLG=-10
                RETURN
        ENDIF
101  CALL CLS
        WRITE(*,*)'CANNOT FIND NASA FORMAT INPUT FILE'
        WRITE(*,*)FILIN
        WRITE(*,*)'ENTER FILESEC { Q = QUIT } '
        READ(*,102)FILIN
        CALL LRDCHAR(FILIN)
        IF(FILIN.EQ.'Q'.OR.FILIN.EQ.' ')THEN
                IFLG=2
                RETURN
        ENDIF
        GOTO 110
100  CONTINUE
        650  ICOUNT=1
        655  READ(54,1010,REC=IADD,END=999,ERR=909)SPEC,(REF(I),I=1,2),
        +REF3,(IE(I),NE(I),I=1,4),PHASE,TRA(1),TRA(3),TRA(2)
        IF(TRA(2).EQ.0.)TRA(2)=TRA(3)
        658  CONTINUE
        660  READ(54,1020,END=999) (F(I),I=1,14)
        CALL CHECK(F,TRA)
        ICOUNT=ICOUNT+1

```



```

70  FORMAT(A4)
1010 FORMAT(A10,2A4,A6,4(A2,A3),A1,2F10.3,1X,F8.0)
1020 FORMAT(5E15.8,/,5E15.8,/,4E15.8)
900  CONTINUE
      RETURN
999  CONTINUE
      IFLG=1
      RETURN
909  CONTINUE
      IFLG=-20
      CLOSE(54,STATUS='KEEP')
      RETURN
END
C
SUBROUTINE CHECK (F,TRA)
      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION TRA(3),F(14),ST1(20),HT1(20),T1(20)
      CHARACTER*1 PHASE
      CHARACTER*2 IE(4)
      CHARACTER*3 NE(4)
      CHARACTER*4 REF(2),INAME
      CHARACTER*6 REF3,XNAME
      CHARACTER*14 UNITS
      COMMON/RTEMP/ST1,HT1,T1,NT
      COMMON/CONFG6/UNITS
C
C-----FIRST COMPUTING HF298 AND S298 FROM THE INPUT PARAMETERS
C----  WANT TO COMPUTE H AND S AT 298 WITH THE LOW TEMP PARAMETERS
C
*  REMEMBER HF IS H/RT
      DO 40  J= 1,NT
          IF(T1(J).LE.TRA(2))THEN
              H=HF(7,T1(J),F)*T1(J)
              S=ST(7,T1(J),F)
          ELSE IF(T1(J).GT.TRA(2))THEN
              H=HF(0,T1(J),F)*T1(J)
              S=ST(0,T1(J),F)
          ENDIF
C  CONVERT H TO H/(1000.*R) FOR OUTPUT
          HT1(J)=H/1000.
          ST1(J)=S
40      CONTINUE
C
50  RETURN
END

```

APPENDIX V - D

FORTRAN SOURCE CODE FOR

THERMPRN

```

          PROGRAM THERMPRN
C
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION TRA(3),F(14),CPL(50)
      CHARACTER*1 PHASE
      CHARACTER*2 IE(4), BLK1
      CHARACTER*3 BLK2,NE(4)
      CHARACTER*4 IFLAG,INAME,ID(10),REF(2)
      CHARACTER*6 XNAME,REF3
          CHARACTER*70 FILIN,FILOUT,NUL1,SPEC,NUL2
          character*14 nul
          LOGICAL EXST1,EXST2
          COMMON/IPOLY/IPOLY,IUNIT,IHF
      DATA IFLAG,BLK1,BLK2/'END ',' ',' ' /
C *****
C      PROGRAMS JANAFST/THERINFO USES COEFFICIENTS IN THE EQUATION
C       $(CP)/R = C1+C2*T+C3*T**2+C4*T**3+C5*T**4$ 
C      BY THE METHOD OF LEAST SQUARES. THE ADDITIVE CONSTANT C6 IN
C       $H/RT = C1+C2/2*T+C3/3*T**2+C4/4*T**4+C6/T$  IS ALSO DETERMINED.
C      (HERE H IS THE TOTAL ENTHALPY -- DEFINED AS HF298+H(T)-H(298))
C      C7 IS DETERMINED BY  $S/R=C1LNT+C2*T+C3/2*T+C3/2*T**2+C4/3*T**3$ 
C       $+C5/4*T**4+C7$ 
C
C      THE INPUT IS TAKEN DIRECTLY FROM THE THERMO DATA USED FOR
C      CHEMKIN
C
C
C      NPTS= NUMBER OF TEMPERATURE POINTS FOR A GIVEN SET
C      INAME= NAME OF SPECIES (FIRST 4 LETTERS)
C      XNAME= NAME OF SPECIES (NEXT 6 LETTERS)
C      GMW= GRAM MOLECULAR WEIGHT OF SPECIES
C      HF298= HEAT OF FORMATION AT 298 K (KCAL/MOLE) (JANAF INPUT)
C      T (1) = TEMP IN DEGREE K
C      CP(I) = HEAT CAPACITY 9JANAF UNITS)
C      S(1)= ENTROPY (JANAF UNITS)
C      H(1)= H(T)-H(298) (JANAF UNITS)
C
C      FILE ASSIGNMENTS ARE
C          FILE 1 - INPUT DATA FITTED IN NASAFIT FORMAT FOR
C                  CHECKING 9SAME FORMAT AS USED FOR INTERPRETER)
C          FILE 3 - OUTPUT LISTING H AND S 298 K AND CP'S OVER TEMP
C                  RANGES
C
C*****
C
C
C      110          CONTINUE
C                  DO 111 I=1,30
C      111          WRITE(*,*)' '
C                  WRITE(*,*)'ENTER INPUT FILENAME (.DAT) '
C                  READ(*,70)FILIN

```

```

CALL FNAME(FILIN,'DAT')
INQUIRE(FILE=FILIN,EXIST=EXST1)
if(exst1)then
    OPEN(1,FILE=FILIN,STATUS='OLD')
    goto 120
endif
write(*,*)' cannot find input file:'
write(*,'(1X,A70)')filin
write(*,*)' hit return to continue or "Q" to abort'
read(*,3)nul
if(nul.eq.'q'.or.nul.eq.'Q')stop 2
goto 110

120 CONTINUE
CALL CLS
WRITE(*,*)' enter species name { Q to end }'
READ(*,'(A70)')SPEC
CALL DBLNK(SPEC,LENGTH,0)
if(spec.eq.' ')goto 120
IF(SPEC.EQ.'Q'.OR.SPEC.EQ.'Q')GOTO 900

CALL LINES(0,2)
WRITE(*,*)'ENTER "1" for both polynomials'
WRITE(*,*)'      "2" switch from low T to high T at Tmid'
write(*,*)' enter option: {2}'
READ(*,3)NUL
CALL READCHAR(NUL)
IF(NUMIN.EQ.'Q')GOTO 120
IPOLY=2
IF(NUL.NE.'2'.AND.NUL.NE.' ')IPOLY=1

CALL LINES (0,3)
WRITE(*,*)'ENTER "0" for { Kcal/mol }'
WRITE(*,*)'      "1" for { KJ/mol }'
write(*,*)' enter option: {0}'
READ(*,3)NUL
CALL READCHAR(NUL)
IF(NUL.EQ.'Q')GOTO 120
IUNIT=0
IF(NUL.NE.'0'.AND.NUL.NE.' ')IUNIT=1

CALL LINES (0,3)
WRITE(*,*)'ENTER "0" for Cp only'
WRITE(*,*)'      "1" for Cp, Hf, & S'
write(*,*)' enter option: {0}'
READ(*,3)NUL
CALL READCHAR(NUL)
IF(NUL.EQ.'Q')GOTO 120
IHF=0
IF(NUL.NE.'0'.AND.NUL.NE.' ')THEN
    WRITE(*,*)'ENTER "0" for Hf(T) & S(T)'
    write(*,*)'      "1" for (Hf(T)-Hf(298 K))'
    write(*,*)'          & (S(T)-S(298 K))'
    write(*,*)' enter option: {0}'

```

```

        READ(*,3)NUL
        CALL READCHAR(NUL)
        IF(NUL.EQ.'Q')GOTO 120
        IHF=1
        IF(NUL.NE.'0'.AND.NUL.NE.' ')THEN
            IHF=2
        ENDIF
    ENDIF
*   end options
3       FORMAT(A14)
70      FORMAT(A70)
130     CONTINUE

        REWIND(1)
131     read(1,'(A70)',end=140)nul1
        NUL1(10:70)=' '
        CALL DEBLNK(NUL1,NUL2,LNUL,0)
        IF(NUL1(:LNUL).EQ.SPEC(:LENGTH))THEN
            BACKSPACE(1)
            GOTO 655
        ELSE
            goto 131
        ENDIF
140     backspace(1)
        backspace(1)
        CALL CLS
        WRITE(*,*)SPEC
        WRITE(*,*)' SPECIES NOT FOUND'
        PAUSE 'HIT RETURN TO CONTINUE '
        GOTO 120

10     READ (1,71) INAME
12     READ (1,71) TNAME
C
C
C   ** READ DATA IN FROM FILES USED BY CHEMKIN, NOT JANAFIT.**
C       OR THERCOEF
C       GET ID FOR PRINTOUT
100    FORMAT(1X,'ENTER ID FOR THERMO FILE')
101    FORMAT(15A4)
650    ICOUNT=1
102    FORMAT (1H1,15A4)
119    FORMAT (1X,'SPECIES',4X,'HF(298)',1X,'S (298) ',1X,' CP300 ',
+ ' CP400 ', ' CP500 ', ' CP600 ', ' CP800 ', ' CP1000 ', 'CP1500 ',
3 8X,' DATE REF ',3X,' ELEMENTS ')
187    FORMAT (1X,28X,'CP2000 CP2500 CP3000 CP4000 CP5000 CP6000 ')
655    READ(1,1010,END=900) INAME, XNAME, (REF(I),I=1,2),REF3,
1 (IE(I),NE(I),I=1,4),PHASE,TRA(1),TRA(3),TMID
        IF (INAME.EQ.IFLAG) GOTO 900
        DO 658 J = 1,4
            IF (NE(J).EQ.0) IE(J) = BLK1
658    CONTINUE
C       TRA(1)=LOW TWMP  TRA(2)=MID-TEMP  TRA(3)=HIGH TEMP
660    READ(1,1020,END=900) (F(I),I=1,14)
C       F(8)-F(14) ARE LOW TEMP COEFFICIENTS

```

```

C      F(1)-F(7) ARE HIGH TEMP COEFFICIENTS
      CALL CHECK(INAME,XNAME,IE,NE,REF,REF3,PHASE,F,TMID)
      ICOUNT=ICOUNT+1
C      IF(ICOUNT.GE.55) GO TO 650
      GO TO 120
      71  FORMAT(A4)
1010  FORMAT(A4,A6,2A4,A6,4(A2,A3),A1,2F10.3,1X,F8.0)
1020  FORMAT(5E15.8,/,5E15.8,/,4E15.8)
      900  CONTINUE
          CLOSE(1,STATUS='KEEP')
          STOP
      END
C
C      SUBROUTINE CHECK
      SUBROUTINE CHECK (INAME,XNAME,IE,NE,REF,REF3,PHASE,F,TMID)
          IMPLICIT REAL *8 (A-H,O-Z)
          DIMENSION F(14)
          CHARACTER*1 PHASE
          CHARACTER*2 IE(4)
          CHARACTER*3 NE(4)
          CHARACTER*4 REF(2),INAME
          CHARACTER*6 REF3,XNAME
          CHARACTER*70 NUL
          COMMON/IPOLY/IPOLY,IUNIT,IHF
C
          IF(IUNIT.EQ.1)THEN
              CONST=4.184
          ELSE
              CONST=1.0
          ENDIF
          WRITE(*,'(1X,A4,A6)')INAME,XNAME
          WRITE(*,*)'ENTER FILENAME FOR TABLE OUTPUT ("PRN")'
          WRITE(*,*)' include file extension '
          READ(*,'(A70)')NUL
          OPEN (43,FILE=NUL,STATUS='UNKNOWN')
          WRITE(43,'(1X,A4,A6)')INAME,XNAME
          IF(IHF.GT.1)THEN
              T=298.15
              HZERO=HF(7,T,F)*1.987*CONST*T/1000.
              SZERO=ST(7,T,F)*1.987*CONST
          ELSE
              HZERO=0.0
              SZERO=0.0
          ENDIF
          *      1 DATA POINT AT 298.15
          *      20 DATA POINTS 300 - 2000 K
          *      9 MORE DATA POINTS 2000 - 6000 K EVERY 500 K
          IF(IPOLY.EQ.1.AND.IHF.EQ.1)THEN
              WRITE(43,*)'      T(K)      Cp(T)l      Cp(T)h      Hf(T)l      Hf(T)h
+      S(T)l      S(T)h'
              ELSEIF(IPOLY.NE.1.AND.IHF.EQ.1)THEN
              WRITE(43,*)'      T(K)      Cp(T)      Hf(T)      S(T)'
              ELSEIF(IPOLY.NE.1.AND.IHF.NE.1)THEN
              WRITE(43,*)'      T(K)      Cp(T)'

```

```

      ELSE
WRITE(43,*)'      T(K)      Cp(T)l      Cp(T)h'
      ENDIF
      DO 40 J= 1,29
      IF(J.EQ.1)THEN
          T=100.
      ELSEIF(J.EQ.2)THEN
          T=200.
      ELSEIF(J.EQ.3)THEN
          T=298.15
      ELSEIF(J.EQ.4)THEN
          T=300.
      ELSEIF(J.GT.4.AND.J.LE.21)THEN
          T=T+100.
      ELSE
          T=T+500.
      ENDIF
      CPTL=CPT(7,T,F)*1.987*CONST
      CPTH=CPT(0,T,F)*1.987*CONST
      HFOFTH=HF(0,T,F)*1.987*CONST*T/1000.
      SOFTH=ST(0,T,F)*1.987*CONST
      HFOFTL=HF(7,T,F)*1.987*CONST*T/1000.
      SOFTL=ST(7,T,F)*1.987*CONST
      IF(IPOLY.EQ.1)THEN
          IF(IHF.EQ.0)THEN
              WRITE(43,'(1X,3(2X,F12.3))')T,CPTL,CPTH
          ELSE
              WRITE(43,'(1X,7(1X,F10.1))')T,CPTL,CPTH,
+          HFOFTL-HZERO,HFOFTH-HZERO,SOFTL-SZERO,SOFTH-SZERO
          ENDIF
      ELSE
          IF(T.LE.TMID)THEN
              IF(IHF.EQ.0)THEN
                  WRITE(43,'(1X,2(2X,F12.3))')T,CPTL
              ELSE
                  WRITE(43,'(1X,4(2X,F12.3))')T,CPTL,
+          HFOFTL-HZERO,SOFTL-SZERO
              ENDIF
          ELSE
              IF(IHF.EQ.0)THEN
                  WRITE(43,'(1X,2(2X,F12.3))')T,CPTH
              ELSE
                  WRITE(43,'(1X,4(2X,F12.3))')T,CPTH,
+          HFOFTH-HZERO,SOFTH-SZERO
              ENDIF
          ENDIF
      ENDIF
40      CONTINUE
165  FORMAT ( 1X,A4,A6,F7.2,2X,F7.2,3X,7(F7.2,1X),2A4,A6,
1      3X,4(A2,A3,1X),A1)
167  FORMAT(30X,6(F7.2,1X))
50  CLOSE(43)
      RETURN
      END

```

APPENDIX V - E

FORTRAN SOURCE CODE FOR
THE THERM SUBROUTINE LIBRARY


```

SUBROUTINE DELCHK(K, ID)
COMMON/DELETE/NDEL, IDEL(500)
ID=0
DO 100 I=1, NDEL
    IF(K.EQ.IDEL(I))THEN
        ID=1
        RETURN
    ENDIF
100 CONTINUE
RETURN
END

```

```

SUBROUTINE LISTGR(AS, A, NGRPT, IFIRST, ILAST, IENTRY, IHELP, NE1, IE1)
C ***** LIST GROUPS CURRENTLY IN THE GROUP db *****
$LARGE
*****
*
* SUBROUTINE LISTGR : Written by : Ed Ritter *
*
* This subprogram lists the group database w/ on-line references. *
* It can also list a species database loaded from a "LST" file. *
*
* VARIABLES: *
* AS : vector of group id (names) which are identified when *
* estimating a species *
* A : matrix containing Hf, S, & Cp(300,400,500,600,800,1000,1500 K)*
* NGRPT: number of entries in AS & A. *
* IFIRST, ILAST : address of first and last entry from each group file*
* IENTRY: a flag which determines which program blocks are executed *
* NE1 matrix of element numbers (used only wfor species data. *
* IE1 matrix of elements for species use only *
*
*
*
*
*****
CHARACTER*14 AS(1), NUL, NUMIN, A1, A2, A3, CS
CHARACTER*70 NUMIN2, S2, KS(25), DUMMY, S1, GRDOC(400), GRDL2(100)
CHARACTER*4 IE1(4, 400)
CHARACTER*14 UNITS, NULS
INTEGER NFILES, I3(25), IND1(70), IND2(70), IND3(70), IGRL2(400)
COMMON/DELETE/NDEL, IDEL(500)
COMMON/GRFNM1/NFILES, I3
COMMON/GRFNM2/KS
COMMON/GROUPD/GRDOC, GRDL2
COMMON/GROUP1/IGRL2
REAL A(400,9), B0(9)
INTEGER IFIRST(1), ILAST(1), IEND, KK, FLG, IENTRY, NE1(4, 400), IND(70),
+IX(2)
COMMON/CONFIG6/UNITS

```

```

C   IENTRY= 8   FOR LISTING SPECIES DB
      IF(IENTRY.EQ.8)THEN
          IEND=NGRPT+1
          I1=1
          I2=3
          CALL CLS
          GOTO 600
      ENDIF
      IF((IENTRY.GT.0).AND.(IENTRY.LE.7))THEN
          IEND=ILAST(IENTRY)
          I1=IFIRST(IENTRY)
          I2=I1+2
          IF(IENTRY.NE.4) CALL CLS
          GOTO 600
      ENDIF
999   CALL CLS
      IF(IENTRY.NE.0)RETURN
      J1=0
      IFLAG=0
      NGR=NGRPT

```

```

C
C*****
C**          LIST GROUPS OPTIONS MENU   *****
C*****

      WRITE(*,1000)
1000  FORMAT(31X,'LIST GROUPS MENU')
*     WRITE(*,*)' '
      WRITE(*,1100)
1100  FORMAT(' ',20X,39(' '))
      WRITE(*,*)' '
      DO 981 I1J=1,NFILES
          IF(I3(I1J).EQ.0)GOTO 981
          CALL SLEN(KS(I3(I1J)),LEN1)
          CALL INDXST(KS(I3(I1J)),'\',NOC1,IND1,LEN1,1,KFLG)
          CALL INDXST(KS(I3(I1J)),'.',NOC2,IND2,LEN1,1,KFLG)
          IF(NOC1.EQ.0.AND.NOC2.EQ.0)THEN
              WRITE(*,*)I1J,KS(I3(I1J))(:LEN1)
              GOTO 981
          ENDIF
          IF(NOC1.NE.0)THEN
              IBEGIN=IND1(NOC1)+1
          ELSEIF(NOC1.EQ.0)THEN
              IBEGIN=1
          ENDIF
          IF(NOC2.EQ.0)THEN
              IEND=LEN1
          ELSE IF(NOC2.NE.0)THEN
              IEND=IND2(NOC2)-1
          ENDIF
          IF(IBEGIN.GE.IEND)GOTO 981
          IF(I1J.GT.15)GOTO 981
          WRITE(*,1200)I1J,KS(I3(I1J))(IBEGIN:IEND)

```

```

981      CONTINUE
1200    FORMAT(' ',18X,I3,' - ',A14)
        WRITE(*,1700)
1700    FORMAT(' ',20X,'A - All Groups in DataBase')
        write(*,1800)
1800    FORMAT(' ',20X,'Q - QUIT { return to previous menu}')
1850    WRITE(*,*)' '
        WRITE(*,*)'          enter option : { Q }'
        read(*,1900) NUMIN
1900    FORMAT(A14)
        CALL READCHAR(NUMIN)
        IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))RETURN
        IF(NUMIN(:1).EQ.'A') THEN
            I1=1
            I2=2+I1
            IEND=NGRPT+1
            CALL CLS
            GOTO 600
        ENDIF

        CALL READNUM(NUMIN,RNUM,KK,FLG)
        IF(FLG.EQ.1)GOTO 999
        I1=IFIRST(KK)
        I2=2+I1
        IEND=ILAST(KK)
        CALL CLS
600     CONTINUE
        if(i1.le.0)i1=1
        I1S=I1
        IF(IENTRY.EQ.4)THEN
            WRITE(*,*)' THE FOLLOWING BOND INCREMENT GROUPS ARE DEFINED:'
            CALL LINES(0,1)
            ENDIF
        IF(IENTRY.EQ.8)THEN
            WRITE(*,691)
691     FORMAT(1X,3('SP#', ' SPECIES ID   ',3X))
            WRITE(*,*)' '
            WRITE(*,606)
            WRITE(*,*)' '
            GOTO 602
        ENDIF
        WRITE(*,601)
        WRITE(*,606)
        WRITE(*,*)' '
606     FORMAT(1X,76(' '))
601     FORMAT(1X,3('GR#', ' GROUP ID   ',5X))
602     ILINE=1
599     CONTINUE
        A1=AS(I1)
        A2=AS(I1+1)
        A3=AS(I1+2)
*     IF IEND.EQ.INGRPT+1 THEN LIST ALL GROUPS HAS BEEN SELECTED
        IF((IENTRY.NE.8.AND.IENTRY.NE.4).AND.IEND.NE.INGRPT+1)THEN
            IF(I1.GT.ILAST(KK))A1=' '

```

```

                IF(I1+1.GT.ILAST(KK))A2=' '
                IF(I1+2.GT.ILAST(KK))A3=' '
ELSE IF(IENTRY.EQ.4)THEN
                IF(I1.GT.IEND)A1=' '
                IF(I1+1.GT.IEND)A2=' '
                IF(I1+2.GT.IEND)A3=' '
ELSE IF(IENTRY.EQ.8)THEN
                DO 2134 LW=1,NDEL
                IF(IDEL(LW).EQ.I1)A1=' '
                IF(IDEL(LW).EQ.I1+1)A2=' '
                IF(IDEL(LW).EQ.I1+2)A3=' '
2134          CONTINUE
                ENDIF
                WRITE(*,69)I1,A1,(I1+1),A2,(I1+2),A3
69          FORMAT(1X,3(I3,2X,'-',2X,A14,4X))
                ILINE=ILINE+1
                I1=I1+3
                I2=I1+2
                IF(I2.GT.IEND)I2=IEND
                IF((ILINE.GT.19).OR.(I1.GT.IEND))THEN
                IF(IENTRY.EQ.4)RETURN
                WRITE(*,*)'HIT RETURN TO CONTINUE { "?" FOR HELP }'
                READ(*,3)NUL
                3          FORMAT(A14)
                4          FORMAT(A70)
                CALL READCHAR(NUL)
                        nuls=nul
                IF (NUL(:1).EQ.'Q')GOTO 999
3543          IF(NUL(:1).EQ.'?')THEN
                CALL CLS
                WRITE(*,*)'      LIST DATABASE OPTIONS'
                WRITE(*,*)'      _____'
                CALL LINES(0,1)
                WRITE(*,*)'  Q - QUIT return to previous menu'
                WRITE(*,*)'  RETURN - TO CONTINUE'
                write(*,*)'  R - REPEAT listing (from beginning)'
                write(*,*)'  E - EXTENDED listing (Hf S Cp)'
                IF(IENTRY.NE.8)THEN
                write(*,*)'  REF- EXTENDED listing with references'
                else if(IENTRY.eq.8)then
                write(*,*)'  A - extended listing as above with'
                write(*,*)'      ATOMIC composition included'
                WRITE(*,*)'  D - Delete a species (by species number)'
                WRITE(*,*)'  U - Undelete a species'
                endif
                call lines(0,1)
                if(nul(:2).ne.'??')write(*,*)'      enter option {continue}'
                if(nul(:2).eq.'??')then
                call lines(0,2)
                Write(*,*)' you will be prompted for a range.'
                if(ientry.ne.8)then
                write(*,*)' use group numbers separated by a '
                endif
                if(ientry.eq.8)then

```

```

        write(*,*) ' use species numbers separated by a '
endif
write(*,*) ' comma OR blank.'
write(*,*) ' example:      '
write(*,*) ' 38 70 OR 38,70 (INTEGERS ONLY)'
write(*,*) ' '
write(*,*) ' will all generate extended listing for '
if(ientry.ne.8)write(*,*) ' groups 38 through 70'
if(ientry.eq.8)write(*,*) ' species 38 through 70'
write(*,*) '      {hit return to continue}'
write(*,*) '      or enter otion:'
endif
read(*,3)nul
      IF(NUL(:3).EQ.'ref')NUL='REF'
      NULS=NUL
      CALL READCHAR(NUL)
      IF (NUL(:1).EQ.'Q')GOTO 999

ENDIF
if(nul.eq.'R')then
if(ientry.ne.8)then
      I1=IFIRST(IENTRY)
      IF(IENTRY.EQ.0)THEN I1=1
      I2=I1+2
      CALL CLS
      GOTO 600

ENDIF
IF(IENTRY.EQ.8)THEN
      I1=1
      I2=3
      CALL CLS
      GOTO 600

ENDIF
endif
IF(NUL(:1).EQ.'D'.AND.IENTRY.EQ.8)THEN
5234 WRITE(*,*)'DELETE which species { 0 to abort }'
      WRITE(*,*) ' or enter species number to delete)'
      read(*,*,err=99999)idelete
      if(idelete.EQ.0)goto 573
      ndel=ndel+1
      idel(ndel)=idelete
      write(*,*)'species # ',idelete
      write(*,*)'has been deleted'
      CALL LINES(0,2)
      WRITE(*,*)' hit return to continue {Q : quit}'
      READ(*,3)A1
      call readchar(A1)
      if(A1(:1).eq.'Q')then
      I1=I1S
      GOTO 600
      endif
      goto 5234

endif
573 continue

```

```

IF(NUL(:1).EQ.'U'.AND.IENTRY.EQ.8)THEN
  CALL CLS
  DO 765 IB=1,NDEL
765     WRITE(*,766)IDEL(IB),AS(IDEL(IB))
766     FORMAT(1X,I3,1X,'-',1X,A14)
  CALL LINES(0,1)
  WRITE(*,*)' undelete which species ( 0 to abort )'
  write(*,*)'   or enter species number to undelete'
  read(*,*,err=99999)idelete
  if(idelete.eq.0)goto 767
  do 769 ib=1,ndel
    if(idel(ib).ne.idelete)goto 769
    do 770 ib1=ib,ndel-1
770     IDEL(ib1)=idel(ib1+1)
    ndel=ndel-1

769  continue
  WRITE(*,*)' hit return to continue { Q : quit }'
  read(*,3)a1
  call readchar(a1)
  if(a1.eq.'Q')then
    I1=I1S
    GOTO 600
  endif
  GOTO 573
endif
767  continue
      IF(NUL(:3).EQ.'ref')NUL(:3)='REF'
  if(nul(:1).eq.'E'.or.(nul(:1).eq.'A'.and.ientry.eq.8)
+.or.(nul(:3).eq.'REF'.and.ientry.ne.8))then

  IF(IENTRY.NE.8)WRITE(*,*)' ENTER RANGE OF GROUPS TO VIEW'
  IF(IENTRY.EQ.8)WRITE(*,*)' ENTER RANGE OF SPECIES TO VIEW'
  READ(*,4)S2
  CALL LRDCHAR(S2)
  IF(S2.EQ.' ' .OR.S2.EQ.'Q')THEN
    NUL='R'
    GOTO 3543

  ENDIF
  DO 1776 INXS=1,70
1776  IF(S2(INXS:INXS).EQ.' ')S2(INXS:INXS)=' '
  CALL DEBLNK(S2,NUMIN2,LEN,1)
  CALL INDXST(S2,' ',NOCCUR,IND,LEN,1,FLG)
  KT=0
  DO 1777 INXS=1,LEN
    IF((ICHAR(S2(INXS:INXS)).GT.57.OR.ICHAR(S2(INXS:INXS))
+.    .LT.48).AND.ICHAR(S2(INXS:INXS)).NE.32)KT=1
1777  CONTINUE
  IF(KT.EQ.1)THEN
    CS=' '
    IF(NOCCUR.EQ.0)THEN
      CS(:LEN)=S2(:LEN)
      CS(LEN+1:10)=' '
      IK=1

```

```

1812          IF(CS(:10).EQ.AS(IK)(:10))GOTO 1813
              IK=IK+1
              IF(IK.LE.NGRPT)GOTO 1812
              WRITE(*,*)'ENTRY NOT FOUND'
              WRITE(*,*)CS(:10)
                  WRITE(*,*)' { hit return to continue }'
                  read(*,4)numin2
                  nul='R'
                  goto 3543
1813          CONTINUE
              IBEGIN=IK
              ISTOP=IK
              ELSE IF(NOCCUR.EQ.1)THEN
                  CS(:IND(1)-1)=S2(:IND(1)-1)
                  CS(IND(1):10)= ' '
                  IK=1
1912          IF(CS(:10).EQ.AS(IK)(:10))GOTO 1913
              IK=IK+1
              IF(IK.LE.NGRPT)GOTO 1912
              WRITE(*,*)'ENTRY NOT FOUND'
              WRITE(*,*)CS(:10)
                  WRITE(*,*)' { hit return to continue }'
                  read(*,4)numin2
                  nul='R'
                  goto 3543
1913          CONTINUE
              IBEGIN=IK
              CS(:LEN-IND(1))=S2(IND(1)+1:LEN)
              CS(LEN-IND(1)+1:10)= ' '
              IK=1
2012          IF(CS(:10).EQ.AS(IK)(:10))GOTO 2013
              IK=IK+1
              IF(IK.LE.NGRPT)GOTO 2012
              WRITE(*,*)'ENTRY NOT FOUND'
              WRITE(*,*)CS(:10)
                  WRITE(*,*)' { hit return to continue }'
                  read(*,4)numin2
                  nul='R'
                  goto 3543
2013          CONTINUE
              ISTOP=IK
              ELSE IF(NOCCUR.GT.1)THEN
                  WRITE(*,*)'ERROR IN INPUT:'
                  WRITE(*,*)S2
                  WRITE(*,*)' { hit return to continue }'
                  read(*,4)S2
                  NUL='R'
                  GOTO 3543
              ENDIF
          ENDIF
      IF(KT.EQ.0)THEN
          IF(NOCCUR.EQ.0)THEN
              NUMIN=S2(:LEN)
              NUL=NUMIN

```

```

ELSE IF(NOCCUR.EQ.1)THEN
    NUMIN=S2(:IND(1)-1)
    NUL=S2(IND(1)+1:LEN)
ELSE IF(NOCCUR.GT.1)THEN
    WRITE(*,*)'ERROR IN INPUT:'
    WRITE(*,*)S2
    WRITE(*,*)' ( hit return to continue )'
    read(*,4)S2
    NUL='R'
    GOTO 3543
ENDIF
CALL READNUM(NUMIN,RNUM,IBEGIN,FLG)
CALL READNUM(NUL,RNUM,ISTOP,FLG)
ENDIF
IF(KFLG.EQ.1)THEN
    NUL='?'
    GOTO 3543
ENDIF
K22=IBEGIN
CALL CLS
7999 INL=0
    if(units.eq.'KCAL')then
        write(*,*)' Hf { Kcal/mol } S & Cp { cal/mol K }'
    else if(units.eq.'KJ')then
        WRITE(*,*)'UNITS: Hf{KJ/mol} S & Cp {J/mol K}'
    endif
    IF(IENTRY.NE.8)THEN
        WRITE(*,*) 'GROUP ID Hf S Cp 300 400 500'
+ 600 800 1000'
    ELSE IF(IENTRY.EQ.8)THEN
        WRITE(*,*) 'SPECIES Hf S Cp 300 400 500'
+ 600 800 1000'
    ENDIF
8000 INL=INL+1
    IF(IENTRY.EQ.8)THEN
        DO 83575 K5=1,NDEL
            if(IDEL(K5).EQ.K22)THEN
                K22=K22+1
                GOTO 8000
            endif
83575 continue
        endif
            if(units.eq.'KJ')then
                do 7672 ik1=1,8
7672 bo(ik1)=a(k22,ik1)*4.184
                    write(*,7100)as(k22),(bo(ik1),ik1=1,8)
7100 format(1x,a14,1x,8(f7.2,1x))
                else if(units.eq.'KCAL')then
                    WRITE(*,7000)AS(K22),(A(K22,I22),I22=1,8)
7000 FORMAT(' ',A14,1X,8(1X,F7.2))
                endif
            if((nuls.eq.'REF'.and.grdoc(k22).ne.' ').and.ientry.ne.8)THEN
                write(*,8743)GRDOC(K22)
8743 FORMAT(1X,A70)

```



```

                                INL=INL+1
                                IF(IGRL2(K22).NE.0)THEN
                                    WRITE(*,8743)GRDL2(IGRL2(K22))
                                    INL=INL+1
                                ENDIF
                                ENDIF
                                IF(NULS.EQ.'A'.AND.IENTRY.EQ.8)WRITE(*,7001)(IE1(I22,K22),
+NE1(I22,K22),I22=1,4)
7001  FORMAT(1X,4(7X,A4,2X,I3))
                                IF(NULS.EQ.'A'.AND.IENTRY.EQ.8)INL=INL+1
                                K22=K22+1
                                IF(INL.GE.19.OR.K22.GT.ISTOP)THEN
                                    WRITE(*,*)' { HIT RETURN TO CONTINUE }'
                                    READ(*,3)NUMIN
                                    CALL READCHAR(NUMIN)
                                    IF(NUMIN(:1).EQ.'Q')THEN
                                        NUL='??'
                                        GOTO 3543
                                    ENDIF
                                    IF(K22.LE.ISTOP)GOTO 7999
                                NUL='??'
                                GOTO 3543
                                ENDIF
                                GOTO 8000
                                endif
                                IF(I1.GE.IEND)GOTO 999
                                CALL CLS
                                GOTO 600
                                ENDIF
                                GOTO 599
200  CONTINUE
100  CONTINUE
99   RETURN
99999 call cls
write(*,*)' ERROR:  INTEGER VALUE(S) EXPECTED'
call lines(0,2)
WRITE(*,*)' check required input and try again'
call lines(0,1)
write(*,*)' { hit return to continue }'
read(*,3)nul
call readchar(nul)
if(nul(:1).eq.'Q')return
nul='??'
goto 3543
END

```

```

SUBROUTINE FILE(LS,RS,B,CP2K,REF,REF3,IE,NE,CS,IX,MM1,E,FLAG,BFLAG
+,TEXT,BLFLAG,FORM,FORMP,SPECP,RS22,CPINF,SYMR,SYMS,SYMM,BD,TS,FIL,
+N,KOUNT,LENF,LENFP,DELB,DOCTYPE,KDOCT,DELTA,IOP)

```

```
C$LARGE
```

```
C
```

```
C*****
```

```
C
```

```
C ----- THIS SUBROUTINE PRODUCES BOTH *.LST & *.DOC FILES -----
```

```
C
```

```
* UD 10/23/88
```

```
C*****
```

```
c +7 column 72 ]
```

```

INTEGER IX(1), E(1), N, NGRPT, Q,EI,FIL,HEADER,KDOCT
INTEGER FLAG, BFLAG, SYMM,SYMS, SYMR, CTRL, Z, NGRP, NATOM
INTEGER IG, Y, NG, P, X, O, D,NE(1),FLG,TFS,TFS2
INTEGER*2 IYR,IMON,IDAY
REAL SCOR, CPINF, CP2K,DELTA(1)
REAL*4 B(2,9),BO(9)
CHARACTER*20 S5
CHARACTER*70 TEXT(1),KS,FS,FS2,NASAFI,NASAFO,F1,dum1,s3,S4
CHARACTER*72 IDLINE
CHARACTER*14 NUMIN,TSS,SPECP,DUMMY,DOCTYPE,COMMAND,OUTPUT,UNITS,
+CS(2,60), LS, RS,CP, TS, DS, RS22,FOUNITS,FIUNITS,NUM2,TRANGE
CHARACTER ES, ANSS,PHASE
CHARACTER*70 FORM,FORMP
CHARACTER*4 IE(1),REF(2)
CHARACTER*6 REF3
CHARACTER*1 CFLAG
COMMON/NASANM/NASAFI,NASAFO
COMMON/CTRL2/COMMAND,OUTPUT
COMMON/CONFG6/UNITS
COMMON/CONFG8/TRANGE
COMMON/UNITSET/FOUNITS,FIUNITS
COMMON/FILEFLG/NCALL
COMMON/DATE/IMON,IDAY,IYR
COMMON/NROTOR/NROT,NROTS
LOGICAL EXST,OPNED,OPNED2
SAVE FS2,FS

TFS=1
TFS2=1
HEADER=0
IF(TRANGE(:4).EQ.'2000')THEN
CFLAG='*'
ELSE
CFLAG=' '
ENDIF
IF(NCALL.EQ.0)GOTO 1494
INQUIRE(34,OPENED=OPNED2)
IF(OPNED2)THEN
INQUIRE(34,NAME=F1)
IF(F1.EQ.FS2)CLOSE(34,STATUS='KEEP')
ENDIF
INQUIRE(52,OPENED=OPNED)

```

```

                IF(OPNED)THEN
                    IF(OUTPUT.EQ.'CLOSE')REWIND(52)
                    GOTO 1944
                ENDIF
                IB=1
                OPEN(52,FILE=FS2,ACCESS='DIRECT',RECL=70,FORM='FORMATTED',
+STATUS='OLD')
1944                READ(52,'(A70)',END=1945)DUMMY
                    IB=IB+1
                    GOTO 1944
1945                BACKSPACE(52)
                    NREC=IB
1956                CONTINUE
                    INQUIRE(7,OPENED=OPNED)
                IF (OPNED.AND.(FIL .EQ. 1.OR.FIL.EQ.2)) GOTO 8990
1494                CALL CLS
                    NCALL=1
                    WRITE(*,*) 'Enter output filename:'
                    WRITE(*,*) '( no file extension is needed ): '
                    READ(*,4) KS
                    CALL LRDCHAR(KS)
                    IF(KS(:1).EQ.'Q'.OR.KS(:1).EQ.' ')THEN
                        FIL=-10
                        RETURN
                    ENDIF
                    JJK=1
                    IF(FIL.EQ.2)GOTO 1995
                    WRITE(*,*) '
                    WRITE(*,*)'   CREATE DOCUMENT FILE [ Y or N ] '
                    WRITE(*,*) '
                    WRITE(*,*)'   enter choice: ( Y )'
                    READ(*,3)NUMIN
3                FORMAT(A14)
                    CALL READCHAR(NUMIN)
                    IF(NUMIN(:1).EQ.' ')THEN
                        FIL=0
                        GOTO 1995
                    ENDIF
                    IF(NUMIN(:1).EQ.'Q')RETURN
                    IF(NUMIN(:1).EQ.'N')FIL=2
1995                IF((KS(JJK:JJK).EQ.' ').OR.(KS(JJK:JJK).EQ.' '))THEN
                    ILNG=JJK
C                THEN THIS IS POSITION OF ' . '
C                WHICH IS FOLLOWED BY APPROPRIATE FILE EXTENSION ".*"
                    GOTO 1996
                ENDIF

                JJK=JJK+1
                GOTO 1995
1996                CONTINUE
                    ILNG2=ILNG+4
                    IF(TFS.EQ.1)THEN
                        FS=KS
                            NASAFO=KS

```

```

        FS(ILNG:ILNG2)='.LST'
        NASAFI=FS
        NASAFO(ILNG:ILNG2)='.DAT'
    ENDIF
    IF(TFS2.EQ.1)THEN
        FS2=KS
        FS2(ILNG:ILNG2)='.DOC'
        IF(TFS.EQ.0)GOTO 1495
    ENDIF
    IF(TFS.EQ.0)GOTO 1495
    INQUIRE(FILE=FS,EXIST=EXST,OPENED=OPNED,ERR=1234)
    IF(OPNED)GOTO 1495
    IF(EXST)THEN
        CALL CLS
        WRITE(*,32)FS
32    FORMAT(' ',A14,2X,' ALREADY EXISTS')
        CALL LINES(0,3)
        WRITE(*,*)' 1 - DELETE (OVERWRITE)'
        WRITE(*,*)' 2 - APPEND (ADD DATA TO END)'
        WRITE(*,*)' 3 - ENTER DIFFERENT FILENAME'
        WRITE(*,*)' Q - CANCEL (RETURN TO PREVIOUS MENU)'
        CALL LINES(0,2)
        WRITE(*,*)' enter option: {Q}'
        READ(*,3)NUMIN
        CALL READCHAR(NUMIN)
        IF(NUMIN.EQ.'Q'.OR.NUMIN.EQ.' ')THEN
            FIL=0
            RETURN
        ENDIF
        IF(NUMIN.EQ.'1'.OR.NUMIN(:1).EQ.'D')THEN
            CALL CLS
            WRITE(*,*)' choose output units for LST file'
            write(*,*)' 1- Kcal/mol (cal/mol K)  2- KJ/mol (J/mol K
+)')
            write(*,*)' enter option ( 1 )'
            read(*,3)num2
            founits='KCAL'
            if(num2(:1).eq.'2')founits='KJ'
            OPEN(7, FILE=FS,STATUS='UNKNOWN')
            if(founits.eq.'KJ')then
                write(7,*)' UNITS:KJ'
            else if(founits.eq.'KCAL')then
                write(7,*)' UNITS:KCAL'
            endif
            TFS=0
        ENDIF
        IF(NUMIN.EQ.'2'.OR.NUMIN(:1).EQ.'A')THEN
            OPEN(7,FILE=FS,STATUS='OLD')
            read(7,70,end=1695)dum1
            format(a70)
            call lrdchar(dum1)
            call deblnk(dum1,s3,len1,0)
            founits='KCAL'
            if(dum1(:8).eq.'UNITS:KJ')founits='KJ'
70

```

```

1493          READ(7,3,END=1695)DUMMY
              TFS=0
              HEADER=1
              GOTO 1493
1695          CONTINUE
              BACKSPACE (7)
C    NO BACKSPACE ON VAX
              IF(FIL.EQ.2)GOTO 1496
              GOTO 1495
          ENDIF
          IF(NUMIN.EQ.'3'.OR.NUMIN(:1).EQ.'N'.OR.NUMIN(:1)
+ .EQ.'F')THEN
              TFS=1
              GOTO 1494
          ENDIF
              IF(FIL.EQ.2)GOTO 1496
              GOTO 1495
          ENDIF
              WRITE(*,*)' choose output units for LST file'
              write(*,*)' 1- Kcal/mol (cal/mol K)  2- KJ/mol (J/mol K
+)')
              write(*,*)'   enter option { 1 }'
              read(*,3)numin
              founits='KCAL'
              if(numin.eq.'2')founits='KJ'
          OPEN(7,FILE=FS,STATUS='NEW')
              if(founits.eq.'KJ')then
                  write(7,*)' UNITS:KJ'
              else if(fouints.eq.'KCAL')then
                  write(7,*)' UNITS:KCAL'
              endif
1495          CONTINUE
          INQUIRE(FILE=FS2,EXIST=EXST,OPENED=OPNED,ERR=1234)
          IF(OPNED)THEN
              INQUIRE(34,OPENED=OPNED,ERR=1234)
              IF(OPNED)THEN
                  CLOSE(34,STATUS='KEEP')
                  IOP=0
              ENDIF
          ENDIF
          IF(EXST)THEN
              CALL CLS
              WRITE(*,32)FS2
              CALL LINES(0,3)
              WRITE(*,*)'  1 - DELETE (OVERWRITE)'
              WRITE(*,*)'  2 - APPEND (ADD DATA TO END)'
              WRITE(*,*)'  3 - ENTER DIFFERENT FILENAME'
              WRITE(*,*)'  Q - ABORT (RETURN TO PREVIOUS MENU)'
              CALL LINES(0,2)
              WRITE(*,*)'   enter option: {Q}'
              READ(*,3)NUMIN
              CALL READCHAR(NUMIN)
              IF(NUMIN.EQ.'Q'.OR.NUMIN.EQ.' ')THEN

```

```

        FIL=0
        GOTO 1492

    ENDIF
    IF(NUMIN.EQ.'1'.OR.NUMIN(:1).EQ.'D')THEN
        OPEN(52, FILE=FS2,ACCESS='DIRECT',RECL=70,FORM='FORMATTED',
+STATUS='UNKNOWN')
            TFS2=0
        ENDIF
        IF(NUMIN.EQ.'2'.OR.NUMIN(:1).EQ.'A')THEN
            OPEN(52,FILE=FS2,ACCESS='DIRECT',RECL=70,FORM='FORMATTED',
+STATUS='OLD')
                IB=1
1483         READ(52,'(A70)',REC=IB,END=1696)DUMMY
                TFS2=0
                    IB=IB+1
                        GOTO 1483
1696         NREC=IB
                BACKSPACE(52)
                GOTO 1496
        ENDIF
        IF(NUMIN.EQ.'3'.OR.NUMIN(:1).EQ.'N'.OR.NUMIN(:1)
+ .EQ.'F')THEN
            TFS2=1
            GOTO 1494
        ENDIF
    ENDIF
    OPEN(52,FILE=FS2,ACCESS='DIRECT',RECL=70,FORM='FORMATTED',
+STATUS='NEW')
        IB=1
        GOTO 1496
1496     CONTINUE
        IF (FIL .EQ. 0.OR.FIL.EQ.2) THEN
            IF(FIL.EQ.0)FIL=1
            IF(HEADER.EQ.1)GOTO 8990
            CALL LINES(0,2)
            WRITE(*,*)'  enter title  for *.LST file output ( blank or Q=
+no title )'
            READ(*,4)IDLINE
4           FORMAT(A70)
            WRITE(7,5)IDLINE
5           FORMAT(1X,A70)
            WRITE(7,3890)
3890        FORMAT(1X,'SPECIES      Hf      S      Cp 300      400      500
+600      800      1000      1500      DATE      ELEMENTS')
            ENDIF
8990        CONTINUE
            IF(FIL.EQ.2)GOTO 1067
250        FORMAT(1X,'SPECIES')
            WRITE(52,250)
            IF(BLFLAG.EQ.1)WRITE(52,38)RS22
38         FORMAT(1X,A14)
                RS22(10:14)=' '
                RS(10:14)=' '
                LS(10:14)=' '

```

```

IF(BFLAG.GE.2)THEN
      WRITE(52,38)RS
ELSE IF (FLAG .EQ. 1 .OR. BFLAG .EQ. 1 ) THEN
      WRITE(52,38)RS
ELSE IF (FLAG .EQ. 0 .AND. BFLAG .EQ. 0 ) THEN
      WRITE(52,38)LS
      ENDIF

      IF(DOCTYPE.EQ.'NOCALC')THEN
            S4='Thermo Data Entered: '
ELSE IF(BFLAG.GE.2)THEN
            S4='Thermo estimation for diradical'
ELSE IF (FLAG .EQ. 1 .OR. BFLAG .EQ. 1 ) THEN
            S4= 'Thermo estimation for radical'
ELSE IF (FLAG .EQ. 0 .AND. BFLAG .EQ. 0 ) THEN
            S4='Thermo estimation for molecule'
ENDIF
      WRITE(52,'(A70)')S4
      X=1
      M=1
      IF (BFLAG .EQ. 1) THEN
            WRITE(52,22) RS22,FORM(:LENF)
22      FORMAT(1X,A14,3X,A50)
23      FORMAT(1X,'RADICAL BASED UPON PARENT ',A14,3X,A30)
            GOTO 9003
      ENDIF
      IF (BFLAG.GE.1) THEN
            WRITE (52,22)RS,FORM(:LENF)
            WRITE(52,23)SPECP
            WRITE(52,9089)FORMP(:LENFP)
9089  FORMAT(1X,'PARENT FORMULA',1X,A30)
            S5='PARENT SYMMETRY '
            WRITE(52,'(A20,1X,I6)')S5,SYMS
      ENDIF
      IF (BFLAG.EQ.0) WRITE(52,22) LS,FORM(:LENF)
* record units
      if(units.eq.'KCAL')S5=' UNITS:KCAL '
      if(units.eq.'KJ')S5=' UNITS:KJ '
      WRITE(52,'(A20)')S5
      WRITE(52,1000)N
1000  FORMAT(' ', 'GROUPS',1X,I3)
9003  CALL WRITEGR(1,N,CS,E,IG,52,LS)
      IF(DOCTYPE.EQ.'NOCALC')WRITE(52,9654)DOCTYPE
9654  FORMAT(1X,A14)
            if(units.eq.'KCAL')then
            WRITE(52,7257)
7257  FORMAT( ' Hf  S  Cp 300  400  500  600  800  1000
+ 1500')
            WRITE(52,10)(B(1,I9),I9=1,9)
10    FORMAT(9F7.2)
            WRITE(52,6) CPINF
6     FORMAT(' ',10X,'CPINF = ',F7.2)
            else if(units.eq.'KJ')then

```

```

WRITE(52,7258)
7258  FORMAT( ' Hf      S      Cp 300      400      500      600      800
+ 1000      1500')
      do 1792 ik1=1,9
1792      bo(ik1)=b(x,ik1)*4.184
          cpio=cpinf*4.184
          write(52,11)(bo(ik1),ik1=1,9)
11      format(1x,2(F8.2),3(F7.2),4(f8.2))
          write(52,6)cpio
          endif
          IF(NROT.NE.0)WRITE(52,8430)NROT
8430      FORMAT(' ',1X,'NROTORS:',I2)
      ICTRL=0
      DO 2200 I=1,9
2200      IF(DELTA(I).NE.0.0)ICTRL=1
          IF(ICTRL.EQ.1)THEN
              WRITE(52,2224)
2224              FORMAT(1X,'DELTA EDIT')
                  if(units.eq.'KJ')then
                      do 1793 ik1=1,9
1793                      bo(ik1)=delta(ik1)*4.184
                          write(52,2225)(bo(i),i=1,9)
                      else if(units.eq.'KCAL')then
                          WRITE(52,2225)(DELTA(I),I=1,9)
                      endif
2225              FORMAT(1X,9(F7.2))
          ENDIF
          IF (BFLAG .EQ. 1.OR.BFLAG.EQ.2) THEN
              WRITE(52,1100)SYMR
1100              FORMAT(' ', 'SYMMETRY ',1X,I6)
                  WRITE(52,7259)
7259              FORMAT( 'R ln(2) has been added to S to account ')
                  WRITE(52,7260)
7260              FORMAT( '      for unpaired electron')
                  if(units.eq.'KCAL')then
                      WRITE(52,1110)BD
                  else if(units.eq.'KJ')then
                      bdu=bd*4.184
                      write(52,1110)bdu
                  endif
1110              FORMAT(' ', 'BOND ',1X,F7.2)
                  if(units.eq.'KCAL')then
                      IF(DELB.NE.0.0)WRITE(52,1122)DELB
                  else if(units.eq.'KJ')then
                      delbu=delb*4.184
                      if(delb.ne.0.0)write(52,1122)delbu
                  endif
1122              FORMAT(' ', 'DELTA BOND ENERGY = ',F10.3)
          ENDIF
          IF (BFLAG .EQ. 1 ) GOTO 900
          WRITE(52,1100) SYMM
900      CONTINUE

          IF(DOCTYPE.NE.'NOCALC')THEN

```



```

                WRITE(52,1132)IMON,IDAY,IYR
1132          FORMAT(1X,' CREATION DATE: ',I2,'/',I2,'/',I2)
                ENDIF

                IF(KOUNT.NE.0)THEN
                WRITE(52,1120)KOUNT
1120          FORMAT(' ',1X,'TEXT',I3)
                DO 1043 IH=1,KOUNT
1043          WRITE(52,4)TEXT(IH)

                ENDIF

                WRITE(52,256)
                S4=' '
                WRITE(52,'(A70)')S4
                WRITE(52,'(A70)')S4
256          FORMAT(' ',1X,'ENDSPECIES')
1492          CONTINUE
1067          X=1
                PHASE(:1)='G'

1066          FORMAT(A1,A10,F7.2,2X,F7.2,3X,7(F6.2,2X),2A4,A6,3X,4(A2,I3,
+ 1X),A1,1X,I1)
1068          FORMAT(A1,A10,F8.2,1X,F8.2,2X,7(F7.2,1X),2A4,A6,3X,4(A2,I3,
+ 1X),A1,1X,I1)
91066         FORMAT(A1,A10,F7.2,2X,F7.2,3X,7(F6.2,2X),I2,2('/',I2),A6,3X,4(A2
+ ,I3,1X),A1,1X,I1)
91068         FORMAT(A1,A10,F8.2,1X,F8.2,2X,7(F7.2,1X),I2,2('/',I2),A6,3X,4(A2
+ ,I3,1X),A1,1X,I1)
                if(founits.eq.'KJ')then
                do 1794 ik1=1,9
1794          bo(ik1)=b(x,ik1)*4.184
                endif
                IF ((BFLAG .EQ. 1.OR.BFLAG.EQ.2).and.founits.eq.'KCAL') THEN
                if(rs.eq.' ')GOTO 1234
                IF(DOCTYPE.EQ.'NOCALC')THEN
                WRITE(7,1066)CFLAG,RS(:10),(B(1,I9),I9=1,9),(REF(1),I=1,2),REF3,
+ (IE(I)(:2),NE(I),I=1,4),PHASE,NROT
                ELSE
                WRITE(7,91066)CFLAG,RS(:10),(B(1,I9),I9=1,9),IMON,IDAY,IYR,REF3,
+ (IE(I)(:2),NE(I),I=1,4),PHASE,NROT
                ENDIF
                elseif ((BFLAG .EQ. 1.OR.BFLAG.EQ.2).and.founits.eq.'KJ') THEN
                if(rs.eq.' ')GOTO 1234
                IF(DOCTYPE.EQ.'NOCALC')THEN
                write(7,1068)CFLAG,rs(:10),(bo(ik1),ik1=1,9),(ref(i),i=1,2),ref3,
+(ie(i)(:2),ne(i),i=1,4),phase,NROT
                ELSE
                write(7,91068)CFLAG,rs(:10),(bo(ik1),ik1=1,9),IMON,IDAY,IYR,ref3,
+(ie(i)(:2),ne(i),i=1,4),phase,NROT
                ENDIF
                ENDIF
                IF (BFLAG .EQ. 0.and.founits.eq.'KCAL') THEN
                if(ls.eq.' ')GOTO 1234

```

```

      IF(DOCTYPE.EQ.'NOCALC')THEN
        WRITE(7,1066)CFLAG,LS(:10),(B(1,19),I9=1,9),(REF(1),I=1,2),REF3,
        +(IE(1):2),NE(1),I=1,4),PHASE,NROT
      ELSE
        WRITE(7,91066)CFLAG,LS(:10),(B(1,19),I9=1,9),IMON,IDAY,IYR,REF3,
        +(IE(1):2),NE(1),I=1,4),PHASE,NROT
      ENDIF
      ELSE IF (BFLAG .EQ. 0.and.founits.eq.'KJ') THEN
        if(ls.eq.' ')GOTO 1234
        IF(DOCTYPE.EQ.'NOCALC')THEN
          write(7,1068)CFLAG,ls(:10),(bo(ik1),ik1=1,9),(ref(i),i=1,2),ref3,
          +(ie(i):2),ne(i),i=1,4),phase,NROT
        ELSE
          write(7,91068)CFLAG,ls(:10),(bo(ik1),ik1=1,9),IMON,IDAY,IYR,ref3,
          +(ie(i):2),ne(i),i=1,4),phase,NROT
        ENDIF
      ENDIF
1234 CONTINUE
      IF(OUTPUT.EQ.'CLOSE')CLOSE(52,STATUS='KEEP')
      RETURN
      END

SUBROUTINE READSP(S,SS,ICNT,IE1,NE1,REF1,REF2,PHSE,IENTRY,IHELP)
  INTEGER IG, Y, NG, P, X, O, D,NE(4),NE1(4,400),FLG,IFIRST(7),
  +ILAST(7),U
  REAL S(400,9)
  LOGICAL EXST,OPNED
  CHARACTER*14 SS(400)
      CHARACTER*70 THERMFIL,dummy,s1
  CHARACTER*14 KS, LS, RS,CP, TS, FS,DS
  CHARACTER PHSE(400),TITLE*30,HEADIN*126
  CHARACTER*14 NUL,NUL1(2,50),funits
  CHARACTER*4 IE1(4,400),REF1(2,400)
  CHARACTER*6 REF3,REF2(400)
70      FORMAT(A70)
14      FORMAT(A14)
      funits='KCAL'
      CALL CLS
      U=65
10000      WRITE(*,*)'      ENTER THERMO SPECIES DATABASE FILENAME
+ { *.LST }'
      CALL LINES (0,4)
      READ(*,70)THERMFIL
897      FORMAT(A14)
      CALL LRDCHAR(THERMFIL)
      IF(THERMFIL.EQ.' '.OR.THERMFIL.EQ.'Q')RETURN
      IIH=0
956      IIH=IIH+1
      IF (THERMFIL(IIH:IIH).EQ.' '.OR.THERMFIL(IIH:IIH).EQ.' ')THEN
        LEN=IIH-1
        GOTO 987
      ENDIF
      GOTO 956
987 CONTINUE

```

```

THERMFIL(LEN+1:LEN+4)='.LST'
INQUIRE(FILE=THERMFIL,EXIST=EXST,OPENED=OPNED,ERR=10001)
IF(EXST)GOTO 10002
CALL CLS
WRITE(*,7000)THERMFIL
7000  FORMAT(' ',5X,A70)
      WRITE(*,*)'          does not exist'
CALL LINES(0,2)
WRITE(*,7001)
7001  FORMAT(' ',20X,'please try again')
      goto 10000
10002 IF(OPNED)THEN
      REWIND(7)
      U=7
      GOTO 10003
ENDIF
OPEN(U,FILE=THERMFIL,STATUS='OLD')
10003 READ(U,70)dummy
      call lrdchar(dummy)
      call deblnk(dummy,s1,len1,0)
      if(dummy(:6).eq.'UNITS:')then
          if(dummy(7:8).eq.'KJ')funits='KJ'
          read(U,70)dummy
      endif
      READ(U,70)dummy
      ICNT=1
988   CONTINUE
      if(funits.eq.'KCAL')then
          READ(U,345,END=346)SS(ICNT)(:10),S(ICNT,1),S(ICNT,2),(S(ICNT,II
+),II=3,9),(REF1(1,ICNT),I=1,2),REF2(ICNT),(IE1(1,ICNT)(:2),NE1(I,
+ICNT),I=1,4),PHSE(ICNT)
345   FORMAT(1X,A10,F7.2,2X,F7.2,3X,7(F6.2,2X),2A4,A6,3X,4(A2,13,
+ 1X),A1)
          else if(funits.eq.'KJ')then
          READ(U,349,END=346)SS(ICNT)(:10),S(ICNT,1),S(ICNT,2),(S(ICNT,II
+),II=3,9),(REF1(1,ICNT),I=1,2),REF2(ICNT),(IE1(1,ICNT)(:2),NE1(I,
+ICNT),I=1,4),PHSE(ICNT)
349   FORMAT(1X,A10,F8.2,1X,F8.2,2X,7(F7.2,1X),2A4,A6,3X,4(A2,13,
+ 1X),A1)
          do 347 ik1=1,8
347   s(icnt,ik1)=s(icnt,ik1)/4.184
          endif

      IF(NE1(1,ICNT).NE.0.OR.NE1(2,ICNT).NE.0.OR.NE1(3,ICNT).NE.0
+.OR.NE1(4,ICNT).NE.0)ICNT=ICNT+1
      GOTO 988
346   CONTINUE
      ICNT=ICNT-1
      IF(OPNED)THEN
          BACKSPACE(7)
          GOTO 10004
      ENDIF
      CLOSE(65,STATUS='KEEP')
10004 IF(IHELP.EQ.0)GOTO 10001

```

```
CALL LISTGR(SS,S,ICNT,IFIRST,ILAST,8,IHELP,NE1,IE1)  
10001 RETURN  
END
```

```
      SUBROUTINE CLS  
C      CLEAR TERMINAL SCREEN BY WRITING 23 BLANK LINES  
      DO 1000 I=1,23  
      WRITE (*,*)' '  
1000 CONTINUE  
      RETURN  
      END
```

```

SUBROUTINE READGR(NGR,CS,TOT,IAC,M1)
C$LARGE
C*****
C*      PROMT THE USER FOR INPUT, READ GROUP      *
C*      DATA, THEN DECOUPLE GROUP ID AND THE NUMBER      *
C*      OF GROUPS WITH THE SAME ID                      *
C*****
      DIMENSION NUM(3)
      INTEGER TOT
      CHARACTER*14 CS(2,60)
      CHARACTER*70 CS1,DUMMY,OPTION,HLP(10)
      CHARACTER B*80,C*80,D*80
      CHARACTER*2 ERRORCK
      COMMON/CONF3/HLP
      COMMON/CONF7/ERRORCK
      IF(ERRORCK.EQ.' ' .AND. IACT.EQ.1)THEN
      WRITE(*,12)NGR
12  FORMAT(1X,'ENTER GROUP # ',I3)
      ENDIF
      READ(*,10)B
10  FORMAT(A72)
      IF(B(:1).EQ.'?')THEN
      OPTION='ENTERGROUP'
      CALL HELP(HLP(3),OPTION)
      IACT=4
      RETURN
      ENDIF
C*****
C  CONVERT TO PROPER FORMAT FOR THE SEARCH
C*****
      CS1=' '
      CS1(:70)=B(:70)
      B=' '
      CALL DEBLNK(CS1,DUMMY,LEN,1)
      B(:14)=CS1(:14)
      IACT=0
      FLAG=0.0
      M=0
      M1=0
      M2=0
      M3=0
      M4=0
      K=1
      TOT=0
      IF(ERRORCK.EQ.'NO' .AND. B.EQ.' ')THEN
      IACT=-10
      RETURN
      ELSEIF(B.EQ.' ')THEN
      IACT=2
      RETURN
      ENDIF
2  IF (FLAG.EQ.1.0)GOTO 50
      IF((B(K:K).EQ.' ' ) .OR. (B(K:K).EQ.' ' ))THEN
      M=K

```

```

                FLAG=1
                GO TO 60
        ENDIF
        IF((B(K:K)).EQ.'0')GOTO 60
50  IF((B(K:K)).EQ.' ')M3=K-1
        IF((B(K:K)).EQ.' ')GOTO 3
60  K=K+1
        IF(K.GE.81)GOTO 4
        GOTO 2
3  IF(M3.LE.M)TOT=1
        M1=M-1
        M2=M+1
        M4=M3-M2+1
        DO 35 IN=1,M1
        IF(ICHAR(B(IN:IN)).GE.97) THEN
                L=ICHAR(B(IN:IN))-32
                B(IN:IN)=CHAR(L)
        ENDIF
35  CONTINUE
        CS(1,NGR) = B(1:M1)
        IF(CS(1,NGR).EQ.'D')IACT=1
        IF(CS(1,NGR).EQ.'Q'.OR.CS(1,NGR).EQ.'QUIT')IACT=2
        IF(CS(1,NGR).EQ.'L')IACT=3
        IF(IACT.NE.0)RETURN
        IF(M3.LE.M)RETURN
        D=B(M2:M3)
        J=0
        NUM(1)=0
        NUM(2)=0
        NUM(3)=0
        DO 11 I=M2,M3
        J=J+1
11  NUM(J)=ICHAR(B(I:I))-48
        IF (J.EQ.2)NUM(1)=10*NUM(1)
        IF (J.EQ.3)NUM(1)=100*NUM(1)
        IF (J.EQ.3)NUM(2)=10*NUM(2)
        TOT=NUM(1)+NUM(2)+NUM(3)
13  FORMAT(3A1)
4  RETURN
END

```

```

SUBROUTINE READCHAR(LS)
C THIS SUBROUTINE RETURNS THE SAME STRING IN CAPITOL LETTERS
C NUMERIC EXPRESSIONS REMAIN THE SAME
CHARACTER*(*) LS
CALL DBLNK(LS,LEN,1)
I12=1
1400 IF(I12.GT.LEN)GOTO 1450
IF(ICHAR(LS(I12:I12)).GE.97)THEN
N28=ICHAR(LS(I12:I12))-32
LS(I12:I12)=CHAR(N28)
ENDIF
I12=I12+1
IF (I12.GT.LEN)GOTO 1450
GOTO 1400
1450 CONTINUE
RETURN
END

```

```

SUBROUTINE LRDCHAR(LS1)
C THIS SUBROUTINE RETURNS THE SAME STRING IN CAPITOL LETTERS
C NUMERIC EXPRESSIONS REMAIN THE SAME
CHARACTER*70 LS
CHARACTER*70 LS1,DUMMY
CALL DEBLNK(LS1,DUMMY,LEN,1)
I12=1
1400 IF(I12.GT.LEN)GOTO 1450
IF(ICHAR(LS1(I12:I12)).GE.97)THEN
N28=ICHAR(LS1(I12:I12))-32
LS1(I12:I12)=CHAR(N28)
ENDIF
I12=I12+1
IF (I12.GE.(LEN+1))GOTO 1450
GOTO 1400
1450 CONTINUE
RETURN
END

```

```

SUBROUTINE RDCH127(LS1)
CHARACTER*127 LS
CHARACTER*127 LS1,DUMMY
CALL DBL127(LS1,LEN,1)
I12=1
1400 IF(I12.GT.LEN)GOTO 1450
IF(ICHAR(LS1(I12:I12)).GE.97)THEN
N28=ICHAR(LS1(I12:I12))-32
LS1(I12:I12)=CHAR(N28)
ENDIF
I12=I12+1
IF (I12.GE.(LEN+1))GOTO 1450
GOTO 1400
1450 CONTINUE
RETURN
END

```



```
SUBROUTINE LINES(D,I)
  INTEGER I,D
  IF(D.EQ.0) THEN
    DO 2020 JJ=1,I
2020   WRITE (*,*)' '
    RETURN
  ENDIF
  DO 2021 JJ=1,I
2021   WRITE (D,*)' '
  RETURN
END
```

```

SUBROUTINE WRITEGR(ISTRN,N,CS,E,IG,IDEV,SPEC)
C$LARGE
C THIS SUBROUTINE WRITES GROUPS FOR CURRENT SPECIES TO
C FILE OR SCREEN
INTEGER IDEV,N,IG,E(1),ISTRN
CHARACTER*14 CS(2,50),SPEC
C FOR VAX TERM : IDEV=6; FOR PC IDEV=0
GOTO 1066
200 FORMAT(' ',2X,'Gr #',1X,'-',2X,'GROUP ID',2X,'-',1X,'Quantity')
300 FORMAT(' ',3X,I3,1X,'-',1X,A14,1X,'-',I3)
1066 IF(N.GT.5)THEN
WRITE(IDEV,400)
IF(FLOAT(N/2).EQ.FLOAT(N)/2.0)THEN
NEND=N/2
ENDIF
IF(FLOAT(N/2).NE.FLOAT(N)/2.0)THEN
NEND=(N/2)+1
ENDIF
DO 1100 I=ISTRN,NEND
IF(I+NEND.GT.N)THEN
WRITE(IDEV,300)I,CS(1,I),E(I)
GOTO 1100
ENDIF
WRITE(IDEV,500)I,CS(1,I),E(I),I+NEND,CS(1,I+NEND),E(I+NEND)
1100 CONTINUE
IF(CS(2,I)(:5).EQ.'ERROR')THEN
WRITE(IDEV,7000)
WRITE(IDEV,7001)CS(1,I)
ENDIF
IF(CS(2,I+NEND)(:5).EQ.'ERROR')THEN
WRITE(IDEV,7000)
WRITE(IDEV,7001)CS(1,I+NEND)
ENDIF
GOTO 1776
ENDIF
IF(N.GT.0) WRITE(IDEV,200)
DO 1101 I=ISTRN,N
WRITE(IDEV,300)I,CS(1,I),E(I)
IF(CS(2,I)(:5).EQ.'ERROR')THEN
WRITE(IDEV,7000)
WRITE(IDEV,7001)CS(1,I)
ENDIF
1101 CONTINUE
1776 CONTINUE
RETURN
400 FORMAT(' ',2(2X,'Gr #',1X,'-',2X,'GROUP ID',2X,'-',1X,'Quantity'))
500 FORMAT(' ',3X,I3,1X,'-',1X,A14,1X,'-',I3,1X,'|',3X,I3,1X,'-',
+1X,A14,1X,'-',I3)
7000 FORMAT(1X,'***** ERROR GROUP ENTRY WAS NOT FOUND ***
+*****')
7001 FORMAT(1X,'-----> ',A14,' not found in current group databas
+e !')
END

```

```

SUBROUTINE FINDGR(AS,NGRPT,CS,IX,IG,ISTAT,MM1)
C$LARGE
INTEGER IX(1),ISTAT,IG,Y,SYMM,SYMR,NGRPT,MM1
CHARACTER*14 AS(1),CS(2,50),COMMAND,OUTPUT
LOGICAL OPNED
COMMON/CTRL2/COMMAND,OUTPUT
I = 1
ISTAT=0
3030 IF (CS(1,IG).EQ.AS(1)) GOTO 3090
I = I + 1
IF (I .GE. NGRPT) GOTO 3052
GOTO 3030
3052 CONTINUE
IF(COMMAND.EQ.'AUTO_RECALC')THEN
INQUIRE(52,OPENED=OPNED)
IF(OPNED)THEN
WRITE(52,7000)
7000 FORMAT(1X,'***** ERROR *****')
WRITE(52,7001)CS(1,IG)
7001 FORMAT(1X,' ENTRY ',A14,' WAS NOT FOUND')
WRITE(52,7002)
7002 FORMAT(1X,' ')
ENDIF
ENDIF
WRITE(*,7000)
WRITE(*,7001)CS(1,IG)
ISTAT=1
RETURN
3090 IX(IG) = I
CS(2,IG)=CS(1,IG)
C remember save the parent for later processing
RETURN
601 CONTINUE
RETURN
END

```

```

SUBROUTINE EDIT(CS,E,B,AS,A,N,RS22,LS,RS,TEXT,BD,TS,IX,FORM,FORMP,
+CPINF,SYMM,SYMR,BFLAG,FLAG,BLFLAG,SCOR,SCORP,NSAVE,IG,NE,IE,
+NGRPT,IFIRST,ILAST,NATOM,KOUNT,SYMS,TEXTS,KOUNTS,SPEC, IHELP,
+LENF,LENFP,EP,NATOMP,IP,NP,ISOURCE,DELB,DOCTYPE,KDOCT,DELTA,NED,
+BSAVE,DOCFIL,FILNM,DOC)

```

C\$LARGE

```

INTEGER IX(50),E(50),N,NGRPT, Q,EI,FIL,Z1,I9(1),NSAVE,NUM,TOT
INTEGER FLAG, BFLAG, SYMM,SYMS, SYMR, CTRL, Z, NGRP, NATOM,ES
INTEGER IG, Y, NG, P, X, O, D,NE(1),FLG,IFIRST(1),ILAST(1),ESAVE,
+EP(1),NP(1),NATOMP,KDOCT,NE1(4,400)
REAL A(400,9), SCOR, CPINF, CP2K,RNUM,DELTA(1)
REAL*4 B(2,9),BSAVE(1),BO(9)
CHARACTER*4 IE1(4,400)
CHARACTER*70 FORM,FORMP,FORMN,DUMMY
CHARACTER*70 DOC(1),OPTION,HLP(10)
CHARACTER*70 TEXT(1),TEXTS(1),FILNM
CHARACTER*14 AS(1),NUMIN,TSS,SPEC,FS2,DOCTYPE,DOCFIL
CHARACTER*14 CS(2,60), WS(1) ,KS, LS, RS,CP, TS, FS,DS,RS22
CHARACTER ANSS,PHASE
CHARACTER*14 NUL,NUL1(2,50),UNITS
CHARACTER*4 IE(1),IP(1),REF(1)
CHARACTER*6 REF3
COMMON/CONF3/HLP
COMMON/CONF6/UNITS
COMMON/NROTOR/NROT,NROTS

```

3 FORMAT(A14)

```

C*****
C*****          EDIT MENU          *****
C*****
10000 CALL CLS
      IF(IHELP.EQ.0.AND.(BFLAG.EQ.0.OR.FLAG.EQ.1))THEN
        WRITE(*,*)'EDIT SPECIES MENU:'
        WRITE(*,*)'1-SYMM, 2-THERMO, 3-FORM, 4-TEXT, 5-RETURN'
        WRITE(*,*)'6-ADD GRP, 7-DELETE GRP, 8-CHANGE GRP'
        GOTO 701
      ENDIF
      IF(IHELP.EQ.0.AND.(BFLAG.NE.0.))THEN
        WRITE(*,*)'EDIT SPECIES MENU:'
        WRITE(*,*)'1-SYMM, 2-THERMO, 3-FORM, 4-TEXT, 5-RETURN'
        WRITE(*,*)'6-CHANGE BD, 7-RESTORE PARENT'
        GOTO 701
      ENDIF
      WRITE(*,100)
100  FORMAT(' ',32X,'EDIT SPECIES MENU')
      WRITE(*,150)
150  FORMAT(' ',25X,35(' '))
          CALL LINES(0,1)
      WRITE(*,200)
200  FORMAT(' ',25X,'1 - CHANGE SYMMETRY NUMBER')
      WRITE(*,450)
450  FORMAT(' ',25X,'2 - CHANGE/MODIFY THERMO')
C    WRITE(*,451)
451  FORMAT(' ',25X,' { changes are recorded as a group }')
      WRITE(*,500)

```

```

500  FORMAT(' ',25X,'3 - CHANGE SPECIES ID / FORMULA')
      WRITE(*,550)
550  FORMAT(' ',25X,'4 - ADD TEXT TO SPECIES SCREEN')
      WRITE(*,600)
600  FORMAT(' ',25X,'5 - RETURN TO SPECIES SCREEN')
      IF(BFLAG.EQ.0.OR.FLAG.EQ.1)THEN
          WRITE(*,250)
250  FORMAT(' ',25X,'6 - ADD A GROUP TO THE CURRENT SPECIES')
          WRITE(*,300)
300  FORMAT(' ',25X,'7 - DELETE A GROUP')
          WRITE(*,350)
350  FORMAT(' ',25X,'8 - CHANGE A GROUP')
          WRITE(*,351)
351  FORMAT(' ',25X,'9 - CHANGE NROTORS')
          GOTO 2000
      ENDIF
      IF(BFLAG.NE.0)THEN
          WRITE(*,400)
400  FORMAT(' ',25X,'6 - CHANGE BOND DISSOCIATION ENERGY')
          WRITE(*,650)
650  FORMAT(' ',25X,'7 - RETURN TO PREVIOUS PARENT MOLECULE')
          WRITE(*,651)
651  FORMAT(' ',25X,'8 - CHANGE NROTORS')
      ENDIF
2000 CONTINUE
          WRITE(*,660)
660  FORMAT(' ',25X,'? - HELP')
701  WRITE(*,700)
700  FORMAT(' ',30X,'enter option : { Q }')
C
C***** END OF EDIT MENU *****
      READ(*,3)NUMIN
      CALL READCHAR(NUMIN)
      IF((NUMIN(:1).EQ.'5').OR.(NUMIN(:1).EQ.' ').OR.
+(NUMIN(:1).EQ.'Q')) GOTO 999

***** HELP *****

          IF(NUMIN(:1).EQ.'?')THEN
              WRITE(*,4343)
4343  FORMAT('+',30X,'HELP ON WHICH OPTION ?')
              READ(*,70)OPTION
70    FORMAT(A70)
              IF(OPTION.EQ.' '.OR.OPTION.EQ.'Q')GOTO 10000
              NUMIN=OPTION(:14)
              CALL READNUM(NUMIN,RNUM,NUMBR,KFLG)
              IF(NUMBR.LE.5.OR.BFLAG.EQ.0)THEN
                  CALL HELP(HLP(7),OPTION)
                  GOTO 10000
              ELSE IF(NUMBR.GE.6.AND.BFLAG.NE.0)THEN
                  OPTION(2:2)='R'
                  CALL HELP(HLP(7),OPTION)
                  GOTO 10000
              ENDIF
          ENDIF

```

```

                                GOTO 10000
ENDIF
***** END OF HELP *****
764  CALL CLS
      IF((NUMIN(:1).EQ.'5').OR.(NUMIN(:1).EQ.' ').OR.
      +(NUMIN(:1).EQ.'Q')) GOTO 999
      CALL CLS
C*****
C                                CHANGE SYMMETRY NUMBER
C*****
      IF(NUMIN(:1).EQ.'1'.OR.NUMIN(:1).EQ.'S')THEN
        IF(BFLAG.EQ.0)THEN
          IF(FLAG.EQ.1)SYMR=SYMM
          WRITE(*,10)SYMM
10      FORMAT('0',15X,'SYMMETRY # = ',13)
          WRITE(*,11)
11      FORMAT('0',15X,'enter new SYMMETRY #')
          READ(*,3)NUMIN
          CALL READCHAR(NUMIN)
          IF(NUMIN(:1).EQ.'Q'.OR.NUMIN(:1).EQ.' ')GOTO 10000
          CALL READNUM(NUMIN,RNUM,SYMM,FLG)
          IF(FLG.EQ.1)THEN
            FLG=0
            GOTO 10000
          ENDIF
            IF(FLAG.EQ.1)THEN
              SYMR=SYMM
            ENDIF
            SYMS=SYMM
            B(1,2)=B(1,2)+SCOR
            SCOR=1.98717*ALOG(SYMM*1.0)
            SCORP=SCOR
            B(1,2)=B(1,2)-SCOR
          ENDIF
          IF(BFLAG.NE.0)THEN
            WRITE(*,10)SYMR
            WRITE(*,11)
            READ(*,3)NUMIN
            CALL READCHAR(NUMIN)
            IF(NUMIN(:1).EQ.'Q'.OR.NUMIN(:1).EQ.' ')GOTO 10000
            CALL READNUM(NUMIN,RNUM,SYMR,FLG)
            IF(FLG.EQ.1)THEN
              FLG=0
              GOTO 10000
            ENDIF
            B(1,2)=B(1,2)+SCOR
            SCOR=1.98717*ALOG(SYMR*1.0)
1999      B(1,2)=B(1,2)-SCOR
          ENDIF
          GOTO 999
        ENDIF
      ENDIF
C*****
C                                CHANGE FORMULA/SPECIES ID
C*****

```

```

IF((NUMIN(:1).EQ.'3').OR.(NUMIN(:1).EQ.'F'))THEN
WRITE(*,20)
20   FORMAT(10X,'CURRENT SPECIES FORMULA IS: ')
      WRITE(*,*)FORM
      WRITE(*,21)
21   FORMAT('0',10X,'ENTER NEW FORMULA FOR SPECIES')
      WRITE(*,54)
54   FORMAT('0',10X,' 70 CHARACTERS MAX ')
77624  FORMAT(A70)
      READ(*,77624)FORMN
      CALL LRDCHAR(FORMN)
      IF((FORMN(:1).EQ.'Q').OR.(FORMN(:1).EQ.' '))GOTO 10000
      IFORM=0
      CALL DEBLNK(FORMN,DUMMY,LENF,0)
      CALL FORMINT(FORMN,LENF,IE,NE,NATOM,IFORM)
      if(iform.lt.0)then
          numin(:1)='3'
          goto 764
      endif
      form=formn
DO 568 KJ=1,4
      IP(KJ)=IE(KJ)
568   NP(KJ)=NE(KJ)
      NATOMP=NATOM
      IF(BFLAG.EQ.0.OR.FLAG.EQ.1)THEN
          FORMP=FORM
          LENFP=LENF
      ENDIF
      WRITE(*,50000)
50000  FORMAT('0',10X,'ENTER NEW NAME FOR SPECIES')
      WRITE(*,50001)
50001  FORMAT('0',10X,'{ " Q " = QUIT : no change }')
      READ(*,3)NUMIN
      CALL READCHAR(NUMIN)
      IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
      IF(FLAG.EQ.1)THEN
          RS22=NUMIN
          RS22(10:14)=' '
          SPECP=NUMIN
          SPECP(10:14)=' '
      ENDIF
      IF(BFLAG.NE.0)THEN
          RS=NUMIN
          RS(10:14)=' '
      ENDIF
      IF(BFLAG.EQ.0.AND.FLAG.EQ.0)THEN
          LS=NUMIN
          LS(10:14)=' '
          SPECP=NUMIN
          SPECP(10:14)=' '
      ENDIF
      GOTO 999
ENDIF

```

C*****

```

C          ENTER TEXT
C*****
7657      IF((NUMIN(:1).EQ.'4').OR.(NUMIN(:1).EQ.'T'))THEN
          IF(KOUNT.EQ.0)THEN
              WRITE(*,25)
25          FORMAT(5X,'ENTER TEXT FOR SPECIES SCREEN')
              WRITE(*,26)
26          FORMAT('0',5X,'ENTER " Q " OR BLANK WHEN FINISHED')
              KOUNT=0
                  WRITE(*,*)' 70 characters max'
30          READ(*,4)TEXT(KOUNT)
4          FORMAT(A70)
          IF(((TEXT(KOUNT)(:1)).EQ.'Q').OR.((TEXT(KOUNT)).EQ.' '))
+          .OR.((TEXT(KOUNT)(:1)).EQ.'q'))GOTO 999
          IF(BFLAG.EQ.0) TEXTS(KOUNT)=TEXT(KOUNT)
          KOUNT=KOUNT+1
          IF(KOUNT.GE.50)THEN
              IF(BFLAG.EQ.0)KOUNTS=KOUNT
              GOTO 999
          ENDIF
          GOTO 30
          ELSE IF (KOUNT.NE.0)THEN
              WRITE(*,*)' ENTER/MODIFY TEXT'
              DO 7655 IJK=1,KOUNT
7655          WRITE(*,7654)IJK,TEXT(IJK)
7654          FORMAT(1X,13,' ':',A70)
              CALL LINES(0,2)
              WRITE(*,*)' enter line# to modify; 0 = clear all; A = append; Q
+= quit (no change)'
              read(*,3)nul
              call readchar(nul)
              IF(NUL.EQ.' ' .OR. NUL.EQ.'Q')GOTO 10000
                  IF(NUL.EQ.'0')THEN
                      KOUNT=0
                      NUMIN='4'
                      GOTO 7657
                  ENDIF
                  IF(NUL.EQ.'A')THEN
                      WRITE(*,25)
                      WRITE(*,26)
                      KOUNT=KOUNT+1
                      WRITE(*,*)' 70 characters max'
32          READ(*,4)TEXT(KOUNT)
          IF(((TEXT(KOUNT)(:1)).EQ.'Q').OR.((TEXT(KOUNT)).EQ.' '))
+          .OR.((TEXT(KOUNT)(:1)).EQ.'q'))GOTO 999
          IF(BFLAG.EQ.0) TEXTS(KOUNT)=TEXT(KOUNT)
          KOUNT=KOUNT+1
          IF(KOUNT.GE.50)THEN
              IF(BFLAG.EQ.0)KOUNTS=KOUNT
              GOTO 999
          ENDIF
          GOTO 32
          ENDIF
          CALL READNUM(NUL,RNUM,LINE,FLG)

```



```

        IF(FLG.EQ.1)GOTO 10000
        IF(LINE.GT.KOUNT.OR.LINE.LE.0)GOTO 10000
        WRITE(*,*)' RE-ENTER TEXT FOR LINE# ',LINE
        READ(*,4)DUMMY
        IF(DUMMY.EQ.' ' .OR.DUMMY.EQ.'Q' .OR.DUMMY.EQ.'q')GOTO 10000
        IF(DUMMY.EQ.'D' .OR.DUMMY.EQ.'d' .OR.DUMMY.EQ.'del' .OR.DUMMY.EQ.
+ 'DEL' .OR.DUMMY.EQ.'DELETE' .OR.DUMMY.EQ.'delete')THEN
                TEXT(LINE)=' '
                GOTO 7657
        ENDIF
        TEXT(LINE)=DUMMY
        GOTO 7657
    ENDIF
ENDIF
ENDIF
*-----
*   CHANGE NUMBER OF ROTORS
*-----
        IF(NUMIN.EQ.'9' .OR.(NUMIN.EQ.8.AND.BFLAG.NE.0))THEN
                CALL CLS
                WRITE(*,*)' number of free rotors at 5000 K'
                write(*,'(10x,i2)')nrot
                call lines(0,2)
                write(*,*)' enter new number of free rotors'
                read(*,'(a)')numin
                call readchar(numin)
                if(numin.eq.'Q' .OR.NUMIN.EQ.' ')goto 10000
                if(numin.eq.'?')then
                        OPTION='NROT'
                        CALL HELP(HLP(8),OPTION)
                        GOTO 10000
                call readnum(numin,rnum,nrot,kflg)
                if(kflg.ne.0)then
                        kflg=0
                        goto 10000
                endif
                if(bflag.ne.0)nrots=nrot
                goto 999
        endif
*-----
C*****
C               RECOVER PARENT/IF RADICAL
C*****
        IF(((NUMIN(:1).EQ.'7') .OR.(NUMIN(:1).EQ.'P')).AND.(BFLAG.NE.0))
+ THEN
                IF(ISOURCE.EQ.0)THEN
                        N=NSAVE
                        DO 896 Y=1,N
                                CS(1,Y)=CS(2,Y)
                                E(Y)=EP(Y)
896         CONTINUE
                        DO 866 Y=1,9
866         B(1,Y)=B(2,Y)

```

```

      IF(FLAG.EQ.0)BFLAG=0
      IF(FLAG.EQ.1.AND.BFLAG.NE.0)BFLAG=0
      NROT=NROTS
      SYMM=SYMS
      SCOR=SCORP
      B(1,2)=B(1,2)-SCOR
      KOUNT=KOUNTS
      FORM=FORMP
      LENF=LENFP
      NATOM=NATOMP
      DO 548 KJ=1,4
      IE(KJ)=IP(KJ)
548      NE(KJ)=NP(KJ)
      NATOMP=NATOM
      DO 867 IZ1=1,KOUNT
867      TEXT(IZ1)=TEXTS(IZ1)
      GOTO 999
    ENDIF
      IF(ISOURCE.EQ.1)THEN
      IENTER=1
      SYMS=0
      SYMM=0
      SYMR=0
      FORM=' '
      FORMP=' '
      N=0
      NSAVE=0
      LS=' '
      RS=' '
      SPEC=' '
      NATOM=0
      NATOMP=0
      FLAG=0
      FLG=0
      BFLAG=0
      BLFLAG=0
      SCOR=0.0
      SCORP=0.0
      BD=0.0
      DELB=0.0
      DO 869 I=1,60
869      CS(1,I)=' '
      CS(2,I)=' '
      DO 873 I=1,50
873      E(I)=0
      IX(I)=0
      DO 871 I=1,4
871      IE(I)=' '
      NE(I)=0
      CALL LOADSP(AS,A,IFIRST,ILAST,NGRPT,CS,B,N,NSAVE,SYMM,SYMS,
+SYMR,SCOR,SCORP,FORM,FORMP,SPECP,IE,NE,NATOM,FLAG,BFLAG,FLG,LS,RS,
+RS22,FILST,DOCFIL,IX,E,LENF,EP,FILNM,DOC,NDOC,TEXT,TEXTS,KOUNT,
+IOP,IDOC,NSPEC,BD,LENFP,IENTER,JC,DELB,DOCTYPE,KDOCT,DELTA)
      IF(FLG.EQ.1)GOTO 10000

```

```

DO 54631 JCOUNT=1,N
IF((IX(JCOUNT).GE.IFIRST(4)).AND.(IX(JCOUNT).LE.ILAST(4)))THEN
    BFLAG=1
    GOTO 54631
ENDIF
IF((IX(JCOUNT).GE.IFIRST(3)).AND.(IX(JCOUNT).LE.ILAST(3)))THEN
    FLAG=1
    GOTO 54631
ENDIF
IF(FLAG.EQ.1)GOTO 54631
FLAG=0
54631 CONTINUE
ISOURCE=1
CPINF = ((3.0*NATOM) - (2.0+(FLOAT(NROT)/2.)))*1.987
CP2K = B(1,9) + .37*(CPINF - B(1, 9))
GOTO 999
ENDIF
ENDIF
C*****
C          EDIT THERMO
C*****
IF((NUMIN(:1).EQ.'2').OR.(NUMIN(:1).EQ.'T'))THEN
2500 CALL CLS
WRITE(*,*)'          EDIT THERMO SCREEN'
WRITE(*,*)'-----'

IF(BFLAG.GE.2)WRITE(*,*)'Thermo estimation for diradical'
    IF(DOCTYPE.EQ.'NOCALC')THEN
        WRITE(*,*) 'Thermo Data Entered: '
    ELSEIF (FLAG .EQ. 1 .OR. BFLAG .EQ. 1 ) THEN
        WRITE(*,*) 'Thermo estimation for radical'
    ELSEIF (FLAG .EQ. 0 .AND. BFLAG .EQ. 0 ) THEN
        WRITE(*,*) 'Thermo estimation for molecule'
    ENDIF
    IF (BFLAG .EQ. 1) THEN
        WRITE(*,22) RS22,FORM
22      FORMAT(1X,A14,3X,A50)
23      FORMAT('0',1X,'RADICAL BASED UPON PARENT ',A14,3X,A50)
        GOTO 9003
    ENDIF
    IF (BFLAG.GE.1) THEN
        WRITE (*,22)RS,FORM(:LENF)
        WRITE(*,23)SPECP,FORMP(:LENFP)
    ENDIF
    IF (BFLAG.EQ.0) WRITE(*,22) LS,FORM(:LENF)
        CALL LINES(0,1)
        CP2K = B(1,9) + .37*(CPINF - B(1, 9))
C9003 CALL WRITEGR(1,N,CS,E,IG,0,LS)
        if(units.eq.'KCAL')write(*,*)'    Hf (Kcal/mol)    S & Cp (cal
+/mol K)'
        if(units.eq.'KJ')write(*,*)'    Hf (KJ/mol)    S & Cp (J/mol K)!'
9003 CALL LINES(0,1)
        if(units.eq.'KJ')then

```

```

do 765 ik1=1,9
765      bo(ik1)=b(1,ik1)*4.184
        cpio=cpinf*4.184
        WRITE(*,93)
93      format(6X,'Hf',6X,'S',4X,'Cp 300',5X,'400',6X,'500',5X,'600'
+ ,5X,'800',5X,'1000',5X,'1500')
        write(*,92)(bo(ik1),ik1=1,9)
92      format(1x,9(f8.2,1x))
        cpio=cpinf*4.184
        write(*,94)cpio
        else if(units.eq.'KCAL')then
            write(*,9368)
9368    format(5X,'Hf',6X,'S',4X,'Cp 300',5X,'400',5X,'500',4X,'600'
+ ,4X,'800',4X,'1000',4X,'1500')
            WRITE(*,9) (B(1,id9),id9=1,9)
9            FORMAT(9F8.2)
            WRITE(*,94) CPINF
94      format(1x, 'CPinf = ',2x,f7.2)
        endif
CALL LINES(0,2)
WRITE(*,*)'1{Hf} 2{S} 3{CP300} 4{CP400} 5{CP500} 6{CP600} 7{CP800}
+ 8{CP1000} 9{CP1500}'
CALL LINES(0,1)
WRITE(*,*)'          enter option { 1-9 : Q=QUIT }'
READ(*,3)NUMIN
CALL READCHAR(NUMIN)
IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
CALL READNUM(NUMIN,RNUM,NUM,FLG)
IF (FLG.EQ.1)THEN
    FLG=0
    GOTO 10000
ENDIF
WRITE(*,*)'          A - ADD CORRECTION OR R - REPLACE'
READ(*,3)NUL
CALL READCHAR(NUL)
IF((NUL(:1).EQ.'Q').OR.(NUL(:1).EQ.' '))GOTO 10000
IF(NUL(:1).EQ.'A')THEN
    WRITE(*,*)'          ENTER CORRECTION'
    READ(*,3)NUL
    CALL READCHAR(NUL)
    IF((NUL(:1).EQ.'Q').OR.(NUL(:1).EQ.' '))GOTO 10000
    CALL READNUM(NUL,RNUM,NUM,FLG)
    IF(FLG.EQ.1)THEN
        FLG=0
        GOTO 10000
    ENDIF
    if(units.eq.'KJ')rnum=rnum/4.184
    IF(RNUM.NE.0.)THEN
        IF(NED.EQ.0)THEN
            DO 10101 I=1,7
10101      BSAVE(I)=B(1,I)
            NED=1
        ENDIF
        B(1,NUM)=B(1,NUM)+RNUM

```

```

        DELTA(NUM)=DELTA(NUM)+RNUM

        ENDIF
        GOTO 2500
ENDIF
IF(NUL(:1).EQ.'R')THEN
    WRITE(*,*)'    ENTER NEW VALUE'
    READ(*,3)NUL
    CALL READCHAR(NUL)
    IF((NUL(:1).EQ.'Q').OR.(NUL(:1).EQ.' '))GOTO 10000
    CALL READNUM(NUL,RNUM,IDUMMY,FLG)
    IF(FLG.EQ.1)THEN
        FLG=0
        GOTO 10000
    ENDIF
    if(units.eq.'KJ')rnum=rnum/4.184
    IF(abs(RNUM-B(1,NUM)).gt.0.01)THEN

        IF(NED.EQ.0)THEN
            DO 10121 I=1,7
10121         BSAVE(I)=B(1,I)
                NED=1
            ENDIF
            DELTA(NUM)=RNUM-BSAVE(NUM)
            B(1,NUM)=RNUM
            ENDIF
            GOTO 2500
        ENDIF
    ENDIF
C*****
C          CHANGE BOND DISSOCIATION/IF RADICAL
C*****

    IF(((NUMIN(:1).EQ.'6').OR.(NUMIN(:1).EQ.'B')).AND.(BFLAG.NE.0))
+THEN
        if(units.eq.'KJ')then
            bj=bd*4.184
            write(*,45)bj
        else if(units.eq.'KCAL')then
            WRITE(*,40)BD
40         FORMAT(' ',10X,'CURRENT BOND DISSOCIATION ENERGY IS',2X,F7.2,
+ ' Kcal/mol')
45         FORMAT(' ',10X,'CURRENT BOND DISSOCIATION ENERGY IS',2X,F7.2,
+ ' KJ/mol')
            endif
            WRITE(*,41)TS
41         FORMAT('0',10X,'BOND TYPE IS',2X,A14)
            WRITE(*,42)
42         FORMAT('0',10X,'ENTER NEW BOND DISSOCIATION ENERGY')
            READ(*,3)NUMIN
            CALL READCHAR(NUMIN)
            IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
            CALL READNUM(NUMIN,BDN,IDUMMY,FLG)
            IF(FLG.EQ.1)THEN

```

```

        FLG=0
        GOTO 10000
    ENDIF
        if(units.eq.'KJ')bdn=bdn/4.184
    WRITE(*,43)
43    FORMAT('0',10X,'CHANGE BOND NAME ( Y or N )')
    READ(*,3)NUMIN
    CALL READCHAR(NUMIN)
    IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
    IF(NUMIN(:1).EQ.'Y')THEN
        WRITE(*,44)
44    FORMAT('0','ENTER NEW BOND NAME : " Q " TO QUIT')
    READ(*,3)NUMIN
    CALL READCHAR(NUMIN)
        if(numin.eq.' ')goto 99
    IF((NUMIN(:1).EQ.'Q'))GOTO 10000
        TS=NUMIN
        GOTO 99
    ENDIF
    TS(12:14)='MOD'
99    BD=BD-DELB
    DELB=BDN-BD
    B(1,1)=B(1,1)+DELB
        BD=BDN
        GOTO 999
    ENDIF
C*****
C          ADD/DELETE/CHANGE GROUP
C          PARENT ONLY
C*****
    IF(BFLAG.NE.0)GOTO 999
    IF(NUMIN(:1).EQ.'A')NUMIN(:1)='6'
    IF(NUMIN(:1).EQ.'D')NUMIN(:1)='7'
    IF(NUMIN(:1).EQ.'C')NUMIN(:1)='8'
    IF((NUMIN(:1).EQ.'6').OR.(NUMIN(:1).EQ.'7').OR.(NUMIN(:1).EQ.
+ '8')) THEN
2600    CALL CLS
        DO 8991 JCOUNT=1,N
            IF((IX(JCOUNT).GE.IFIRST(3)).AND.(IX(JCOUNT).LE.LLAST(3)))THEN
                FLAG=1
                GOTO 8991
            ENDIF
        FLAG=0
8991    CONTINUE
        IF((NUMIN(:1).EQ.'6'))WRITE(*,50)
        IF((NUMIN(:1).EQ.'7'))WRITE(*,51)
        IF((NUMIN(:1).EQ.'8'))WRITE(*,52)
50    FORMAT(' ',25X,'ADD GROUP SCREEN')
51    FORMAT(' ',25X,'DELETE GROUP SCREEN')
52    FORMAT(' ',25X,'CHANGE GROUP SCREEN')
    WRITE(*,*)'-----'
+-----'

```

```

                IF(DOCTYPE.EQ.'NOCALC')THEN
                    WRITE(*,*)'Thermo Data Entered: '
                ELSE IF(BFLAG.GE.2)THEN
                    WRITE(*,*)'Thermo estimation for diradical'
                ELSE IF (FLAG .EQ. 1 .OR. BFLAG .EQ. 1 ) THEN
                    WRITE(*,*) 'Thermo estimation for radical'
                ELSE IF (FLAG .EQ. 0 .AND. BFLAG .EQ. 0 ) THEN
                    WRITE(*,*) 'Thermo estimation for molecule'
                ENDIF
                IF (BLFLAG .EQ. 1) THEN
                    WRITE(*,22) RS22,FORM(:LENF)
                    GOTO 2300
                ENDIF
                IF (BFLAG.GE.1) THEN
                    WRITE (*,22)RS,FORM (:LENF)
                    WRITE(*,23)SPECP,FORMP(:LENFP)
                ENDIF
                IF (BFLAG.EQ.0) WRITE(*,22) LS,FORM(:LENF)
2300          CALL LINES(0,1)
                CP2K = B(1,9) + .37*(CPINF - B(1, 9))
                if(units.eq.'KCAL')write(*,*)'      Hf (Kcal/mol)    S & Cp (cal
+/mol K)'
                if(units.eq.'KJ')write(*,*)'      Hf (KJ/mol)    S & Cp (J/mol K)'
                CALL LINES(0,1)
                if(units.eq.'KJ')then
7652          do 7652 ik1=1,9
                    bo(ik1)=b(1,ik1)*4.184
                    bo(8)=cp2k*4.184
                    cpio=cpinf*4.184
                    WRITE(*,93)
                    write(*,92)(bo(ik1),ik1=1,9)
                    cpio=cpinf*4.184
                    write(*,94)cpio
                else if(units.eq.'KCAL')then
                    WRITE(*,9368)
                WRITE(*,9) (B(1,ID9),ID9=1,9)
                    WRITE(*,94) CPINF
                endif
                CALL LINES(0,1)
                WRITE(*,*)'          CURRENT GROUPS'
                CALL WRITEGR(1,N,CS,E,N,6,LS)
C----- ADD A GROUP BLOCK -----
                IF((NUMIN(:1).EQ.'6').OR.(NUMIN(:1).EQ.'A'))THEN
                    N=N+1
                    IACT=0
7766          CALL READGR(N,CS,TOT,IACT,MM1)
                    IF(IACT.EQ.0)GOTO 7765
                    IF(IACT.EQ.2)THEN
                        IACT=0
                        N=N-1
                        GOTO 10000
                    ENDIF
                    IF(IACT.EQ.3)THEN
                        IENTRY=0

```

```

CALL LISTGR(AS,A,NGRPT,IFIRST,ILAST,IENTRY,IHELP,NE1,IE1)
  CALL CLS
  IACT=0
  N=N-1
  GOTO 2600
ENDIF
IF(IACT.EQ.1)THEN
  CALL CLS
  IACT=0
  N=N-1
  WRITE(*,*)'          USE OPTION 2 TO DELETE A GROUP'
  CALL LINES(0,4)
  WRITE(*,*)'          { hit return to continue }'
  READ(*,3)NUL
  NUMIN(:1)='6'
  GOTO 2600
ENDIF
7765 CONTINUE
      ISTAT=0
CALL FINDGR(AS,NGRPT,CS,IX,N,ISTAT,MM1)
  IF(ISTAT.EQ.1)THEN
    ISTAT=0
    GOTO 7766
  ENDIF
  CS(2,N)=CS(1,N)
  IF((IX(N).LE.ILAST(3)).AND.(IX(N).GE.IFIRST(3)))FLAG=1
  IF((IX(N).LE.ILAST(4)).AND.(IX(N).GE.IFIRST(4)))THEN
    CALL CLS
    WRITE(*,*)'          ERROR : YOU CANNOT ENTER'
    WRITE(*,*)'          BOND DISSOCIATION GROUPS'
    WRITE(*,*)'          ON THIS SCREEN'
    CALL LINES(0,3)
    WRITE(*,*)'          { hit return to continue }'
    call lines(0,3)
    N=N-1
    READ(*,3)NUMIN
    NUMIN(:1)='6'
    GOTO 2600
  ENDIF

      E(N)=TOT
      EP(N)=TOT
      DO 7767 Y=1,7
      B(1,Y)=B(1,Y)+(E(N)*A(IX(N),Y))
      B(2,Y)=B(2,Y)+(E(N)*A(IX(N),Y))
7767 CONTINUE
      NSAVE=N
      IG=IG+1
      NUMIN(:1)='6'
      GOTO 2600
ENDIF
C----- END OF ADD A GROUP BLOCK -----
C
C----- DELETE A GROUP BLOCK -----

```



```

        IF((NUMIN(:1).EQ.'7').OR.(NUMIN(:1).EQ.'D'))THEN
            IACT=0
7667      WRITE(*,747)
747      FORMAT('0',10X,'ENTER # OF GROUP TO BE DELETED')
            READ(*,3)NUMIN
            CALL READCHAR(NUMIN)
            IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
            IF(((ICCHAR(NUMIN(:1))).GT.57).OR.((ICCHAR(NUMIN(:1))).LT.48))
+THEN
                CALL CLS
                WRITE(*,*)'   ERROR : ENTER ONLY THE GROUP NUMBER'
                CALL LINES(0,2)
                WRITE(*,*)'   { hit return to continue }'
                READ(*,3)NUL
                GOTO 10000
            ENDIF
            CALL READNUM(NUMIN,RNUM,IADD,FLG)
            IF (FLG.EQ.1)THEN
                FLG=0
                GOTO 10000
            ENDIF
C NOW WE HAVE THE GROUP ID #
            DO 7776 Y=1,7
                B(1,Y)=B(1,Y)-(E(IADD)*A(IX(IADD),Y))
                B(2,Y)=B(2,Y)-(E(IADD)*A(IX(IADD),Y))
7776      CONTINUE

C WE SHIFT THE GROUPS IN ARRAY TO PUT VACANCY AT END OF ARRAY
C THEN SHORTEN THE ARRAY BY 1
            DO 11111 III=1,N
                IF(III.GT.IADD)THEN
                    IX(III-1)=IX(III)
                    CS(1,III-1)=CS(1,III)
                    CS(2,III-1)=CS(1,III)
                    E(III-1)=E(III)
                    EP(III-1)=EP(III)
                ENDIF
11111      CONTINUE
            N=N-1
            IG=IG-1
            NSAVE=N
            NUMIN(:1)='7'
            GOTO 2600
        ENDIF
C----- END OF DELETE A GROUP BLOCK -----
C
C----- CHANGE A GROUP -----
2021      IF((NUMIN(:1).EQ.'8').OR.(NUMIN(:1).EQ.'C'))THEN
            CONTINUE
                IF(ISTAT.EQ.1)THEN
                    WRITE(*,*)'   ENTRY NOT FOUND'
                    ISTAT=0
                ENDIF
            WRITE(*,2020)

```

```

2020     FORMAT('0',10X,'ENTER # OF GROUP TO CHANGE')
        READ(*,3)NUMIN
        IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
        IF(((ICCHAR(NUMIN(:1))).GT.57).OR.((ICCHAR(NUMIN(:1))).LT.48))
+THEN
        CALL CLS
        WRITE(*,*)'  ERROR : ENTER ONLY THE GROUP NUMBER'
        CALL LINES(0,2)
        WRITE(*,*)'      { hit return to continue }'
        READ(*,3)NUL
        GOTO 2021
        ENDIF
        CALL READNUM(NUMIN,RNUM,IADD,FLG)
        IF (FLG.EQ.1)THEN
            FLG=0
            GOTO 10000
        ENDIF
C  NOW WE HAVE THE GROUP ID #
        WRITE(*,2022)
2022     FORMAT('0',10X,'{ 1 - NEW GROUP ID }')
        WRITE(*,2023)
2023     FORMAT(' ',10X,'{ 2 - DIFFERENT QUANTITY }')
        WRITE(*,2024)
2024     FORMAT(' ',10X,'{ 3 - CHANGE BOTH ID & QUANTITY }')
        WRITE(*,2025)
2025     FORMAT('0',10X,' enter option : { Q }')
        read(*,3)NUMIN
        CALL READCHAR(NUMIN)
            IF(NUMIN(:1).EQ.'2')GOTO 88889
        IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
        IF ((NUMIN(:1).EQ.'3').OR.(NUMIN(:1).EQ.'1'))THEN
            IF(NUMIN(:1).EQ.'1')ESAVE=E(IADD)
            DO 8776 Y=1,7
                B(1,Y)=B(1,Y)-(E(IADD)*A(IX(IADD),Y))
                B(2,Y)=B(2,Y)-(E(IADD)*A(IX(IADD),Y))
8776     CONTINUE
            IACT=0
8766     CALL READGR(IADD,CS,TOT,IACT,MM1)
            IF(IACT.EQ.0)GOTO 8765
            IF(IACT.EQ.1)THEN
                IACT=0
                GOTO 10000
            ENDIF
            IF(IACT.EQ.3)THEN
                IENTRY=0
                CALL LISTGR(AS,A,NGRPT,IFIRST,ILAST,IENTRY,IHELP,NE1,IE1)
                CALL CLS
                IACT=0
                NUMIN(:1)='8'
                GOTO 2600
            ENDIF
            IF(IACT.EQ.2)THEN
                CALL CLS
                IACT=0

```

```

        WRITE(*,*)'                USE OPTION 2 TO DELETE A GROUP'
        CALL LINES(0,4)
        WRITE(*,*)'                { hit return to continue }'
        READ(*,3)NUL
        NUMIN(:1)='8'
        GOTO 2600
    ENDIF
8765    CONTINUE
        ISTAT=0
        CALL FINDGR(AS,NGRPT,CS,IX,IADD,ISTAT,MM1)
        IF(ISTAT.EQ.1)THEN
            NUMIN(:1)='8'
            GOTO 2600
        ENDIF
        CS(2,IADD)=CS(1,IADD)
        IF((IX(IADD).LE.ILAST(3)).AND.(IX(IADD).GE.IFIRST(3)))FLAG=1
        IF((IX(IADD).LE.ILAST(4)).AND.(IX(IADD).GE.IFIRST(4)))THEN
            CALL CLS
            WRITE(*,*)'                ERROR : YOU CANNOT ENTER'
            WRITE(*,*)'                BOND DISSOCIATION GROUPS'
            WRITE(*,*)'                ON THIS SCREEN'
            CALL LINES(0,3)
            WRITE(*,*)'                { hit return to continue }'
            call lines(0,3)
            READ(*,3)NUMIN
            NUMIN(:1)='8'
            GOTO 2600
        ENDIF
        IF(NUMIN(:1).EQ.'3')E(IADD)=TOT
        IF(NUMIN(:1).EQ.'3')EP(IADD)=TOT
        IF(NUMIN(:1).EQ.'1')E(IADD)=ESAVE
        DO 8767 Y=1,7
            B(1,Y)=B(1,Y)+(E(IADD)*A(IX(IADD),Y))
            B(2,Y)=B(2,Y)+(E(IADD)*A(IX(IADD),Y))
8767    CONTINUE
            NUMIN(:1)='8'
            GOTO 2600
        ENDIF
88889    CONTINUE
        IF(NUMIN(:1).EQ.'2')THEN
            WRITE(*,8790)IADD
8790    FORMAT('0',10X,' ENTER NEW QUANTITY FOR GR#,2X,13)
            READ(*,3)NUMIN
            IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.' '))GOTO 10000
            CALL READNUM(NUMIN,RNUM,ES,FLG)
            IF(FLG.EQ.1)THEN
                FLG=0
                NUMIN(:1)='8'
                GOTO 2600
            ENDIF
            DO 9767 Y=1,7
                B(1,Y)=B(1,Y)+((ES-E(IADD))*A(IX(IADD),Y))
                B(2,Y)=B(2,Y)+((ES-E(IADD))*A(IX(IADD),Y))
9767    CONTINUE

```

```

                E(IADD)=ES
                EP(IADD)=ES
                IF (ES.EQ.0)THEN
C WE SHIFT THE GROUPS IN ARRAY TO PUT VACANCY AT END OF ARRAY
C THEN SHORTEN THE ARRAY BY 1
                DO 22222 III=1,N
                    IF(III.LE.1)GOTO 22222
                    IF(III.GT.IADD)THEN
                        E(III-1)=E(III)
                        EP(III-1)=EP(III)
                        CS(1,III-1)=CS(1,III)
                        CS(2,III-1)=CS(1,III)
                        IX(III-1)=IX(III)
                    ENDIF
22222          CONTINUE
                N=N-1
                IG=IG-1
                NSAVE=N
                ENDIF
                NUMIN(:1)='8'
                GOTO 2600
                ENDIF
            ENDIF
C----- END OF CHANGE A GROUP BLOCK -----
C
C*****
C  END OF MAIN BLOCK FOR GROUP OPERATIONS
C*****
                ENDIF
9999 WRITE(*,*)'ERROR IN INPUT OR OPTION IS NOT YET AVAILABLE'
                WRITE(*,*) '
                WRITE(*,*)' (hit return to continue)'
                READ(*,3)NUL
999  CONTINUE
                RETURN
                END

```

```

SUBROUTINE READNUM(NUMIN,RNUM,NUM,FLG)
C THIS SUBROUTINE RETURNS NUMERIC VALUE OF CHARACTER IF IT EXISTS
C ELSE USER IS PROMPTED TO RE-ENTER NUMERIC VALUE
CHARACTER*(*) NUMIN
REAL RNUM,RNUM(132)
INTEGER NUM,FLG,M,INTG,MDOT,FLAG,MULT,MULTFL
INTEGER INUM(132),NUM1
CALL DBLNK(NUMIN,LEN,0)
5 FLAG=0
  FLG=0
  M=0
    NUM1=0
  NUM=0
  RNUM=0.0
  MDOT=0
  INTG=0
  MULT=1
  MULTFL=0
  I=1
C IF NUMIN IS A NULL STRING NUM DEFAULTS TO NUM=1
  IF(NUMIN.EQ.' ')THEN
    NUM1=1
    NUM=1
    RNUM=1.0
    GOTO 400
  ENDIF
100 M=ICHAR(NUMIN(I:I))
  IF(M.EQ.32)THEN
    I=I-1
    GOTO 200
  ENDIF
  IF(NUMIN(I:I).EQ.'-')THEN
    MULT=INT(-1.0)
    MULTFL=I
    I=I+1
    GOTO 100
  ENDIF
  IF(NUMIN(I:I).EQ.'.')THEN
    MDOT=I
    INTG=I-1
    I=I+1
    FLAG=1
    GOTO 100
  ENDIF
34 IF (((M.GT.57).OR.(M.LT.45).OR.(M.EQ.47)))THEN
  CALL CLS
  FLAG=0
  WRITE(*,*)' '
  WRITE(*,*)' ERROR IN NUMERIC INPUT'
  WRITE(*,*)' NUMERIC EXPRESSION EXPECTED'
  WRITE(*,'(1X,A)')NUMIN,NUMIN(I:I)
  WRITE(*,*)' PLEASE RE-ENTER (Q = "QUIT")'
  READ(*,3)NUMIN

```

```

3      FORMAT(A)
      IF((NUMIN(:1).EQ.'Q').OR.(NUMIN(:1).EQ.'q'))THEN
          FLG=1
          GOTO 400
      ENDIF
      GOTO 5
  ENDF
  IF((M.GE.48).AND.(M.LE.57))THEN
      INUM(I)=M-48
      I=I+1
      GOTO 100
  ENDF
200 CONTINUE
  DO 300 J=1,I
      IF(MDOT.EQ.0)INTG=I
      IF(J.EQ.MULTFL)GOTO 300
      IF(J.EQ.MDOT)GOTO 300
      IF((MDOT.NE.0).AND.(J.GT.MDOT))GOTO 233
      INUM(J)=(10**(INTG-J))*INUM(J)
      NUM1=NUM1+INUM(J)
      RNUM=RNUM+(1.0*INUM(J))
      GOTO 300
233   RENUM(J)=((INUM(J)*1.0)/(10.0**(J-MDOT)))
      RNUM=RNUM+RENUM(J)
300 CONTINUE
400 CONTINUE
      RNUM=RNUM*FLOAT(MULT)
      NUM1=NUM1*MULT
      IF(NUM1.GT.32000)THEN
          NUM=0
      ELSE
          NUM=NUM1
      ENDIF
      RETURN
  END

```

```

SUBROUTINE DEBLNK(S1,S2,LST,CCSW)
CHARACTER*(*) S1,S2
INTEGER LS1,CCSW,FLG
FLG=0
LST=LEN(S1)
NNB=0
KOUNT=0
3   FORMAT(A70)
    S2=S1
    DO 100 I=1,LST
    IF(S1(I:I).NE.' ')NNB=NNB+1
    IF(S1(I:LST).EQ.' ')THEN
        LST=I-1
        GOTO 450
    ENDIF
100  CONTINUE
450  CONTINUE
400  I=1
    KOUNT=KOUNT+1
300  CONTINUE
    IF(I.GT.LST)GOTO 200
    IF(S1(I:I).EQ.' '.AND.(CCSW.EQ.0.OR.I.EQ.1))THEN
        S1(I:LST-1)=S1(I+1:LST)
        S1(LST:LST)=' '
        LST=LST-1
    ENDIF
    IP1=I+1
    IF(S1(I:I).EQ.' '.AND.S1(IP1:IP1).EQ.' '.AND.CCSW.EQ.1)THEN
        S1(I:LST-1)=S1(I+1:LST)
        S1(LST:LST)=' '
        LST=LST-1
    ENDIF
    I=I+1
    GOTO 300
200  CONTINUE
    IF(KOUNT.GT.LST)GOTO 500
    IF(LST.GT.NNB)GOTO 400
500  CONTINUE
    RETURN
END

```

```

SUBROUTINE DBLNK(S1,LST,CCSW)
CHARACTER*(*) S1
INTEGER LS1,CCSW,FLG
FLG=0
LST=LEN(S1)
NNB=0
KOUNT=0
3   FORMAT(A70)
DO 100 I=1,LST
IF(S1(I:I).NE.' ')NNB=NNB+1
IF(S1(I:LST).EQ.' ')THEN
    LST=I-1
    GOTO 450
ENDIF
100 CONTINUE
450 CONTINUE
400 I=1
KOUNT=KOUNT+1
300 CONTINUE
IF(I.GT.LST)GOTO 200
IF(S1(I:I).EQ.' '.AND.(CCSW.EQ.0.OR.I.EQ.1))THEN
    S1(I:LST-1)=S1(I+1:LST)
    S1(LST:LST)=' '
    LST=LST-1
ENDIF
IP1=I+1
IF(S1(I:I).EQ.' '.AND.S1(IP1:IP1).EQ.' '.AND.CCSW.EQ.1)THEN
    S1(I:LST-1)=S1(I+1:LST)
    S1(LST:LST)=' '
    LST=LST-1
ENDIF
I=I+1
GOTO 300
200 CONTINUE
IF(KOUNT.GT.LST)GOTO 500
IF(LST.GT.NNB)GOTO 400
500 CONTINUE
RETURN
END

```



```

SUBROUTINE FORMINT(FORM,LEN1,IE,NE,NATOMT,IENTRY)
$LARGE
CHARACTER*2 ELEM(50)
CHARACTER*70 FORM,DUMMY
CHARACTER*4 IE(4),IES(4),IE1(4,400),B,C,TMP
INTEGER NE(4),M,M1,N(4),L,ITEMP,LEN1,ID(70),NOC1(70),
+ NOC2(70),IN2C(35,4),IN1C(70,4),I2CH(35),I1CH(50),N2CH,N1CH,
+ IFM(4),IG(35),NG,INUM(70),NUMBER(70),NNUM,NES(4),NLP,IDLP(70),
+ NRP,IDRP(70),NSLASH,IDSLSH(70),IFOUND(4),NE1(4,400),NNZERO,
+ NELT(20),IELEM(10),NEL(20),IEL(4),ISSQ(20)
COMMON/CONFIG1/ELEM
COMMON/CONFIG2/NELEM,N1CH,N2CH,I1CH,I2CH
DO 234 I=1,NELEM
234 NELT(I)=0
DO 123 I=1,4
NES(I)=0
NE(I)=0
IES(I)=' '
123 IE(I)=' '
DO 345 I=1,LEN1
IF(FORM(I:I).EQ.'['.OR.FORM(I:I).EQ.'(')FORM(I:I)='('
IF(FORM(I:I).EQ.'],'.OR.FORM(I:I).EQ.')]')FORM(I:I)=')')
345 CONTINUE
NSUBS=0
NATOMT=0
NATOM1=0
IF(LEN1.EQ.1)THEN
IE(1)(:1)=FORM(:1)
NE(1)=1
NATOM=1
GOTO 71
*
* XFER TO OUTPUT/RETURN BLOCK
ENDIF
*****
* SEARCH FOR NUMERIC CHARACTERS *
*****
CALL INDXNUM(FORM,LEN1,NNUM,NUMBER,INUM,KFLG)
*****
*
*****
* SEARCH FOR PARENTHESES
*****
CALL INDXST(FORM,'(',NLP,IDLP,LEN1,1,KFLG)
CALL INDXST(FORM,')',NRP,IDRP,LEN1,1,KFLG)
CALL INDXST(FORM,'/',NSLASH,IDSLSH,LEN1,1,KFLG)
*****
IF(NLP.EQ.0.AND.NRP.EQ.0.AND.NSLASH.EQ.0)THEN
CALL FINTERP(FORM,LEN1,IE,NE,NATOMT,IENTRY)
GOTO 71
*
* XFER TO OUTPUT/RETURN BLOCK
ELSE IF(NSLASH.NE.0.AND.(NLP.NE.0.OR.NRP.NE.0))THEN
*
CAN'T MIX STRING OPTIONS
IENTRY=-3
GOTO 71

```

```

*                                     XFER TO OUTPUT/RETURN BLOCK
ELSE IF(NLP.NE.NRP)THEN
*       UNBALANCED PARENTHESES
        IENTRY=-2
        GOTO 71
*                                     XFER TO OUTPUT/RETURN BLOCK
ELSE IF(NSLASH.NE.0)THEN
*       DECOMPOSE SUBSTRINGS AND PASS PIECEWISE
        IF(NSLASH.EQ.1.AND.IDSLSH(1).EQ.1)THEN
            IENTRY=-4
            GOTO 71
*                                     XFER TO OUTPUT/RETURN BLOCK
        ENDIF
        IF(IDSLSH(1).NE.1)THEN
            DUMMY=' '
            DUMMY=FORM(:IDSLSH(1)-1)
            CALL SLEN(DUMMY,LENS)
            CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
            NATOMT=NATOMT+NATOM1
            NSUBS=1
            DO 1001 IK=1,4
                IE1(IK,1)=IES(IK)
                NE1(IK,1)=NES(IK)
1001
            ENDIF
            DO 2001 JK=1,NSLASH-1
                DUMMY=' '
                IF(IDSLSH(JK)+1.GT.IDSLSH(JK+1)-1)GOTO 2001
                NSUBS=NSUBS+1
                DUMMY=FORM(IDSLSH(JK)+1:IDSLSH(JK+1)-1)
                CALL SLEN(DUMMY,LENS)
                CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
                NATOMT=NATOM1+NATOMT
                DO 1002 IK1=1,4
                    IE1(IK1,1+JK)=IES(IK1)
                    NE1(IK1,1+JK)=NES(IK1)
1002
2001
                CONTINUE
                IF(LEN1.NE.IDSLSH(NSLASH))THEN
                    DUMMY=' '
                    NSUBS=NSUBS+1
                    DUMMY=FORM(IDSLSH(NSLASH)+1:LEN1)
                    CALL SLEN(DUMMY,LENS)
                    CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
                    NATOMT=NATOM1+NATOMT
                    DO 1003 IK1=1,4
                        IE1(IK1,NSUBS)=IES(IK1)
                        NE1(IK1,NSUBS)=NES(IK1)
1003
                    ENDIF
                    GOTO 81
*       SUM ELEMENTS OVER ALL SUBSTRINGS
ELSE IF(NLP.EQ.NRP)THEN
*       DECOMPOSE PARENTHETICAL SUBSTRINGS AND PASS
        DO 5101 J=1,NRP
        DO 5201 I=J,NNUM
            ISSQ(J)=1

```

```

                IF(INUM(I).EQ.IDRP(J)+1)THEN
                    ISSQ(J)=NUMBER(I)
                    GOTO 5101
                ENDIF
5201          CONTINUE
5101          CONTINUE
                DO 6301 I=1,NRP-1
                IF(IDRP(I).GT.IDLP(I+1))THEN
                    WRITE(*,*)' TOO MANY LEVELS OF PARENTHESES'
                    PAUSE ' hit return to continue'
                    IENTRY=-6
                    GOTO 71
                ENDIF
6301          CONTINUE
                IF(IDRP(NRP).LT.IDLP(NLP))THEN
                    WRITE(*,*)' TOO MANY LEVELS OF PARENTHESES'
                    PAUSE ' hit return to continue'
                    IENTRY=-6
                    GOTO 71
                ENDIF
                IF(IDLP(1).NE.1)THEN
                    DUMMY=' '
                    DUMMY=FORM(:IDLP(1)-1)
                    NSUBS=NSUBS+1
                    CALL SLEN(DUMMY,LENS)
                CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
                    NATOMT=NATOMT+NATOM1
                    DO 5001 IK=1,4
                    IE1(IK,NSUBS)=IES(IK)
                    NE1(IK,NSUBS)=NES(IK)
5001          format(1x,4(4x,a4,i3))
787          ENDIF
                DO 6201 J=1,NRP
                NCHARN=1
                DUMMY=' '
                IF(ISSQ(J).GT.9)NCHARN=2
                IF(ISSQ(J).GT.99)NCHARN=3
                IF(ISSQ(J).GT.999)NCHARN=4
                IF(ISSQ(J).GT.9999)NCHARN=5
                IF(J.LT.NRP)THEN
                    IF(IDLP(J+1)-1.EQ.IDRP(J))GOTO 6201
                    IF(IDRP(J)+NCHARN+1.LT.IDLP(J+1))THEN
                        DUMMY=FORM(IDRP(J)+NCHARN+1:IDLP(J+1)-1)
                        GOTO 91
                    ENDIF
                ENDIF
91          GOTO 6201
                CONTINUE
                CALL SLEN(DUMMY,LENS)
                CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
                NATOMT=NATOM1+NATOMT
                NSUBS=NSUBS+1
                DO 5301 IK=1,4

```

```

      IE1(IK,NSUBS)=IES(IK)
5301      NE1(IK,NSUBS)=NES(IK)
6201      CONTINUE

              IF(IDRP(NRP)+NCHARN+1.LE.LEN1)THEN
                      DUMMY=FORM(IDRP(NRP)+NCHARN+1:LEN1)
                      CALL SLEN(DUMMY,LENS)
      CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
                      NATOMT=NATOM1+NATOMT
                      NSUBS=NSUBS+1
                      DO 5321 IK=1,4
                                IE1(IK,NSUBS)=IES(IK)
5321                                NE1(IK,NSUBS)=NES(IK)

      ENDIF
      DO 6001 J=1,NRP
      DUMMY=' '
      DUMMY=FORM(IDLP(J)+1:IDRP(J)-1)
      CALL SLEN(DUMMY,LENS)
      CALL FINTERP(DUMMY,LENS,IES,NES,NATOM1,IENTRY)
      NATOMT=(NATOM1*ISSQ(J))+NATOMT
      NSUBS=NSUBS+1
      DO 5401 IK=1,4
                IE1(IK,NSUBS)=IES(IK)
5401                NE1(IK,NSUBS)=(NES(IK)*ISSQ(J))
6001      CONTINUE
      GOTO 81

*          SUM ELEMENTS OVER ALL SUBSTRINGS
      ENDIF
*****
*          SUBSTRING ELEMENT SUMMATION BLOCK
*****
81          CONTINUE
      DO 850 IK2=1,NSUBS
      CALL NATOMS(IK2,IE1,NE1,IEL,NEL,NATOM)
      DO 950 I1=1,4
1950      NELT(IEL(I1))=NELT(IEL(I1))+NEL(IEL(I1))
850      CONTINUE
      NNZERO=0
      DO 750 I1=1,NELEM
      IF(NELT(I1).NE.0)THEN
              NNZERO=NNZERO+1
              IELEM(NNZERO)=I1

      ENDIF
750      CONTINUE
      IF(NNZERO.GT.4)THEN
              IENTRY=-1
              GOTO 71

*          XFER TO OUTPUT/RETURN BLOCK

      ENDIF
      DO 650 I1=1,NNZERO
      NE(I1)=NELT(IELEM(I1))
      IE(I1)=ELEM(IELEM(I1))
650      CONTINUE
*****
*          OUTPUT/RETURN BLOCK

```

```
*****  
71      CONTINUE  
      IF(IENTRY.EQ.0)THEN  
          WRITE(*,*)'FORMULA ENTERED :'  
          WRITE(*,*)FORM  
          call lines(0,2)  
          WRITE(*,*)' ELEMENTAL COMPOSITION:'  
          call lines(0,1)  
          DO 23 I=1,4  
23      WRITE(*,*)IE(I),NE(I)  
      ENDIF  
      RETURN  
      END
```

```

SUBROUTINE INDXNUM(S1,LEN1,N,NUM,IND,KFLG)
$LARGE
CHARACTER*(*) S1,S2*14
INTEGER N,NUM(132),IND(132),KFLG,LEN1,ITMP(132),NOC
70  FORMAT(A)
    KFLG=0
    N=0
    LSTR=LEN(S1)
    DO 10 I=1,LSTR
10  IND(I)=0
    NOC=0
    DO 200 I=1,LEN1
    IF(ICHAR(S1(I:I)).LE.57.AND.ICHAR(S1(I:I)).GE.48)THEN
        NOC=NOC+1
        ITMP(NOC)=I
    ENDIF
200  CONTINUE
    IF(NOC.EQ.0)THEN
        KFLG=1
        RETURN
    ENDIF
    IF(NOC.EQ.1)THEN
        N=1
        S2=S1(ITMP(1):ITMP(1))
        CALL READNUM(S2,RN,NUM(1),KFLG)
        IND(1)=ITMP(1)
        RETURN
    ENDIF
    I=0
3000 I=I+1
    IF(ITMP(I).NE.ITMP(I+1)-1)THEN
        N=N+1
        S2=S1(ITMP(I):ITMP(I))
        CALL READNUM(S2,RN,NUM(N),KFLG)
        IND(N)=ITMP(I)
    ELSE IF(ITMP(I).EQ.ITMP(I+1)-1)THEN
        N=N+1
        S2=S1(ITMP(I):ITMP(I+1))
        CALL READNUM(S2,RN,NUM(N),KFLG)
        IND(N)=ITMP(I)
        I=I+1
    ENDIF
    IF(I.LT.NOC-1)GOTO 3000
    IF(ITMP(NOC-1)+1.NE.ITMP(NOC))THEN
        N=N+1
        S2=S1(ITMP(NOC):ITMP(NOC))
        CALL READNUM(S2,RN,NUM(N),KFLG)
        IND(N)=ITMP(NOC)
    ENDIF
    RETURN
END

```

```

SUBROUTINE FINTERP(FORM,LEN1,IE,NE,NATOM,IENTRY)
$LARGE
CHARACTER*2 ELEM(50)
CHARACTER*70 FORM,DUMMY
CHARACTER*4 IE(4),B,C,IE1(70),TMP
INTEGER NE(4),M,M1,N(4),L,NE1(70),ITEMP,LEN1,ID(70),NOC1(70),
+ NOC2(70),IN2C(35,4),IN1C(70,4),I2CH(35),I1CH(50),N2CH,N1CH,
+ IFM(4),IG(35),NG,INUM(70),NUMBER(70),NNUM
COMMON/CONFIG1/ELEM
COMMON/CONFIG2/NELEM,N1CH,N2CH,I1CH,I2CH
* INITIALIZE ARRAYS
DO 1234 I=1,4
IE(I)=' '
1234 NE(I)=0
* IF(LEN1.EQ.1)GOTO 1000
*****
* SEARCH FOR NUMERIC CHARACTERS *
*****
CALL INDXNUM(FORM,LEN1,NNUM,NUMBER,INUM,KFLG)
*****
* BEGIN SEARCH FOR 2 CHARACTER ELEMENTS *
*****
I1=0
DO 1000 I=1,N2CH
DUMMY=ELEM(I2CH(I))(:2)
CALL INDXST(FORM,DUMMY,NOC,ID,LEN1,2,KFLG)
IF(NOC.NE.0)THEN
I1=I1+1
NOC2(I1)=NOC
IFM(I1)=I2CH(I)
DO 100 J=1,NOC
DO 150 K1=1,NNUM
IF(ID(J)+2.EQ.INUM(K1))THEN
NOC2(I1)=NOC2(I1)+NUMBER(K1)-1
ENDIF
150 CONTINUE
100 IN2C(J,I1)=ID(J)
ENDIF
NEL2=I1
NELTOT=I1
IF(NELTOT.GT.4)THEN
CALL CLS
WRITE(*,*)' ERROR : FORMULA APPEARS TO CONTAIN'
WRITE(*,*)' MORE THAN 4 ELEMENTS and CANNOT BE'
WRITE(*,*)' PUT INTO NASA FORMAT FOR USE WITH CHEMKIN.'
3 READ(*,3)B
FORMAT(A4)
IENTRY=-1
RETURN
ENDIF
1000 CONTINUE

```

```

*
*****
*          BEGIN SEARCH FOR 1 CHARACTER ELEMENTS          *
*****
      I1=0
      N1C=0
      DO 2000 I=1,N1CH
      DUMMY=ELEM(I1CH(I))(:1)
      N1CS=N1C
      CALL INDXST(FORM,DUMMY,NOC,ID,LEN1,1,KFLG)
      IF(NOC.NE.0)THEN
          ISAME=0
          I1=I1+1
      DO 30 J=1,NEL2
      IF(ELEM(I1CH(I))(:1).EQ.ELEM(IFM(J))(:1))THEN
          ISAME=1
          NO1CA=0
          NG=0
      DO 41 I3=1,NOC
      DO 40 I2=1,NOC2(J)
          IF(ID(I3).EQ.IN2C(I2,J))THEN
              NG=NG+1
              IG(NG)=I3
          ENDIF
40      CONTINUE
41      CONTINUE
      DO 45 I2=1,NOC
      IST=0
          DO 46 I3=1,NG
          IF(I2.EQ.IG(I3))IST=1
          IF(IST.EQ.0)THEN
              NO1CA=NO1CA+1
          DO 350 K1=1,NNUM
          IF(ID(I2)+1.EQ.INUM(K1))THEN
              NO1CA=NO1CA+NUMBER(K1)-1
          ENDIF
350      CONTINUE
              IN1C(I2,I1)=ID(I2)
          ENDIF
45      CONTINUE
      ENDIF
30      CONTINUE
      IF(ISAME.EQ.0)THEN
          NOC1(I1)=NOC
          IFM(NEL2+I1)=I1CH(I)
          DO 50 I2=1,NOC
          DO 250 K1=1,NNUM
          IF(ID(I2)+1.EQ.INUM(K1))THEN
              NOC1(I1)=NOC1(I1)+NUMBER(K1)-1
          ENDIF
250      CONTINUE
50      IN1C(I2,I1)=ID(I2)
          NIC=I1

```



```

ELSE IF(ISAME.NE.0)THEN
    IF(NO1CA.EQ.0)THEN
        I1=I1-1
    ELSE IF(NO1CA.NE.0)THEN
        IFM(NEL2+I1)=I1CH(I)
        NOC1(I1)=NO1CA
    ENDIF
    NIC=I1
ENDIF
IF(NEL2+I1.GT.4)THEN
    CALL CLS
    WRITE(*,*)' ERROR : FORMULA APPEARS TO CONTAIN'
    WRITE(*,*)' MORE THAN 4 ELEMENTS and CANNOT BE'
    WRITE(*,*)' PUT INTO NASA FORMAT FOR USE WITH CHEMKIN.'
    READ(*,3)B
    IENTRY=-1
    RETURN
ENDIF
ENDIF
2000 CONTINUE
NEL1=I1
NATOM=0
DO 324 J2=1,NEL1
324     NATOM=NATOM+NOC1(J2)
DO 325 J2=1,NEL2
325     NATOM=NATOM+NOC2(J2)
DO 60 I=1,NEL2
60     IE(I)(:2)=ELEM(IFM(I))
    NE(I)=NOC2(I)
DO 70 I=1,NEL1
70     IE(I+NEL2)(:2)=ELEM(IFM(I+NEL2))
    NE(I+NEL2)=NOC1(I)
71 CONTINUE
RETURN
END

```

```

SUBROUTINE SLEN (S1,LSTR)
$LARGE
CHARACTER*(*) S1
INTEGER LSTR, I
LSTR=LEN(S1)
IF(S1.EQ.' ')THEN
    LSTR=0
    GOTO 2000
ENDIF
J=0
1000 I=I+1
IF(S1(I+1:LSTR).EQ.' ')THEN
    LSTR=I
ELSEIF(I.LE.LSTR)THEN
    GOTO 1000
ENDIF
2000 CONTINUE
RETURN
END

```

```

SUBROUTINE INDXST(S1,S2,N,INDX,LS1,LS2,FLG)
$LARGE
CHARACTER S1*(*),S2*(*)
INTEGER N,INDX(*),LS1,LS2,FLG
*****
*
* SUBROUTINE INDXST : INDeX STring
*
*
* The purpose of this subroutine is to search string S1 (arbitrary
* length) for all occurrences of substring S2. S2 must be shorter
* than S1. Returned are the number of occurrences of S2 in S1; the
* vector of starting addresses of each occurrence; string lengths for
* both S1 and S2 if not supplied; and an error flag.
*
* Variable definitions:
* S1 - input string to be searched (character length defined by
* calling routine).
* S2 - target substring; length determined by calling routine.
* N - number of occurrences of substring S2 in S1.
* INDX(*)- vector giving the starting address for each occurrence of
* S2 in S1.
* LS1- length (non-blank) of S1; if not supplied it is determined
* and returned to the calling routine.
* LS2- length ( = 1 for a single blank ) of target substring S2;
* if not supplied it is determined and returned to the calling
* routine.
* FLG- error flag. FLG = 0 if no error encountered
* FLG < 0 if LS2 > LS1 or other error occurs
*
*
*****
LMAX=LEN(S1)
DO 10 I=1,LMAX
10 INDX(I)=0
N=0
FLG=0
* DETERMINE STRING LENGTH IF NOT PASSED TO THIS ROUTINE
IF(LS1.EQ.0.AND.LS2.EQ.0)THEN
DO 100 I=1,LMAX
IP1=I+1
IF(I.GT.1)THEN
IM1=I-1
ELSE
IM1=1
ENDIF
IF(LS1.EQ.0.AND.S1(I:I).EQ.' ' .AND.S1(IP1:IP1).EQ.' ')
+ LS1=IM1
IF(LS2.EQ.0.AND.S2(I:I).EQ.' ' .AND.S2(IP1:IP1).EQ.' ')
+ LS2=IM1
100 CONTINUE
ENDIF
150 CONTINUE
IF(LS1.LT.LS2)THEN

```

```
                FLG=-10
                RETURN
            ENDF
        IFOUND=0
        DO 200 I=1,LS1
            I2=I+LS2-1
            IF((I2-1).GT.LS2)GOTO 200
            IF(S1(I:I2).EQ.S2(:LS2))THEN
                IFOUND=IFOUND+1
                INDX(IFOUND)=I
            ENDF
200    CONTINUE
        N=IFOUND
        RETURN
    END
```

```

SUBROUTINE MATBAL(NLHS,LX,NRHS,RX,IE1,NE1,COEF,IERR)
  INTEGER LX(*),RX(*),NE1(4,400),IELL(4),NELL(50),IELR(4),
+NELR(20),NELLT(20),NELRT(20),NELEM,I1CH(50),I2CH(35),LNATOM,
+RNATOM
  REAL*8 COEF(*),DNELL(50),DNELLT(50),DNELR(50),DNELRT(50)
  CHARACTER*4 IE1(4,400)
  CHARACTER*2 ELEM(50)
  COMMON/CONFIG1/ELEM
  COMMON/CONFIG2/NELEM,N1CH,N2CH,I1CH,I2CH
  DO 10 I=1,NELEM
    DNELLT(I)=0.0
    DNELL(I)=0.0
    NELLT(I)=0
    DNELR(I)=0.0
    DNELRT(I)=0.0
10    NELRT(I)=0
    LNATOM=0
    RNATOM=0
    DO 800 I=1,NLHS
      CALL NATOMS(LX(I),IE1,NE1,IELL,NELL,NATOM)
      DO 850 I1=1,NELEM
        DNELL(I1)=COEF(I)*FLOAT(NELL(I1))
        DNELLT(I1)=DNELLT(I1)+DNELL(I1)
850      CONTINUE
      LNATOM=NATOM
800      CONTINUE
      DO 900 I=1,NRHS
        CALL NATOMS(RX(I),IE1,NE1,IELL,NELL,NATOM)
        DO 950 I1=1,NELEM
          DNELR(I1)=COEF(I+NLHS)*FLOAT(NELL(I1))
          DNELRT(I1)=DNELRT(I1)+DNELR(I1)
950        CONTINUE
        RNATOM=NATOM
900        CONTINUE
      DO 1000 I=1,NELEM
        IF(INT(100.*DNELRT(I)).NE.INT(100.*DNELLT(I)))THEN
          WRITE(*,*)' REACTION DOES NOT BALANCE!'
          WRITE(*,*)'# of ',ELEM(I),' on LHS= ',DNELLT(I)
          WRITE(*,*)'# of ',ELEM(I),' on RHS= ',DNELRT(I)
          IERR=1
          RETURN
        ENDIF
1000      CONTINUE
      IERR=0
      RETURN
    END
  END

```

```

SUBROUTINE NATOMS(J,IE1,NE1,IEL,NEL,NATOM)
INTEGER NE1(4,400),NELEM,N1CH,N2CH,I1CH(50),I2CH(35),IEL(*),
+NEL(*),NATOM
CHARACTER*2 ELEM(50)
CHARACTER*4 IE1(4,400)
CHARACTER*14 NUL
COMMON/CONFIG1/ELEM
COMMON/CONFIG2/NELEM,N1CH,N2CH,I1CH,I2CH
DO 10 I=1,4
10  IEL(I)=0
DO 20 I=1,NELEM
20  NEL(I)=0
NATOM=0
I1=0
DO 1000 I=1,4
DO 1050 K=1,NELEM
IF(ELEM(K)(:2).EQ.IE1(I,J)(:2))THEN
I1=I1+1
IEL(I1)=K
NEL(K)=NEL(K)+NE1(I,J)
ENDIF
1050 CONTINUE
1000 CONTINUE
RETURN
END

```

```

SUBROUTINE ATOMSORT(ISORT,NE1,IE1,ICNT,KEY)
  INTEGER ISORT(1),NE1(4,400),ICNT,LEVEL,KEY(10),IL1(50),
+IL2(50),INC,ICTRL,IK,J,I,K,ITMP,NELEM,N1CH,N2CH,I1CH(50),
+I2CH(35),IEL(4),NEL(50)
  CHARACTER*2 ELEM(50)
  CHARACTER*4 IE1(4,400)
  CHARACTER*14 NUL
  COMMON/CONFIG1/ELEM
  COMMON/CONFIG2/NELEM,N1CH,N2CH,I1CH,I2CH
  COMMON/CONFIG5/NKEYS
C   INITIALIZE INDIRECT ADDRESS VECTOR: ISORT
  DO 10 I=1,ICNT
10  ISORT(I)=I
C   INITIALIZE DEFAULT SORT KEY VECTOR. KEY IS DEFINED AS THE FIRST
C       6 ELEMENTS LISTED IN FILE : "THERM.CFG"
  DO 20 I=1,NKEYS
20  KEY(I)=I
  DO 10000 LEVEL=1,NKEYS
  ICTRL=0
  J=0
  DO 1000 I=1,ICNT-1
    IF(ICTRL.EQ.1)RETURN
    ICTRL=1
    INC=1
    J=0
    DO 2000 IK=1,ICNT-I
      J=J+INC
    CALL NATOMS(ISORT(J),IE1,NE1,IEL,NEL,NATOM)
    DO 1500 I1=1,NELEM
1500  IL1(I1)=NEL(I1)
    CALL NATOMS(ISORT(J+INC),IE1,NE1,IEL,NEL,NATOM)
    DO 1600 I1=1,NELEM
1600  IL2(I1)=NEL(I1)
    IF(LEVEL.EQ.1)THEN
      K=LEVEL
      IF(IL2(KEY(K)).GT.IL1(KEY(K)))GOTO 2000
      GOTO 150
    ENDIF
    DO 100 K=1,LEVEL
      IF(IL2(KEY(K)).GT.IL1(KEY(K)))GOTO 2000
100  CONTINUE
150  CONTINUE
    ICTRL=0
    ITMP=ISORT(J)
    ISORT(J)=ISORT(J+INC)
    ISORT(J+INC)=ITMP
2000 CONTINUE
1000 CONTINUE
10000 CONTINUE
3   FORMAT(A14)
  CALL CLS
  RETURN
  END

```

```

SUBROUTINE LOADSP(AS,A,IFIRST,ILAST,NGRPT,CS,B,NG,NSAVE,SYMM,SYMS,
+SYMR,SCOR,SCORP,FORM,FORMP,SPECP,IE,NE,NATOM,FLAG,BFLAG,FLG,LS,RS,
+RS22,FILST,DOCFIL,IX,E,LENF,EP,FILNM,DOC,NDOC,TEXT,TEXTS,KOUNT,
+IOP,IDOC,NSPEC,BD,LENFP,IENTER,JC,DELB,DOCTYPE,KDOCT,DELTA)
LOGICAL EXST,OPNED
REAL*4 B(2,9),BO(9)
REAL A(400,9),SCOR,SCORP,DELTA(1)
INTEGER FLAG,BFLAG,FLG,SYMM,SYMS,SYMR,NG,NSAVE,NGRPT,ILAST(1),
+IFIRST(1),NE(1),NATOM,LNG(60),NOCCUR,IND(70),U,E(1),IX(1),Y,
+IND1,IND2,EP(50),IDOC(1),NSPEC,ICOUNT,KDOCT,JIND(70),NE1(4,400)
CHARACTER*70 TEXT(1),TEXTS(1)
CHARACTER*70 DOC1(100)
CHARACTER*14 DOC(1)
CHARACTER*70 SI,NUL,NUL1,DUMMY,FORM,FORMP,TXT,FILNM,FILNM2
CHARACTER*14 AS(1),NUMIN,SPEC,SPECP,CS(2,60),DOCFIL,RS,RS22,
+LS,DOCTYPE,DUM1,DUM2,DUM3,DUM4,A1,UNITS,FUNITS
CHARACTER*4 IE(1),IE1(4,400)
COMMON/DELETE/NDEL,IDEL(500)
COMMON/CONTRL/FIL
COMMON/CONFIG6/UNITS
COMMON/ELEM1/NE1
COMMON/ELEM2/IE1
COMMON/NROTOR/NROT,NROTS
70  FORMAT(A70)
    ILIST=0
    DO 10 II=1,KOUNT
        TEXT(II)=' '
        TEXTS(II)=' '
10  CONTINUE
    KOUNT=0
    DO 92 I=1,9
92  DELTA(I)=0.0
        IF(KDOCT.EQ.0.OR.KDOC.EQ.1)DOCTYPE=' '
        IF(KDOCT.EQ.2)DOCTYPE='NOCALC'
        LS=' '
        FORM=' '
        FORMP=' '
        SPEC=' '
        NUL=' '
        LEN=0
        SI=' '
        NG=0
        DO 20 I=1,9
20  B(1,I)=0
        B(2,I)=0
        IF(IENTER.EQ.1.AND.IOP.NE.0)THEN
            SPEC=SPECP
            IENTER=0
            J1=0
            GOTO 1777
        ENDIF
        IF((IENTER.EQ.2.OR.IENTER.EQ.10).AND.IOP.NE.0)THEN
            J1=JC

```

U=34


```

                GOTO 1878
ENDIF
SPECP=' '
IF(IOP.EQ.0)THEN
CALL CLS
WRITE(*,700)
WRITE(*,701)
700 FORMAT(' ',15X,'enter document filename')
701 FORMAT('0',15X,'for species input')
CALL LINES(0,2)
IF(FILNM.NE.' ')WRITE(*,708)FILNM
708 FORMAT(' ',1X,'( ',A70,' )')
READ(*,70)FILNM2
1  FORMAT(A14)
CALL READCHAR(FILNM2)
IF(FILNM2.EQ.'Q'.OR.(FILNM2.EQ.' '.AND.FILNM.EQ.' '))THEN
    FLG=1
    RETURN
ENDIF
IF(FILNM2.NE.' ')FILNM=FILNM2
CALL FNAME(FILNM,'DOC')
1000 INQUIRE(FILE=FILNM,EXIST=EXST,OPENED=OPNED,ERR=90000)
IF(OPNED)THEN
    INQUIRE(34,OPENED=OPNED)
    IF(OPNED)THEN
        U=34
        GOTO 1003
    ENDIF
    INQUIRE(52,OPENED=OPNED)
    IF(OPNED)THEN
        U=52
        GOTO 1003
    ENDIF
ENDIF
ENDIF
IF(EXST)THEN
    OPEN(34,FILE=FILNM,ACCESS='DIRECT',RECL=70,FORM='FORMATTED'
+,STATUS='OLD')
    U=34
    GOTO 1003
ENDIF
CALL CLS
WRITE(*,702)FILNM
702 FORMAT(' ',10X,A14,2X,'does not exist')
WRITE(*,703)
703 FORMAT(' ',10X,'( hit return to continue )')
READ(*,3)NUL
3  FORMAT(A70)
4  FORMAT(' ',A70)
IF(NUL.EQ.' ')GOTO 10
FLG=1
RETURN
ENDIF
1003 CONTINUE
IF(IENTER.EQ.3)THEN

```

```

        NDEL=0
        GOTO 1066

ENDIF
IF(IOP.NE.1)THEN
    NDEL=0
    ILIST=1
    GOTO 1066

ENDIF
CALL CLS
WRITE(*,704)
704  FORMAT('0',10X,'enter species id ( "?" for options)')
CALL LINES(0,3)
READ(*,1)SPEC
CALL READCHAR(SPEC)
IF(SPEC.EQ.'Q'.OR.SPEC.EQ.' ')THEN
    FLG=1
    RETURN
ENDIF
NUL1=' '
NUL1(:14)=SPEC(:14)
CALL DBLNK(NUL1,LENSP,0)
SPEC(:14)=NUL1(:14)
IF(SPEC.EQ.'?')THEN
    CALL CLS
    WRITE(*,*)'          READ SPECIES DOCUMENT OPTIONS'
    WRITE(*,*)'          _____'
    CALL LINES(0,1)
    WRITE(*,*)'          1 - CHANGE DATAFILE'
    WRITE(*,*)'          2 - CONTINUE'
    IF(IOP.NE.0)THEN
        WRITE(*,*)'          3 - LIST SPECIES'
        CALL LINES(0,1)
    ENDIF
    WRITE(*,*)'          enter option: { 2 }'
    READ(*,1)NUMIN
    CALL READCHAR(NUMIN)
    IF (NUMIN(:1).EQ.' ' .OR. NUMIN(:1).EQ.'2')GOTO 1003
    IF(NUMIN(:1).EQ.'1')THEN
        IOP=0
        CLOSE(34,STATUS='KEEP')
        GOTO 10
    ENDIF
    IF(IOP.NE.0)THEN
        IF(NUMIN(:1).EQ.'3')THEN
            ilist=1
            goto 41234
23          FORMAT(1X,3(5X,A10))
1067          CONTINUE
        ENDIF
        GOTO 1003
    ENDIF
    GOTO 1003
ENDIF
1066 CONTINUE

```

```

IF(IOP.EQ.0)THEN
  NSPEC=0
  CALL CLS
  write(*,*)'          INITIALIZING'
  WRITE(*,*)'          THERMO DOCUMENTATION FILE'
  CALL LINES(0,3)
  I=0
  J2=0
  NJ=0
  WRITE(*,*)'          PLEASE WAIT'
  CALL LINES(0,3)
  I=0
  NDEL=0
  READ(U,'(A70)',REC=1)NUL
10000  I=I+1
  IF(I.NE.1)READ(U,'(A70)',REC=I,END=99000)NUL
  CALL DBLNK(NUL,LEN,0)
  IF(NUL(:10).EQ.'ENDSPECIES')THEN
    JSAVE=NSPEC
    GOTO 10000
  ENDIF
  IF(NUL(:7).EQ.'SPECIES'.OR.NUL(:8).EQ.' SPECIES'
+.OR.NUL(:9).EQ.'O SPECIES'.OR.NUL(:9).EQ.' SPECIES'.OR.NUL(:7)
+.EQ.'DELETED'.OR.NUL(:8).EQ.' DELETED'
+.OR.NUL(:9).EQ.'O DELETED'.OR.NUL(:9).EQ.' DELETED')THEN
    NSPEC=NSPEC+1
    J2=J2+1
    I=I+1
    IDOC(J2)=I+1
    IF(NUL(:7).EQ.'DELETED'.OR.NUL(:8).EQ.' DELETED'
+.OR.NUL(:9).EQ.'O DELETED'.OR.NUL(:9).EQ.' DELETED')THEN
      NDEL=NDEL+1
      IDEL(NDEL)=J2
    ENDIF
    READ(U,'(A70)',REC=I,END=99000)NUL
    DOC(J2)=NUL(:14)
7      format(1x,5(2x,a10))
      I=I+2
      READ(U,'(A70)',REC=I,END=99000)NUL
      CALL LRDCHAR(NUL)
      CALL DBLNK(NUL,LEN,1)
      CALL INDXST(NUL,' ',NOCCUR,IND,LEN,1,FLG)
      IF(NOCCUR.EQ.0)THEN
        WRITE(*,*)'ERROR : CAN'T FIND SPECIES FORMULA'
        WRITE(*,*)DOC(J2)
        RETURN
      ENDIF
      FORM=NUL(IND(1)+1:LEN)
      LENF=LEN-IND(1)
      CALL FORMINT(FORM,LENF,IE,NE,NATOM,1)
      WRITE(*,876)J2,DOC(J2)(:14),(IE(JCNT),NE(JCNT),JCNT=1,4)
876  FORMAT(1X,13,2X,A14,2X,4(2X,A4,13))
      DO 1776 IKT=1,4
      NE1(IKT,J2)=NE(IKT)

```

```

                                IE1(IKT,J2)=IE(IKT)
1776                                CONTINUE
                                ENDIF
                                GOTO 10000
99000                                CONTINUE
                                IF(NSPEC.NE.JSAVE)NSPEC=JSAVE
                                NDOC=1
                                IOP=1
                                ENDIF
41234  continue
                                IF(COMMAND.NE.'AUTO_RECALC'.and.iop.eq.1)THEN
                                if(ilist.eq.1)then
                                    nul(:1)='?'
                                    goto 699
                                endif
***** LIST SPECIES SCREEN *****
***** DELETE/UNDELETE/VIEW *****
                                WRITE(*,*)'{ hit return to continue : ? for options }'
                                read(*,3)NUL
699                                IF(NUL(:1).EQ.'?')THEN
600                                CALL CLS
                                ILINE=0
                                DO 5235 IJKN=1,NSPEC+4,4
                                ILINE=ILINE+1
                                IF(ILINE.GT.22)THEN
                                    WRITE(*,*)'{ hit return or enter option " D / U / V " }'
                                    read(*,'(a70)')nul
                                    call readchar(nul)
                                    if(nul.eq.'D'.or.nul.eq.'U'.or.nul.eq.'V')then
                                        goto 5333
                                    else
                                        iline=0
                                    endif
                                ENDIF
                                dum1=' '
                                dum2=' '
                                dum3=' '
                                dum4=' '
                                IJK2=IJKN+1
                                IJK3=IJKN+2
                                IJK4=IJKN+3
                                call delchk(ijkn,i1)
                                call delchk(ijk2,i2)
                                call delchk(ijk3,i3)
                                call delchk(ijk4,i4)
                                IF(IJKN.LE.NSPEC.AND.I1.EQ.0)DUM1=DOC(IJKN)(:14)
                                IF(IJK2.LE.NSPEC.AND.I2.EQ.0)DUM2=DOC(IJK2)(:14)
                                IF(IJK3.LE.NSPEC.AND.I3.EQ.0)DUM3=DOC(IJK3)(:14)
                                IF(IJK4.LE.NSPEC.AND.I4.EQ.0)DUM4=DOC(IJK4)(:14)
                                IF(DUM1.EQ.' '.AND.DUM2.EQ.' '.AND.DUM3.EQ.' '.AND.DUM4.EQ.' ')
+ GOTO 5235
                                WRITE(*,5236)IJKN,DUM1,IJK2,DUM2,IJK3,DUM3,IJK4,DUM4
5236                                FORMAT(1X,4(13,1X,A14))
5235                                CONTINUE

```

```

***** GET SPECIES OPTIONS *****
WRITE(*,*)' enter "D" to delete; "U" to undelete; "V" to view; or
+hit return to continue'
      read(*,3)nul
      call lrdchar(nul)
      if(nul.eq.' ')goto 767
5333  continue
*-----
*           delete species
*-----
      IF(NUL(:1).EQ.'D')THEN
5234  WRITE(*,*)'DELETE which species { 0 to abort }'
      WRITE(*,*)' or enter species number to delete)'
      read(*,*,err=600)idelete
          CALL DELCHK(IDELETE,ID)
      if(idelete.EQ.0.OR.ID.EQ.1)goto 600
      ndel=ndel+1
      idel(ndel)=idelete
      write(*,*)'species # ',idelete
      write(*,*)'has been deleted'
          J55=IDOC(IDELETE)-2
          NUL=' DELETED'
          WRITE(U,'(A70)',REC=J55,ERR=600)NUL
          goto 600
      endif
573  continue
*-----
*           undelete species
*-----
      IF(NUL(:1).EQ.'U')THEN
          CALL CLS
          DO 765 IB=1,NDEL
575  WRITE(*,766)IDEL(IB),DOC(IDEL(IB))(:14)
576  FORMAT(1X,I3,1X,'-',1X,A14)
          CALL LINES(0,1)
          WRITE(*,*)' undelete which species { 0 to abort }'
          write(*,*)' or enter species number to undelete'
          read(*,*,err=600)idelete
          if(idelete.eq.0)goto 600
          do 769 ib=1,ndel
              if(idel(ib).ne.idelete)goto 769
                  J55=IDOC(IDELETE)-2
                  NUL=' SPECIES'
                  WRITE(U,'(A70)',REC=J55,ERR=600)NUL
              do 770 ib1=ib,ndel-1
577  IDEL(ib1)=idel(ib1+1)
              ndel=ndel-1
579  continue
              GOTO 600
          endif
*-----
*           view species
*-----
      IF(NUL(:1).EQ.'V')THEN

```

```

WRITE(*,*)' view which species { enter species number }'
read(*,*,err=600)iview
if(iview.lt.nspec)then
    j55=idoc(iview)-2
    j56=idoc(iview+1)-4
elseif(iview.eq.nspec)then
    j55=idoc(iview)-2
    j56=ndoc-4
else
    goto 600
endif
call cls
iline=0
do 9123 irecord=j55,j56
iline=iline+1
if(iline.ge.22)then
    pause '{ hit return to continue }'
    iline=0
else
    read(U,'(a70)',rec=irecord,err=600,end=600)nul
    write*,'(1x,a70)')nul
endif
9123 continue
pause '{ hit return to continue }'
goto 600

ENDIF
*****
767 continue
ENDIF
***** end of if (nul(:1).eq.'?') block *****
ENDIF
IF(IENTER.EQ.3)RETURN
if(ilist.eq.1)then
    ilist=0
    goto 1003
endif

J1=0
1777 J1=J1+1
1778 CONTINUE
IF(J1.GT.NSPEC)GOTO 95000
DUMMY=' '
DUMMY(:14)=DOC(J1)(:14)
CALL DBLNK(DUMMY,NUM,0)
DOC(J1)(:14)=DUMMY(:14)
IF(SPEC(:14).NE.DOC(J1)(:14).AND.J1.LT.NSPEC)GOTO 1777
1878 CONTINUE
* REWIND(U)
* DO 99099 J5=1,IDOC(J1)-2
READ(U,'(A70)',REC=IDOC(J1)-2,END=90000)NUL
99099 CONTINUE
CWRITE(*,*)NUL

IF(J1.LT.NSPEC)THEN

```

```

DO 99088 J5=1,(IDOC(J1+1)-IDOC(J1))
J55=IDOC(J1)-2+J5
READ(U,'(A70)',REC=J55,END=90000)NUL
DOC1(J5)=NUL(:70)
CONTINUE
99088
CWRITE(*,*)DOC1(J5)
ENDIF
IF(J1.EQ.NSPEC)THEN
DO 99089 J5=1,(NDOC-IDOC(J1)-1)
J55=IDOC(J1)-2+J5
READ(U,'(A70)',REC=J55,END=90000)NUL
DOC1(J5)=NUL(:70)
99089
ENDIF
C READ DOCUMENT ARRAY JUST LOADED!
FUNITS='KCAL'
IDAT=0
DELB=0.0
ISTAT=0
TYPE='M'
IDONE=0
NROT=0
FLG=0
J=0
1254 J=J+1
CALL DBLNK(DOC1(J),NUM,1)
IF(J1.LT.NSPEC.AND.(J.GT.IDOC(J1+1)-IDOC(J1)))GOTO 95000
IF(J1.EQ.NSPEC.AND.(J.GT.NDOC-IDOC(J1)))GOTO 95000
J=J+2
1255 CALL DBLNK(DOC1(J),LEN,1)
CALL INDXST(DOC1(J),' ',NOCCUR,IND,LEN,1,FLG)
INDX=IND(1)-1
LS(:INDX)=DOC1(J)(:INDX)
FORM=' '
FORM(:LEN-(IND(1)+1)+1)=DOC1(J)(IND(1)+1:LEN)
FORMP=FORM
LENF=LEN-(IND(1)+1)+1
CALL FORMINT(FORM,LENF,IE,NE,NATOM,1)
20000 CONTINUE
J=J+1
CALL DBLNK(DOC1(J),LEN,0)
IF(DOC1(J)(:6).EQ.'UNITS:')THEN
IF(DOC1(J)(7:8).EQ.'KJ')FUNITS='KJ'
GOTO 20000
ENDIF
IF(DOC1(J)(:6).EQ.'NOCALC'.AND.(KDOC.EQ.0.OR.KDOC.EQ.2))
+THEN
DOCTYPE='NOCALC'
GOTO 20000
ENDIF
IF(DOC1(J)(:7).EQ.'RADICAL'.OR.DOC1(J)(:8).EQ.'ORADICAL'
+.OR.(TYPE.EQ.'R'.AND.IDONE.NE.1))THEN
BFLAG=1

```

```

        IF(TYPE.EQ.'M')THEN
        IF(DOC1(J)(:10).EQ.'ENDSPECIES')GOTO 95000
            TYPE='R'
            IF(DOC1(J)(18:23).EQ.'PARENT')SPECP=DOC1(J)(24:LEN)
            IF(DOC1(J)(17:22).EQ.'PARENT')SPECP=DOC1(J)(23:LEN)
                RS=LS
                LS=SPECP
        ENDIF
            J=J+1
            CALL DBLNK(DOC1(J),LEN,0)
            IF(DOC1(J)(:LEN).EQ.'ENDSPECIES')GOTO 95000
            IF(DOC1(J)(:13).NE.'PARENTFORMULA')GOTO 20000
            IF(LEN.GT.13)THEN
                FORMP=DOC1(J)(14:LEN)
                LENFP=LEN-14+1
            ENDIF
            IF(LEN.EQ.13)THEN
                J=J+1
                CALL DBLNK(DOC1(J),LEN,0)
                FORMP=DOC1(J)(:LEN)
                LENFP=LEN
            ENDIF
            J=J+1
            CALL DBLNK(DOC1(J),LEN,0)
            IF(DOC1(J)(:14).NE.'PARENTSYMMETRY')GOTO 20000
            NUMIN=' '
            NUMIN=DOC1(J)(15:LEN)
            CALL READNUM(NUMIN,RNUM,SYMS,KFLG)
            IDONE=1

        ENDIF
C      SEARCHING FOR KEYWORD "GROUPS"
        IF(DOC1(J)(:6).NE.'GROUPS'.AND.J.LT.(IDOC(J1+1)-IDOC(J1)))
+GOTO 20000
        NG=0
        IF(LEN.EQ.7)THEN
            NG=ICHAR(DOC1(J)(7:7))-48
            GOTO 1111
        ENDIF
        IF(LEN.EQ.8)THEN
            NG=10*(ICHAR(DOC1(J)(7:7))-48)+ICHAR(DOC1(J)(8:8))-48
            GOTO 1111
        ENDIF
1111 CONTINUE
        IF(NG.EQ.0)THEN
            DOCTYPE='NOCALC'
            GOTO 3001
        ENDIF

        NSAVE=NG
        J=J+1
        I1=0
223 CONTINUE
        J=J+1

```



```

      IF(J.LT.(NDOC-INX).AND.DOC1(J).EQ.' ')GOTO 223
      CALL DBLNK(DOC1(J),LEN,0)
      IF(J.LT.NDOC.AND.DOC1(J)(:2).EQ.'Gr')GOTO 223
      CALL INDXST(DOC1(J),'-',NOCCUR,IND,LEN,1,FLG)
      LEN1=LEN
      IF(NOCCUR.EQ.4)THEN
      CALL INDXST(DOC1(J),'|',NOCR,JIND,LEN1,1,FLG)
      IGS1=1
      IGE1=IND(1)-1
      IGS2=JIND(1)+1
      IGE2=IND(3)-1
      NUMIN=' '
      NUMIN=DOC1(J)(IGS1:IGE1)
      CALL READNUM(NUMIN,RNUM,KG1,KFLG)
      NUMIN=' '
      NUMIN=DOC1(J)(IGS2:IGE2)
      CALL READNUM(NUMIN,RNUM,KG2,KFLG)
      JINDS=JIND(1)-1
      IN1P1=IND(1)+1
      IN2M1=IND(2)-1
      IN1P2=IND(3)+1
      IN2M2=IND(4)-1
      IND1=IND(2)+1
      IND3=IND(4)+1
      IF(JINDS.EQ.IND1)E(KG1)=ICHAR(DOC1(J)(IND1:IND1))-48
      IF(LEN1.EQ.IND3)E(KG2)=ICHAR(DOC1(J)(IND3:IND3))-48
      IF(JINDS.EQ.IND(2)+2)THEN
      IND2=IND(2)+2
      E(KG1)=10*(ICHAR(DOC1(J)(IND1:IND1))-48)+ICHAR(DOC1(J)
+(IND2:IND2))-48
      ENDIF
      IF(LEN1.EQ.IND(4)+2)THEN
      IND2=IND(2)+2
      IND4=IND(4)+2
      E(KG2)=10*(ICHAR(DOC1(J)(IND3:IND3))-48)+ICHAR(DOC1(J)(IND4:
+IND4))-48
      ENDIF
      EP(KG1)=E(KG1)
      EP(KG2)=E(KG2)
      LNG(KG1)=IND(2)-IND(1)-1
      LNG(KG2)=IND(4)-IND(3)-1
      CS(1,KG1)(:LNG(KG1))=DOC1(J)(IN1P1:IN2M1)
      CS(1,KG2)(:LNG(KG2))=DOC1(J)(IN1P2:IN2M2)
      CALL FINDGR(AS,NGRPT,CS,IX,KG2,ISTAT,LNG(1))
      IF(ISTAT.EQ.1)THEN
      CS(2,KG1)=' '
      CS(2,KG1)(:5)='ERROR'
      IX(KG1)=0
      ELSE
      CS(2,KG1)=CS(1,KG1)
      ENDIF
      CALL FINDGR(AS,NGRPT,CS,IX,KG1,ISTAT,LNG(1))
      IF(ISTAT.EQ.1)THEN
      CS(2,KG2)=' '

```

```

                CS(2,KG2)(:5)='ERROR'
                IX(KG2)=0
        ELSE
                CS(2,KG2)=CS(1,KG2)
        ENDIF
        I1=I1+2
    ENDIF
    IF(NOCUR.EQ.2)THEN
        IGS1=1
        IGE1=IND(1)-1
        NUMIN=' '
        NUMIN=DOC1(J)(IGS1:IGE1)
        CALL READNUM(NUMIN,RNUM,KG1,KFLG)
        IN1P1=IND(1)+1
        IN2M1=IND(2)-1
                IND1=IND(2)+1
    IF(LEN.EQ.IND1)E(KG1)=ICHAR(DOC1(J)(IND1:IND1))-48
    IF(LEN.EQ.IND(2)+2)THEN
        IND2=IND(2)+2
        E(KG1)=10*(ICHAR(DOC1(J)(IND1:IND1))-48)+ICHAR(DOC1(J)
+(IND2:IND2))-48
    ENDIF
        EP(KG1)=E(KG1)
        LNG(KG1)=IND(2)-IND(1)-1
        CS(1,KG1)(:LNG(KG1))=DOC1(J)(IN1P1:IN2M1)
        CALL FINDGR(AS,NGRPT,CS,IX,KG1,ISTAT,LNG(I))
                IF(ISTAT.EQ.1)THEN
                        CS(2,KG1)=' '
                        CS(2,KG1)(:5)='ERROR'
                        IX(KG1)=0
                ELSE
                        CS(2,KG1)=CS(1,KG1)
                ENDIF
        I1=I1+1
    ENDIF
222  IF(I1.LT.NG)GOTO 223
3001  CONTINUE
        J=J+1
        CALL LRDCHAR(DOC1(J))
        CALL DBLNK(DOC1(J),LEN,0)
                IF(DOC1(J)(:8).EQ.'NROTORS:')THEN
                        NUL=' '
                        NUL(:LEN-8)=DOC1(J)(9:LEN)
                        CALL READNUM(NUL,RNUM,NROT,KFLG)
                        IF(KFLG.NE.0)THEN
                                NROT=0
                        ENDIF
                        NROTS=NROT
                        GOTO 3001
                ENDIF
        IF(DOC1(J)(:10).EQ.'ENDSPECIES')THEN
                IF(IDONE.NE.2)SYMM=1
                GOTO 6000
        ENDIF

```

```

IF(DOC1(J)(:6).EQ.'NOCALC'.AND.(KDOC.EQ.0.OR.KDOC.EQ.2))
+THEN
    DOCTYPE='NOCALC'
    GOTO 3001
ENDIF
IF(DOCTYPE.EQ.'NOCALC'.AND.IDAT.EQ.0)THEN
    IF(DOC1(J)(:2).EQ.'HF'.OR.DOC1(J)(:2).EQ.'Hf')THEN
        J=J+1
        CALL DBLNK(DOC1(J),LEN,1)
        IF(LEN.EQ.0)THEN
            WRITE(*,*)'ERROR CONVERTING THERMO'
            WRITE(*,*)'DOCTYPE RESET TO "CALC"'
            WRITE(*,*)'IF # GROUPS > 0 , ELSE ABANDON'
            WRITE(*,*)'HIT RETURN TO CONTINUE'
            READ(*,3)NUL
            IF(NG.EQ.0)THEN
                ISTAT=2
                FLG=2
                RETURN
            ENDIF
            DOCTYPE=' '
            GOTO 3001
        ENDIF
        CALL INDXST(DOC1(J),' ',NOCCUR,IND,LEN,1,FLG)
        NUL=DOC1(J)(:IND(1)-1)
        CALL READNUM(NUL,B(1,1),NUM,KFLG)
        DO 298 K8=1,NOCCUR-1
            NUL=DOC1(J)(IND(K8)+1:IND(K8+1)-1)
            CALL READNUM(NUL,B(1,K8+1),NUM,KFLG)
298        CONTINUE
            NUL=DOC1(J)(IND(NOCCUR)+1:LEN)
            CALL READNUM(NUL,B(1,NOCCUR+1),NUM,KFLG)
            IDAT=1
                if(funits.eq.'KJ')then
                    do 579 ik1=1,noccur+1
                    b(1,ik1)=b(1,ik1)/4.184
579                endif
        IF(IENTER.EQ.10)THEN
            DO 1957 IIU=1,NG
                IF(CS(1,I)(:2).EQ.'OI')THEN
                    B(1,2)=B(1,2)-A(IX(IIU),2)
                ENDIF
1957            CONTINUE
        ENDIF
        GOTO 3001
    ENDIF
ENDIF
IF(DOC1(J)(:9).EQ.'DELTAEDIT')THEN
    J=J+1
    CALL DBLNK(DOC1(J),LEN,1)
    IF(LEN.EQ.0)THEN
        WRITE(*,*)'ERROR CONVERTING THERMO'
        WRITE(*,*)'DELTA EDIT GROUP IGNORED'
        WRITE(*,*)'HIT RETURN TO CONTINUE'
    ENDIF
ENDIF

```

```

READ(*,3)NUL
GOTO 3001
ENDIF
CALL INDXST(DOC1(J),' ',NOCCUR,IND,LEN,1,FLG)
NUL=DOC1(J)(:IND(1)-1)
CALL READNUM(NUL,DELTA(1),NUM,KFLG)
DO 598 K8=1,NOCCUR-1
NUL=DOC1(J)(IND(K8)+1:IND(K8+1)-1)
CALL READNUM(NUL,DELTA(K8+1),NUM,KFLG)
598 CONTINUE
NUL=DOC1(J)(IND(NOCCUR)+1:LEN)
CALL READNUM(NUL,DELTA(NOCCUR+1),NUM,KFLG)
      if(funits.eq.'KJ')then
578         do 578 ik1=1,noccur+1
           delta(ik1)=delta(ik1)/4.184
        endif
      GOTO 3001
ENDIF
IF(DOC1(J)(:4).EQ.'BOND'.AND.TYPE.EQ.'R')THEN
  NUMIN=' '
  NUMIN=DOC1(J)(5:LEN)
  CALL READNUM(NUMIN,BD,NUM,KFLG)
  if(funits.eq.'KJ')bd=bd/4.184
  GOTO 3001
ENDIF
IF(DOC1(J)(:16).EQ.'DELTABONDENERGY=')THEN
  NUMIN=DOC1(J)(17:LEN)
  CALL READNUM(NUMIN,DELB,NUM,KFLG)
  IF(DOCTYPE.NE.'NOCALC')B(1,1)=B(1,1)+DELB
  if(funits.eq.'KJ')delb=delb/4.184
  GOTO 3001
ENDIF
IF(DOC1(J)(:4).EQ.'TEXT')THEN
  NUMIN=DOC1(J)(5:LEN)
  CALL READNUM(NUMIN,RNUM,KOUNT,KFLG)
  DO 634 IJ=1,KOUNT
      J=J+1
      IF(DOC1(J)(:10).EQ.'ENDSPECIES')GOTO 635
      TEXT(IJ)=DOC1(J)
634 CONTINUE
      GOTO 3001
  ENDIF
635 IF(DOC1(J)(:10).EQ.'ENDSPECIES')THEN
  IF(IDONE.NE.2)SYMM=1
  GOTO 6000
ENDIF
IF(DOC1(J)(:8).NE.'SYMMETRY')GOTO 3001
  IDONE=2
  IF(LEN.EQ.9)SYMM=ICHAR(DOC1(J)(9:9))-48
  IF(LEN.EQ.10)SYMM=10*(ICHAR(DOC1(J)(9:9))-48)+ICHAR(DOC1(J)(10:
+10))-48
  IF(LEN.EQ.11)SYMM=100*(ICHAR(DOC1(J)(9:9))-48)+10*(ICHAR(DOC1(J)
+(10:10))-48)+ICHAR(DOC1(J)(LEN:LEN))-48
  GOTO 3001

```

```

6000 CONTINUE
      IF(TYPE.NE.'R') SYMS=SYMM
      IF(TYPE.EQ.'R') SYMR=SYMM
      SCOR=1.987*LOG(SYMM*1.0)
          IF(IENTER.EQ.10.AND.DOCTYPE.EQ.'NOCALC')THEN
              B(1,2)=B(1,2)+SCOR
          ENDIF
      IF(DOCTYPE.EQ.'NOCALC'.AND.IDAT.EQ.1)THEN
          ISTAT=1
          RETURN
      ENDIF
*****
*****          CALCULATE SPECIES PROPERTIES          *****
*****
      NTEMPS=7
      DO 3100 I2=1,NG
          IF(IX(I2).NE.0)THEN
              IF(A(IX(I2),9).EQ.0.0.AND.A(IX(I2),8).NE.0.0)NTEMPS=6
          DO 850 Y=1,9
              IF(IENTER.EQ.10.AND.AS(IX(I2))(:2).EQ.'OI')GOTO 3100
              B(1,Y)=E(I2)*A(IX(I2),Y)+B(1,Y)
              IF(IX(I2).LT.IFIRST(4).OR.IX(I2).GT.ILAST(4))THEN
                  B(2,Y)=E(I2)*A(IX(I2),Y)+B(2,Y)
              ENDIF
          CONTINUE
          IF(IX(I2).LT.IFIRST(4).OR.IX(I2).GT.ILAST(4))GOTO 3100
          B(1,1)=B(1,1)-52.1
          ENDIF
      3100 CONTINUE
          IF(NTEMPS.EQ.6)THEN
              B(1,9)=0.0
              B(2,9)=0.0
          ENDIF
          DO 568 Y=1,9
              IF(DELTA(Y).NE.0)THEN
                  B(1,Y)=B(1,Y)+DELTA(Y)
                  B(2,Y)=B(2,Y)+DELTA(Y)
              ENDIF
          CONTINUE
          IF(IENTER.NE.10)THEN
              B(1,2)=B(1,2)-SCOR
              SCORP=1.987*LOG(SYMS*1.0)
              IF(TYPE.NE.'R')SCORP=SCOR
              ENDIF
          ISTAT=1
          IF(ISTAT.EQ.2.AND.FLG.EQ.2)GOTO 90000
          IF(FLG.EQ.1)RETURN
          IF(IDOC(J1).GT.NDOC)GOTO 95000
          FLG=0
          RETURN
*****
90000 CALL CLS
      WRITE(*,*)          ERROR : SPECIES NOT FOUND'
      CALL LINES (0,2)

```

```
WRITE(*,*)'          ( hit return to continue )'  
READ(*,3)NUL  
1492   FLG=1  
      CLOSE(U,STATUS='KEEP')  
      RETURN  
95000  FLG=1  
      WRITE(*,*)'   J1 > NSPEC'  
      WRITE(*,*)' J1 = ',J1  
      WRITE(*,*)' NSPEC= ',NSPEC  
      WRITE(*,*)'          ERROR : SPECIES NOT FOUND'  
      CALL LINES (0,2)  
      WRITE(*,*)'          ( hit return to continue )'  
      READ(*,3)NUL  
      RETURN  
      END
```

```

SUBROUTINE CONFIG(ELEM,NFILES,KS,ISTAT,OUTPUT)
CHARACTER*70 NUL,DUMMY,KS(1),HLP(10),ERRORMSG
CHARACTER*14 NUMIN,OUTPUT,UNITS,TRANGE
CHARACTER*2 ELEM(1),DRIVE1,DRIVE2,DRIVE3,ERRORCK
INTEGER I,LEN1,NELEM,NFILES,ISTAT,I1CH(50),I2CH(35)
COMMON/CONFIG2/NELEM,N1CH,N2CH,I1CH,I2CH
COMMON/CONFIG3/HLP
COMMON/CONFIG4/DRIVE1,DRIVE2,DRIVE3
COMMON/CONFIG5/NKEYS
COMMON/CONFIG6/UNITS
COMMON/CONFIG7/ERRORCK
COMMON/CONFIG8/TRANGE
TRANGE='2000'
UNITS='KCAL'
OUTPUT='QUICK'
DRIVE1=' '
DRIVE2=' '
DRIVE3=' '
NKEYS=3
ERRORCK=' '
2      FORMAT(A2)
14     FORMAT(A14)
70     FORMAT(A70)
ISTAT=0
OPEN(96,FILE='THERM.CFG',STATUS='OLD',ERR=9999)
ERRORMSG=' KEYWORD " #FILES " MISSING OR NOT FIRST LINE'
READ(96,70,END=9999)NUL
CALL LRDCHAR(NUL)
CALL DEBLNK(NUL,DUMMY,LEN1,0)
IF(NUL(:6).NE.'#FILES')GOTO 9999
NUMIN=NUL(7:LEN1)
CALL READNUM(NUMIN,RNUM,NFILES,KFLG)
ERRORMSG=' FEWER FILES FOUND THAN SPECIFIED IN " #FILES " '
DO 10 I=1,NFILES
READ(96,70,END=9999)KS(I)
CALL DBLNK(KS(I),LEN1,0)
IF(KS(I).EQ.'#ELEMENTS')GOTO 9999
10     CONTINUE
ERRORMSG=' KEYWORD " #ELEMENTS " IS MISSING'
READ(96,70,END=9999)NUL
CALL LRDCHAR(NUL)
CALL DEBLNK(NUL,DUMMY,LEN1,0)
IF(NUL(:9).NE.'#ELEMENTS')GOTO 9999
NUMIN=NUL(10:LEN1)
CALL READNUM(NUMIN,RNUM,NELEM,KFLG)
N1CH=0
N2CH=0
ERRORMSG=' FEWER ELEMENTS FOUND THAN SPECIFIED IN " #ELEMENTS"'
DO 20 I=1,NELEM
READ(96,70,END=9999)NUL
CALL DEBLNK(NUL,DUMMY,LEN1,0)
ELEM(I)=NUL(:LEN1)
IF(LEN1.EQ.1)THEN
      N1CH=N1CH+1

```

```

                I1CH(N1CH)=I
                GOTO 20
ENDIF
IF(LEN1.EQ.2)THEN
    N2CH=N2CH+1
    I2CH(N2CH)=I
ENDIF
IF(LEN1.GT.2)THEN
    GOTO 9999
ENDIF
20 CONTINUE
ERRORMSG=' KEYWORD " #HELP " MISSING'
READ(96,70,END=9999)NUL
CALL LRDCHAR(NUL)
CALL DEBLNK(NUL,DUMMY,LEN1,0)
IF(NUL(:5).NE.'#HELP')GOTO 9999
NUMIN=NUL(6:LEN1)
CALL READNUM(NUMIN,RNUM,NHELP,KFLG)
ERRORMSG=' FEWER HELP FILES FOUND THAN SPECIFIED IN " #HELP "'
DO 60 I=1,NHELP
    READ(96,70,END=9999)HLP(I)
    CALL DBLNK(HLP(I),LEN1,0)
    IF(HLP(I)(:6).EQ.'OPTION')GOTO 9999
60 CONTINUE

*
* OPTIONS ANY ORDER IS ACCEPTABLE
*
* DEFAULTS ARE DEFINED: ONLY NECESSARY IF WANT TO SPECIFY
* OPTION DIFFERENT FROM DEFAULT
*
10000 CONTINUE
READ(96,70,END=9777)NUL
CALL DEBLNK(NUL,DUMMY,LEN1,0)
IF(NUL(:12).EQ.'THERMFIT.EXE')THEN
    IF(NUL(13:14).NE.' ')DRIVE1=NUL(13:14)
ELSE IF(NUL(:12).EQ.'THERMLST.EXE')THEN
    IF(NUL(13:14).NE.' ')DRIVE2=NUL(13:14)
ELSE IF(NUL(:12).EQ.'THERMRXN.EXE')THEN
    IF(NUL(13:14).NE.' ')DRIVE3=NUL(13:14)
ELSEIF(NUL(:5).EQ.'#KEYS')THEN
    NUMIN=NUL(6:LEN1)
    CALL READNUM(NUMIN,RNUM,NKEYS,KFLG)
ELSEIF(NUL(:11).EQ.'ERRORCK=OFF')THEN
    ERRORCK='NO'
    ELSEIF(NUL(:9).EQ.'TRANGE=EX'.OR.NUL(:8).EQ.'TRANGE=5')THEN
    TRANGE='5000'
ELSEIF(NUL(:6).EQ.'UNITS:')THEN
    IF(NUL(7:8).EQ.'KJ')UNITS='KJ'
ELSEIF(NUL(:7).EQ.'OUTPUT:')THEN
    IF(NUL(8:LEN1).EQ.'CLOSE')OUTPUT='CLOSE'
ENDIF
GOTO 10000
9777 CLOSE(96,STATUS='KEEP')
```



```
          ISTAT=0
          RETURN
9999      ISTAT=1
          CALL LINES(0,1)
          WRITE(*,'(1X,A70)'ERRORMSG
          CALL LINES(0,1)
          WRITE(*,*)'  ERROR ENCOUNTERED IN THERM.CFG'
          WRITE(*,*)'  REQUIRED CONFIG DATA IS MISSING'
          CLOSE(96,STATUS='KEEP')
          RETURN
          END
```

```

SUBROUTINE HELP(FNAME,OPTION)
CHARACTER*70 FNAME
CHARACTER*70 NUL,NUMIN,S2,OPTION
LOGICAL EXST
1 CONTINUE
INQUIRE(FILE=FNAME,EXIST=EXST,ERR=9900)
70 FORMAT(A70)
71 FORMAT(2X,A70)
IF(EXST)THEN
CALL DEBLNK(OPTION,S2,LEN2,0)
OPEN(69,FILE=FNAME,STATUS='OLD')
IF(OPTION(:LEN2).EQ.'A')GOTO 200
I=0
100 I=I+1
READ(69,70,END=9900)NUL
IF(NUL(:1).NE.'0'.and.nul(:2).ne.' 0')GOTO 100
CALL DEBLNK(NUL,S2,LEN1,0)
IF(NUL(7:LEN1).NE.OPTION(:LEN2))GOTO 100
222 CALL CLS
J=0
200 J=J+1
IF(J.GE.22)THEN
WRITE(*,*)' { hit return to continue }'
READ(*,70)S2
GOTO 222
ENDIF
READ(69,70,END=9900)NUL
IF(NUL(:3).NE.'END'.AND.NUL(:3).NE.'end'.AND.NUL(:4)
+.NE.' END'.AND.NUL(:4).NE.' end')THEN
WRITE(*,70)NUL
GOTO 200
ENDIF
WRITE(*,*)' { hit return to continue }'
READ(*,70)S2
IF(OPTION(:LEN2).NE.'A')THEN
CLOSE(69,STATUS='KEEP')
RETURN
ENDIF
GOTO 222
ENDIF
CALL CLS
WRITE(*,*)' CAN'T FIND HELP FILE'
WRITE(*,71)FNAME
WRITE(*,*)' HELP FILES MUST RESIDE IN THE CURRENT DIRECTORY !!'
CALL LINES(0,2)
WRITE(*,*)' HIT RETURN TO ENTER A NEW DRIVE/DIRECTORY SPEC'
WRITE(*,*)' OR ENTER "Q" TO ABORT HELP'
READ(*,70)NUL
IF(NUL.EQ.' ')THEN
PAUSE 'ENTER DOS COMMAND TO CHANGE DIRECTORY/DISK'
GOTO 1
ENDIF
CALL LRDCHAR(NUL)
IF(NUL.EQ.'Q')RETURN

```

9900

```
CALL CLS  
WRITE(*,*)' NO FURTHER HELP AVAILABLE'  
WRITE(*,*)' { hit return to continue }'  
READ(*,70)S2  
CLOSE(69,STATUS='KEEP')  
RETURN  
END
```

```

SUBROUTINE FNAME (S1,S2)
*
*
*   S1 = CHARACTER*(*) INPUT FILENAME
*   S3 = CHARACTER*(*) FILE EXTENSION
*
*
CHARACTER*(*) S1
CHARACTER*(*) S2
INTEGER IND(70),FLG,LEN
CALL READCHAR(S1)
CALL DBLNK(S1,LEN,0)
CALL INDXST(S1,'.',NOC,IND,LEN,1,FLG)
IF(NOC.EQ.0)THEN
    S1(LEN+1:LEN+1)='.'
    S1(LEN+2:LEN+4)=S2
    S1(LEN+5:70)=' '
ELSE IF(NOC.NE.0)THEN
    S1(IND(1)+1:IND(1)+3)=S2
    S1(IND(1)+4:70)=' '
ENDIF
RETURN
END

```

```

SUBROUTINE FINDSP(S1,DOC,NSPEC,IDOC,IREC,ISTAT)
$LARGE
CHARACTER*14 S1,DOC(1)
CHARACTER*70 NUL, DUMMY
INTEGER NSPEC,IRECN,IDOC(1),ISTAT
70  FORMAT(A70)
14  FORMAT(A14)
    ISTAT=0
    DO 100 I=1,NSPEC
    DUMMY=' '
    DUMMY(:14)=DOC(I)(:14)
    CALL DEBLNK(DUMMY,NUL,NUM,0)
    DOC(I)(:14)=DUMMY(:14)
    IF(S1(:14).EQ.DOC(I)(:14))THEN
        IREC=I
        RETURN
    ENDIF
100  CONTINUE
    ISTAT=1
    WRITE(*,*)'SPECIES ',S1(:14),' NOT FOUND'
    READ(*,14)S2
    RETURN
END

```

```

                SUBROUTINE INQNUM(S1,IANS,NUMLEN,LEN,IBL)
*****
*
*               written by Ed Ritter : 11/20/88
*
*****
*
*       THIS SUBROUTINE SCANS STRING S1 FOR A LEADING NUMBER
*       The search is carried out from left to right.
*       The first non-numeric character encountered ends
*       the numeric substring.
*
*       return codes :IANS
*
*       IANS = 0 : the string is non-numeric
*       = 1 : string S1 is an integer
*       = 2 : S1 is a decimal
*       = 3 : S1 has a leading integer of length NUMLEN
*       = 4 : S1 has a leading decimal of length NUMLEN.
*
*       NUMLEN : the length of the leading numeric portion of S1
*       LEN : the length of the S1 without blanks
*       IBL : allows the calling routine to control blank
*             removal in subroutine DEBLNK
*             IBL=0 : leave no blanks in S1
*             IBL=1 : leave one remaining blank in each blank
*                   field
*****
$large
CHARACTER*(*) S1
INTEGER IANS,NUMLEN,LEN,ICTRL,IDEC,IBL
*
* ICTRL <> 0, when a non-numeric character has been encountered in S1.
* IDEC <> 0, if a decimal point is encountered in a numeric field;
* in this case IDEC = address of decimal point.
10  continue
    NUMLEN=0
    ICTRL=0
    IDEC=0
    IANS=0
    CALL DBLNK (S1,LEN,IBL)
    DO 100 I=1,LEN
        IF((ICHAR(S1(I:1)).GE.48.AND.ICHAR(S1(I:1)).LE.57).OR.
+ (S1(I:1).EQ.'.'.AND.IDEC.EQ.0))THEN
            IF(ICTRL.EQ.0)THEN
                NUMLEN=NUMLEN+1
                IF(S1(I:1).EQ.'.')IDEC=I
            ENDIF
        ELSE
            ICTRL=1
        ENDIF
100  CONTINUE
    IF(NUMLEN.EQ.0)THEN

```

```
          IANS=0
ELSEIF(NUMLEN.EQ.LEN)THEN
  IF(IDEQ.EQ.0)THEN
    IANS=1
  ELSEIF(IDEQ.NE.0)THEN
    IANS=2
  ENDIF
ELSEIF(NUMLEN.LT.LEN)THEN
  IF(IDEQ.EQ.0)THEN
    IANS=3
  ELSEIF(IDEQ.NE.0)THEN
    IANS=4
  ENDIF
ENDIF
99999  CONTINUE
      RETURN
      END
```

```

SUBROUTINE TBREAK(TMID,TINIT)
$LARGE
    IMPLICIT REAL*8 (A-H,O-Z)
    DIMENSION T(30),F(14)
    COMMON/TEMPFIT/T,F
    ITER=0
1    CONTINUE
    ITER=ITER+1
    TNEXT=TINIT-(FDIF(TINIT)/DFDIF(TINIT))
    IF(ABS(TNEXT-TINIT).GT.1.0)THEN
        TINIT=TNEXT
        IF(ITER.LT.500)GOTO 1
    ENDIF
    TMID=TNEXT
    RETURN
END

FUNCTION FDIF(X)
$LARGE
*
*   THIS FUNCTION RETURNS THE SUM OF THE SQUARE OF THE DIFFERENCE
*   BETWEEN VALUES OF TWO POLYNOMIALS AND THEIR DERIVATIVE AT A SPECIFIC
*   TEMPERATURE (X).
*
    IMPLICIT REAL*8 (A-H,O-Z)
    DIMENSION T(30),F(14)
    COMMON/TEMPFIT/T,F
    AX=(CPT(0,X,F)-CPT(7,X,F))
    BX=(DCPT(0,X,F)-DCPT(7,X,F))
    FDIF=(AX**2)+(BX**2)
    RETURN
END

FUNCTION DFDIF(X)
$LARGE
    IMPLICIT REAL*8 (A-H,O-Z)
    DIMENSION T(30),F(14)
    COMMON/TEMPFIT/T,F
    AX=(CPT(0,X,F)-CPT(7,X,F))
    BX=(DCPT(0,X,F)-DCPT(7,X,F))
    TERM1=(F(2)-F(9))+(2.0*X*(F(3)-F(10)))+(3.0*(X**2)*(F(4)-F(11)))
+ + (4.0*(X**3)*(F(5)-F(12)))
    TERM2=(2.*(F(3)-F(10)))+(6.*X*(F(4)-F(11)))
+ + (12.*(X**2)*(F(5)-F(12)))
    DFDIF=(2.*AX*TERM1)+(2.*BX*TERM2)
    RETURN
END

```



```

SUBROUTINE CSTRING(S,N)
$LARGE
CHARACTER*(*) S(*)
100 CONTINUE
DO 200 I=1,N
IF(S(I).EQ.' ')THEN
300 DO 300 I1=I+1,N
S(I1-1)=S(I1)
N=N-1
GOTO 100
ENDIF
200 CONTINUE
RETURN
END

```

```

SUBROUTINE DCREAL(X,N)
$LARGE
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION X(*)
100 CONTINUE
DO 200 I=1,N
IF(X(I).EQ.0.0)THEN
300 DO 300 I1=I+1,N
X(I1-1)=X(I1)
N=N-1
GOTO 100
ENDIF
200 CONTINUE
RETURN
END

```

```

SUBROUTINE DREADNUM(S1,DNUM,IFLG)
$LARGE
CHARACTER*(*)S1,S2*20
REAL*8 DNUM,COEF,EXPONENT
IFLG=0
call slen(s1,lstr)
CALL INQNUM(S1,IANS,NLEN,LSTR,0)
IF(IANS.EQ.0)THEN
IFLG=-10
RETURN
ELSEIF(IANS.EQ.1.AND.LSTR.GT.10)THEN
IFLG=-5
DNUM=0.
RETURN
ELSEIF(IANS.EQ.2.AND.LSTR.GT.11)THEN

```

```

        IFLG=-6
        DNUM=0.0
        RETURN
    ELSEIF(IANS.EQ.1.OR.IANS.EQ.2)THEN
        CALL READNUM(S1,RNUM,num,IFLG)
        IF(IFLG.NE.0)THEN
            RETURN
        ELSE
            DNUM=DBLE(RNUM)
            RETURN
        ENDIF
    ELSE
        S2=' '
        S2(:NLEN)=S1(:NLEN)
        CALL READNUM(S2,RNUM,num,IFLG)
        IF(IFLG.NE.0)RETURN
        COEF=DBLE(RNUM)
        S2=' '
        LSTR1=LSTR-(NLEN+1)
        S2(:LSTR1)=S1(NLEN+2:LSTR)
        IF(S2(:1).EQ.'+')THEN
            S2(:1)=' '
        ENDIF
        CALL INQNUM(S2,IANS2,LEXP,LLSTR,0)
        IF(IANS2.NE.1.AND.S2(:1).NE.'-')THEN
            IFLG=-20
            RETURN
        ELSE
            CALL READNUM(S2,RNUM,num,IFLG)
            IF(IFLG.NE.0)RETURN
            IF(NUM.GT.130.OR.NUM.LT.-130)THEN
                IFLG=-30
                RETURN
            ENDIF
            EXPONENT=10.0**NUM
        ENDIF
        DNUM=COEF*EXPONENT
    ENDIF
    RETURN
    END

```

```

SUBROUTINE LINLSQ (X,Y,B,NRXNS,NEXP,NSPC,NRT,SSR,AVGERR)
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION XT(15,31,1),X(31,15,1),XTX(15,15,1),BP(15,1,1)
  DIMENSION XINV(15,15,1),WORK(15,15,1),DELPCT(100)
  DIMENSION Y(31,25,5),B(16,25,5),XTY(15,1,1),YP(31,1,1)
C  X0 IS THE INTERCEPT: ie.; DIMENSION = 1 + # OF VARIABLES
  NRXN=NRXNS+1
C  SET THE VECTOR X(1,N,1)=1.0
  DO 99 K=1,NEXP
    99 X(K,1,1)=1.0
C  DEFINE THE TRANSPOSE OF X : ie.; XT
  DO 2000 J=1,NRXN
    DO 1000 I=1,NEXP
      1000 XT(J,I,1)=X(I,J,1)
    2000 CONTINUE
C  COMPUTE THE MATRIX PRODUCT XTX
  CALL PMATRIX(XT,X,XTX,NRXN,NEXP,NRXN,1)
C  COMPUTE THE INVERSE OF XTX
  CALL INVERT(NRXN,XTX,XINV,WORK,1)
C  DEFINE THE VECTOR YP(I,1,1): THESE ARE THE FUNCTION VALUES
  DO 335 I=1,NEXP
    335 YP(I,1,1)=Y(I,NRT,NSPC)
C  COMPUTE THE MATRIX VECTOR PRODUCT XTY
  CALL PMATRIX(XT,YP,XTY,NRXN,NEXP,1,1)
C  COMPUTE THE VECTOR OF LINEAR COEFFICIENTS
  CALL PMATRIX(XINV,XTY,BP,NRXN,NRXN,1,1)
  DO 336 I=1,NRXN
    336 B(I,NRT,NSPC)=BP(I,1,1)
  SSR=0.
  DELSUM=0.
  AVGERR=0.
C  CALCULATE PREDICTED RESPONSE, AVG ABS ERROR, AND SUM OF SQUARES
C  WRITE(9,*)'LINEAR PREDICTION SUMMARY'
C  WRITE(9,*)'          Y          YCALC          %DELTA'
C  DO 444 J=1,NEXP
  YCALC=0.
  DO 333 I=1,NRXN
    333 YCALC=YCALC+(B(I,NRT,NSPC)*X(J,I,1))
  DEL= Y(J,NRT,NSPC)-YCALC
  IF(Y(J,NRT,NSPC).EQ.0.0)GO TO 334
  DELPCT(J)=(DEL/Y(J,NRT,NSPC))*100.
C  WRITE(9,*)Y(J,NRT,NSPC),YCALC,DELPCT(J)
  334 DELSUM=DELSUM+DABS(DELPCT(J))
  444 SSR=SSR+(DEL**2)
  AVGERR=DELSUM/NEXP
  RETURN
  END

```

```

SUBROUTINE PMATRIX (A,B,C,I,J,K,N1)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(15,31,1),B(31,15,1),C(15,15,1)
DO 103 M=1,I
DO 102 N=1,K
TSUM=0.
DO 101 L=1,J
101 TSUM=TSUM+(A(M,L,1)*B(L,N,N1))
102 C(M,N,1)=TSUM
103 CONTINUE
RETURN
END

```

```

SUBROUTINE INVERT(NCON,C,CIN,B,N)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION C(15,15,1),CIN(15,15,1),B(16,15,1)
C CREATE THE IDENTITY MATRIX B
DO 10 I=1,NCON
DO 20 J=1,NCON
B(I,J,1)=0.0
IF(J.EQ.I) B(I,J,1)=1.0
20 CONTINUE
10 CONTINUE
NR=NCON
C WRITE(7,*)'IDENTITY MATRIX ='
C DO 30 I=1,NCON
C WRITE(7,*)(B(I,J,1),J=1,NCON)
C 30 CONTINUE
CALL GJELIM(NCON,NR,N,C,B,CIN)
RETURN
END

```

```

SUBROUTINE GJELIM(NCON,NR,NA,C,B,CIN)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION C(15,15,1),B(16,15,1),CIN(15,15,1)
IF(NCON.EQ.1) GO TO 1120
LAST=NCON-1
DO 1700 I=1, LAST
M=I
ITEMP=I+1
DO 1100 J=ITEMP,NCON
IF(ABS(C(M,I,NA)).GT.ABS(C(J,I,NA))) GO TO 1100
M=J
1100 CONTINUE
IF(ABS(C(M,I,NA)).LT.1.E-15) GO TO 1130
IF(M.EQ.I) GO TO 1400
DO 1200 J=I,NCON
TEMP=C(M,J,NA)
C(M,J,NA)=C(I,J,NA)
1200 C(I,J,NA)=TEMP
DO 1300 J=1,NR
TEMP=B(M,J,NA)
B(M,J,NA)=B(I,J,NA)
1300 B(I,J,NA)=TEMP
1400 DO 1600 J=ITEMP,NCON
TEMP=C(J,I,NA)/C(I,I,NA)
C(J,I,NA)=0.0
DO 1500 K=ITEMP,NCON
1500 C(J,K,NA)=C(J,K,NA)-TEMP*C(I,K,NA)
DO 1600 K=1,NR
1600 B(J,K,NA)=B(J,K,NA)-TEMP*B(I,K,NA)
1700 CONTINUE
IF(ABS(C(NCON,NCON,NA)).LT.1.E-15) GO TO 1130
DO 1800 J=1,NR
1800 CIN(NCON,J,NA)=B(NCON,J,NA)/C(NCON,NCON,NA)
K=NCON-1
1900 DO 1111 J=1,NR
IT=K+1
TEMP=0.0
DO 1110 I=IT,NCON
1110 TEMP=TEMP+C(K,I,NA)*CIN(I,J,NA)
1111 CIN(K,J,NA)=(B(K,J,NA)-TEMP)/C(K,K,NA)
K=K-1
IF(K.NE.0) GO TO 1900
RETURN
1120 CIN(NCON,NR,NA)=B(NCON,NR,NA)/C(NCON,NCON,NA)
RETURN
1130 CONTINUE
WRITE(*,120)
120 FORMAT(/10X,'*** MATRIX IS SINGULAR ***' )
WRITE(*,*)'ERROR IN SUBROUTINE GJELIM: MATRIX FOLLOWS'
DO 1066 I=1,NCON
WRITE(*,*)(C(I,J,NA),J=1,NCON)
1066 CONTINUE
STOP
END

```

```

FUNCTION HF(I,T,F)
$LARGE
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION F(*)
  HF = F(1+I)+(F(6+I)/T)+((F(2+I)/2.)*T)+((F(3+I)/3.)*(T**2))
+ ((F(4+I)/4.)*(T**3))+((F(5+I)/5.)*(T**4))
  RETURN
  END

FUNCTION DHF(I,T,F)
$LARGE
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION F(*)
  DHF=(F(2+I)/2.)+(-1.*F(6+I)/(T**2))+((2./3.)*F(3+I)*T)+
+ ((3./4.)*F(4+I)*(T**2))+((4./5.)*F(5+I)*(T**3))
  RETURN
  END

FUNCTION CPT(I,T,F)
$LARGE
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION F(*)
  CPT=F(1+I)+(F(2+I)*T)+(F(3+I)*(T**2))+((F(4+I)*(T**3))+
+ (F(5+I)*(T**4)))
  RETURN
  END

FUNCTION DCPT(I,T,F)
$LARGE
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION F(*)
  DCPT=F(2+I)+(2.*F(3+I)*T)+(3.*F(4+I)*(T**2))+((4.*F(5+I)*(T**3))
  RETURN
  END

FUNCTION ST(I,T,F)
$LARGE
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION F(*)
  ST=F(7+I)+(F(1+I)*LOG(T))+((F(2+I)*T)+((F(3+I)/2.)*(T**2))+
+ ((F(4+I)/3.)*(T**3))+((F(5+I)/4.)*(T**4)))
  RETURN
  END

FUNCTION DST(I,T,F)
$LARGE
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION F(*)
  DST=(F(1+I)/T)+F(2+I)+(F(3+I)*T)+(F(4+I)*(T**2))+((F(5+I)*(T**3))
  RETURN
  END

```

```

                FUNCTION F6(I,HOFT,T,F)
$LARGE
                IMPLICIT REAL*8(A-H,O-Z)
                DIMENSION F(*)
                X=HOFT-((T*F(1+I))+((F(2+I)/2.)*(T**2))+((F(3+I)/3.)*
                #(T**3))+((F(4+I)/4.)*(T**4))+((F(5+I)/5.)*(T**5)))
                F6=X
                RETURN
                END

```

```

                FUNCTION F7(I,SOFT,T,F)
$LARGE
                IMPLICIT REAL*8(A-H,O-Z)
                REAL*8 T,F7
                DIMENSION F(*)
                X=SOFT-((F(1+I)*DLOG(T))+((F(2+I)*T))+((F(3)/2.)*(T**2))
                #+((F(4+I)/3.)*(T**3))+((F(5+I)/4.)*(T**4)))
                F7=X
                RETURN
                END

```

```

                SUBROUTINE CVVIB(FREQ,T,CV,THETA)
$LARGE
                IMPLICIT REAL*8(A-H,O-Z)
                REAL*8 HP,KB,C,X,THETA,TEST
                HP=6.62517E-34
                KB=1.3804E-23
                C=2.998E+10
                IF(FREQ.GT.25000.0.OR.FREQ.LT.1.)THEN
                        CV=1000.
                        RETURN
                ENDIF
                IF(FREQ.NE.0.0)THEN
                        THETA=((HP*C)/KB)*FREQ
                ELSE
                        IF(THETA.EQ.0.)THEN
                                CV=1000.
                                RETURN
                        ENDIF
                ENDIF
                X=THETA/T
                IF(X.GT.230.)THEN
                        CV=1000.
                        RETURN
                ENDIF
                TEST=DEXP(X)
                IF(TEST-1.0.LT.10.0E-6)THEN
                        CV=100.
                        RETURN
                ENDIF

```

```

TOP=EXP(X)
BOTTOM=(TOP-1.0)**2
CV=(X**2)*(TOP/BOTTOM)
RETURN
END

```

```

SUBROUTINE SIGMACP(B)
IMPLICIT REAL*8(A-H,O-Z)
CHARACTER*70 FILPRN
DIMENSION B(*),CONST(3)
COMMON/CONST/CONST,NTERMS
WRITE(*,*)'ENTER PRN FILENAME'
READ(*,70)FILPRN
70  FORMAT(A70)
OPEN(12,FILE=FILPRN,STATUS='UNKNOWN')
T=100.
DO 100 I=1,60
CP=0.
DO 200 J=1,NTERMS
THETA=0.0
IF(NTERMS.EQ.1)THEN
CALL CVVIB(B(2),T,CV,THETA)
ELSE
CALL CVVIB(B(NTERMS+J-1),T,CV,THETA)
ENDIF
IF(J.NE.NTERMS.OR.NTERMS.EQ.1)THEN
TERM=B(J)*CV
ELSE IF(J.EQ.NTERMS.AND.NTERMS.NE.1)THEN
SUM=0.0
234 DO 234 IK=1,NTERMS-1
SUM=SUM+B(IK)
TERM=(CONST(2)-SUM)*CV
ENDIF
CP=CP+TERM
200 CONTINUE
CP=(CP+4.0)*1.987*CONST(1)
WRITE(12,*)T,CP
T=T+100.
100 CONTINUE
CLOSE(12,STATUS='KEEP')
RETURN
END

```



```

FUNCTION CP SERIES(B,T)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION B(6),CONST(3)
COMMON/CONST/CONST,NTERMS
CP=0.0
CV=0.0
DO 100 I=1,3
      CALL CVVIB(B(I+3),T,CV,THETA)
      CP=CP+(B(I)*CV)
100  CONTINUE
      IF(CONST(3).EQ.0.)THEN
*          NON-LINEAR
          CP=(CP+4.0)
      ELSE
*          LINEAR
          CP=(CP+(7./2.))
      ENDIF
CP SERIES=CP
RETURN
END

```

```

SUBROUTINE FOFX(I,X,B,Y,Z)
$LARGE
      IMPLICIT REAL*8(A-H,O-Z)
      DOUBLE PRECISION B,CONST,XIN,THETA,CV,TERM(3),SUM
      DIMENSION X(*),B(*),CONST(3)
      COMMON /CONST/ CONST,NTERMS
      XIN=X(1)
*      write(*,*)x(1),y
      Z=0.0
      DO 100 II=1,NTERMS
      THETA=0.0
      IF(NTERMS.EQ.1)THEN
          CALL CVVIB(B(2),XIN,CV,THETA)
      ELSE
          CALL CVVIB(B(NTERMS+II-1),XIN,CV,THETA)
      ENDIF
      IF(II.NE.NTERMS.OR.NTERMS.EQ.1)THEN
          TERM(II)=B(II)*CV
      ELSE IF(II.EQ.NTERMS.AND.NTERMS.GT.1)THEN
          SUM=0.0
234      DO 234 IK=1,NTERMS-1
          SUM=SUM+B(IK)
          TERM(II)=(CONST(2)-SUM)*CV
      ENDIF
      Z=Z+TERM(II)
100     CONTINUE
      IF(CONST(3).EQ.0.)THEN
*         non-linear molecule
          Z=(Z+4.0)*1.987*CONST(1)
      ELSE
*         linear molecule
          Z=(Z+(7./2.))*1.987*CONST(1)
      ENDIF
      RETURN
      END

```

```

SUBROUTINE PD(NDATA,X,NPARM,B,Y,ZZ,Z,PDERIV,NORMAL,WORK,POIN01)
$LARGE
      IMPLICIT REAL*8(A-H,O-Z)
      DOUBLE PRECISION NORMAL(7,7),WORK(*),B(*),DEL,POIN01,
+CONST(3),U,U1,DU,DU1,V,V1,DV,DV1,ALPHA,PRD,TERM1,TERM2,TERM3,
+TERM4,HP,KB,C
      DIMENSION X(1,20),Y(*),PDERIV(6,20),Z(*)
      INTEGER NDATA,NPARM
      COMMON/CONST/CONST,NTERMS
      HP=6.62517E-34
      KB=1.3804E-23
      C=2.998E+10

C      INITIALIZE NORMAL TO 0.0, ONLY THE PART OF
C      THE ARRAY THAT WILL BE USED
C
      DO 101 I = 1,NPARM+1
      DO 100 J = 1,NPARM+1
      NORMAL(J,I) = 0.0
100      CONTINUE
101      CONTINUE
*****
*      REPLACE THIS SECTION WITH EXPLICIT JACOBIAN
*
C      CALCULATE THE PARTIAL DERIVATIVES OF THE FUNCTION
C      VALUES WITH RESPECT TO THE PARAMETER VALUES FOR
C      EACH SET OF DATA POINTS. THESE DERIVATIVES WILL BE
C      STORED IN PDERIV.
C
      DO 200 J = 1,NDATA
      ALPHA=(HP*C)/(KB*X(1,J))
      U2=EXP(ALPHA*B(5))
      TERM3=(ALPHA*B(5))**2
      TERM4=(U2/((U2-1.0)**2))
      PRD=TERM3*TERM4
      DO 150 I=1,2
      U1=EXP(ALPHA*B(I+2))
      TERM1=(ALPHA*B(I+2))**2
      TERM2=(U1/((U1-1.0)**2))
      PDERIV(I,J)=(TERM1*TERM2-PRD)*1.987*CONST(1)
150      CONTINUE
      DO 1000 I=3,5
      U=(ALPHA*B(I))**2
      DU=2.0*(ALPHA**2)*B(I)
      U1=EXP(ALPHA*B(I))
      DU1=ALPHA*U1
      V1=(U1-1.0)**2
      DV1=(2.0*(U1-1.0)*DU1)
      V=U1/V1
      DV=((1.0/V1)*DU1)-((U1/(V1**2))*DV1)
      PDERIV(I,J)=(U*DV)+(V*DU)
      IF(I.LT.5)THEN
          PDERIV(I,J)=PDERIV(I,J)*B(I-2)*1.987*CONST(1)

```

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                ELSE
                    PDERIV(1,J)=PDERIV(1,J)*(CONST(2)-(B(1)+B(2)))*1.987*
+CONST(1)
                ENDIF
1000            CONTINUE
200            CONTINUE
*****
C
C            COMPUTE THE NORMAL EQUATIONS
C
DO 240 J1 = 1,NDATA
DO 230 J2 = 1,NPARM
230            WORK(J2) = PDERIV(J2,J1)
            WORK(NPARM+1) = Y(J1) - Z(J1)
DO 240 J3 = 1,NPARM+1
DO 240 J4 = J3,NPARM+1
240            NORMAL(J4,J3) = NORMAL(J4,J3) + WORK(J3) * WORK(J4)
            RETURN
            END

```