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The Thermal Dehydration of Magnesium Sulfite  
Hexahydrate ( $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ ) and Magnesium Sulfite  
Trihydrate ( $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ );

A mechanistic Study using Thermo-analytical  
Techniques and the Development of an Analytical  
Method for Quantitating Mixtures of the Hydrates

BY

RAAFAT F. ABDEL-MALEK

A THESIS

PRESENTED IN PARTIAL FULFILLMENT OF

THE REQUIREMENTS FOR THE DEGREE

OF

MASTER OF SCIENCE

AT

NEW JERSEY INSTITUTE OF TECHNOLOGY

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Newark, New Jersey  
1975

### ABSTRACT

The thermal dehydration of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  and  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  have been studied by differential thermal analysis, differential scanning calorimetry and thermal gravimetric analysis.

Similar studies by other groups led to contradictory conclusions. In this investigation, these results were reconciled and it was concluded that  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ , under equilibrium conditions, dehydrates in two steps through the intermediate formation of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ .

One consequence of this work is the development of a simple analytical procedure, using TGA, for the quantitative determination of both hydrates in mixtures and in the presence of thermally inactive material.

APPROVAL OF THESIS

The Thermal Dehydration of Magnesium Sulfite  
Hexahydrate ( $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ ) and Magnesium Sulfite  
Trihydrate ( $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ );

A mechanistic Study using Thermo-analytical  
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RAAFAT F. ABDEL-MALEK

FOR

DEPARTMENT OF CHEMISTRY

NEW JERSEY INSTITUTE OF TECHNOLOGY

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FACULTY COMMITTEE

APPROVED: \_\_\_\_\_  
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NEWARK, NEW JERSEY

JUNE, 1975

### ACKNOWLEDGMENT

The author wishes to express his gratitude to Professor Leonard Dauerman for his interest, suggestions, advice, encouragement and guidance which made the conduct of this investigation possible.

TABLE OF CONTENTS

ABSTRACT	i
APPROVAL PAGE	ii
ACKNOWLEDGMENT	iii
TABLE OF CONTENTS	iv
LIST OF TABLES	v
LIST OF FIGURES	vi
INTRODUCTION	1
EXPERIMENTAL	4
RESULTS AND DISCUSSION	6
APPLICATION	11
REFERENCES	15
TABLES 1-6 inclusive	16-21
FIGURES 1-22 inclusive	22-43

LIST OF TABLES

<u>No.</u>		<u>Page</u>
1.	Starting Temperature of Thermal Dehydration of $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$	16
2.	Starting Temperature of Thermal Dehydration of $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$	17
3.	Calculated and Observed Values of Water Content in Synthetic Mixtures	18
4.	$\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ Content from TGA	19
5.	$\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ Content from TGA	20
6.	TGA Results of a Synthetic Mixture Containing Thermally Inactive Material	21



LIST OF FIGURES

<u>No.</u>		<u>Page</u>
1	DTA of $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$	22
2	DTA of $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$	23
3	DSC of $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$	24
4	DSC of $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$	25
5	TGA of $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$	26
6	TGA of $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$	27
7	TGA of $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ under self-generated atmosphere	28
8	TGA of $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ under self-generated atmosphere	29
9	TGA of Std #1	30
10	TGA of Std #2	31
11	TGA of Std #3	32
12	TGA of Std #4	33
13	TGA of Std #5	34
14	TGA of Std #6	35
15	TGA of Std #7	36
16	TGA of Std #8	37
17	TGA of Std #9	38
18	TGA of Std #10	39
19	TGA of Std #11	40
20	TGA of a mixture of $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ , $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ and glass beads	41
21	Water content versus % $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$	42
22	Water content versus % $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$	43

## INTRODUCTION

The thermal dehydration of the two known stable hydrates of magnesium sulfite, namely, magnesium sulfite hexahydrate ( $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ ) and magnesium sulfite trihydrate ( $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ ) have been studied. On the one hand, this work is of practical importance because in the Magnesia Scrubbing Regeneration Process (CHEMICO)<sup>(8)</sup>, the thermal dehydration of the magnesium sulfite hydrates is a significant step. On the other hand, this study is of scientific interest because the mechanism of the dehydration has been the subject of controversy.

In the Magnesia Scrubbing Regeneration Process (CHEMICO), sulfur dioxide in the flue gas is removed by scrubbing with a magnesia ( $\text{MgO}$ ) base slurry. Hydrates of  $\text{MgSO}_3$  are formed; also  $\text{MgSO}_4$  is formed by oxidation. A portion of the slurry is withdrawn and centrifuged. The solid is separated from the liquid, which is recycled. The solids are then dehydrated in a dryer and, afterwards, calcined at  $1400^\circ\text{F}$ - $1600^\circ\text{F}$  with coke added to the solids. Heating is sufficient to effect the thermal decomposition of  $\text{MgSO}_3$ ; the coke reduces  $\text{MgSO}_4$  to  $\text{MgSO}_3$ . The useful products of calcination are  $\text{MgO}$ , which is recycled back to the slurry, and  $\text{SO}_2$ , which is converted to sulfuric acid.

Turning to the scientific relevance of this study, thermal dehydration studies have been reported by three groups and the results were apparently contradictory. Okabe and

Hori<sup>(5)</sup> used three different techniques to study the dehydration: Differential Thermal Analysis (DTA), X-ray and Infrared (IR). From the DTA and X-ray results, they concluded that  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  loses three water molecules between  $60^\circ\text{C}$  and  $100^\circ\text{C}$  to form  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ . The latter at  $200^\circ\text{C}$  completely dehydrates to yield amorphous anhydrous  $\text{MgSO}_3$ . But in the infrared investigation, they reported that the spectra does not change when the trihydrate goes to the anhydrous state at  $200^\circ\text{C}$ . It does not seem plausible that the transformation suggested could have occurred without any change in the infrared spectra. The band in the  $3500 \text{ cm}^{-1}$  region is obviously an O-H stretching band, therefore, if the salt is dehydrated it would be expected that this band would disappear.

Two other investigations using DTA were carried out by groups at the Tennessee Valley Authority (TVA). These studies were not published, but are presented, in part, in an EPA-sponsored critical analysis of the Magnesia Process prepared by TVA<sup>(6)</sup>. In the above cited report, Jordan's work based upon DTA leads to the conclusion that the thermal dehydration of  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  takes place in one step starting at  $100^\circ\text{C}$  and that  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  dehydrates in one step, starting at  $160^\circ\text{C}$ .

In the other study, Hatfield and co-workers reported that  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  loses nearly all its water when heated in a stream of argon or air at  $104^\circ\text{C}$  for 16 hrs. This, too, supports the inference that the thermal dehydration of the hexahydrate occurs in one step. It is also reported that

$\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  is partially dehydrated when heated in air for 16 hrs. at  $160^\circ\text{C}$ .

In the above-cited EPA report, it is suggested that the apparently contradictory results may be due to differences in experimental conditions. It was speculated that the samples were heated in sealed tubes in the work of Okabe and Hori, although such information was not provided in that paper. Without presenting a critical analysis of the effects of having the samples open or closed to the atmosphere, it is concluded in the TVA report that the results of the TVA groups, in which the samples are open to the atmosphere, are valid and that  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  dehydrates in one step to  $\text{MgSO}_3$  at  $100^\circ\text{C}$ .

The purpose of this study is to reconcile the contradictory results. Thermoanalytical techniques are used exclusively: Differential Thermal Analysis (DTA), Differential Scanning Calorimetry (DSC) and Thermal Gravimetric Analysis (TGA). Other groups in this laboratory have studied the thermal dehydration using Mass Spectroscopy and Infrared Spectroscopy. These results will be reported separately.

### EXPERIMENTAL

$\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  (97.9%) and  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  (99.0%) used in this study were laboratory prepared samples. Each hydrate was studied individually; also synthetic mixtures of both hydrates were studied.

The DuPont thermal analyzer was employed in this investigation. This included the DuPont 900 differential thermal analyzer (DTA) equipped with both the standard DTA cell and the differential calorimetric cell (DSC). The DuPont 950 TGA unit, which is an attachment to the DuPont 900, was also used.

DTA<sup>(9)</sup> is a thermal technique in which the heat effects, associated with chemical or physical changes, are recorded as a function of temperature or time as the substance is heated at a uniform rate. Enthalpic changes, either endothermic or exothermic, are recorded. The sample temperature is continuously compared with a reference material temperature; the difference in temperature is recorded as a function of furnace temperature or time. DTA is reported to have been first used by LeChatelier<sup>(4)</sup> in 1887 for studying clay. Since that date many developments have been introduced and the literature has grown exponentially. DTA has been used for the study of the thermal dehydration of hydrates. For example, the reader is referred to the work of Wendlant and Hoiberg<sup>(10)</sup>.

In contrast to DTA, in which the temperature difference

between the sample and the reference is measured, in DSC it is the heat necessary to equalize the temperature between the sample and the reference which is measured. This technique thus can be used to measure enthalpic changes quantitatively.

TGA is a technique in which a sample is continuously weighed as it is heated at a linear rate. The resulting thermogram gives information concerning the thermal stability of the substance under investigation. TGA was first described by Honda (2) in 1915. Griffith (1) has applied TGA to the study of mixtures of hydrates and anhydrous salts.

Thermal methods of analysis are uniquely applicable for study of dehydration processes. Dehydration can be observed as endothermic changes in DTA, heats of dehydration in DSC, and as weight losses in TGA.

## RESULTS AND DISCUSSION

First, the DTA results will be considered. A typical thermogram for the dehydration of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  is shown in Figure 1. Only one endothermic transition is observed, starting at  $190^\circ\text{C}$ . On the other hand, in the thermogram of  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  shown in Figure 2, two endothermic transitions are observed. One starts at  $90^\circ\text{C}$  and the other coinciding with the endotherm observed for the trihydrate, starts at  $190^\circ\text{C}$ . The inference to be drawn from this data is that the hexahydrate does degrade in two steps and that the two steps involve a transition from the hexaform to the triform.

Next, studies were carried out using DSC. In this case, it is the heat input rather than the temperature which is measured. The DSC thermogram of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  is shown in Figure 3. Only one endothermic transition was observed starting at  $100^\circ\text{C}$  with a peak maximum at  $160^\circ\text{C}$ . Both DTA and DSC analyses indicate that the thermal dehydration of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  is a one step process. From DSC data, it appears that the dehydration of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  starts at a low temperature,  $100^\circ\text{C}$ , in contrast to the DTA data from which it is inferred that  $190^\circ\text{C}$  is the starting temperature.

The DSC thermogram of  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  is shown in Figure 4. It is significant to note that only one endothermic transition was observed starting at  $45^\circ\text{C}$  with a peak maximum at  $90^\circ\text{C}$ . DSC results suggest that the thermal dehydration of  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$

takes place in one step starting at 45°C, in contrast to the two step mechanism starting at 90°C to be drawn from the DTA results.

Since the phenomena measured by DTA and DSC is the same, it was expected that the results would be consistent. Surprisingly, this was not the case. From the DSC data, it appears that the dehydration of both hydrates starts at a lower temperature and the hexaform dehydrates in one step and not in two steps as was inferred from the DTA results.

The apparent contradiction between the DTA and the DSC results can be rationalized by considering the relationship between the dehydration reaction and the sample environmental conditions. In any dehydration reaction water is liberated; if the latter is continuously removed from the reaction atmosphere two consequences are observed. First, the dehydration starts at a lower temperature, and, secondly, equilibrium is not attained.

On the one hand in the DSC studies, the sample is placed in an open dish and is heated under a sweeping stream of nitrogen. Under these conditions the liberated water is continuously removed from the reaction environment. On the other hand, in the DTA studies, the sample is heated in a self-generated atmosphere because it is placed in a capillary tube. Under the open conditions encountered in DSC, thermal dehydration starts at a lower temperature, 45°C versus 90°C



and only one endothermic transition is observed for the hexaform, whereas in the DTA studies two were observed.

To confirm the above rationalization of the differences between the DTA and the DSC studies, the thermal dehydration was studied by another independent technique, TGA, in which it was possible to heat the samples either in an open condition or in a self-generated atmosphere. TGA thermograms, under open conditions, were obtained by the conventional procedure in which the sample is placed in an open platinum dish under a sweeping blanket of nitrogen. TGA, under self-generated atmosphere, was achieved by placing the sample in a capillary tube with a thermocouple inside. Then, the whole tube was placed in the platinum dish.

In Figure 5, the TGA of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ , under open conditions is shown. Thermal dehydration starts at  $100^\circ\text{C}$  and takes place in one step. The weight loss of the sample is 34.0%, which corresponds to the loss of 3 moles of water. The effect of operating under open conditions is shown in Figure 6 for  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ . Thermal dehydration of the hexaform starts at  $70^\circ\text{C}$  and takes place in one step. The weight loss of the sample is 51%, which corresponds to the loss of 6 moles of water.

The thermograms for the trihydrate and the hexahydrate, respectively, under the conditions of a self-generated atmosphere are shown in Figures 7 and 8.  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ , as

shown in Figure 7, loses 34.5% of its weight in one step. This is in a very good agreement with TGA under open conditions, but thermal dehydration starts at 220°C, i.e., at a higher temperature, because of the self-generated atmosphere conditions. The weight loss for the hexahydrate under a self-generated atmosphere, as shown in Figure 8, is 51%, which corresponds to the loss of 6 moles of water. It is significant to note that the thermal dehydration of the hexaform starts at a higher temperature and takes place in two steps, with a weight loss of 25.5% in each step. In other words,  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  loses 3 moles of water in each dehydration step.

Thus, when the TGA study of the hexaform is carried out under a non-equilibrium condition, because of heating the sample under a sweeping blanket of nitrogen, equilibrium is not attained due to the continuous removal of the liberated water. As a result, thermal dehydration starts at a lower temperature and takes place in one step. On the other hand, if equilibrium is attained, because of heating the sample in a self-generated atmosphere, the TGA results showed that thermal dehydration starts at a higher temperature and takes place in two steps. First, dehydration leads to the formation of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ , then, to the anhydrous  $\text{MgSO}_3$ . These TGA observations are consistent with the explanation of the differences observed in the DTA and the DSC studies. The results are summarized in Table 1 for  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  and in

Table 2 for  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ . The onset of the endotherms as a function of the method are compared.

### APPLICATION

The observations made in the TGA studies were used as bases for developing a new analytical method for quantitating mixtures of the tri- and hexahydrates. It had been observed that although the second weight loss for the hexahydrate overlapped that of the trihydrate, nevertheless, from a knowledge of the first weight loss of the hexahydrate, the contribution of the hexahydrate to the second weight loss could be calculated.

The accuracy of the method was investigated by analyzing the thermograms of synthetic mixtures of the hexahydrate and the trihydrate ranging from 10% to 90%. The thermograms are shown in Figures 9-19.

From these thermograms, the water content and the magnesium sulfite content could be calculated. First, the water content calculations will be considered and compared to the theoretical values. The water content of each hydrate in a mixture can be obtained from the TGA thermogram, by taking into account the fact that the weight loss in the first dehydration step at 175°C represents the first three moles of water in  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ , i.e., 50% of the water content of the hexaform. Thus the water content can be calculated, from the TGA thermogram, as follows:

$$\begin{aligned} \% \text{H}_2\text{O in MgSO}_3 \cdot 6\text{H}_2\text{O in a mixture} &= (\% \text{ weight loss} \\ &\text{in the first step at 175°C}) (2) \end{aligned}$$

% H<sub>2</sub>O in MgSO<sub>3</sub>.3H<sub>2</sub>O in a mixture = (% weight loss in the second step at 400°C) - (% weight loss in the first step at 175°C)

The theoretical values of the water content are calculated as follows:

% H<sub>2</sub>O in MgSO<sub>3</sub>.6H<sub>2</sub>O in a mixture = % MgSO<sub>3</sub>.6H<sub>2</sub>O in the mixture

$$\frac{\text{X } 6\text{H}_2\text{O}}{\text{MgSO}_3 \cdot 6\text{H}_2\text{O}}$$

$$\text{X } 100$$

$$= \% \text{MgSO}_3 \cdot 6\text{H}_2\text{O} \text{ in the mixture}$$

$$\text{X } \frac{108}{212.3} \text{ X } 100$$

$$= \% \text{MgSO}_3 \cdot 6\text{H}_2\text{O} \text{ in the mixture}$$

$$\text{X } 50.9$$

% H<sub>2</sub>O in MgSO<sub>3</sub>.3H<sub>2</sub>O in a mixture = % MgSO<sub>3</sub>.3H<sub>2</sub>O in the mixture

$$\frac{\text{X } 3 \text{ H}_2\text{O}}{\text{MgSO}_3 \cdot 3\text{H}_2\text{O}} \text{ X } 100$$

$$= \% \text{MgSO}_3 \cdot 3\text{H}_2\text{O} \text{ in the mixture}$$

$$\text{X } \frac{54}{158.3} \text{ X } 100$$

$$= \% \text{MgSO}_3 \cdot 3\text{H}_2\text{O} \text{ in the mixture}$$

$$\text{X } 34.1$$

Both theoretical and observed values of the water content are shown in Table 3. The percent water (observed values) is plotted versus magnesium sulfite content in Figure 21 for MgSO<sub>3</sub>.3H<sub>2</sub>O and in Figure 22 for MgSO<sub>3</sub>.6H<sub>2</sub>O.

The magnesium sulfite content can be calculated from the TGA thermograms by considering the same aspects mentioned in the water content calculations, and, taking into account that 6 moles of water represent 50.9% by weight of  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$ , and that 3 moles of water represent 34.1% by weight of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ . Thus the percent of each hydrate in a mixture is calculated as follows:

$$\% \text{MgSO}_3 \cdot 6\text{H}_2\text{O} \text{ in a mixture} = \% \text{ weight loss at } 175^\circ\text{C} \times 2 \times \frac{100}{50.9}$$

$$\% \text{MgSO}_3 \cdot 3\text{H}_2\text{O} \text{ in a mixture} = (\% \text{ weight loss between } 175^\circ \text{ and } 400^\circ\text{C} \text{ } \underline{\hspace{1cm}} \% \text{ weight loss at } 175^\circ\text{C}) \times \frac{100}{34.1}$$

The data obtained is compared versus the theoretical values in Table 4 for the triform and in Table 5 for the hexaform. The accuracy of the method, as shown in Tables 4 and 5, was found to be  $\pm 3\%$  if no calibration curve is used. A value of less than 1% is to be expected if a calibration curve is used.

Furthermore, the TGA method was tested in the presence of TGA inactive material. This was achieved by analyzing a mixture of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ ,  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  and glass beads. The mixture was subjected to the same experimental conditions of a self-generated atmosphere. The TGA thermogram is shown in Figure 20. From the results summarized in Table 6, it is concluded that this method does not suffer any interferences due to the presence of thermally inactive materials.

Relevant to the nature of the materials obtained in the Magnesia Process, the quantitative analysis of mixtures of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$  and  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  has to be considered in the light of the following contexts: one, only these two hydrates are present; two, in the presence of  $\text{MgO}$ , three, in the presence of another hydrate,  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$ . The latter is a common product in the Magnesia Process.

When only the two hydrates are present, methods available include total sulfite by iodine titration<sup>(3)</sup>, X-ray analysis<sup>(5)</sup>, and a wet chemical method developed by Dr. Ray which will be referred to as Ray's Method<sup>(7)</sup>.

In the presence of  $\text{MgO}$  and/or  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$  the measurement of the sulfite content cannot be used to determine the ratio of the hydrates. From the available literature which is limited to the one paper previously cited<sup>(5)</sup>, it is not clear as to whether or not quantitative analysis is possible using the X-ray method in the presence of  $\text{MgO}$  and/or  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$ . Ray's method is applicable in the presence of these materials.

The TGA method is simpler than Ray's method but it is not applicable in the presence of  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$ . On the other hand, Dr. Ray<sup>(7)</sup> has developed a simple procedure for quantitatively stripping  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$  from mixtures of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ ,  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$  and  $\text{MgO}$ . Therefore it appears that the TGA technique in conjunction with Ray's stripping procedure is the optimum method.

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Table 1Starting Temperature of ThermalDehydration of  $\text{MgSO}_3 \cdot 3\text{H}_2\text{O}$ 

<u>Technique</u>	<u>Experimental Conditions</u>	<u>Onset of the Endotherm</u>
DTA	self-generated	190°C
DSC	open conditions	100°C
TGA	open conditions	100°C
TGA	self-generated	200°C

Table 2  
Starting Temperature of  
Thermal Dehydration of  $\text{MgSO}_3 \cdot 6\text{H}_2\text{O}$

<u>Technique</u>	<u>Experimental Condition</u>	<u>First Endotherm</u>	<u>Second Endotherm</u>
DTA	self-generated	90°C	190°C
DSC	open conditions	45°C	not observed
TGA	open conditions	70°C	not observed
TGA	self-generated	125°C	220°C

Table 3  
Calculated and Observed Values  
of Water Content in  
Synthetic Mixtures

<u>Std#</u>	<u>Composition</u>		<u>Calculated H<sub>2</sub>O content in</u>			<u>Observed H<sub>2</sub>O content in</u>		
	<u>%MgSO<sub>3</sub>·3H<sub>2</sub>O</u>	<u>%MgSO<sub>3</sub>·6H<sub>2</sub>O</u>	<u>Triform</u>	<u>Hexaform</u>	<u>Total</u>	<u>Triform</u>	<u>Hexaform</u>	<u>Total</u>
1	0.0%	100%	0%	50.9%	50.9%	0%	52%	52%
2	10.29%	84.71%	3.5%	45.56%	49.06%	3.4%	44.4%	47.8%
3	18.96%	81.04%	6.46%	41.19%	47.65%	6.6%	39.4%	46%
4	29.37%	70.63%	10%	35.9%	45.9%	9.0%	35.0%	44%
5	38.24%	61.76%	13.03%	31.39%	44.42%	12%	32%	44%
6	50%	50%	17.04%	25.42%	42.46%	16.4%	26%	42.4%
7	59.84%	40.16%	20.39%	20.41%	40.8%	19.8%	20.4%	40.2%
8	70.19%	29.81%	23.91%	15.15%	39.06%	23%	16%	39%
9	79.34%	20.66%	27.03%	10.5%	37.53%	26.4%	10.6%	37%
10	90.18	9.82%	30.72%	4.99%	35.71%	30.2%	5%	35.2%
11	100%	0%	34.1%	0%	34.1%	34.8%	0%	34.8%

Table 4MgSO<sub>3</sub>·3H<sub>2</sub>O Content from TGA

<u>Std#</u>	<u>Theoretical Value</u>	<u>Observed Value</u>	<u>Deviation</u>
1	0%	0%	0%
2	10.29%	10.26%	-.03%
3	18.96%	19.35%	+.39%
4	29.37%	26.39%	-2.98%
5	38.24%	35.24%	-3.00%
6	50.0%	48.1%	-1.9%
7	59.84%	58.06%	-1.78%
8	70.19%	67.45%	-2.74%
9	79.34%	77.42%	-1.92%
10	90.18%	88.56%	-1.62%
11	100.00%	102.0%	+2.0%

Table 5  
MgSO<sub>3</sub>.6H<sub>2</sub>O Content  
From TGA

<u>Std#</u>	<u>Theoretical Value</u>	<u>Observed Value</u>	<u>Deviation</u>
1	100%	102.2%	+2.2%
2	89.71%	87.3%	-2.41%
3	81.04%	78.45%	-2.54%
4	70.63%	68.8%	-1.83%
5	61.76%	62.9%	+1.14%
6	50%	51.11%	+1.11%
7	40.16%	40.1%	-.06%
8	29.81%	31.45%	+1.64%
9	20.66%	20.84%	+.18%
10	9.82%	9.83%	+.01%
11	0%	0%	0%

Table 6  
TGA results of a synthetic  
mixture containing thermally  
inactive compound

	<u>Theoretical Value</u>	<u>Observed Value</u>
MgSO <sub>3</sub> .3H <sub>2</sub> O	44.3%	43.2%
MgSO <sub>3</sub> .6H <sub>2</sub> O	30.0%	29.3%
glass beads	25.7%	27.5%*

\*This value was obtained by difference



SAMPLE: MgSO<sub>3</sub>·3H<sub>2</sub>O

Fig. No. 1

ORIGIN:

SIZE 6 mg

REF. glass beads

PROG. MODE heat

RATE 10 <sup>°C</sup>/MIN, START 30 °C

ATM. self-generated MM

SCALE

SHIFT

T

50 <sup>°C</sup>/IN.

0 IN.

Δ T

2 <sup>°C</sup>/IN.

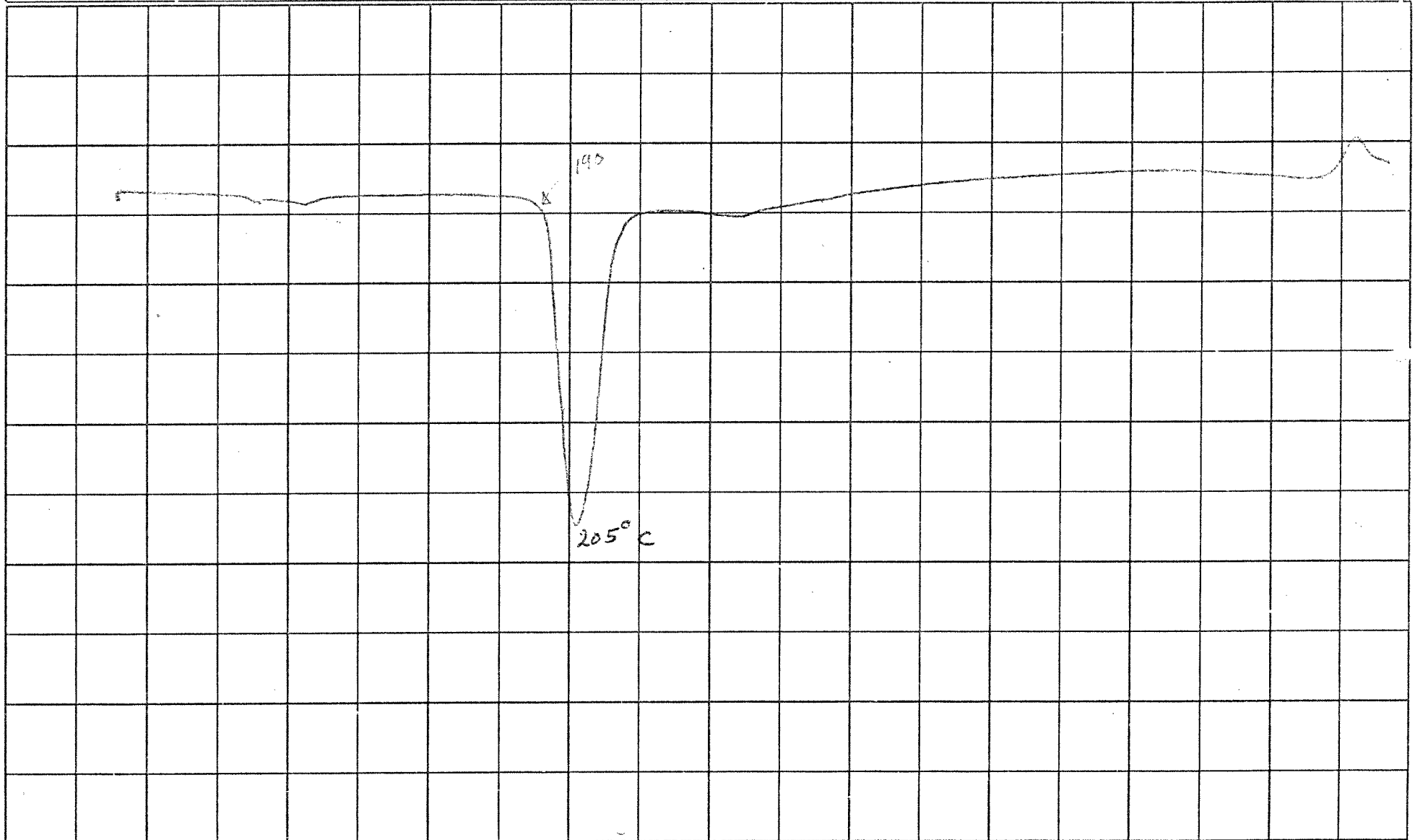
0 IN.

RUN NO. 1

DATE 11/8/74

OPERATOR RM

BASE LINE SLOPE 0



SAMPLE:

RUN NO.:



23

SAMPLE: $MgSO_3 \cdot 6H_2O$  Fig. No. 2  ORIGIN:	SIZE <u>8 mg</u>	ATM. <u>self-generated</u> MM	RUN NO. <u>J</u>
	REF. <u>glass beads</u>	T	DATE <u>11/8/74</u>
	PROG. MODE <u>heat</u>	SCALE <u>50</u> $\frac{^{\circ}C}{IN.}$	OPERATOR <u>RM</u>
	RATE <u>10</u> $\frac{^{\circ}C}{MIN.}$ , START <u>30</u> $^{\circ}C$	SHIFT <u>0 IN.</u>	BASE LINE SLOPE <u>0</u>

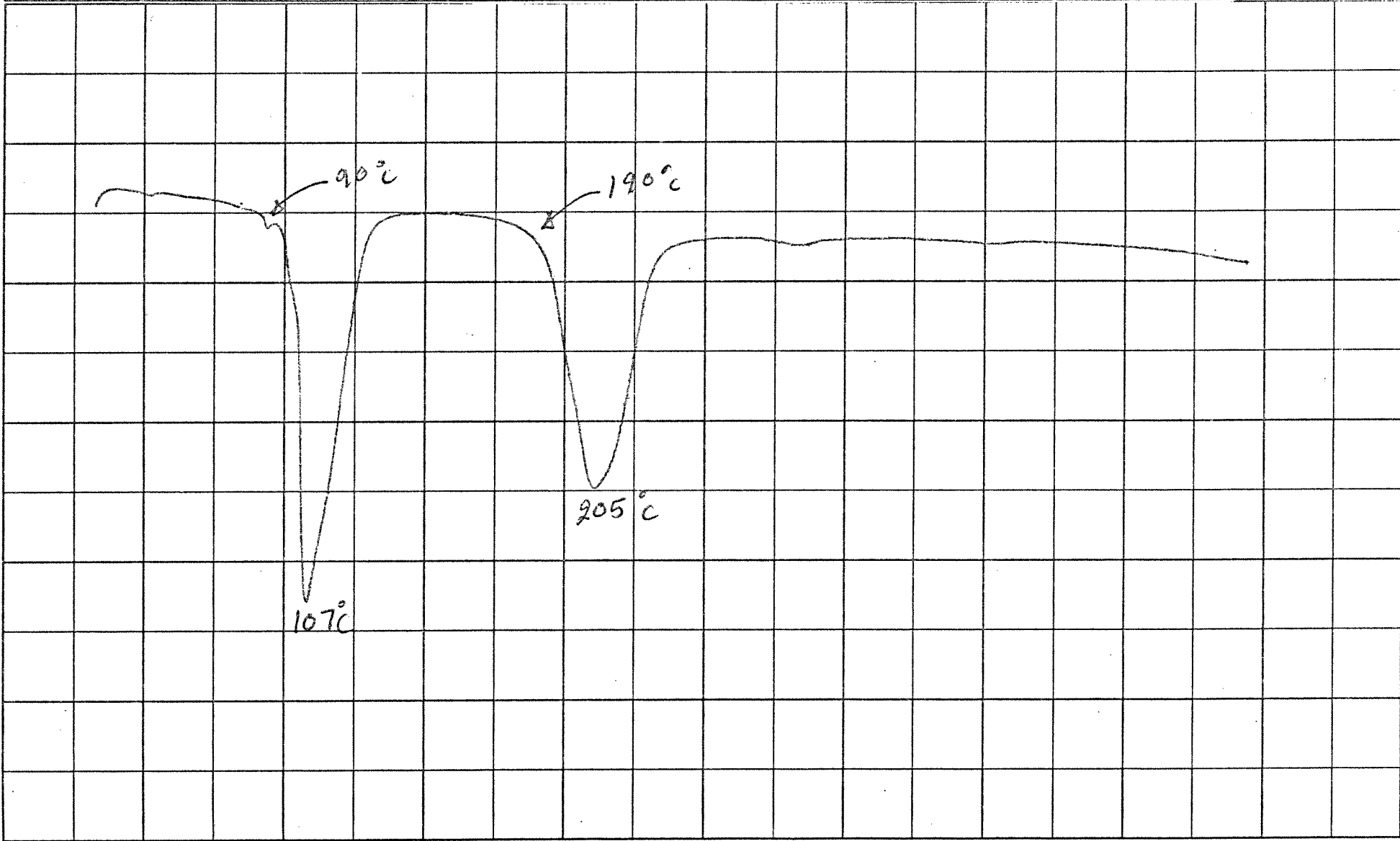
EXO



$\Delta T$



ENDO



SAMPLE:

RUN NO.:





SAMPLE: MgSO<sub>3</sub> · 3H<sub>2</sub>O

Fig. No. 3

SIZE 12 mg

REF. empty pan

PROG. MODE heat

RATE 10 °C/MIN, START 25 °C

ATM. N<sub>2</sub>

30 MM

RUN NO. 1

T

Δ T

DATE 11/9/74

SCALE

50 °C/IN.

1 °C/IN.

OPERATOR RM

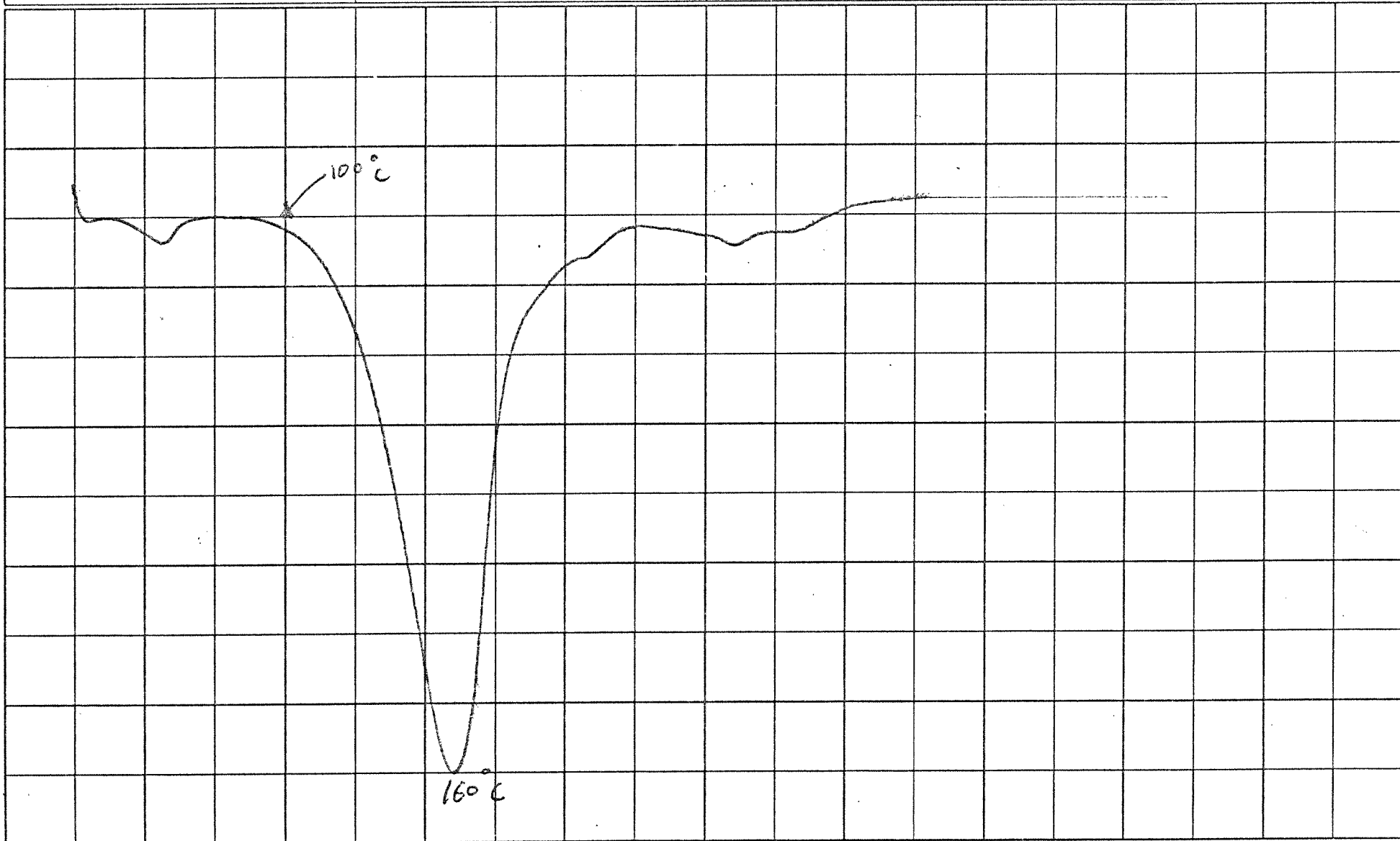
SHIFT

0 IN.

0 IN.

BASE LINE SLOPE 0

ORIGIN:



SAMPLE: \_\_\_\_\_  
RUN NO.: \_\_\_\_\_



25

SAMPLE:  $MgSO_3 \cdot 6H_2O$

Fig. No. 4

SIZE 5 mg

ATM.  $N_2$ , 30 MM

RUN NO. 1

REF. empty pan

T

$\Delta T$

DATE 11/9/74

PROG. MODE heat

SCALE

50  $\frac{^\circ C}{IN.}$

1  $\frac{^\circ C}{IN.}$

OPERATOR RM

ORIGIN:

RATE 10  $\frac{^\circ C}{MIN.}$ , START 30  $^\circ C$

SHIFT

0 IN.

0 IN.

BASE LINE SLOPE 0

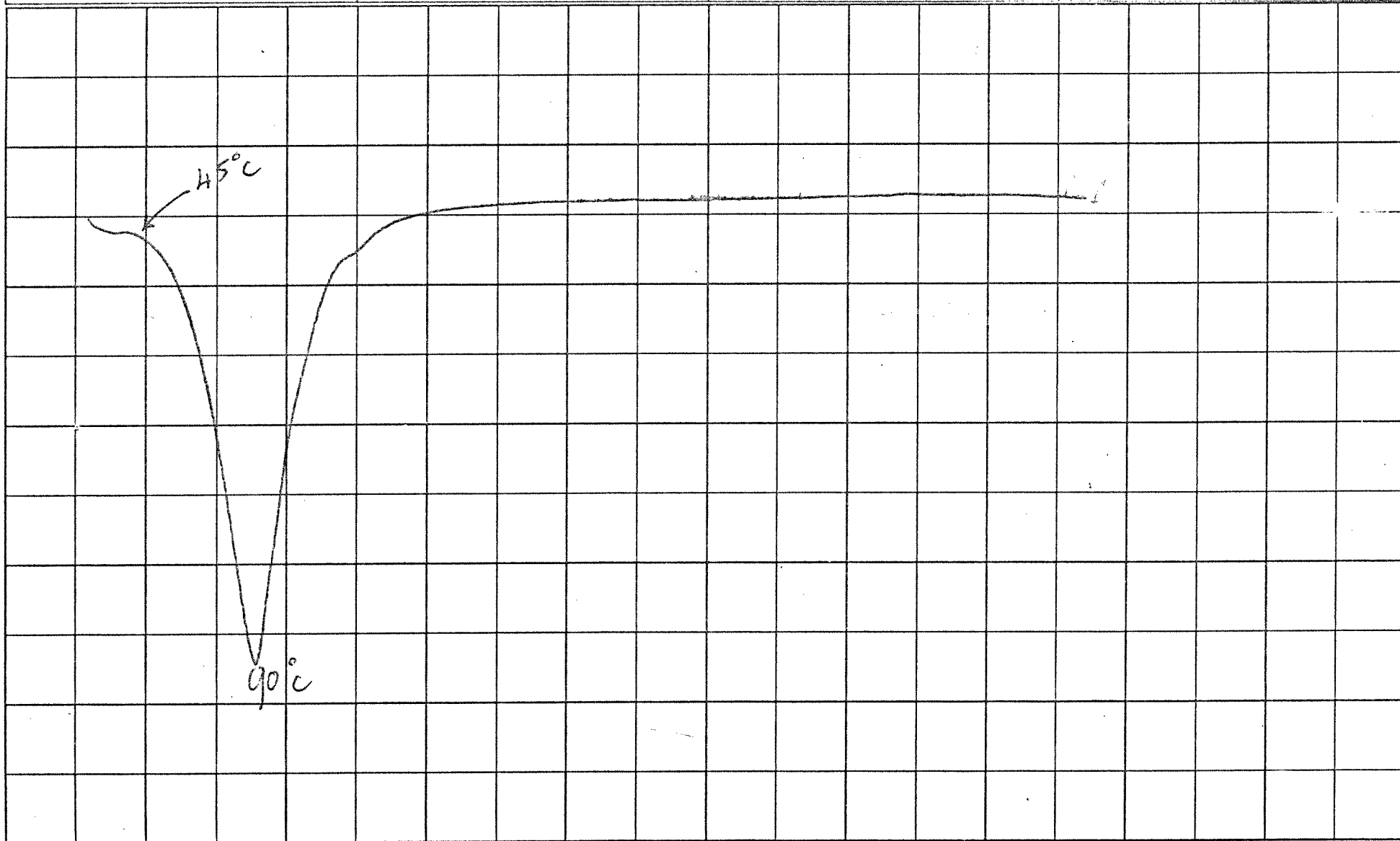
EXU

↑

$\Delta T$

↓

ENDU



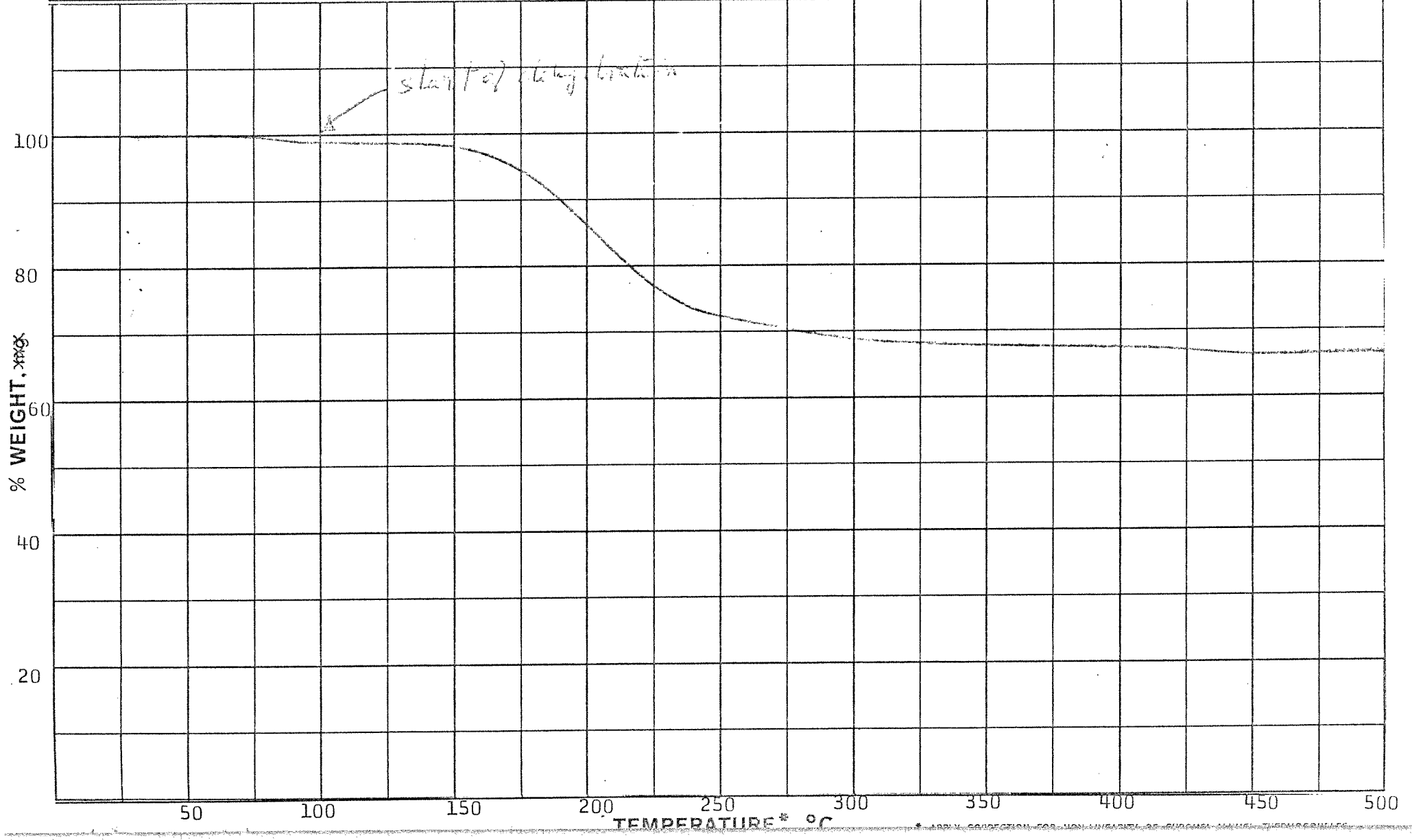
SAMPLE:

RUN NO.:



26

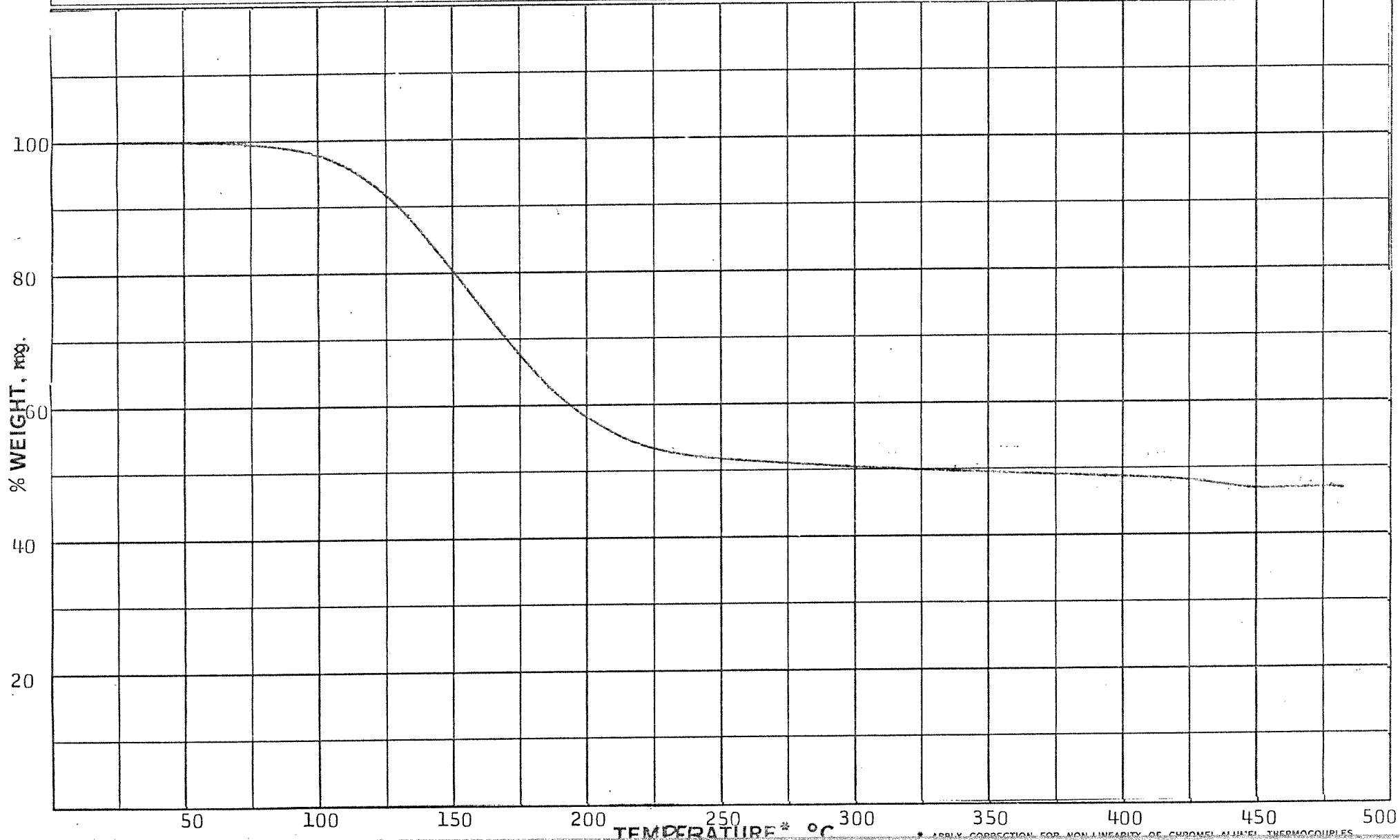
<b>SAMPLE:</b> $MgSO_3 \cdot 3H_2O$  Fig. No. 5  SIZE 20 mg.	<b>X-AXIS</b>	<b>Y-AXIS</b>	RUN NO. 1    DATE 11/12/74
	TEMP. SCALE 50 $^{\circ}C$ / inch SHIFT 0 inch TIME SCALE (ALT.)	SCALE 4 mg. / inch (SCALE SETTING X 2)  SUPPRESSION 50 mg.	OPERATOR RM HEATING RATE 10 $^{\circ}C$ / min. ATM. $N_2$ , 30 ml/min. TIME CONSTANT 1 sec.



\* APPLY CORRECTION FOR NON-LINEARITY OF CURVE AS SHOWN IN THE USER'S MANUAL



<b>SAMPLE:</b> $MgSO_3 \cdot 6H_2O$ Fig. No. 6 SIZE <u>20</u> mg.	<b>X-AXIS</b>		<b>Y-AXIS</b>		RUN NO. <u>1</u> DATE <u>11/12/74</u>	
	TEMP. SCALE <u>50</u> $^{\circ}C$ inch	SCALE <u>4</u> $\frac{mg.}{inch}$ (SCALE SETTING X 2)	OPERATOR <u>RM</u>	HEATING RATE <u>10</u> $^{\circ}C$ min.	ATM. <u>N<sub>2</sub></u> , <u>30</u> ml/min.	TIME CONSTANT <u>1</u> sec.
	SHIFT <u>0</u> inch	TIME SCALE (ALT.) _____	SUPPRESSION <u>5</u> mg.			

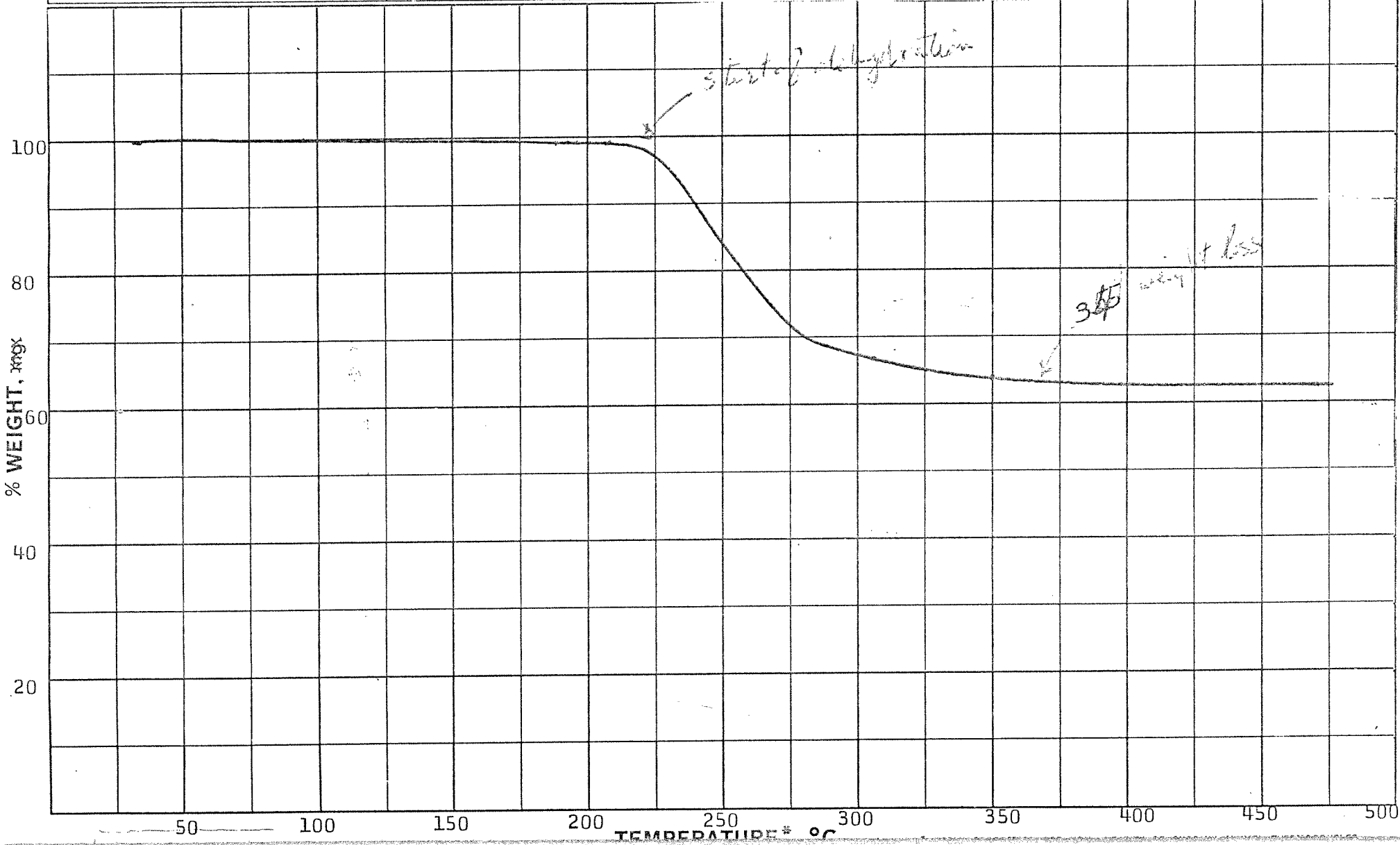


\* APPLY CORRECTION FOR NON-LINEARITY OF CHROMEL-ALUMEL THERMOCOUPLES



28

<b>SAMPLE:</b> $MgSO_3 \cdot 3H_2O$ Fig. No. 7 SIZE 5 mg.	<b>X-AXIS</b>		<b>Y-AXIS</b>		RUN NO. 1    DATE 11/15/71
	TEMP. SCALE 50 $^{\circ}C$ inch	SCALE 2 $\frac{mg.}{inch}$ (SCALE SETTING X 2)	OPERATOR RM		HEATING RATE 10 $^{\circ}C$ min.
	SHIFT 0 inch	SUPPRESSION 60 mg.	ATM. self-generated		TIME CONSTANT 1 sec.





29

SAMPLE:  $MgSO_3 \cdot 6H_2O$

Fig. No. 8

SIZE 5 mg.

X-AXIS

TEMP. SCALE 50 °C  
inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 1 mg.  
inch

(SCALE SETTING X 2)

SUPPRESSION 60 mg.

RUN NO. 1 DATE 11/16/74

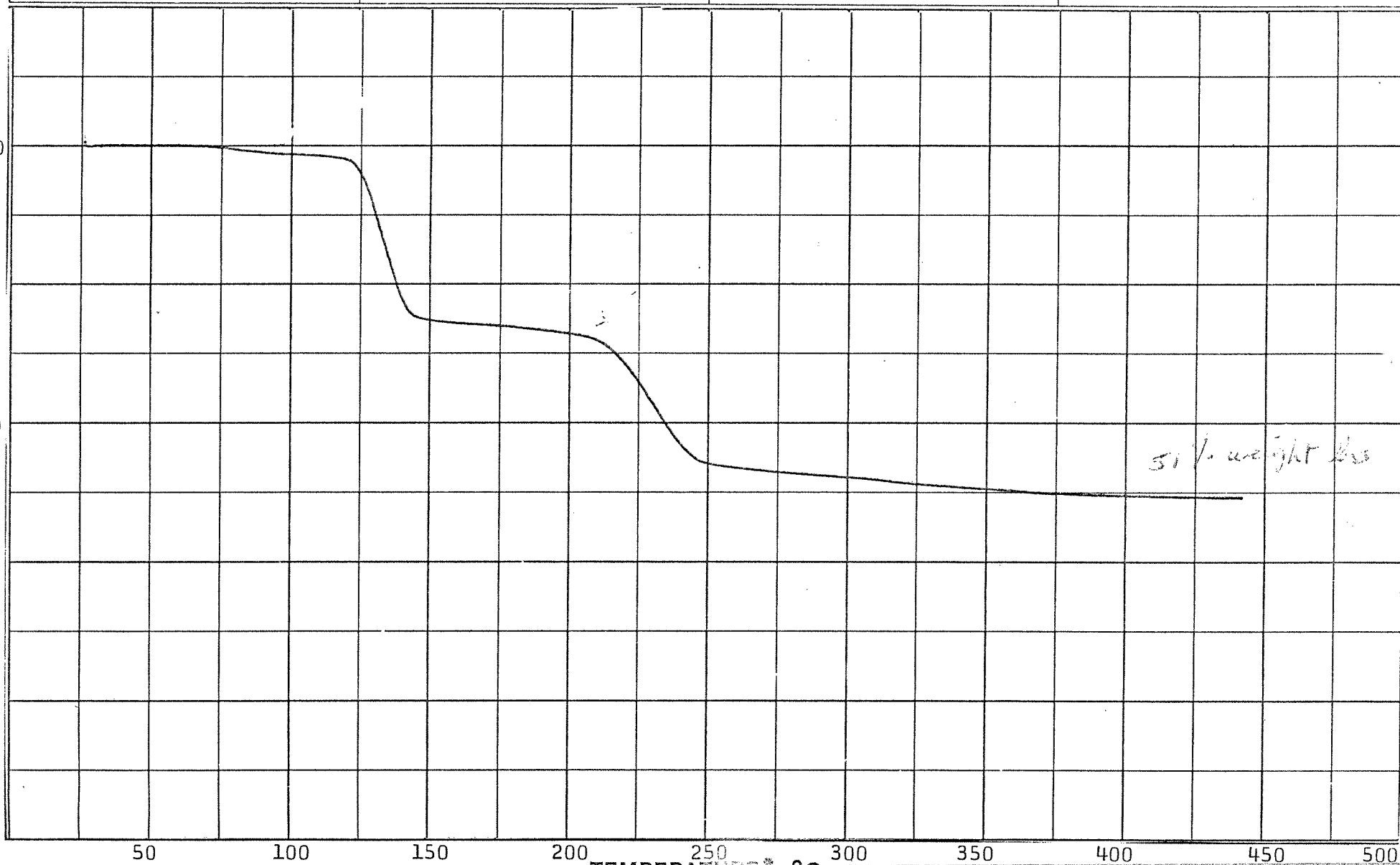
OPERATOR RM

HEATING RATE 10 °C  
min.

ATM. self-generated

TIME CONSTANT sec.

%WEIGHT, RES.





30

SAMPLE: Std #1  
100% MgSO<sub>3</sub>.6H<sub>2</sub>O

Fig. No. 9

SIZE 12 mg.

X-AXIS

TEMP. SCALE 50 °C  
inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 2 mg.  
inch  
(SCALE SETTING X 2)

SUPPRESSION 50 mg.

RUN NO. 1 DATE 11/17/74

OPERATOR RM

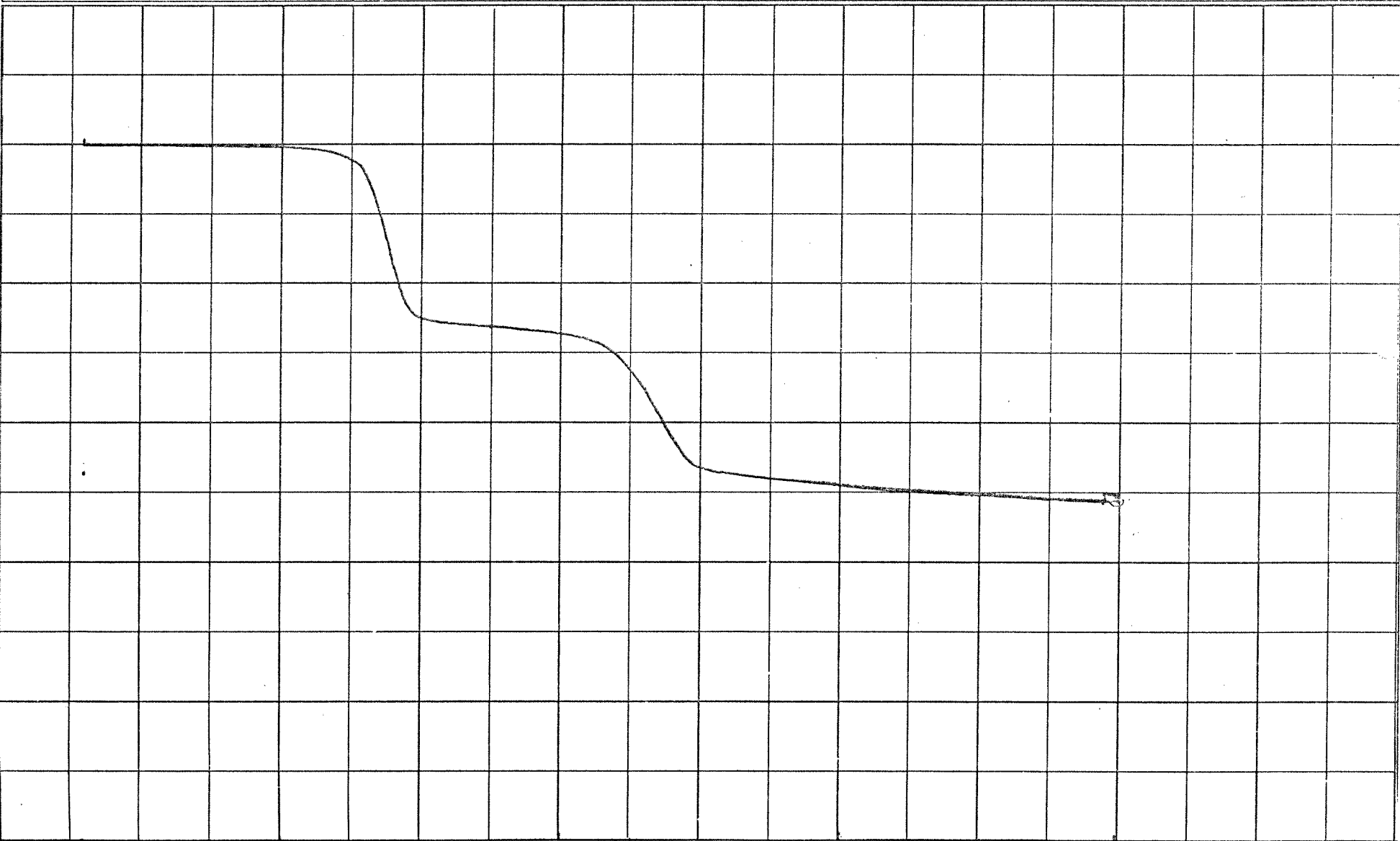
HEATING RATE 10 °C  
min.

ATM. self-generated

TIME CONSTANT 1 sec.

100  
80  
60  
40  
20

% WEIGHT, mg.



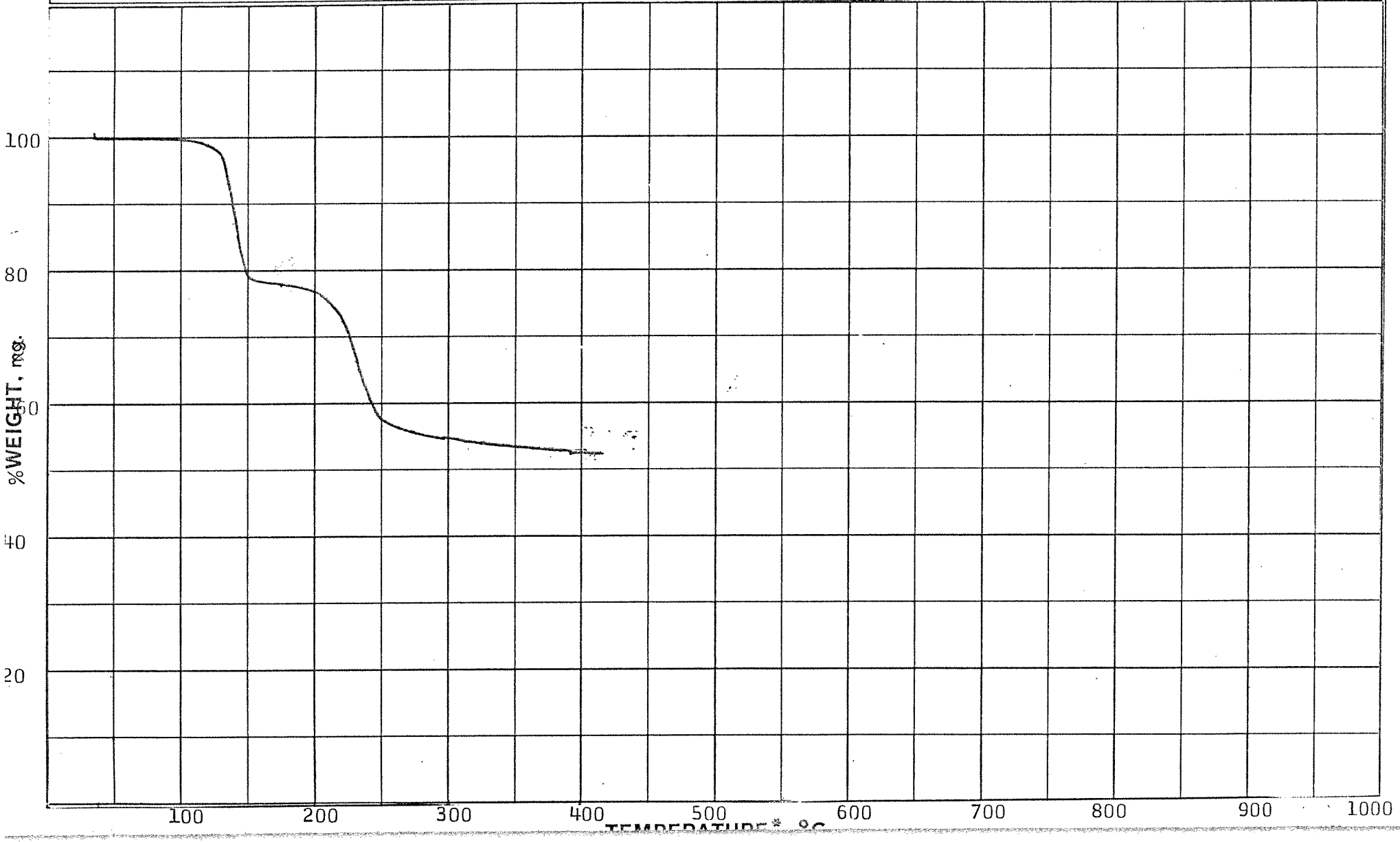
50 100 150 200 250 300 350 400 450 500

TEMPERATURE, °C



31

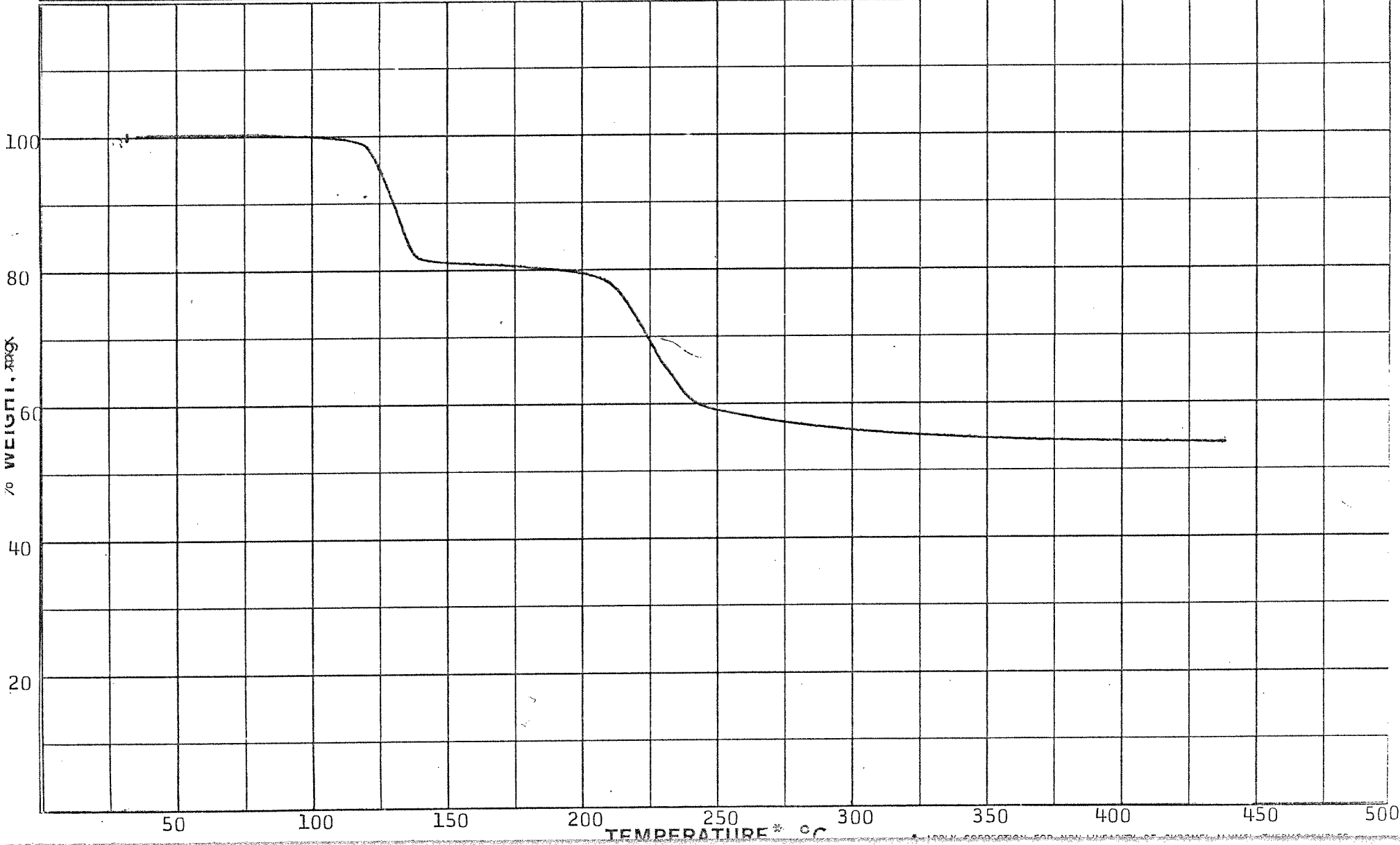
<b>SAMPLE:</b> Std #2 10.29% MgSO <sub>3</sub> .3H <sub>2</sub> O 89.71% MgSO <sub>3</sub> .6H <sub>2</sub> O  Fig. No. 10 SIZE 10 mg.	<b>X-AXIS</b>	<b>Y-AXIS</b>	RUN NO. 1 DATE 11/20/74
	TEMP. SCALE 100 °C / inch SHIFT 0 inch TIME SCALE (ALT.)	SCALE 2 mg. / inch (SCALE SETTING X 2) SUPPRESSION 50 mg.	OPERATOR RM HEATING RATE 10 °C / min. ATM. self-generated TIME CONSTANT 1 sec.







<b>SAMPLE:</b> Std #3 18.96% $MgSO_3 \cdot 3H_2O$ 81.04% $MgSO_3 \cdot 6H_2O$  Fig. No. 11 SIZE 15 mg.	<b>X-AXIS</b>		<b>Y-AXIS</b>		RUN NO. 1	DATE 11/21/74
	TEMP. SCALE	50 °C inch	SCALE	2 mg. inch	OPERATOR	RM
	SHIFT	0 inch	(SCALE SETTING X 2)		HEATING RATE	10 °C min.
	TIME SCALE (ALT.)		SUPPRESSION	50 mg.	ATM.	self-generated
					TIME CONSTANT	1 sec.





33

SAMPLE: Std #4  
 29.37% MgSO<sub>3</sub>·3H<sub>2</sub>O  
 70.63% MgSO<sub>3</sub>·6H<sub>2</sub>O

Fig. No. 12

SIZE 10 mg.

X-AXIS

TEMP. SCALE 50 °C / inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 2 mg. / inch  
(SCALE SETTING X 2)

SUPPRESSION 50 mg.

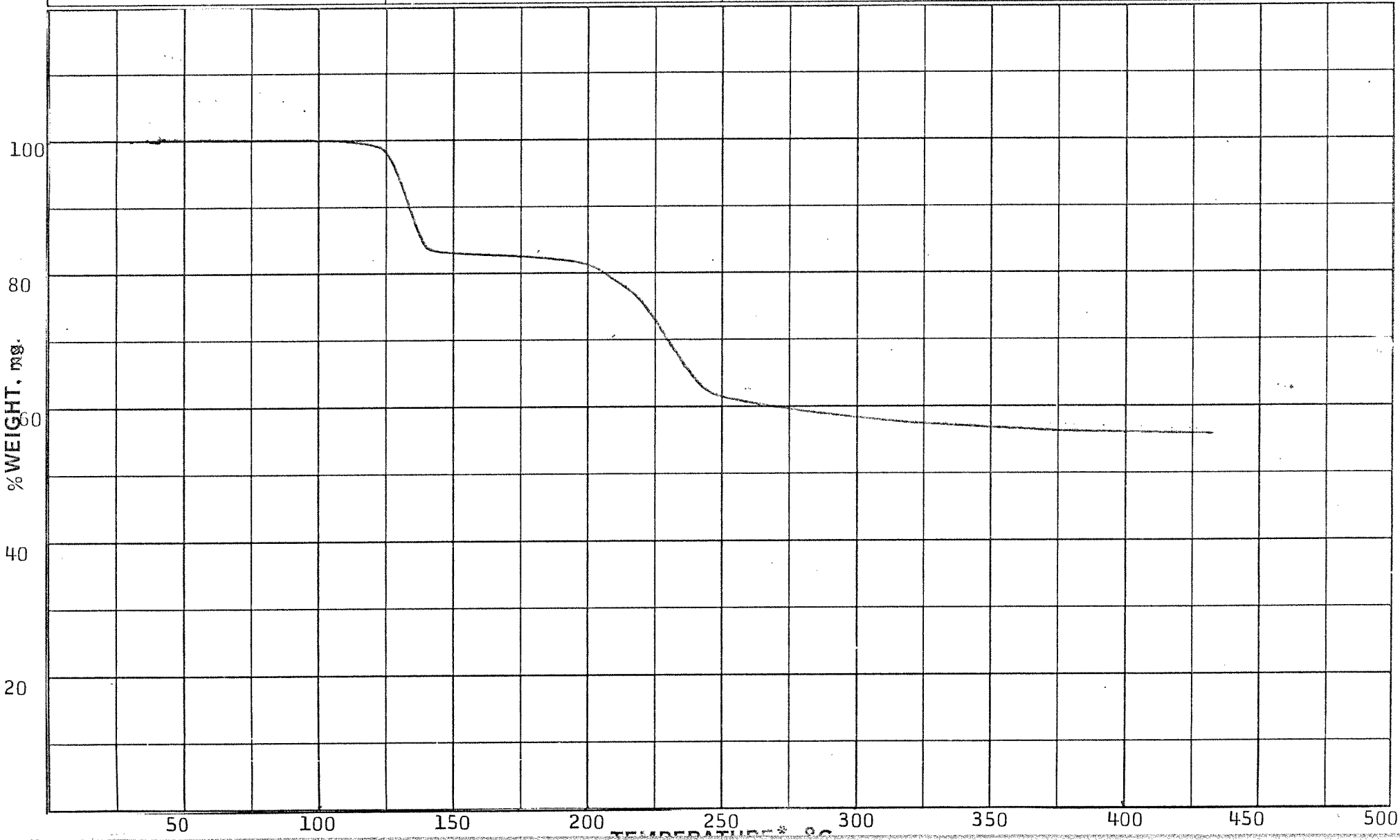
RUN NO. 1 DATE 11/22/74

OPERATOR RM

HEATING RATE 10 °C / min.

ATM. self-generated

TIME CONSTANT 1 sec.



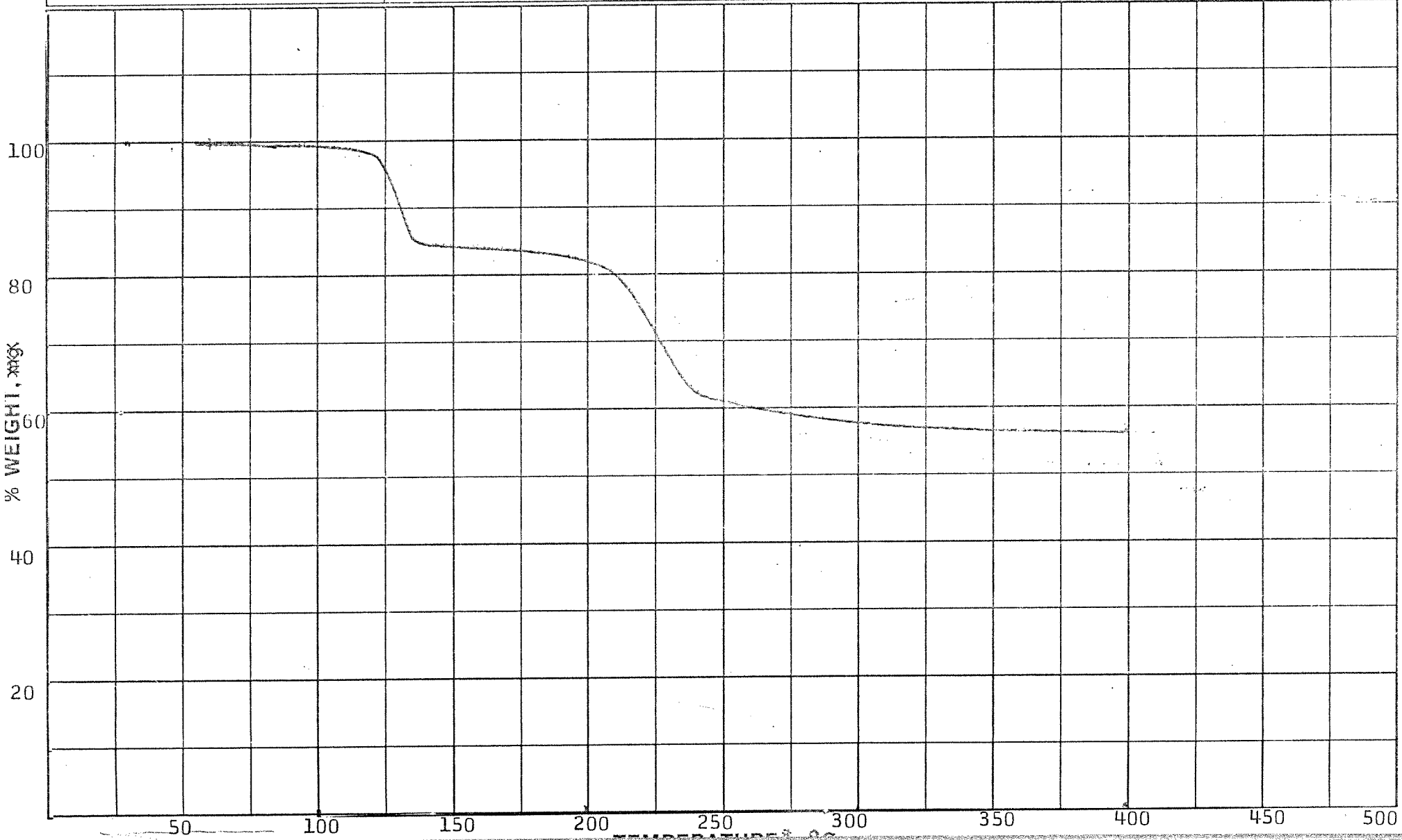


SAMPLE: Std #5  
 38.24% MgSO<sub>3</sub>·3H<sub>2</sub>O  
 61.76% MgSO<sub>3</sub>·6H<sub>2</sub>O  
 Fig. No. 13  
 SIZE 12 mg.

X-AXIS  
 TEMP. SCALE 50 °C / inch  
 SHIFT 0 inch  
 TIME SCALE (ALT.)

Y-AXIS  
 SCALE 2 mg. / inch  
 (SCALE SETTING X 2)  
 SUPPRESSION 50 mg.

RUN NO. 1 DATE 11/25/74  
 OPERATOR RM  
 HEATING RATE 10 °C / min.  
 ATM. self-generated  
 TIME CONSTANT 1 sec.





35

SAMPLE: Std #6  
50% MgSO<sub>3</sub>.3H<sub>2</sub>O  
50% MgSO<sub>3</sub>.6H<sub>2</sub>O

Fig. No. 14

SIZE 10 mg.

X-AXIS

TEMP. SCALE 50 °C  
inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 2 mg.  
inch  
(SCALE SETTING X 2)

SUPPRESSION mg.

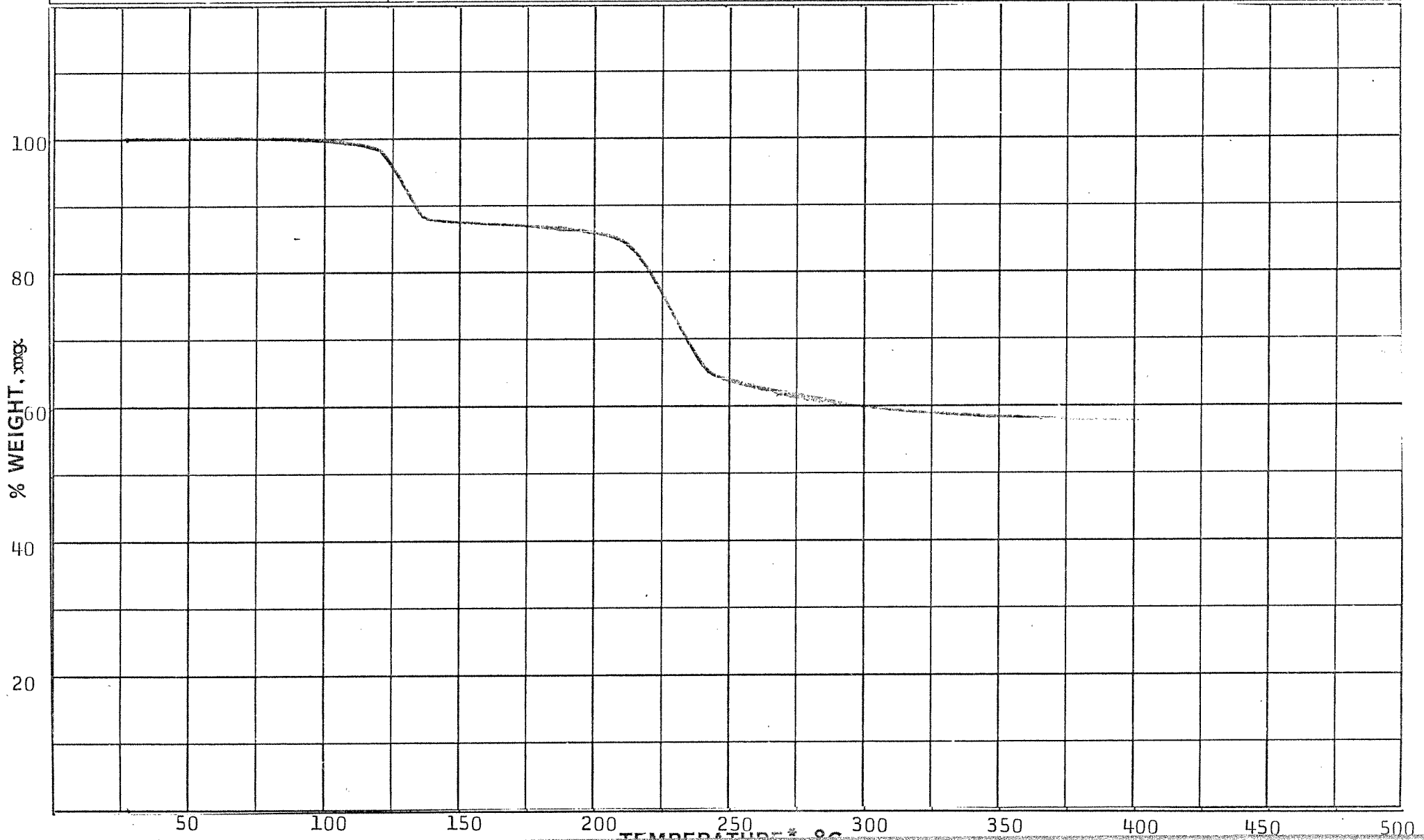
RUN NO. 1 DATE 11/25/74

OPERATOR RM

HEATING RATE 10 °C  
min.

ATM. self-generated

TIME CONSTANT 1 sec.





36

SAMPLE: Std #7  
59.84%  $MgSO_3 \cdot 3H_2O$   
40.16%  $MgSO_3 \cdot 6H_2O$

Fig. No. 15

SIZE 12 mg.

X-AXIS

TEMP. SCALE 50  $^{\circ}C$   
inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 2  $\frac{mg.}{inch}$   
(SCALE SETTING X 2)

SUPPRESSION 50 mg.

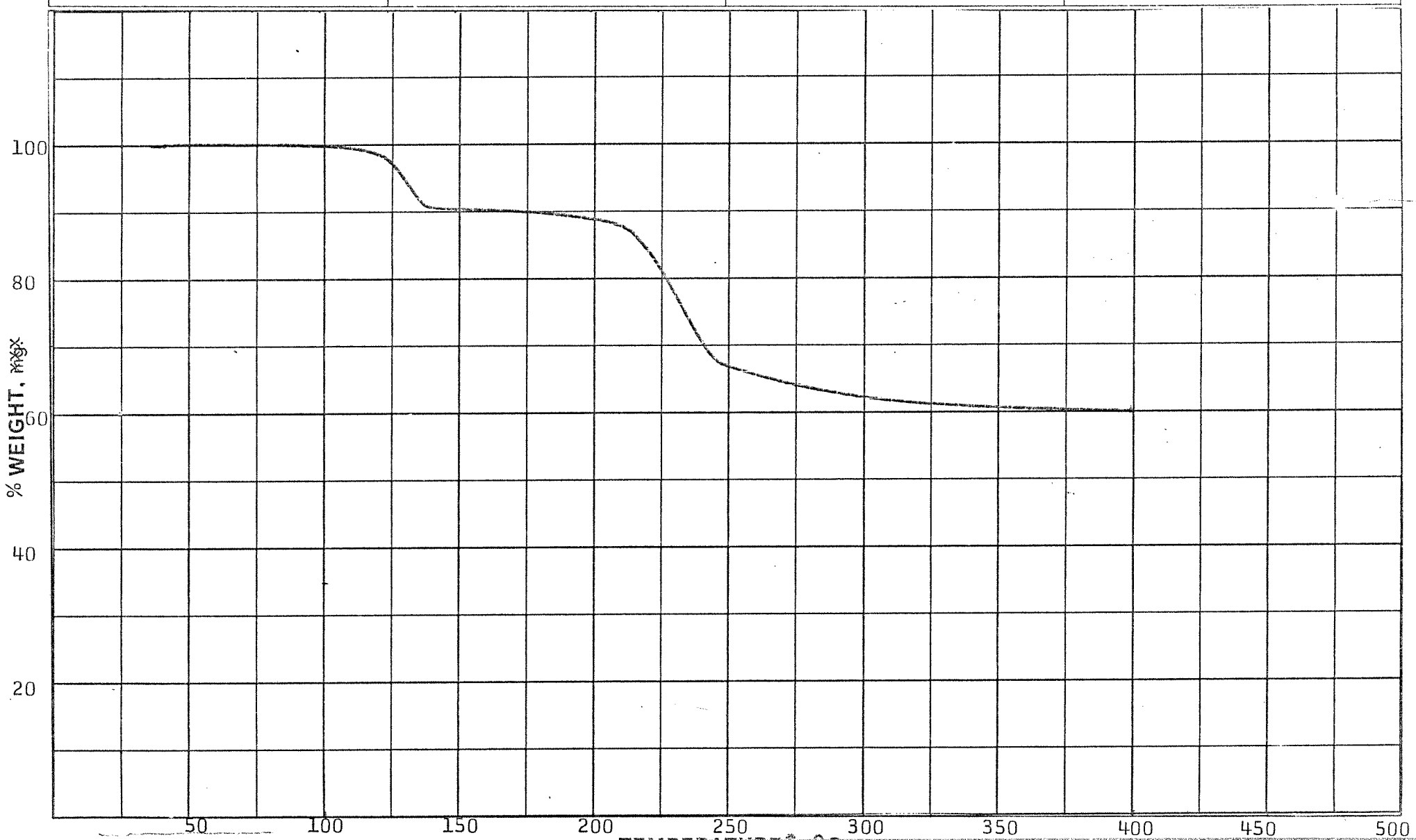
RUN NO. 1 DATE 11/27/74

OPERATOR RM

HEATING RATE 10  $^{\circ}C$   
min.

ATM. self-generated

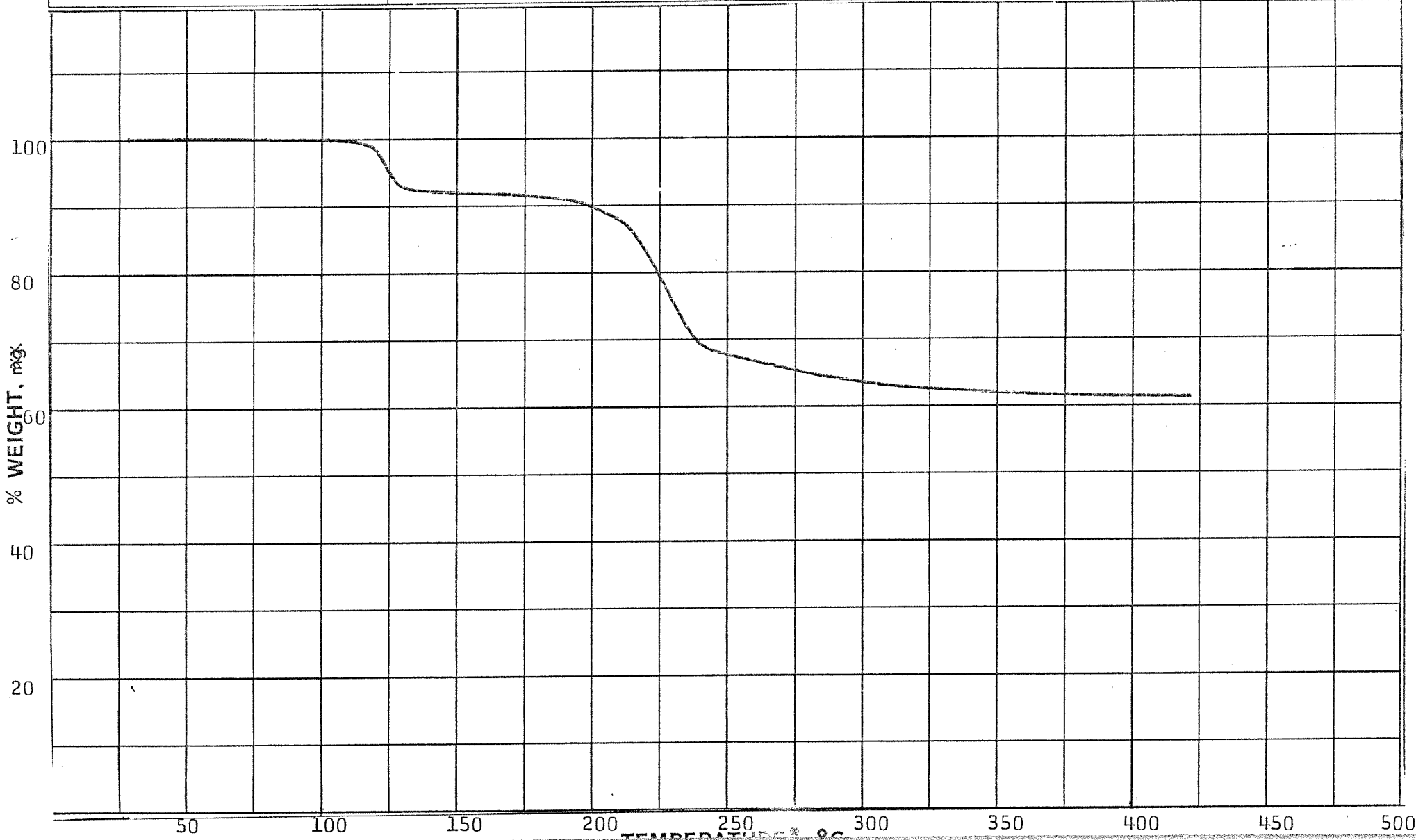
TIME CONSTANT 1 sec.





5/

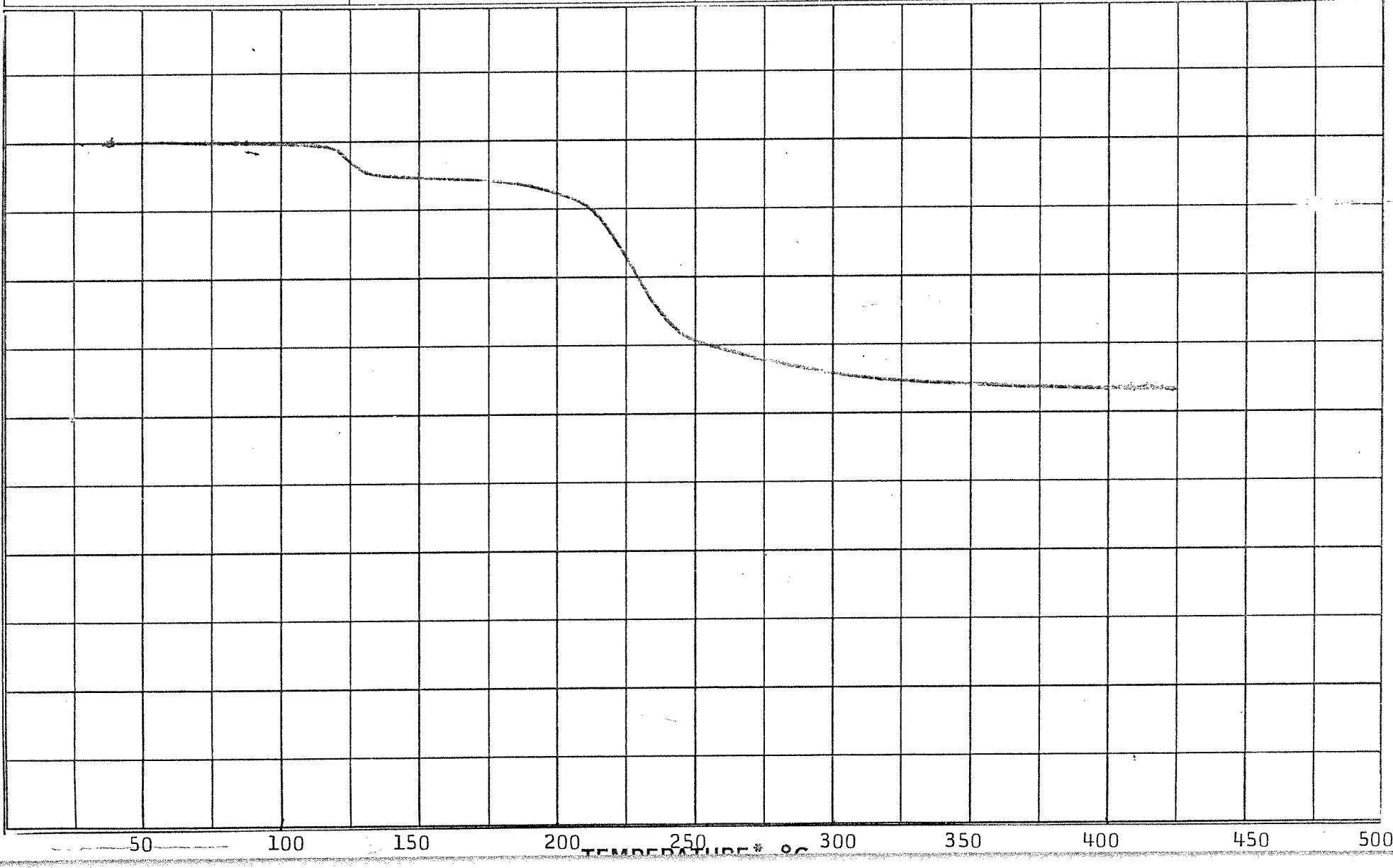
<b>SAMPLE:</b> Std #8 70.19% MgSO <sub>3</sub> .3H <sub>2</sub> O 29.81% MgSO <sub>3</sub> .6H <sub>2</sub> O  Fig. No. 16  <b>SIZE</b> 12 mg.	<b>X-AXIS</b>	<b>Y-AXIS</b>	<b>RUN NO.</b> 1 <b>DATE</b> 11/25/74
	<b>TEMP. SCALE</b> 50 $\frac{^{\circ}\text{C}}{\text{inch}}$ <b>SHIFT</b> 0 inch <b>TIME SCALE (ALT.)</b>	<b>SCALE</b> 2 $\frac{\text{mg.}}{\text{inch}}$ (SCALE SETTING X 2)  <b>SUPPRESSION</b> 50 mg.	<b>OPERATOR</b> RM <b>HEATING RATE</b> 10 $\frac{^{\circ}\text{C}}{\text{min.}}$ <b>ATM.</b> self-generated <b>TIME CONSTANT</b> 1 sec.





38

<p>SAMPLE: Std #9                  79.34% MgSO<sub>3</sub>.3H<sub>2</sub>O                  20.66% MgSO<sub>3</sub>.6H<sub>2</sub>O                  Fig. No. 17                  SIZE 14 mg.</p>	<p>X-AXIS</p>		<p>Y-AXIS</p>		<p>RUN NO. 1 DATE 11/27/74</p>
	<p>TEMP. SCALE 50 °C                  inch</p>	<p>SHIFT 0 inch</p>	<p>SCALE 2 mg.                  inch                  (SCALE SETTING X 2)</p>	<p>SUPPRESSION 50 mg.</p>	<p>OPERATOR RM</p>
<p>TIME SCALE (ALT.)</p>				<p>ATM. self-generated</p>	<p>TIME CONSTANT 1 sec.</p>





SAMPLE: Std #10  
 90.18% MgSO<sub>3</sub>.3H<sub>2</sub>O  
 9.82% MgSO<sub>3</sub>.6H<sub>2</sub>O

Fig. No. 18

SIZE 16 mg.

X-AXIS

TEMP. SCALE 50 °C / inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 2 mg. / inch  
(SCALE SETTING X 2)

SUPPRESSION 50 mg.

RUN NO. 1 DATE 11/30/74

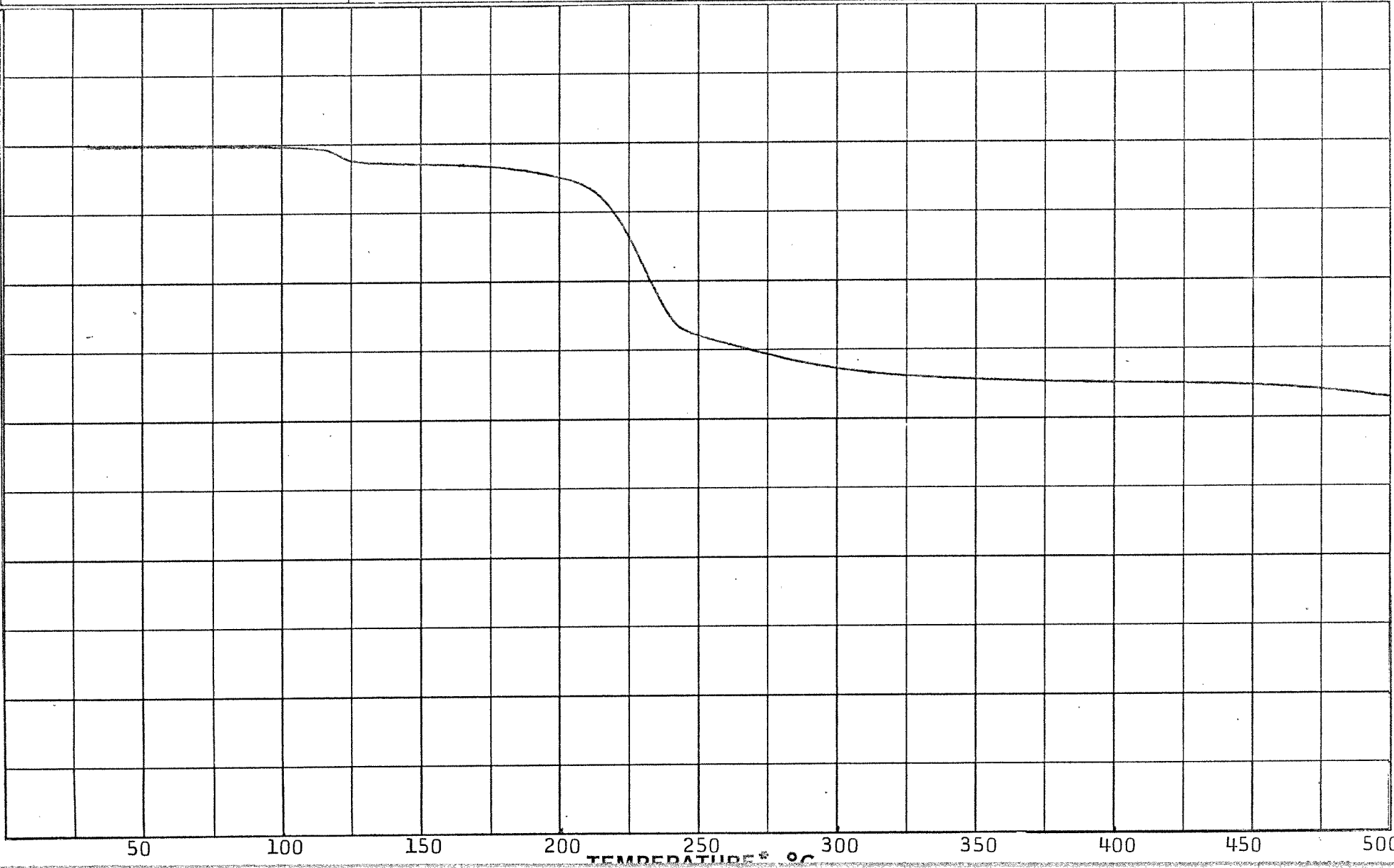
OPERATOR RM

HEATING RATE 10 °C / min.

ATM. self-generated

TIME CONSTANT 1 sec.

39  
100  
80  
60  
40  
20



TEMPERATURE °C





SAMPLE: Std #11  
100% MgSO<sub>3</sub>.3H<sub>2</sub>O

Fig. No. 19

SIZE 14 mg.

X-AXIS

TEMP. SCALE 50 °C  
inch

SHIFT 0 inch

TIME SCALE (ALT.)

Y-AXIS

SCALE 2 mg.  
inch  
(SCALE SETTING X 2)

SUPPRESSION 50 mg.

RUN NO. 1 DATE 12/1/74

OPERATOR RM

HEATING RATE 10 °C  
min.

ATM. self-generated

TIME CONSTANT 1 sec.

40

100

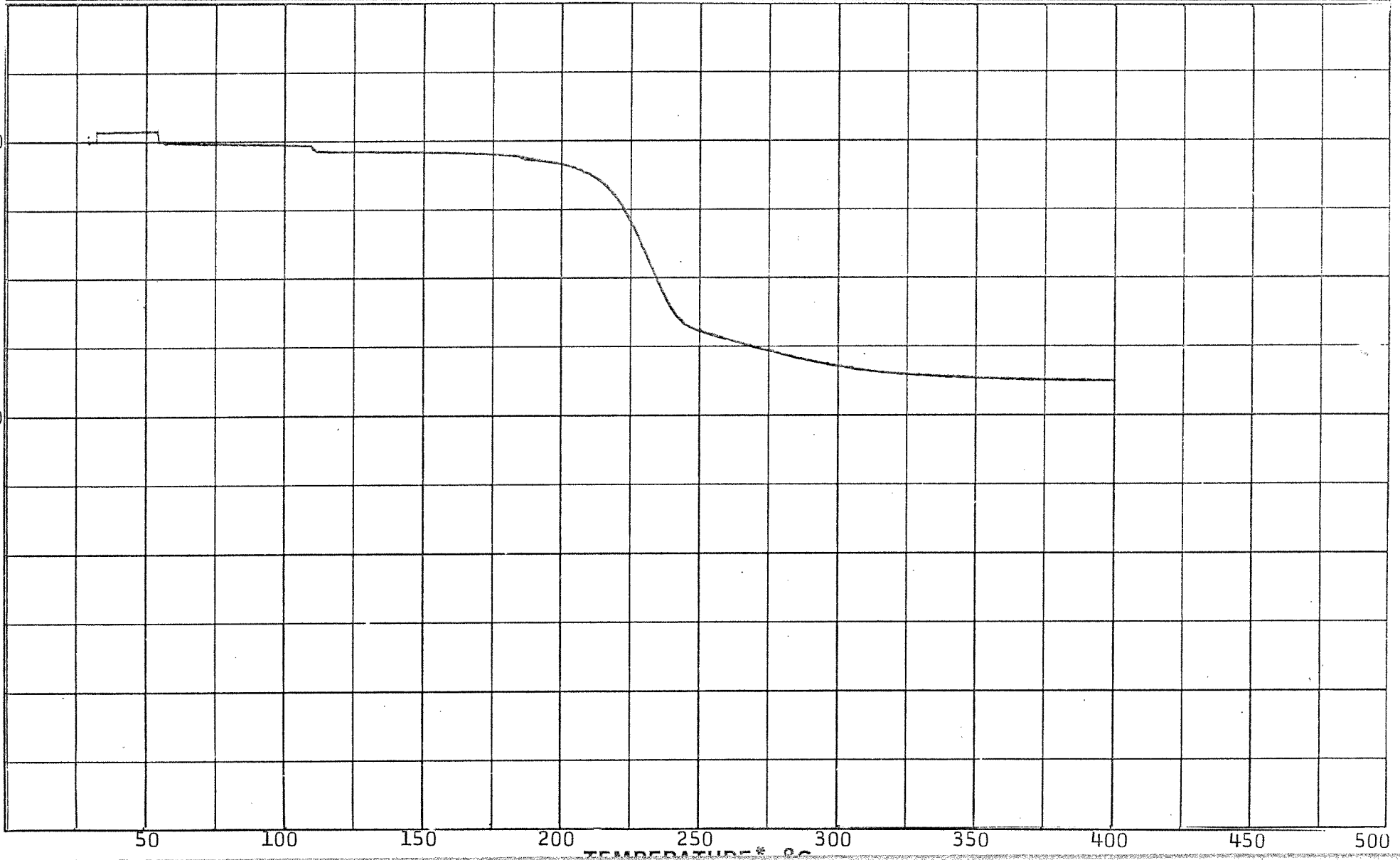
80

% WEIGHT, mg.

60

40

20



50

100

150

200

250

300

350

400

450

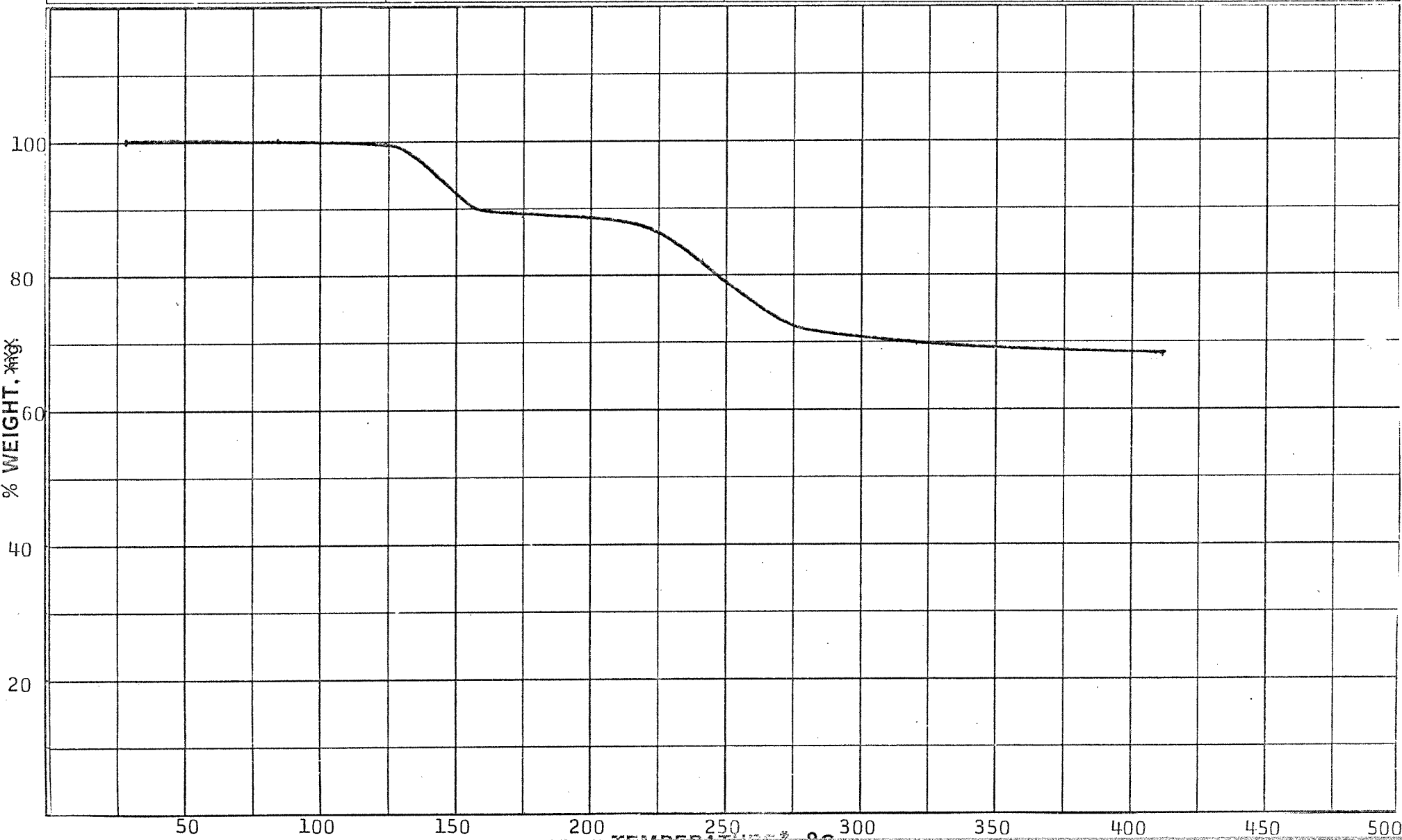
500

TEMPERATURE °C



41

<p><b>SAMPLE:</b> A mixture of:          44.3% <math>MgSO_3 \cdot 6H_2O</math>          30.0% <math>MgSO_3 \cdot 3H_2O</math>          25.7% glass beads          Fig. No. 20          SIZE 15 mg.</p>	<b>X-AXIS</b>		<b>Y-AXIS</b>		RUN NO. 1 DATE 12/1/74
	TEMP. SCALE	50 °C inch	SCALE	2 mg. inch	OPERATOR RM
	SHIFT	0 inch	(SCALE SETTING X 2)		HEATING RATE 10 °C min.
	TIME SCALE (ALT.)		SUPPRESSION	50 mg.	ATM. self-generated
					TIME CONSTANT 1 sec.



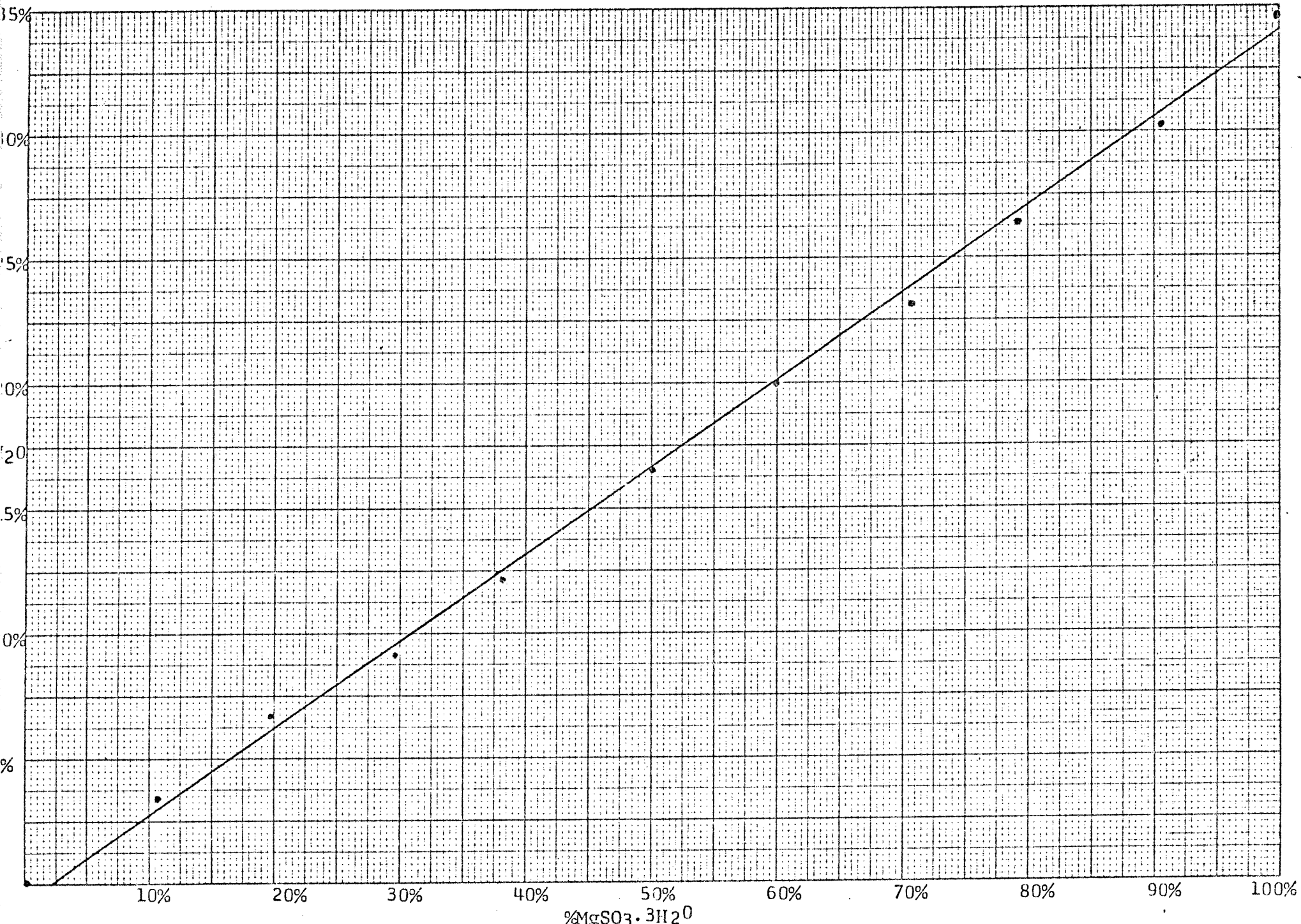
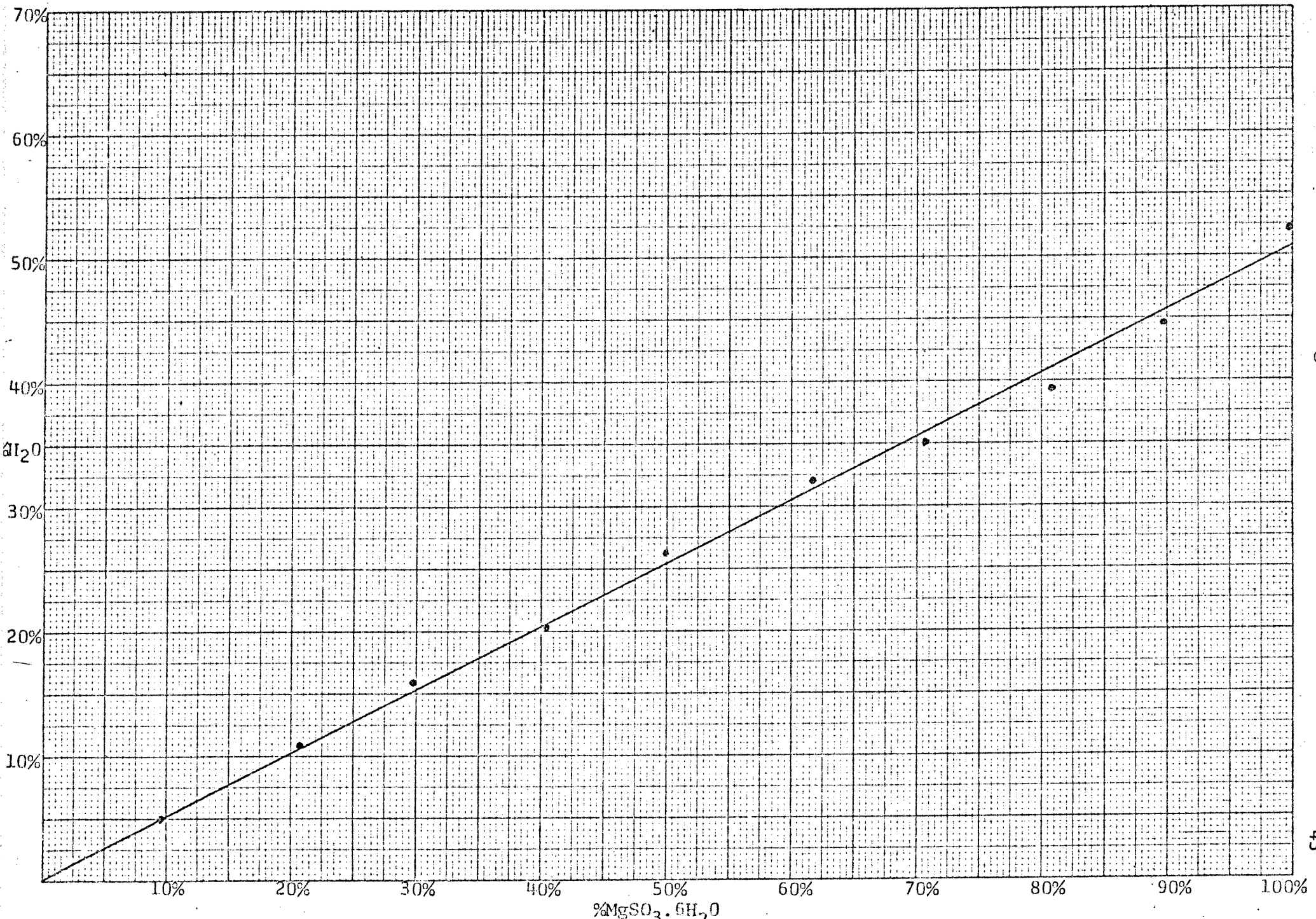


Fig. No. 21



18. IN. 27

43