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# AN EXPERIMENTAL STUDY OF SEMI-CONTINUOUS <br> PH-PARAMETRIC PUMPING WITH A CENTER FEED 

BY
JOHN S. DELL'OSSO

A THESIS
PRESENTED IN PARTIAL FULFILLMENT OF
THE REQUIREMENTS FOR THE DEGREE
OF
MASTER OF SCIENCE IN CHEMICAL ENGINEERING
AT
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#### Abstract

Parametric pumping represents a new development in separation science. It has attracted considerable attention both because of its novelty and because it permits continuous operation in small equipment with very high separation factors. The basic principle of parametric pumping is to utilize the coupling of periodic changes in equilibrium conditions caused by periodic changes in some intensive variables (temperature, pH , electric field, etc.), and periodic changes in flow direction to separate the components of fluid which flows past a solid adsorbent. Applications of parametric pumping involving the separation of valuable materials such as proteins would be very attractive and profitable to investigate.


Many proteins are often processed batchwise. Parametric pumping offers the possibility of continuous processing, thereby tending to minimize both processing time and degradation. The overall objective of this research is to determine the feasibility of operating a semi-continuous pH-parametric pump for protein separation. The model system used is hemoglobin-albumin on sephadex ion exchange. It is hoped that the results of this work would be general enough to be invaluable in the separation of binary or multi-protein mixtures, and will provide necessary technical information for the design of full-scale parametric pumps with a sound engineering and economic basis.

# APPROVAL OF THESIS <br> AN EXPERIMENTAL STUDY OF SEMI-CONTINUOUS PH-PARAMETRIC PUMPING WITH A CENTER FEED BY <br> JOHN S. DELL'OSSO <br> FOR <br> DEPARTNENT OF CHEMICAL ENGINEERING <br> NE'N JERSEY INSTITUTE OF TECHNOLOGY 

BY

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APPROVED:

-


NEWARK, NEW JERSEY OCTOBER, 1976

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TABTE OF CONTENTS
Page
Scope 1.
Conclusions and Recommendations ..... 3.
Experimental 4.
Results and Discussion ..... 17.
Notation ..... 35.
References ..... 36.
Appendix ..... 38.
Table 1 ..... 39.
Table 2

$$
40
$$Table 341.

Table 4 ..... 42.
Table 5 ..... 43.
Table 6 ..... 45.
Table 7 ..... 46.
Table 8 ..... 48.
Table 9 ..... 54.
Table 10 ..... 60.
Table 11 ..... 66.

## TABIS CAPTIONG

```
TABLE 1: Calibration Curve (Hemoglobin-403mu)
TABLE 2: Calibration Curve (Hemoglobin-280mu)
TABIE 3: Calibration Curve (Albumin-280mu)
TABLE 4: Experimental Conditions for Batch Runs
TABIE 5: Experimental Conditions for Semi-Continuous Runs
Table 6: Batch Runs (Al,A2,A3)
Table 7: Run A4
Table 8: Run T1
TABLE 9: Run T2
TABLE 10: Run T3
TABLE 11: Separation Factors
```


## FIGURE CAPTIONS

| FIGURE 1: | Equipment Layout |
| :---: | :---: |
| FIGURE 2: | Calibration Curve (Hemoglobin-403mu) |
| FIGURE 3: | Calibration Curve (Hemoglobin-280mu) |
| FIGURE 4: | Calibration Curve (Albumin-280mu) |
| Figure 5: | Slope VS. PH (Hemoglobin-403mu) |
| FIGURE 6: | Slope VS. PH (Hemoglobin-280mu) |
| FIGURE 7: | Concentration Transient (Albumin - RunA 4 ) |
| Figure 8: | Concentration Transient (Hemoglobin - Run Tl) |
| FIGURE 9: | Concentration Transient (Albumin - Run Tl) |
| FIGURE 10: | Concentration Transient (Hemoglobin - Run T2) |
| FIGURE 11: | Concentration Transient (Albumin - Run T2) |
| FIGURE 12: | Concentration Transient (Hemoglobin - Run T3) |
| FIGURE 13: | Concentration Transient (Albumin - Run T3) |
| FIGURE 14: | Separation Factor VS. Cycles (Run A4) |
| FIGURE 15: | Separation Factor VS. Cycles (Run Tl) |
| FIGURE 16: | Separation Factor VS. Cycles (Run T2) |
| FIGURE 17: | Separation Factor VS. Cycles (Run T3) |
| FIGURE 18: | Hemoglobin Top Froducts |

SCOPE

The name "parametric pumping" was applied to the separation process in 1966 by the inventor of the batch pump, the late R. H. Wilhelm of Princeton University. Since the time of that invention, many experimental and theoretical extensions have been done on separation by thermal and heatless (or pressure cycling) parametric pumping. They include Wilhelm et. al. (1966, 1968), Jenczewski and Meyors (1968, 1970), Wilhelm and Sweed (1968), Pigford et. al. (1968), Horn and Lin (1969), Rolke and Wilhelm (1969), Aris (1968), Gregory and Sweed (1970, 1971, 1972), Turnock and Kadlec (1971), Butts et. al. (1972), Kowler and Kadlec (1972), Shendelman and Michell (1972), Weaver and Hamrin (1974), and Chen et. al. (1971, 1972, 1973, 1974a, 1974b, 1974c,1975, 1976) Comprehensive reviews of the subject have been made by sweed (1971), Wankat (1974), and Chen (1976). However, much less studies have been done on the pH -parametric pumping. Sabadell and sweed (1970) used pH changes to remove $\mathrm{K}^{\dagger}$ and $\mathrm{Na}^{\dagger}$ from $\mathrm{H}_{2} \mathrm{O}$. Shaffer and Hamrin (1975) studied trypsin removal from $\alpha$-chymotrypsin-trypsin mixtures by affinity chromatography and parametric pumping. In this work a semicontinuous pH-parametric pump for separating proteins will be experimentally investigated. The pump considered here has a center feed between an enriching column and stripping column, and is operated batchwise during upflow and continuous during downflow.

Techniques commonly used for the separation of proteins include: gel filtration, affinity chromatography, ion exchange chromatography, etc. The proposed semi-continuous pH-parametric pumping has several advantages over the conventional separation methods.

1) Many proteins are often processed batchwise. Parametric pumping offers the possibility of continuous processing, thereby tending to minimize both processing time and degradation.
2) No regeneration chemicals are needed for the continuous process, and no regenerant can contaminate the product.
3) The continuous process can be achieved with very high separation factors, and the components removed can be concentrated to any desired practical level by setting the flow rate of the product stream containing these components at the required value.
4) Control problems for the continuous process may be simpler compared to those for competing batch processes.

## CONCLUSIONS AND RECOMENDATTONS

Semi-continuous pH-parametric pumping for separating hemoglobin and albumin was experimentally investigated. A sephadex ion exchange was used as an adsorbent. The feed is introduced between the enriching and stripping columns. The pump is operated batchwise during upflow and continuous during downflow. It has been shown that the pump has the capibility for separating protein mixtures.

It is recommended to try different ion exchanges and to extend the process to a true continuous one, that is with feed and product removal during both up and down flow. Also, the effect of the buffer's ionic strength on the separation should be studied or investigated.

## EXPERIMENTAL

## A. EQUIPVENT

The experimental apparatus used in this research is shown in figure l. The equipment consists of two jacketed Pharmacia chromatographic columns (1.6 X 40 cm. ) packed with a sephadex gel. The top column can be considered the stripping section, while the bottom is the enriching section. Feed is introduced between the enriching and stripping sections. Constant temperature of the column is maintained by the use of a Brinkmann Instrument unit. It circulates cooling water at $281^{\circ} \mathrm{K}$, which prevents the proteins from denaturing, The reciprocating pumping of the reservoirs and the introduction of the feed into the system was accomplished by the use of two infusion-withdrawal syringe pumps, which were manufactured by Harvard Apparatus. The reservoir pumps are fitted with two $50-\mathrm{cm} 3$ glass syringes and the feed pump is fitted with one. The fluid is pumped through the system using capillary tubing ( $0.1 \mathrm{~cm} . i d, 0.18 \mathrm{~cm}$. od). To insure perfect mixing, small magnetic stirrers were employed in both reservoir syringes,

The change of pH was accomplished by the use of two dialysis cells. The particular cells used were made by Bio-Rad and were the bio-fiber 50 beaker model. The fibers
are made of cellulose and have a total surface area of $900 \mathrm{~cm}^{2}$. The nominal molecular weight cut off for this model is 5,000. The jacket volume is 100 cm . A buffer is ciroulated in the jacket part of the dialysis cell, while the solution which wishes to change its pH is passed through the fibers. The buffer employed is a mixture of monobasic sodium phosphate and dibasic sodium phosphate. For the low pH reservoir $(\mathrm{pH}=6.0)$, the proportion is $87.7 \%$ monobasic sodium phosphate and $12.3 \%$ dibasic sodium phosphate. For the high pH reservoir ( $\mathrm{pH}=8.0$ ) , the proportion is $5.3 \%$ monobasic sodium phosphate and $94.7 \%$ dibasic sodium phosphate (Colowick \& Kaplin, 1955). The concentration strength of both buffers is $0.1 \mathrm{M} . \mathrm{A} 2,000 \mathrm{~cm}$. reservoir is used for the circulation of fresh buffer through each dialysis cell. A Bio-Rad peristaltic pump is used to circulate the buffer at $0.33 \mathrm{~cm}^{3}$ per second. To eliminate stagnation of the buffer, magnetic stirrers are placed in the bottom of the dialysis cells.

Top and bottom product samples are collected with Gilmont micrometric capillary valves. These valves are used both to regulate and to impose a small back pressure on the flow of the fluid in the system. The samples are measured on a Beckmann DU spectrophotometer. A minimum of $2.6 \mathrm{~cm}^{3}$ is needed for analysis.

Prior to each run, all the air is removed from the
connecting tubing. This is done by filling all the lines with feed solution. Low pH feed is used for the tubing leading to and from the enriching section, while high pH feed is used for the lines leading to and from the stripping section.

The specific packing used is SP-sephadex (C-50). Preparation of the packing has been standardized in order to produce similar starting conditions for the runs. Initially, the packing was allowed to expand in $40 \mathrm{~cm}^{3}$ of low pH buffer. After 24 hours, $10 \mathrm{~cm}^{3}$ of the top liquid was decanted off and replaced with $100 \mathrm{~cm}^{3}$. of low pH feed. After another 24 hours, $100 \mathrm{~cm}^{3}$. of the liquid phase was decanted off, leaving the gel ready to be poured into the column. The pouring of the packing into the column has to be done in a careful manner. The technique employed is to pour the gel slowly down a glass rod, allowing the packing to settle without trapping any air. The remaining air in the tubing leading into the connectors of the column is blown out by compressing the packing slightly, replacing the air with some of the fluid phase. Then the column is sealed and the run is ready to start.


## B. MEASUREMENI

In order to determine the concentrations of the samples, three calibration curves must be prepared. Hemoglobin will absorb light at a wavelength of 403 mu and 280 mu , while albumin will absorb light only at 280 mu . A wavelength of 403 mu is in the visible spectrum, while 280 mu is in the ultra-violet range. For the hemoglobin, twenty known concentrations ranging from a weight percent of 0.001 to a weight percent of 0.010 in equal increments are measured at both wavelengths. Three sets of data points are made up for pH's of $6.0,7.0$, and 8.0 . Initially, the four cells that are to be used for the measurements are filled with deionized water in order to calibrate them for any differences in transmission that they may have. The readings of the samples are then divided by this correction factor and multiplied by one hundred in order to get the actual transmission of the sample. When the readings for the samples are made, the first cell is the reference and is filled with the corresponding $p H$ buffer as of the sample. The buffer is 0.05 M and is of the same type that is actually used in the experiment. The remaining three cells are filled with the samples, and the readings are recorded in percent transmission. The absorbance is found by the simple relationship that it is equal to the common $\log$ of one hundred divided by the transmission $A \log (100 / T)$. Now absorbance is plotted
against percent concentration on linear coordinates. A linear regression is performed on each set of data points, and the best straight line that passes through the origin is dram. For 403 mu the slope, $\lambda$, at $\mathrm{pH}=6.0$ is 59.82, at $\mathrm{pH}=7.0 \hat{\lambda}=56.12$, and at $\mathrm{pH}=8.0 \lambda=53.88$. This calibration curve is depicted in figure 2. As the pH decreases the slope increases. For $280 \mathrm{mu} \lambda$ at $\mathrm{pH}=6.0$ is 16.49 , at $\mathrm{pH}=7.0$ $\lambda=27.40$, and at $\mathrm{pH}=8.0 R=14.95$. This calibration curve is shown in figure 3. At this wavelength, a maximum at a certain pH seems to occur. A rough working plot of slope verus pH is done at both frequencies (figures 5 \& 6). Although these plots will not give exact slopes at a particular pH, they will give one within the accuracy of the spectrophotometer readings.

The albumin calibration curve at 280 mu (figure 4) is done in a similar fashion with the exception that the concentration range is increased because of the less sensitivy of the absorbance of albumin. There are twenty-two points ranging from a percent concentration of 0.005 to 0.100. The corresponding slopes for pH's of $6.0,7.0$, and 8.0 are $5.054,5.013$, and 4.995 respectively. The slopes seem to be relatively constant, indicating that pH has little affect on the readings of the samples. An average slope of 5.021 will be used in the calculations.

The samples for the runs are measured in the following manner. The first cell will contain the reference. For the top product, the reference will be the low pH buffer and for the bottom product it will be the high pH buffer. The remaining three cells will contain the samples. Readings will be taken at both 403 mu and 280 mu . The same procedure as before is used to calculate the absorbance of both the samples and the feed. Each sample is tested for pH and the appropriate slopes, which are obtained from figures 5 and 6, is used in the following calculations. for hemoglobin, the procedure for calculating the concentration is straight forward. The absorbance of the sample is divided by the slope of the calibration curve at 403 mu . The feed absorbance is also divided by its slope to determine the feed concentration. To normalize the results the concentration of the sample is divided by the concentration of the feed.

Since the concentrations that are used in the experiment are dilute, advantage can be taken of the additive property of absorbances for two components at a certain frequency in order to calculate the concentration of albumin. First the contribution of hemoglobin is found by multipling the concentration of hemoglobin, which was already found at 403 mu , by the corresponding slope of the calibration curve at 280 mu . This will give the absorbance
that is contributed by the hemoglobin. This value is subtracted from the total absorbance at 280 mu , and this will give the contribution due to albumin. This value is then divided by the slope of the albumin calibration curve, which finally leads to the concentration of albumin. The same procedure is followed for the feed reading and the sample is normalized as before.


FIGURE 2
CALIBRATION CURVE
(HEMOGLOBIN -403 mu )

figure 3

CALIBRATION CURVE
(HEMOGLOBIN-280 mu)


FIGURE 4

CALIBRATION CURVE
(ALBUMIN-280 mu)


FIGURE 5

SLOPE VS. PH
(HEMOGLOBIN - 403 mu )


FIGURE 6

SLOPE VS. PH
(HEMOGLOBIN - 280 mu )

## RESULTS AND DISCUSSION

Seven runs were carried out on the system, four were binaries and three were ternaries. Tables 4 and 5 lists the experimental conditions for all the batch and semicontinuous runs. Tables 6-10 contain the experimental data and results, and the final table, number ll, contains the separation factors for the runs. Comprising the binary runs were three batch operations and one of the semi-continuous mode done on the albumin-water system. The batch operation is a slight modification of figure 1 . The exceptions are that it was performed with a single column and there is no feed or product removal. Initially, 15 cm . of feed solution was put in the top syringe and $5 \mathrm{~cm}^{3}$. was put in the bottom syringe. The run started with a downward half-cycle and proceeded with its reciprocating motion for the required amount of cycles. The semi-continuous mode is one where the feed and the product removal is done on only one of the halfcycles. Run 44 was performed with a sincle column and both feed introduction and product removal was done on the downward half-cycle.

The batch runs indicate that there is very little difference in the concentrations at the top and bottom of the column. This can be expected because the column is operated between pH reservoirs of 6.0 and 8.0 , and the isoelectric point of albumin is 4.9. The isoelectric point is the particular
pH that a protein exhibits a net charge of zero. Above this point the protein will exhibit a net negative charge and below this point the net charge would be positive. The sephadex packing is negative and hence the albumin will be repelled, allowing it to flow through the column with little resistance. The concentration of albumin at the top of the column seems to be slightly higher than that of the bottom. This slight difference can be contributed to the fact that the pH of the top is 6.0 versus 8.0 at the bottom. At a pH of 6.0, albumin is a little bit less negative than at 8.0, and this difference will cause a slight attraction towards the top. The lower concentrations for run A3 is due to the added number of cycles. Ten cycles are not enough for the system to reach steady state. Eventually at steady state, the ratio of the concentrations in the reservoirs to that of the feed will approach unity. The results of the batch runs are listed in table 6.

The semi-continuous binary run for albumin seems to follow the batch results. Initially, there is a transient period with a lot of scattering and then both the top and bottom product concentrations approach unity. Pigure 7 is a plot of sample concentration divided by feed concentration versus cycles ( $Y_{A S} / Y_{A F} V S, n$ ) for run A4. Another plot for run $A 4$ is separation factor versus cycles and this is shown in figure 14. Separation factor is defined as the concentration
of the bottom product divided by the concentration for the top product.

The three ternary runs consist of two done with the single column, similar to run $A 4$, and the last run performed with the double column, run T3. The experimental conditions for runs Tl and T2 where similar with the exception that in run $\mathrm{T} 2,0.05 \mathrm{M} \mathrm{NaCl}$ was added to both the feed and the packing. Salt was added to try to break up the attration albumin and hemoglobin would have for each other due to opposite charges. The results indicated that the salt had little or no effect and this can be seen by the similarity between figures 8 and 10 . For the bottom hemoglobin product, both curves show an initial peak followed by a steady decline and then a leveling out to a value of a little bit under the feed. The top products seem to exhibit an initial transient period and then the concentrations level off. The separation factor for the hemoglobin for both runs is about 1.2. The plots for the separation factor versus cycles are also similar. The curves can be compared to the characteristic shape of the bottom products, an initial peak followed by a decline and leveling ofr. These plots are devicted in rigures 15 and 16.

The plots for the albumin, figures 9 and 11, have a great deal of scattering in them, but the general trend seems to agree with the binary results. Eventually after
an initial transient period the concentration at the top and the bottom of the column will level off to unity. The scattering in the curves can be contributed to two main factors. The first is the sensitivity of the albumin calibration curve compared with the hemoglobin calibration curve. Albumin is much less sensitive to ultra-violet light than hemoglobin. Through the manipulations that have to be performed to get a final albumin concentration, any error or fluctuation in the initial reading would lead into a considerable difference in the final results. It is recommended that further study should be made in albumin measuring technique. The second factor is that the semicontinuous runs were performed on two separate days, with a stoppage in operation between days. This stoppage can be seen in the sharp rise in the concentration of the albumin. Some of these points were eliminated from the graphs for this reason. The concentration rise is due to the mass transfer of the albumin. Since albumin and the packing have the same charge, the albumin wants to escape from the packing and go into the reservoirs.

For runs A4, Tl, and T2 the top product was combined for each three consecutive cycles. The products were combined in order to get enough sample for measurement. The concentration for these samples were reported for the middle cycle.

The final run performed on the system was T3, which used the apparatus pictured in figure 1. By using stripping and enriching sections with feed introduced between sections, the separation was vastly improved. The hemoglobin can now be trapped in the bottom or enriching section, while the top or stripping section can be relatively free of hemoglobin. Ficure l2 helps point out these results, by showing the concentrations of the top and bottom products for hemoglobin. Figure 13 is a plot for albumin and follows the preceding albumin results. The scattering can also be explained by the two preceding reasons. Separation factor versus cycles has been plotted in figure 17. The final separation factor is around 4 which is far superior to runs Tl and T2 which had separation factors around 1.2. A final plot, figure 18, is a comparison of the top hemoglobin products for runs H14(Falcon, 1976). T1, and T3. The plot exemlifies two points. The first is the superiority of the double column over the single one. The second is the lowering of the efficiency of the column by the attraction between the hemoglobin and albumin. Runs 114 and Tl were performed under the same conditions except for the fact that TI had the additional protein albumin. Even with this lowering of the efficiency, the double column produced a low concentration of hemoglobin in the top or stripping section.

No attempt at optimizing the process was tried in this thesis. The primary objective was to show the future for pH -parametric pumping. The results from run T3 are good enough to indicate the viability of pH-parametric pumping as a separation process for human or natural proteins.



FIGURE 8 (RUN T1)
CONCENTRATION TRANSIENT (hemoglobin)


CONCENTRATION TRANSIENT
(ALBUMIN)






FIGURE 14 (RUN A4)

SEPARATION FACTOR VS. CYCLES


SEPARATION FACTOR VS. CYCLES


SEPARATION FACTOR VS. CYCLES


SEPARATION FACTOR VS.CYCLES


FIGURE 18

HEMOGLOBIN TOP PRODUCTS

## NOTATION

A - Absorbance
n - number of cycles
S.F. - Separation Factor

T - Transmission
Y - Concentration
$Y_{4 s}$ - Hemoglobin concentration of the sample
$Y_{H F}$ - Hemoglobin concentration of the feed
Yas - Albumin concentration of the sample
$Y_{A F}$ - Albumin concentration of the feed
$\lambda$ - Slope

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APPENDIX

TABLES

## ZASLE 1: CALIBRAPIOR CUEVE - KBOGECBIE 403mu

| CONCMTRPASION | $\begin{gathered} (\mathrm{PH}=6.0) \\ \mathrm{ABSOQBAPCE} \end{gathered}$ | $\begin{gathered} (\mathrm{PH}=7.0) \\ \text { ABSOREAICCE } \end{gathered}$ | $\begin{gathered} (\mathrm{PH}=8.0) \\ \mathrm{ABSOR} \mathrm{ABCB} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| 0.001 | 0.047 | 0.091 | 0.056 |
| 0.002 | 0.090 | 0.101 | 0.076 |
| 0.003 | 0.161 | 0.162 | 0.107 |
| 0.004 | 0.227 | 0.217 | 0.262 |
| 0.005 | 0.276 | 0.261 : | 0.302 |
| 0.006 | 0.342 | 0.303 | 0.326 |
| 0.007 | 0.409 | 0.410 | 0.428 |
| 0.008 | 0.465 | 0.467 | 0.440 |
| c. 009 | 0.538 | 0.479 | 0.561 |
| 0.010 | 0.590 | 0.573 | 0.578 |
| 0.011 | 0.652 | 0.640 | 0.572 |
| 0.012 | 0.730 | 0.629 | 0.629 |
| 0.013 | 0.783 | 0.699 | 0.697 |
| 0.014 | 0.830 | 0.807 | 0.728 |
| 0.015 | 0.893 | 0.848 | 0.848 |
| 0.016 | 0.955 | 0.955 | 0.827 |
| 0.017 | 1.051 | 0.951 | 0.914 |
| 0.018 | 1.086 | 1.032 | 0.996 |
| 0.019 | 1.125 | 1.076 | 0.991 |
| 0.020 | 1.208 | 1.076 | 1.046 |
| $\begin{array}{ll} A=59.82 C & (P H=6.0) \\ A=56.12 C & (P H=7.0) \\ A=53.88 C & (P H=8.0) \end{array}$ |  |  |  |

TABLE 2: CALIBRATION CURVE - HMOOIOSII SSOM

| CONCATR2ATION | $\begin{gathered} (\mathrm{PH}=6.0) \\ \mathrm{ABSORBANCE} \end{gathered}$ | $\begin{gathered} (\mathrm{PH}=7.0) \\ \mathrm{ABSORBA} \mathrm{CE} \end{gathered}$ | $\begin{gathered} (\mathrm{PH}=\mathrm{B}, 0) \\ \mathrm{ABSO9BM50} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| 0.001 | 0.021 | ------ | 0.028 |
| 0.002 | 0.030 | 0.034 | 0.052 |
| 0.003 | 0.052 | 0.071 | 0.082 |
| 0.004 | 0.077 | 0.048 | 0.085 |
| 0.005 | 0.093 | 0.099 | 0.116 |
| 0.006 | 0.107 | 0.114 | 0.114 |
| 0.007 | 0.120 | 0.126 | 0.115 |
| 0.008 | 0.128 | 0.144 | 0.118 |
| 0.009 | 0.137 | 0.164 | ----- |
| 0.010 | 0.162 | 0.156 | 0.139 |
| 0.011 | 0.192 | 0.212 | 0.153 |
| 0.012 | 0.193 | 0.207 | 0.203 |
| 0.013 | 0.213 | ------ | 0.214 |
| 0.014 | 0.244 | 0.240 | 0.207 |
| 0.015 | 0.245 | 0.278 | 0.239 |
| 0.016 | 0.268 | ------ | 0.222 |
| 0.017 | 0.283 | 0.285 | 0.228 |
| 0.018 | ---- | 0.313 | 0.261 |
| 0.019 | 0.305 | - | 0.282 |
| 0.020 | 0.322 | 0.335 | 0.286 |
|  | $\begin{aligned} & A=16.49 \mathrm{C} \\ & A=17.40 \mathrm{C} \\ & A=14.95 \mathrm{C} \end{aligned}$ | $\begin{aligned} & (\mathrm{PH}=6.0) \\ & (\mathrm{PH}=7.0) \\ & (\mathrm{PH}=8.0) \end{aligned}$ |  |

TABLE 3: CALTBRAPIOX CURVE - ALBUMI. 280Mu

| CONCTITRATION | $\begin{gathered} (\mathrm{PH}=6.0) \\ \mathrm{ABSORBANCE} \end{gathered}$ | $\begin{gathered} (\mathrm{PH}=7.0) \\ \mathrm{ABSORBANCD} \\ \hline \end{gathered}$ | $\begin{array}{r} (P=8.0) \\ -A B S O 2 . E A C B \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: |
| 0.005 | 0.028 | 0.011 | 0.004 |
| 0.008 | 0.032 | 0.036 | 0.008 |
| 0.011 | 0.038 | 0.042 | 0.029 |
| 0.014 | 0.068 | 0.049 | 0.047 |
| 0.017 | 0.072 | 0.052 | 0.062 |
| 0.020 | 0.109 | 0.080 | 0.073 |
| 0.025 | 0.138 | 0.135 | 0.122 |
| 0.030 | 0.149 | 0.154 | 0.146 |
| 0.035 | 0.178 | 0.178 | 0.178 |
| 0.040 | 0.204 | 0.206 | 0.184 |
| 0.045 | 0.224 | 0.221 | 0.277 |
| 0.050 | 0.257 | 0.246 | 0.244 |
| 0.055 | 0.280 | 0.281 | 0.235 |
| 0.060 | 0.295 | 0.321 | 0.289 |
| 0.065 | 0.323 | 0.331 | 0.298 |
| 0.070 | 0.353 | 0.354 | 0.354 |
| 0.075 | 0.373 | 0.373 | 0.363 |
| 0.080 | 0.389 | 0.410 | 0.393 |
| 0.085 | 0.434 | 0.424 | 0.441 |
| 0.090 | 0.450 | 0.441 | 0.481 |
| 0.095 | 0.491 | 0.478 | 0.502 |
| 0.100 | 0.520 | 0.498 | 0.493 |
|  | $\begin{aligned} & A=5.054 C \\ & A=5.013 C \\ & A=4.995 C \end{aligned}$ <br> Averace S | $\begin{gathered} (\mathrm{PH}=6.0) \\ (\mathrm{PH}=7.0) \\ (\mathrm{PH}=8.0) \\ \mathrm{PDe}=5.021 \end{gathered}$ |  |

## Packing Height

Al - 9.6 Cm .
A? - 10.1 Cm .
A3 - 11.3 Cm .
Displacement
$10 \mathrm{Cm}^{3}$. for all runs
Dead Volumn
$5 \mathrm{Cm}^{3}$. for all runs
Plow Rate for Sjringe Reservoirs
$0.00833 \mathrm{~cm}^{3}$. $/ \mathrm{sec}$ 。
High PH Buffer
PH-8.0 (.05M) for all runs
Low PH Burfer
PH-6.0 (.05M) for all runs
Initial Reservoir Concentration
$.05 \%$ Albumin for a.ll runs
Initial PH of Packina

$$
\text { AI }-6.0
$$

A2 -8.0
A3 -6.0
number of cycles for the Run
Al - 10
A2 - 10
A3-17

## Type of Bun

A4 - binary for Albumin performed with single column
Tl - ternary performed with single column
T 2 - teraary with .05 M \%aCl added to feed and packing performed with single column
T3 - ternary performed with double column with reed between columns

Packing Height

$$
\mathrm{A} 4-9.4 \mathrm{Cm} .
$$

$$
\mathrm{Tl}-9.1 \mathrm{~cm} .
$$

$$
\mathrm{T} 2-8.3 \mathrm{~cm} .
$$

$$
\mathrm{T} 3-8.6 \mathrm{~cm} \cdot \text { (bottom), } 8.5 \mathrm{Cm} . \text { (top) }
$$

Displacement
$12 \mathrm{Cn}^{3}$. for all runs
Dead Volumn
5 Cm . for all runs
Flow 只ate for Syringe Reservoirs
$0.00833 \mathrm{Cm}_{3}^{3} / \mathrm{sec}$ 。
Flow Rate for Peed
$0.00283 \mathrm{Cr}^{3}$. $/ \mathrm{sec}$. for $\mathrm{A} 4, \mathrm{Tl}, \mathrm{T} 2$
$0.00417 \mathrm{~cm} 3 / \mathrm{sec}$. for T 3
High PH Buffer
PH-8.0 (.10H) for all runs
Low PH Buffer
PH-6.0 (.10M) for all runs
Feed Concentration
A4 - . O1\% Albumin (High PH)
T1 - . Ol\% Albumin, . Oi\% Hemoglobin (High PH)
T2-.01\% Albumin, .01\% Hemoglobin, . O5 HaCl (high PH )
T3 - . $01 \%$ albumin, . $01 \%$ hemoglobin (Low PH)

## TABLE 5 - Continued

Initial PH of Packins
6.0 for all runs

Yumber of Cycles for the Bun
21 for all runs

## PABLD 6: BATCH RUNS (AI, A2, A3)

| RUN | SAMPLT | $\begin{gathered} (280) \\ \text { TRAMMSION } \\ \hline \end{gathered}$ | $\begin{gathered} (280) \\ \text { ABSORSACE } \end{gathered}$ | ALbUMI: COHCESTRAMION | $\frac{Y_{A S}}{Y_{A F}}$ | eparation FACMOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Al | RB | 40.9 | 0.388 | 0.07728 | 1.61 |  |
|  | RT | 37.2 | 0.429 | 0.08544 | 1.78 | 0.90 |
|  | PEED | 57.4 | 0.241 | 0.04800 | ---- |  |
| A2 | 2 B | 37.2 | 0.429 | 0.08544 | 1.65 |  |
|  | RT | 35.6 | 0.449 | 0.03942 | 1.73 | 0.96 |
|  | FED | 54.9 | 0.260 | 0.05178 | ---- |  |
| A3 | $2 B$ | 44.9 | 0.348 | 0.06931 | 1.35 |  |
|  | RT | 41.7 | 0.380 | 0.07568 | 1.47 | 0.92 |
|  | F32 | 55.2 | 0.258 | 0.05138 | ---- |  |


| GAMPLE | Amounc OOLLBCH | $)^{3}$ <br> PH | $\begin{gathered} (280) \\ \text { MRANSISSION } \end{gathered}$ | $\begin{gathered} (280) \\ \text { ABSORBAHCE } \end{gathered}$ | ALBUMIN <br> CONCHITRATION | $\frac{\text { YAS }}{Y_{A F}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IB | 2.6 | 7.25 | 62.2 | 0.206 | 0.04103 | 2.78 |
| 1T | 1.1 | ---- | ---- | ------ | -------- | ---- |
| 23 | 2.7 | 7.40 | 64.4 | 0.191 | 0.03804 | 2.58 |
| 2 T | 1.0 | 6.05 | 66.4 | 0.178 | 0.03545 | 2.41 |
| 3B | 2.7 | 7.65 | 72.6 | 0.139 | 0.02768 | 1.88 |
| $3 T$ | 1.0 | ---- | ---- | ------ |  | ---- |
| 4 B | 2.8 | 7.80 | 71.4 | 0.147 | 0.02928 | 1.99 |
| 4 T | 1.2 | ---- | ---- | ----- | -------- |  |
| 5 B | 2.7 | 7.80 | 67.5 | 0.170 | 0.03386 | 2.30 |
| 5 P | 0.9 | 6.00 | 75.6 | 0.122 | 0.02430 | 1.64 |
| 6 B | 2.9 | 7.85 | 69.2 | 0.160 | 0.03187 | 2.16 |
| $6 T$ | 1.1 | ---- | ---- | ------ | -------- | ---- |
| 7 B | 2.9 | 7.90 | 60.3 | 0.220 | 0.04382 | 2.97 |
| 7T | 1.1 | ---- | ---- | ----- | -------- | ---- |
| 8B | 2.9 | 7.95 | 77.7 | 0.110 | 0.02191 | 1.49 |
| 89 | 1.0 | 6.05 | 75.7 | 0.121 | 0.02410 | 1.64 |
| 93 | 2.9 | 8.00 | 69.7 | 0.157 | 0.03127 | 2.12 |
| 9 T | 1.1 | ---- | ---- | ----- | -------- | ---- |
| 10 B | 2.7 | 7.90 | 66.5 | 0.177 | 0.03525 | 2.39 |
| 109 | 1.6 | ---- | ---- | ------ | -------- | ---- |
| 11 B | 2.8 | 8.00 | 72.5 | 0.140 | 0.02788 | 1.89 |
| 117 | 0.8 | 6.10 | 61.9 | 0.208 | 0.04143 | 2.81 |
| 12 B | 2.8 | 7.95 | 66.4 | 0.178 | 0.03545 | 2.41 |
| 12 T | 0.9 | ---- | ---- | ----- | -------- | ---- |
| 13 B | 2.7 | 7.90 | 68.4 | 0.165 | 0.03286 | 2.23 |
| 13T | 1.2 | ---- | ---- | ----- | ------ | ---- |

## MABLE 7- Continued

| SAMPLE | Arfourt <br> COLSTCT | $i^{3}$ | $\begin{gathered} (280) \\ \text { MRTMISSION } \end{gathered}$ | $\begin{gathered} (280) \\ \text { ABSOPBAMCE } \end{gathered}$ | $\begin{aligned} & \text { GLBMMIN } \\ & \text { CONCEMRAIION } \\ & \hline \end{aligned}$ | $\begin{aligned} & Y A S \\ & Y \mathrm{YAF} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 143 | 3.0 | 8.00 | 66.5 | 0.177 | 0.03525 | 2.39 |
| 14T | 1.0 | 6.05 | 71.2 | 0.148 | 0.02948 | 2.00 |
| 15B | 2.8 | 8.00 | 74.0 | 0.131 | 0.02609 | 1.77 |
| 15T | 1.0 | ---- | ---- | ---- | -------- | ---- |
| 16B | 3.0 | 7.95 | 72.1 | 0.142 | 0.02828 | 1.92 |
| 16T | 1.0 | ---- | ---- | ----- |  | ---- |
| 17B | 3.0 | 8.00 | 76.7 | 0.115 | 0.02290 | 1.55 |
| 179 | 1.1 | 6.10 | 64.5 | 0.190 | 0.03784 | 2.57 |
| 183 | 3.0 | 8.00 | 73.1 | 0.136 | 0.02709 | 1.84 |
| 18T | 0.9 | ---- | --- | ----- | -------- | ---- |
| 19B | 2.6 | 8.00 | 77.1 | 0.113 | 0.02251 | 1.53 |
| 19T | 0.7 | ---- | ---- | ----- | -------- | ---- |
| 20 B | 2.9 | 8.00 | 78.3 | 0.106 | 0.02111 | 1.43 |
| 207 | 2.3 | 6.15 | 67.6 | 0.170 | 0.03386 | 2.30 |
| 21. ${ }^{\text {B }}$ | 3.2 | 8.00 | 82.7 | 0.082 | 0.01633 | 1.11 |
| 211 | 1.1 | -- | ---- | ----- | ------- | ---- |
| RB | --- | 7.90 | 81.0 | 0.092 | 0.01832 | 1.24 |
| RT | - | 6.10 | 64.2 | 0.192 | 0.03824 | 2.59 |
| FAED | --- | 8.00 | 84.4 | 0.074 | 0.01474 | ---- |


| SATPLE | $\begin{aligned} & \text { AMOUNT (MA) } \\ & \text { COLIECTED } \end{aligned}$ | $3$ <br> $\xrightarrow{\mathrm{PH}}$ | $\begin{gathered} (403) \\ \text { TRASMSION } \end{gathered}$ | $\begin{gathered} (280) \\ \text { RPAKISSION } \end{gathered}$ | $\begin{gathered} (403) \\ \text { ABSORBANCE } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1B | 3.0 | 6.95 | 52.7 | 58.4 | 0.278 |
| $1 T$ | 1.0 | ---- | ---- | ---- | ----- |
| 2 B | 3.3 | 7.20 | 26.1 | 51.8 | 0.583 |
| 2 T | 0.9 | 6.05 | 41.5 | 48.6 | 0.382 |
| 3 B | 3.0 | 7.30 | 15.8 | 45.7 | 0.801 |
| 3 T | 1.1 | ---- | ---- | ---- | ----- |
| $4 B$ | 3.0 | 7.55 | 14.1 | 41.1 | 0.851 |
| 4 T | 1.0 | ---- | ----- | ---- | ----- |
| 5B | 3.2 | 7.70 | 16.2 | 41.8 | 0.790 |
| 5 T | 0.8 | 6.00 | 39.8 | 63.6 | 0.400 |
| 6 B | 2.9 | 7.80 | 20.4 | 46.8 | 0.690 |
| 6 T | 1.3 | ----- | ---- | ---- |  |
| 7 B | 3.0 | 7.80 | 23.9 | 49.7 | 0.622 |
| 7 T | 1.1 | ---- | --- | ---- | ----- |
| 8B | 2.8 | 7.90 | 25.4 | 53.0 | 0.596 |
| 8T | 1.3 | 6.10 | 34.2 | 66.9 | 0.466 |
| 9 B | 3.0 | 7.90 | 27.0 | 43.8 | 0.568 |
| $9 T$ | 0.9 | --- | - | --- | ------ |
| 10B | 3.0 | 7.95 | 30.4 | 53.1 | 0.517 |
| 10T | 1.0 | -- | ---- | -- | ---m- |
| I1B | 3.0 | 7.95 | 32.8 | 56.8 | 0.484 |
| 11T | 1.0 | 6.10 | 39.8 | 59.4 | 0.400 |
| 12 B | 3.1 | 7.90 | 32.5 | 35.4 | 0.488 |
| 12T | 1.1 | ---- | ---- | -- | -----. |
| 13B | 2.9 | 8.00 | 32.3 | 34.6 | 0.491 |
| 13T | 1.0 | ---- | --- | ---- | ----- |

## TABLE 8 - Continued

AMOUTM (CM) ${ }^{3}$ (403) (280) (403)

SAMPLE COLLECTED PH TRMSMISSICN PRASMISSION ABSORBANCE

| 14B | 3.0 | 7.95 | 34.7 | 42.3 | 0.460 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14 T | 1.1 | 6.10 | 36.7 | 54.5 | 0.435 |
| 15B | 3.0 | 7.90 | 37.6 | 49.4 | 0.424 |
| 15T | 1.0 | ---- | ---- | ---- | ------ |
| 16 B | 3.0 | 7.95 | 37.3 | 47.0 | 0.428 |
| $16 T$ | 1.0 | --- | ---- | --- | --- |
| 178 | 3.0 | 8.10 | 36.3 | 54.4 | 0.440 |
| 17 T | 1.2 | 6.15 | 39.4 | 53.7 | 0.405 |
| $18 B$ | 3.1 | 8.00 | 37.1 | 54.2 | 0.430 |
| 181 | 1.1 | -- | ---- | ---- | ------ |
| 19B | 3.1 | 7.95 | 37.1 | 61.0 | 0.430 |
| 19 T | 1.0 | ----- | ---- | ---- | ----- |
| 20B | 3.0 | 8.00 | 36.9 | 57.1 | 0.433 |
| 20 T | 1.4 | 6.10 | 40.1 | 63.1 | 0.397 |
| 213 | 3.1 | 7.95 | 37.9 | 63.6 | 0.421 |
| 211 | 0.9 | ---- | ---- | --- | ------ |
| RB | --- | 7.95 | 37.6 | 61.7 | 0.424 |
| RT | --- | 6.15 | 35.4 | 62.6 | 0.451 |
| FEED | --- | 8.00 | 32.3 | 60.8 | 0.491 |


| SMPLT | $\begin{gathered} \text { (280) } \\ \text { ABSORSACE } \end{gathered}$ | HBMOGIO BIit (280) contribution | albumill (280) COMTRIBUTION | $\underline{\lambda H 403}$ | 入H280 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 B | 0.235 | 0.086 | 0.149 | 56.23 | 17.36 |
| 17 | ----- | ------ | ----- | ----- |  |
| 2 B | 0.285 | 0.180 | 0.105 | 55.62 | 17.14 |
| 27 | 0.313 | 0.106 | 0.207 | 59.45 | 16.55 |
| 3B | 0.340 | 0.245 | 0.095 | 55.37 | 16.95 |
| 3 T | ----- | ----- | ----- | ----- | ----- |
| 4 B | 0.386 | 0.254 | 0.132 | 54.78 | 16.35 |
| 4 T | ----- | ----- | ----- | ----- | ----- |
| 53 | 0.379 | 0.231 | 0.148 | 54.45 | 15.93 |
| 57 | 0.197 | 0.110 | 0.087 | 59.82 | 16.49 |
| 63 | 0.330 | 0.199 | 0.131 | 54.25 | 15.63 |
| 6T | -- | ----- | ----- | ------ | ----- |
| 7 B | 0.304 | 0.179 | 0.125 | 54.25 | 15.63 |
| $7{ }^{1}$ | -- | ----- | ----- | ----- | ----- |
| 8 B | 0.276 | 0.169 | 0.107 | 54.05 | 15.29 |
| 8 T | 0.174 | 0.131 | 0.043 | 59.15 | 16.60 |
| 9 B | 0.311 | 0.161 | 0.150 | 54.05 | 15.29 |
| $9 T$ | ----- | ----- | ----- | ---- | ----- |
| 10 B | 0.275 | 0.145 | 0.130 | 53.96 | 15.12 |
| 107 | ----- | ----- | ----- | ---- | ----- |
| IIB | 0.246 | 0.136 | 0.110 | 53.96 | 15.12 |
| 11 T | 0.226 | 0.112 | 0.114 | 59.15 | 16.60 |
| 12 B | 0.451 | 0.138 | 0.313 | 54.05 | 15.29 |
| 12 T | -- | - | ----- | ----- | ----- |
| 133 | 0.460 | 0.136 | 0.324 | 53.88 | 14.95 |
| 13 T | -- | ----- | ----- | ---- | ---- |

TABLE 8-Continued

| SAMPLE | $\begin{gathered} (280) \\ \text { ABSORBATCE } \end{gathered}$ | HEMOGIOBIN (280) CONTRIBUSION | ALBUMIII (280) COS TRIBUTION | 2H403 | $\underline{\lambda H 280}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14 B | 0.373 | 0.129 | 0.244 | 53.96 | 15.12 |
| 14. | 0.264 | 0.122 | 0.142 | 59.15 | 16.60 |
| 15B | 0.306 | 0.120 | 0.186 | 54.05 | 15.29 |
| 151 | ---- | ------ | ------ | ----- | ------ |
| 16B | 0.328 | 0.120 | 0.208 | 53.96 | 15.12 |
| 16T | ----- | ------ | ------ | ------ |  |
| 17B | 0.265 | 0.122 | 0.143 | 53.88 | 14.95 |
| 17 T | 0.232 | 0.115 | 0.117 | 58.88 | 16.95 |
| 18B | 0.266 | 0.119 | 0.147 | 53.88 | 14.95 |
| 18 T | ----- | ----- | ----- | ----- |  |
| 19B | 0.214 | 0.121 | 0.093 | 53.96 | 15.12 |
| 19T | ---.-- | ----- | ------ | ----- |  |
| 20 B | 0.243 | 0.120 | 0.123 | 53.88 | 14.95 |
| 20 T | 0.200 | 0.111 | 0.089 | 59.15 | 16.60 |
| 21B | 0.197 | 0.118 | 0.079 | 53.96 | 15.12 |
| 219 | ----- | ------ | ----- | ----- | ----- |
| RB | 0.210 | 0.119 | 0.091 | 53.96 | 15.12 |
| RT | 0.203 | 0.128 | 0.075 | 58.88 | 16.65 |
| FESD | 0.216 | 0.136 | 0.080 | 53.88 | 14.95 |

TABIE 8 - Continued

| SATPLE | $\begin{aligned} & \text { HMYOGIOBII } \\ & \text { CO. CE ERARION } \end{aligned}$ | $\frac{Y_{H s}}{Y_{H F}}$ | $\begin{gathered} \text { ALBUMIN } \\ \text { COL CETPRATOE } \end{gathered}$ | $\frac{Y_{A S}}{Y_{A F}}$ |
| :---: | :---: | :---: | :---: | :---: |
| IB | 0.00494 | 0.54 | 0.02968 | 1.86 |
| 1T | -------- | -- | --- | ---- |
| 2 B | 0.01048 | 1.15 | 0.02091 | 1.31 |
| $2 \pm$ | 0.00643 | 0.71 | 0.04123 | 2.59 |
| 33 | 0.01447 | 1.59 | 0.01892 | 1. 19 |
| 39 | -------- | ---- | -------- | ---- |
| 4 B | 0.01553 | 1.70 | 0.02629 | 1. 65 |
| 41 | -------- | ---- | --------- | ---- |
| 5 B | 0.01451 | 1.59 | 0.02948 | 1.85 |
| 5 T | 0.00669 | 0.73 | 0.01733 | 1.09 |
| 6 B | 0.01272 | 1.40 | 0.02609 | 1.64 |
| 6 T | - | -- | ---- | ---- |
| 7 B | 0.01147 | 1.26 | 0.02490 | 1.56 |
| 7 T | ------- | ---- | -------- | ---- |
| 8B | 0.01103 | 1.21 | 0.02131 | 1.34 |
| 8 T | 0.00788 | 0.86 | 0.00856 | 0.54 |
| $9 B$ | 0.01051 | 1.15 | 0.02987 | 1. 88 |
| 9 T | ------- | ---- | -------- | ---- |
| 10B | 0.00958 | 1.05 | 0.02589 | 1. 63 |
| 10 T | ------ | ---- | -------- | ---- |
| 11B | 0.00897 | 0.98 | 0.02191 | 1.38 |
| 11T | 0.00676 | 0.74 | 0.02270 | 1.42 |
| 123 | 0.00903 | 0.99 | 0.06234 | 3.91 |
| 12 T | --- | ---- | --- | ---- |
| 13B | 0.00908 | 1.00 | 0.06453 | 4.05 |
| 137 | --------- | --- | -------- | ---- |

TABLE 8-Continued

| SMPPLE | HMMOGLOBIN CONCEMTRATION | $\frac{Y \mu s}{Y_{H}}$ | $\begin{gathered} \text { ALBUMIN } \\ \text { COES CMTRATIOH } \end{gathered}$ | $\frac{Y_{A S}}{Y_{A F}}$ |
| :---: | :---: | :---: | :---: | :---: |
| $14 . \mathrm{B}$ | 0.00852 | 0.94 | 0.04860 | 3.05 |
| 14 T | 0.00735 | 0.81 | 0.02828 | 1.78 |
| 15B | 0.00784 | 0.86 | 0.03704 | 2.33 |
| 15T | -------- | ---- | -------- | ---- |
| 16B | 0.00793 | 0.87 | 0.04143 | 2.60 |
| 16T | ------- | ---- | -------- | ---- |
| 17B | 0.00817 | 0.90 | 0.02848 | 1.79 |
| 17T | 0.00688 | 0.76 | 0.02330 | 1.46 |
| 18 B | 0.00798 | 0.88 | 0.02928 | 1.84 |
| 18 T | -------- | ---- | -------- | ---- |
| 19B | 0.00797 | 0.87 | 0.01852 | 1.16 |
| 199 | -------- | ---- | -------- | ---- |
| 203 | 0.00804 | 0.88 | 0.02450 | 1.54 |
| 207 | 0.00671 | 0.74 | 0.01773 | 1.11 |
| 21.8 | 0.00780 | 0.86 | 0.01573 | 0.99 |
| 217 | -- | ---- | -------- | ----- |
| RB | 0.00786 | 0.86 | 0.01812 | 1.14 |
| RT | 0.00766 | 0.84 | 0.01494 | 0.94 |
| FEED | 0.00911 | ---- | 0.01593 | --- |


| SAFPIE | $\begin{aligned} & A \operatorname{OUNT}(\mathrm{CM})^{3} \\ & \text { COLIGOID } \end{aligned}$ | PH | $\begin{gathered} \text { (403) } \\ \text { TRASMSSION } \end{gathered}$ | $\begin{gathered} (280) \\ \text { TRA } \operatorname{SMISSIO} \\ \hline \end{gathered}$ | $\begin{array}{r} (403) \\ \angle B S O Z=A M C E \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1B | 3.0 | 7.15 | 40.2 | 38.2 | 0.395 |
| $1 T$ | 1.0 | - | ---- | ---- | ----- |
| 2 B | 3.1 | 7.25 | 32.5 | 38.2 | 0.488 |
| $2 T$ | 1.0 | 6.30 | 37.3 | 50.4 | 0.428 |
| 3 B | 3.0 | 7.40 | 21.2 | 35.3 | 0.673 |
| 3T | 0.9 | ---- | ---- | ---- | ------ |
| 43 | 3.0 | 7.55 | 20.6 | 34.0 | 0.687 |
| 4 T | 1.4 | ---- | ---- | ---- | ------ |
| $5 B$ | 3.0 | 7.75 | 21.8 | 36.1 | 0.662 |
| 5 T | 0.9 | 6.40 | 42.7 | 45.5 | 0.369 |
| 6 B | 2.8 | 7.80 | 26.7 | 33.3 | 0.573 |
| 6 T | 1.0 | - | ---- | ---- | ----- |
| 7 B | 2.9 | 7.85 | 28.4 | 40.3 | 0.546 |
| 7 T | 1.0 | ---- | ---- | ---- | ----- |
| 83 | 2.8 | 7.90 | 31.0 | 41.3 | 0.509 |
| 8 T | 1.0 | 6.35 | 38.4 | 60.6 | 0.415 |
| 93 | 3.0 | 8.00 | 31.2 | 45.2 | 0.505 |
| 9 T | 1.1 | ----- | ---- | ---- | ------ |
| 10B | 2.9 | 8.00 | 30.5 | 46.7 | 0.516 |
| 10T | 1.9 | -- | ---- | ---- | ----- |
| 11B | 3.1 | 7.90 | 35.2 | 35.1 | 0.454 |
| $11 T$ | 1.0 | 6.55 | 33.4 | 43.8 | 0.476 |
| 123 | 2.9 | 7.95 | 35.5 | 33.0 | 0.450 |
| 12 T | 0.9 | ---- | ---- | ---- | ----- |
| 13B | 2.9 | 8.00 | 38.3 | 38.6 | 0.417 |
| 13T | 1.0 | ---- | --- | -- | ---- |

TABIE 9-Continued

| SMPITE | $\begin{aligned} & \text { AROUNT (CI) }{ }^{3} \\ & \text { COLISCIED } \end{aligned}$ | PH | $\begin{gathered} (403) \\ \text { TRASMISSION } \end{gathered}$ | $\begin{gathered} (280) \\ \text { TRACMISSIOM } \end{gathered}$ | $\begin{gathered} (403) \\ \text { ASSOREABCE } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14 B | 2.8 | 8.00 | 37.7 | 40.3 | 0.424 |
| 14 T | 0.9 | 6.25 | 40.3 | 51.3 | 0.394 |
| 153 | 3.1 | 8.10 | 38.8 | 43.2 | 0.411 |
| 15T | 1.1 | ---- | ---- | ---- | ----- |
| 163 | 3.0 | 7.95 | 38.6 | 44.1 | 0.414 |
| 16T | 1.1 | ---- | ---- | ---- | ----- |
| 17B | 3.1 | 8.00 | 38.8 | 45.3 | 0.411 |
| 179 | 0.9 | 6.25 | 43.6 | 55.2 | 0.360 |
| 188 | 3.0 | 8.10 | 40.8 | 50.4 | 0.390 |
| 18T | 1.0 | ---- | ---- | ---- | ----- |
| 19B | 3.1 | 8.00 | 39.5 | 46.5 | 0.403 |
| 199 | 1.5 | ---- | ---- | ---- | ----- |
| 20B | 3.0 | 8.00 | 39.4 | 43.7 | 0.405 |
| 201 | 1.0 | 6.10 | 42.5 | 56.5 | 0.371 |
| 21B | 3.0 | 7.95 | 41.3 | 52.2 | 0.385 |
| $21 T$ | 0.8 | ---- | ---- | ---- | ----- |
| R.B | --- | 7.90 | 38.1 | 50.7 | 0.419 |
| RT | --- | 6.10 | 36.1 | 54.0 | 0.443 |
| FEED | --- | 8.00 | 33.6 | 64.6 | 0.473 |

## quese 9 - Continued

| SAMPIE | $\begin{gathered} (290) \\ \text { ABSOPB4CE } \end{gathered}$ | HEMOGIDBII (280) COWPRIBUTION | al buifin (280) COM Taiburton | 21:403 | 入\# 280 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1B | 0.418 | 0.122 | 0.96 | 55.75 | 17.23 |
| 1 T | ------ | ----- | ----- | ----- | ----- |
| 2 B | 0.418 | 0.150 | 0.268 | 55.50 | 17.05 |
| 2 T | 0.298 | 0.123 | 0.175 | 58.22 | 16.80 |
| 33 | 0.452 | 0.204 | 0.248 | 55.14. | 16.73 |
| 3 T | ------ | ----- | ----- | ----- | ----- |
| $4 B$ | 0.459 | 0.205 | 0.264 | 54.73 | 16.35 |
| 4 T | -- | - | ------ | ------ | ----- |
| 5B | 0.442 | 0.192 | 0.250 | 54.35 | 15.78 |
| 57 | 0.342 | 0.108 | 0.234 | 57.87 | 16.90 |
| 68 | 0.478 | 0.165 | 0.313 | 54.25 | 15.63 |
| 69 | - | - | ----- | ----- | - |
| 7 B | 0.395 | 0.151 | 0.244 | 54.15 | 14.96 |
| 71 | - | - | ----- | --.-- | ------ |
| 8 B | 0.384 | 0.144 | 0.240 | 54.05 | 15.29 |
| 89 | 0.218 | 0.120 | 0.098 | 58.05 | 16.85 |
| 93 | 0.345 | 0.140 | 0.205 | 53.88 | 14.95 |
| 9 T | ----- | ----- | ------ | ----- | ------ |
| 10 B | 0.330 | 0.143 | 0.187 | 53.88 | 14.95 |
| 109 | ------ | ------ | ------ | ------ | ----- |
| 113 | 0.454 | 0.123 | 0.326 | 54.05 | 15.29 |
| 117 | 0.359 | 0.142 | 0.217 | 57.36 | 17.05 |
| $12 B$ | 0.482 | 0.126 | 0.356 | 53.96 | 15.12 |
| 12 T | ------ | ----- | ------ | ------ | ----- |
| 13B | 0.414 | 0.116 | 0.298 | 53.83 | 14.95 |
| 13T | - | -- | -- | ---- | ----- |

## MABE 9-Continued

| SAMPIS | $\begin{gathered} (280) \\ A B S O 29401 \end{gathered}$ | $\begin{aligned} & \text { HOGLOBIN ( } 280 \text { ) } \\ & \text { CONTPIBUMION } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { ALBUMTN (280) } \\ & \text { COMTARIBUIION } \end{aligned}$ | 2H403 | 2H280 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14 B | 0.395 | 0.118 | 0.277 | 53.88 | 14.95 |
| 14 T | 0.290 | 0.113 | 0.177 | 58.43 | 16.75 |
| 15 B | 0.365 | 0.114 | 0.251 | 53.88 | 14.95 |
| 15T | ----- | ----- | ----- | ----- |  |
| 16B | 0.355 | 0.176 | 0.239 | 53.96 | 15.12 |
| 16T | ----- | ----- | ----- | ----- | ----- |
| 17B | 0.344 | 0.114 | 0.230 | 53.88 | 14.95 |
| 179 | 0.258 | 0.103 | 0.155 | 58.43 | 16.75 |
| 18 B | 0.298 | 0.100 | 0.198 | 53.88 | 14.95 |
| 187 | ----- | ----- | ----- | ----- |  |
| 19B | 0.333 | 0.108 | 0.225 | 53.88 | 14.95 |
| 19T | ----- | ----- | ----- | ----- |  |
| 20B | 0.312 | 0.112 | 0.200 | 53.88 | 14.95 |
| 20T | 0.248 | 0.114 | 0.134 | 59.15 | 16.60 |
| 21B | 0.282 | 0.108 | 0.174 | 53.96 | 15.12 |
| 21.1 | ----- | ----- | ----- | ----- | ----- |
| R.B | 0.295 | 0.118 | 0.177 | 54.05 | 15.29 |
| RT | 0.267 | 0.124 | 0.143 | 59.15 | 16.60 |
| FEED | 0.190 | 0.132 | 0.058 | 53.88 | 14.95 |

PABLE 9-Continued

| SAPPLE | $\begin{gathered} \text { HMOGEOBIN } \\ \text { CONCMNRATION } \end{gathered}$ | $\begin{aligned} & Y_{H S} \\ & Y_{H F} \end{aligned}$ | ALBUMIIN CONCEITTRATION | $\frac{Y_{A S}}{Y_{A F}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 B | 0.00709 | 0.81 | 0.05595 | 5.10 |
| 1T | -------- | ---- | -------- | --- |
| 2B | 0.00879 | 1.00 | 0.05338 | 4.62 |
| $2 T$ | 0.00735 | 0.84 | 0.03485 | 3.02 |
| 3B | 0.01221 | 1.39 | 0.04939 | 4.28 |
| 37 | -------- | ---- | -------- | ---- |
| 4 B | 0.01254 | 1.43 | 0.05258 | 4.55 |
| 4T | - | ---- | -------- | ---- |
| 5 B | 0.01218 | 1.38 | 0.04979 | 4.31 |
| 5 T | 0.00638 | 0.73 | 0.04660 | 4.03 |
| $6 B$ | 0.01056 | 1. 20 | 0.06234 | 5.40 |
| 6 T | ------- | ---- | ---.-.--- | ---- |
| 73 | 0.01008 | 1.15 | 0.04860 | 4.21 |
| 7 T | -------- | ---- | -------- | ---- |
| $8 B$ | 0.00942 | 1.07 | 0.04780 | 4.14 |
| 8 T | 0.00715 | 0.81 | 0.01952 | 1.69 |
| 98 | 0.00937 | 1.07 | 0.04083 | 3.53 |
| 9 T | ------- | --- |  | -- |
| 10B | 0.00958 | 1.09 | 0.03724 | 3.22 |
| IOT | -- | ---- | -------- | -- |
| 118 | 0.00840 | 0.95 | 0.06493 | 5.62 |
| 11T | 0.00830 | 0.94 | 0.04322 | 3.74 |
| 12 B | 0.00834 | 0.95 | 0.07090 | 6.14 |
| 12 T | -------- | - | --------- | ---- |
| 13B | 0.00774 | 0.88 | 0.05935 | 5.14 |
| 13' | ------- | -- | --------- | --- |

## TABIE 9 - Continued

| SAMPIE | $\begin{aligned} & \text { HBHOGIOBIN } \\ & \text { CONCIWTRARION } \end{aligned}$ | $\frac{Y_{H S}}{Y_{H F}}$ | $\begin{gathered} \text { ALBUMIN } \\ \text { CONCETYRARION } \\ \hline \end{gathered}$ | $\begin{aligned} & Y_{A S} \\ & \underline{Y_{A F}} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| 14B | 0.00787 | 0.89 | 0.05517 | 4.78 |
| 14 T | 0.00674 | 0.77 | 0.03525 | 3.05 |
| 15B | 0.00763 | 0.87 | 0.04999 | 4.33 |
| 15T | --- | ---- | -------- | ----- |
| 16 B | 0.00767 | 0.87 | 0.04760 | 4.12 |
| 16T | - | ---- | --- | ---- |
| 17B | 0.00763 | 0.87 | 0.04581 | 3.97 |
| 179 | 0.00616 | 0.70 | 0.03087 | 2.67 |
| 18B | 0.00668 | 0.76 | 0.03943 | 3.41 |
| 189 | -------- | ---- | -------- | ---- |
| 19B | 0.00724 | 0.82 | 0.04481 | 3.88 |
| 19 T | -----.--- | ---- | --------- | ---- |
| 203 | 0.00748 | 0.85 | 0.03983 | 3.45 |
| 20 T | 0.00685 | 0.79 | 0.02669 | 2.31 |
| 21 B | 0.00713 | 0.81 | 0.03465 | 3.00 |
| 21 T | ----- | --- | -- | ---- |
| RB | 0.00775 | 0.83 | 0.03525 | 3.05 |
| RT | 0.00749 | 0.85 | 0.02348 | 2.47 |
| FEED | 0.00880 | ---- | 0.01155 | ---- |


| SAMPIE | $\begin{aligned} & \text { HOUNT (CD) } \\ & \text { COLUSTED } \end{aligned}$ | PH |  | $\begin{gathered} (280) \\ \text { RQMSMISSION } \end{gathered}$ | $\begin{gathered} (403) \\ \text { ADSOREAPCE } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1B | 3.0 | 7.20 | 40.4 | 53.7 | 0.394 |
| 1T | 3.0 | 6.00 | 38.4 | 57.8 | 0.416 |
| $2 B$ | 3.0 | 6.85 | 55.2 | 72.6 | 0.258 |
| $2 T$ | 3.1 | 6.00 | 38.2 | 61.2 | 0.418 |
| $3 B$ | 2.9 | 7.20 | 29.4 | 55.1 | 0.532 |
| 3 T | 3.0 | 6.00 | 45.0 | 66.9 | 0.347 |
| 43 | 2.9 | 7.20 | 29.9 | 61.0 | 0.524 |
| 4 T | 3.0 | 6.00 | 55.1 | 68.8 | 0.259 |
| 53 | 3.0 | 7.35 | 31.1 | 54.4 | 0.508 |
| 5 T | 3.0 | 6.00 | 57.7 | 70.5 | 0.239 |
| 68 | 2.9 | 7.40 | 34.1 | 49.6 | 0.467 |
| $6 T$ | 3.0 | 6.00 | 56.1 | 73.5 | 0.251 |
| 7 B | 2.9 | 7.50 | 36.8 | 60.6 | 0.434 |
| 7 T | 3.0 | 6.00 | 67.1 | 67.3 | 0.173 |
| 8 B | 3.0 | 7.65 | 37.1 | 61.2 | 0.430 |
| 8 T | 3.0 | 6.00 | 65.2 | 72.8 | 0.186 |
| $9 B$ | 3.0 | 7.55 | 42.3 | 63.6 | 0.374 |
| 99 | 3.0 | 6.00 | 64.3 | 69.5 | 0.192 |
| 108 | 3.0 | 7.50 | 43.6 | 66.1 | 0.360 |
| 109 | 3.1 | 6.00 | 74.4 | 71.3 | 0.129 |
| I1B | 3.0 | 7.60 | 41.2 | 43.4 | 0.385 |
| 117 | 3.1 | 6.00 | 78.5 | 62.2 | 0.105 |
| 128 | 3.0 | 7.60 | 38.9 | 44.0 | 0.410 |
| 127 | 3.1 | 6.05 | 76.8 | 60.7 | 0.114 |
| 13B | 2.8 | 7.50 | 36.5 | 43.6 | 0.438 |
| 13T | 3.0 | 6.00 | 74.9 | 68.0 | 0.125 |

TABLIT10-Continued

| GAMPLE | AHOUN (CM) ${ }^{3}$ <br> COLTOTED | PH | $\begin{gathered} (403) \\ \text { TRA SMISSIOT } \\ \hline \end{gathered}$ | $\begin{gathered} (280) \\ \text { TRASMISGION } \end{gathered}$ | $\begin{array}{r} (403) \\ \text { assoremace } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14 B | 3.0 | 7.60 | 36.5 | 48.6 | 0.437 |
| 14T | 3.0 | 6.00 | 77.3 | 64.7 | 0.112 |
| 15B | 3.0 | 7.50 | 38.0 | 54.1 | 0.420 |
| 159 | 3.0 | 6.00 | 82.3 | 69.6 | 0.085 |
| 16B | 2.8 | 7.50 | 43.4 | 60.9 | 0.362 |
| 16 T | 3.0 | 6.00 | 80.3 | 73.0 | 0.095 |
| 17B | 3.0 | 7.50 | 47.1 | 66.8 | 0.327 |
| 17 T | 3.1 | 6.00 | 80.2 | 69.3 | 0.096 |
| 18B | 2.9 | 7.45 | 42.1 | 61.6 | 0.376 |
| 18 T | 3.1 | 6.00 | 82.6 | 70.3 | 0.083 |
| 19B | 3.1 | 7.50 | 42.4 | 66.7 | 0.373 |
| 199 | 3.1 | 6.00 | 81.0 | 69.5 | 0.092 |
| 2013 | 3.1 | 7.45 | 45.7 | 68.0 | 0.340 |
| 20 T | 3.2 | 6.00 | 81.3 | 72.6 | 0.090 |
| 213 | 2.9 | 7.40 | 43.1 | 66.8 | 0.366 |
| 217 | 3.1 | 6.00 | 77.9 | 73.4 | 0.109 |
| RB | --- | 7.40 | 47.7 | 79.4 | 0.321 |
| RT | --- | 6.00 | 80.2 | 71.5 | 0.096 |
| TEED | --- | 6.00 | 29.5 | 62.4 | 0.530 |

## TABLE 10 - Continued

| SAFPLS | $\begin{gathered} (280) \\ \text { ABSOSBAICE } \end{gathered}$ | HBMOGLOBIT (280) <br> CONTPIBUTION | ALBUMI. (280) CONTRIBUTICN | $\lambda_{4403}$ | $\lambda_{\mathrm{H} 280}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 B | 0.270 | 0.121 | 0.149 | 55.62 | 17.14 |
| 1T | 0.238 | 0.115 | 0.123 | 59.82 | 16.49 |
| 2 B | 0.139 | 0.079 | 0.060 | 56.48 | 17.29 |
| 2 T | 0.213 | 0.115 | 0.098 | 59.82 | 16.49 |
| $3 B$ | 0.259 | 0.164 | 0.095 | 55.62 | 17.14 |
| $3 T$ | 0.174 | 0.096 | 0.078 | 59.82 | 16.49 |
| $4 B$ | 0.214 | 0.161 | 0.053 | 55.62 | 17.14 |
| 4 T | 0.163 | 0.071 | 0.092 | 59.82 | 16.49 |
| 53 | 0.264 | 0.155 | 0.109 | 55.25 | 16.85 |
| 5 T | 0.152 | 0.066 | 0.086 | 59.82 | 16.49 |
| 63 | 0.304 | 0.142 | 0.162 | 55.14 | 16.73 |
| 6 T | 0.134 | 0.069 | 0.065 | 59.82 | 16.49 |
| 73 | 0.218 | 0.130 | 0.088 | 54.90 | 16.48 |
| 7 T | 0.172 | 0.048 | 0.124 | 59.8? | 16.49 |
| 83 | 0.213 | 0.127 | 0.086 | 54.56 | 16.08 |
| 8T | 0.138 | 0.051 | 0.087 | 59.82 | 16.49 |
| 93 | 0.197 | 0.112 | 0.085 | 54.78 | 16.35 |
| 92 | 0.158 | 0.053 | 0.105 | 59.82 | 16.49 |
| 10B | 0.180 | 0.108 | 0.072 | 54.90 | 16.48 |
| 109 | 0.147 | 0.036 | 0.111 | 59.32 | 16.49 |
| 11B | 0.363 | 0.114 | 0.249 | 54.67 | 16.22 |
| 119 | 0.206 | 0.029 | 0.177 | 59.82 | 16.49 |
| 12B | 0.356 | $0.12 ?$ | 0.234 | 54.67 | 16.22 |
| 12 T | 0.176 | 0.032 | 0.144 | 59.45 | 16.55 |
| 13B | 0.361 | 0.132 | 0.229 | 54.90 | 16.48 |
| 13T | 0.167 | 0.034 | 0.133 | 59.82 | 16.49 |

## TABLI 10 - Continued

| SMEL | $\begin{gathered} (280) \\ A B \in O R B A I C E \end{gathered}$ | HENOGLOBII (280) CONTPIBUSION | ALbuhin (230) CONTPIEUTIOR | 21403 | 24280 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 143 | 0.313 | 0.130 | 0.183 | 54.67 | $16.2 ?$ |
| 14 T | 0.189 | 0.031 | 0.158 | 59.82 | 16.49 |
| 153 | 0.267 | 0.126 | 0.141 | 54.90 | 16.48 |
| 15 T | 0.157 | 0.023 | 0.134 | 59.82 | 16.49 |
| 16 B | 0.215 | 0.109 | 0.106 | 54.90 | 16.48 |
| 16T | 0.137 | 0.026 | 0.111 | 59.82 | 16.49 |
| 17 B | 0.175 | 0.098 | 0.077 | 54.90 | 16.48 |
| 179 | 0.159 | 0.026 | 0.133 | 59.82 | 16.49 |
| 18 B | 0.210 | 0.114 | 0.096 | 55.00 | 16.60 |
| 18 T | 0.153 | 0.023 | 0.130 | 59.32 | 16.49 |
| 19B | 0.176 | 0.112 | 0.064 | 54.90 | 16.48 |
| 19 T | 0.158 | 0.025 | 0.133 | 59.82 | 16.49 |
| 20 B | 0.168 | 0.102 | 0.066 | 55.00 | 16.60 |
| 20 T | 0.139 | 0.025 | 0.114 | 59.82 | 16.49 |
| 21 B | 0.175 | 0.111 | 0.064 | 55.14 | 16.73 |
| 21T | 0.134 | 0.030 | 0.104 | . 59.82 | 16.49 |
| RB | 0.100 | 0.097 | 0.003 | 55.14 | 16.73 |
| RT | 0.146 | 0.026 | 0.120 | 59.82 | 16.49 |
| $\operatorname{FEDD}$ | 0.205 | 0.146 | 0.059 | 59.82 | 16.49 |

LABTE 10-Continued

| SAitPLE | $\begin{gathered} \text { HBMGIOBII } \\ \text { CONCMTRATON } \\ \hline \end{gathered}$ | $\frac{Y H S}{Y_{H F}}$ | ALBUNTIT CONCATRATION | $\begin{aligned} & Y A S \\ & Y_{A F} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| $1 B$ | 0.00708 | 0.80 | 0.02968 | 2.53 |
| 1 T | 0.00695 | 0.78 | 0.02450 | 2.09 |
| 23 | 0.00457 | 0.52 | 0.01195 | 1.02 |
| 27 | 0.00699 | 0.79 | 0.01952 | 1.66 |
| 3B | 0.00956 | 1.08 | 0.01852 | 1.61 |
| 3 T | 0.00580 | 0.65 | 0.01553 | 1.32 |
| 4B | 0.00942 | 1.06 | 0.01056 | 0.90 |
| 4 T | 0.00433 | 0.49 | 0.01852 | 1.56 |
| 5B | 0.00919 | 1.04 | 0.02171 | 1.85 |
| 5 T | 0.00400 | 0.45 | 0.01713 | 1.46 |
| 6 B | 0.00847 | 0.96 | 0.03226 | 2.75 |
| 67 | 0.00420 | 0.47 | 0.01295 | 1.10 |
| 7 B | 0.00791 | 0.89 | 0.01753 | 1.49 |
| 7 T | 0.00289 | 0.33 | 0.02470 | 2.10 |
| 8B | 0.00788 | 0.89 | 0.01713 | 1.46 |
| $8{ }^{1}$ | 0.00311 | 0.35 | 0.01733 | 1.47 |
| 9 B | 0.00683 | 0.77 | 0.01693 | 1.44 |
| 9T | 0.00321 | 0.36 | 0.02091 | 1.78 |
| 10B | 0.00656 | 0.74 | 0.01434 | 1.22 |
| 10T | 0.00216 | 0.24 | 0.02211 | 1.88 |
| 11B | 0.00704 | 0.79 | 0.04959 | 4.22 |
| 11T | 0.00176 | 0.20 | 0.03525 | 3.00 |
| 123 | 0.00750 | 0.85 | 0.04660 | 3.97 |
| 129 | 0.00192 | 0.22 | 0.02868 | 2.44 |
| 13B | 0.00798 | 0.90 | 0.04561 | 3.88 |
| 13T | 0.00209 | 0.24 | 0.02649 | 2.25 |

MABE 10 - Continued

| SAPIPLS | $\begin{gathered} \text { HMCGIOBIH } \\ \text { CONCMTRARION } \end{gathered}$ | $\frac{Y_{H S}}{Y_{H E}}$ | $\begin{gathered} \text { ALBUMT } \\ \text { CONCEMTPATION } \\ \hline \end{gathered}$ | $\frac{Y A S}{Y A F}$ |
| :---: | :---: | :---: | :---: | :---: |
| 14B | 0.00799 | 0.90 | 0.03645 | 3.10 |
| 14. | 0.00187 | 0.21 | 0.03147 | 2.68 |
| 15B | 0.00765 | 0.86 | 0.02808 | 2.39 |
| 157 | 0.00142 | 0.16 | 0.02669 | 2. 27 |
| 16 B | 0.00659 | 0.74 | 0.02111 | 1.80 |
| 16T | 0.00159 | 0.18 | 0.02211 | 1.88 |
| 17B | 0.00596 | 0.67 | 0.01534 | 1.31 |
| 17 T | 0.00160 | 0.18 | 0.02649 | 2.25 |
| 18 B | 0.00684 | 0.77 | 0.01912 | 1.63 |
| 18T | 0.00139 | 0.16 | 0.02589 | 2.20 |
| 19B | 0.00679 | 0.77 | 0.01275 | 1.09 |
| 197 | 0.00154 | 0.17 | 0.02649 | 2.25 |
| 203 | 0.00618 | 0.70 | 0.01314 | 1.12 |
| 20 T | 0.00150 | 0.17 | 0.02970 | 1.93 |
| 213 | 0.00664 | 0.75 | 0.01275 | 1.09 |
| 217 | 0.00182 | 0.21 | 0.02071 | 1.76 |
| RB | 0.00582 | 0.66 | 0.00060 | 0.05 |
| RT | 0.00160 | 0.18 | 0.02390 | 2.03 |
| FEED | 0.00886 | ---- | 0.01175 | ---- |

## SABLE 11: SEPARATICN FACIORS

| CYCLS | $\begin{gathered} A 4 \\ (A l b .) \\ \hline \end{gathered}$ | $\begin{gathered} \text { Tl } \\ \left(\begin{array}{l} \text { Hem. } \end{array}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{Tl} \\ (\mathrm{Alb.}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T2} \\ \text { (Hem.) } \\ \hline \end{gathered}$ | $\begin{gathered} T 2 \\ (\text { Alb. }) \\ \hline \end{gathered}$ | $\begin{gathered} 93 \\ \text { (Hem.) } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T3} \\ (\mathrm{Alb} .) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | --- | - | --- | -- | ---- | 1.02 | 1.21 |
| 2 | 1.07 | 1.62 | 0.51 | 1. 20 | 1.53 | 0.65 | 0.61 |
| 3 | - | ---- | ---- | ---- | --- | 1.65 | 1.22 |
| 4 | --- | ---- | ---- | ---- | ---- | 2.18 | 0.58 |
| 5 | 1.39 | 2.18 | 1.70 | 1.91 | 1.07 | 2.30 | 1.27 |
| 6 | - | ---- | ---- | ---- | --- | 2.17 | 2.49 |
| 7 | --- | --- | ---- | ---- | ---- | 2.74 | 0.71 |
| 8 | 0.91 | 1.41 | 2.48 | 1.32 | 2.45 | 2.53 | 0.99 |
| 9 | ---- | ---- | ---- | ---- | ---- | 2.13 | 0.81 |
| 10 | - | ---- | ---- | ----- | ---- | 3.04 | 0.65 |
| 11 | 0.67 | 1.32 | 0.97 | 1.01 | 1.50 | 4.00 | 1.41 |
| 12 | ---- | ---- | ---- | ---- | ---- | 3.91 | 1.62 |
| 13 | ---- | ---- | ---- | ---- | ---- | 3.82 | 1.72 |
| 14 | 1.20 | 1.16 | 1.71 | 1.17 | 1.57 | 4.27 | 1.16 |
| 15 | ---- | ---- | ---- | ---- | ---- | 5.39 | 1.05 |
| 16 | ---- | ---- | - | ---- | ----- | 4.14 | 0.95 |
| 17 | 0.60 | 1.18 | 1.23 | 1. 24 | 1.48 | 3.72 | 0.58 |
| 18 | ---- | ---- | --- | ---- | ---- | 4.92 | 0.74 |
| 19 | -- | ---- | ---- | ---- | ---- | 4.41 | 0.43 |
| 20 | 0.62 | 1.19 | 1.39 | 1.09 | 1.49 | 4.12 | 0.58 |
| 21 | -- | -- | - | ---- | -- | 3.65 | 0.62 |
| R | 0.49 | 1.02 | 1. 21 | 1.03 | 1.24 | 3.64 | 0.03 |

