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SIDEWISE FORCE EXERTED ON SLOWLY FALLING SPHERES  
INSIDE A CIRCULAR CYLINDER

BY

GARY MARK GREENSTEIN

A THESIS

PRESENTED IN PARTIAL FULFILLMENT OF  
THE REQUIREMENTS FOR THE DEGREE  
OF  
MASTER OF SCIENCE IN CHEMICAL ENGINEERING  
AT  
NEWARK COLLEGE OF ENGINEERING

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Newark, New Jersey

September, 1974

APPROVAL OF THESIS  
SIDEWISE FORCE EXERTED ON SLOWLY FALLING SPHERES  
INSIDE A CIRCULAR CYLINDER

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FOR

DEPARTMENT OF CHEMICAL ENGINEERING  
NEWARK COLLEGE OF ENGINEERING

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NEWARK, NEW JERSEY

SEPTEMBER, 1974

## ACKNOWLEDGEMENTS

I wish to thank the Exxon Research and Engineering Company for the use of its Computer Center in carrying out the numerical evaluations described in this work. I am also most grateful to Dr. T. Greenstein for his advice and constant support. I would also like to thank my devoted wife, Joan, for her patience and encouragement, and for typing this manuscript.

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## ABSTRACT

Numerical values are provided for the forces that must be applied to a reference sphere to prevent its sidewise motion when two equal-sized spheres settle through a viscous liquid bounded by a cylindrical tube. These values are presented for two independent set of circumstances:

(1) - the spheres are translating but not rotating

(2) - the spheres are rotating but not translating

Forces have been calculated assuming various distances between the sphere centers and with the line of centers at various angles to the horizontal. The results are discussed for the case where the spheres are both translating and rotating and compared to previous theoretical predictions as well as experimental results.

## NOMENCLATURE

$a$	sphere radius
$b$	distance from sphere center to cylinder axis
$E(\eta, \beta)$	dimensionless eccentricity function defined by eq. (3.4)
$E(\psi, \beta)$	dimensionless eccentricity function defined by eq. (3.2)
$\vec{F}$	frictional force on particle
$\vec{F}_x$	component of frictional force on particle in sidewise (or radial) direction
$\vec{F}_z$	component of frictional force on particle in z-direction
$\vec{i}, \vec{j}, \vec{k}$	Cartesian unit vectors
$l(\eta, \beta)$	dimensionless eccentricity function defined in Section 3
$l(\psi, \beta)$	dimensionless eccentricity function defined in Section 3
$N(\eta, \beta)$	dimensionless eccentricity function defined by eq. (4.4)
$N(\psi, \beta)$	dimensionless eccentricity function defined by eq. (4.2)
$n(\eta, \beta)$	dimensionless eccentricity function defined in Section 4
$n(\psi, \beta)$	dimensionless eccentricity function defined in Section
$p$	dynamic pressure
$r$	distance between sphere centers when the angle between the line joining their centers and the horizontal is other than $90^\circ$
$R_0$	radius of circular cylinder
$\vec{U}, U$	translational velocity and speed, respectively, of sphere center relative to cylinder wall
$\vec{V}$	local fluid velocity
$x, y, z$	rectangular Cartesian coordinates
$z_1$	vertical distance between the sphere centers when the angle between the line joining their centers and the horizontal is $90^\circ$

- $\beta$  dimensionless eccentricity,  $b/R_0$
- $\epsilon$  angle from the vertical of the path of the spheres
- $\eta$  dimensionless distance between spheres when the angle between the line joining their centers and the horizontal is  $90^\circ$ ,  $z_1/R_0$
- $\mu$  fluid viscosity
- $\psi$  angle between line joining the sphere centers and the horizontal
- $\vec{\Omega} = \hat{i}\Omega_1 + \hat{j}\Omega_2 + \hat{k}\Omega_3$  angular particle velocity

#### SUPERSCRIPTS

11S<sub>1</sub>, 12C, 13S<sub>1</sub>, 23S<sub>1</sub>, 21S<sub>2</sub>, 22C, 22S<sub>1</sub> definition follows in Section 2; see also figure 3

## 1. INTRODUCTION

Prediction of the frictional force in a radial direction on one of two identical particles settling at small Reynolds numbers through a bounded, quiescent, viscous fluid finds application in the fields of rheology and biomedical engineering. Early work by Smoluchowski<sup>(1)</sup> identified the radial migration effect when two spheres fall in a viscous fluid by utilizing the "method of reflections", but assuming an unbounded medium. The "method of reflections" has been described in detail by Happel and Brenner<sup>(2)</sup>.

A recent investigation by Greenstein and Happel<sup>(3)</sup> broadened Smoluchowski's work by including wall effects in analyzing the two-sphere problem using the "method of reflections". The latter study, however, was primarily concerned with the frictional forces on the two spheres in their direction of motion. Numerical values for the sidewise forces were not given in their work.

In this work, we have concentrated solely on the frictional forces in the sidewise or radial direction. We have used the "method of reflections" and included wall effects to evaluate numerically the analytical expressions for these sidewise forces.

## 2. DESCRIPTION OF THE PROBLEM

Let us consider the slow translation or rotation of two equally sized spherical particles in a viscous incompressible fluid confined within an infinitely long circular cylindrical tube. Two independent sets of circumstances were investigated:

(1) the spheres move with arbitrary constant translational velocity ( $\vec{U} = -\vec{k}U$ ) but do not rotate.

(2) the spheres rotate with arbitrary constant angular velocity ( $\vec{\Omega} = j\Omega_2$ ) but do not translate.

Figures 1 and 2 illustrate the geometric configurations studied. In Figure 1, the spheres are situated at an angle  $\psi$  between the line of centers and the horizontal. The radius of each sphere is  $a$ , the cylinder radius is  $R_0$ , and the centers of Sphere-1 and Sphere-2 are situated at distances  $b$  from the cylinder axis. The distance between the centers of Spheres 1 and 2 is  $r$ .

In Figure 2, the spheres are located in the same vertical plane and the sphere centers are displaced from the cylindrical axis by a distance  $b$ . Again, the radius of each sphere is  $a$  and the cylinder radius is  $R_0$ . The spheres are separated by a vertical distance,  $z_1$ .

If we consider only translation, we say that the center of each sphere translates with velocity  $\vec{U}$  relative to the cylinder wall in the negative  $z$  direction, parallel to the cylinder axis ( $\vec{U} = -\vec{k}U$ ). If we consider only rotation, we say that each sphere rotates with angular velocity  $\vec{\Omega}$  relative to the cylinder wall about axes parallel to the  $y$ -coordinate axis ( $\vec{\Omega} = j\Omega_2$ ). In both cases, at  $|z| = \infty$ , the fluid is at rest.

The translation and rotation problems can be solved

independently, assuming that the fluid motion is governed by the creeping motion and continuity equations:

$$\mu \nabla^2 \vec{V} = \nabla p \quad (2.1)$$

$$\nabla \cdot \vec{V} = 0 \quad (2.2)$$

where  $\vec{V}$  is the fluid velocity with respect to a coordinate system that moves with Sphere-1,  $p$  is the dynamic pressure, and  $\mu$  the fluid viscosity. The boundary conditions necessary to solve these problems are:

- (1) at fluid -solid interfaces there is no relative motion
- (2) at  $|z| = \infty$  the fluid is at rest

Both of these boundary value problems can be solved by a technique of successive approximations known as the method of reflections (described by Happel and Brenner (2)). Figure 3 outlines a schematic representation of this calculation technique. An initial disturbance is reflected from the boundaries involved and produces smaller and smaller effects with each successive reflection.

The following superscript notation has been adopted to describe the velocity fields

$\vec{V}_{ijS_i}$  and  $\vec{V}_{ijC}$  (3) :

$i$  = the sphere at which a disturbance originates

$j$  = the number of times that reflections have occurred to produce this disturbance

$S_1$  = the latest disturbance reflected from Sphere-1

$S_2$  = the latest disturbance reflected from Sphere-2

$C$  = the latest disturbance produced by the cylinder wall

As shown in Figure 3, Sphere-2 will disturb the motion of Sphere-1 in two ways:

- 1) by a direct reflection of its own Stokes field,  $\vec{V}_{21S_2}$

2) by the reflection of this field from the cylinder wall  
and then to Sphere-1,  $\vec{V}^{22C}$

Since the equations of motion and boundary conditions are linear, the frictional force  $\vec{F}_{II}$  exerted on the reference sphere (Sphere-1) is obtained by adding the frictional forces resulting from each of the individual fields. Hence,

$$\vec{F}_{II} = \vec{F}^{11S_1} + \vec{F}^{13S_1} + \vec{F}^{22S_1} + \vec{F}^{23S_1} + \dots$$

where  $\vec{F}^{iJS_1}$  is the frictional force associated with the field  $\vec{V}^{iJS_1}$ . This work has considered only the component of  $\vec{F}_{II}$  in the radial direction perpendicular to the cylindrical axis, i.e.,  $\vec{F}_x$ .

### 3. RESULTS FOR THE SIDEWISE FORCE EXERTED ON ONE OF TWO SLOWLY TRANSLATING SPHERES INSIDE A CIRCULAR CYLINDER

If the spheres are only translating, let us consider the system shown in Figure 1. Two equally sized spheres situated at an angle  $\psi$  between the line of centers and the horizontal settle through a quiescent fluid in a direction parallel to the cylindrical axis. The frictional force in the radial direction  $\vec{F}_x^{23S1}$ , exerted by the fluid on the spheres, due to the wall-sphere interaction effect is given by

$$\vec{F}_x^{23S1} = 16\pi\mu aUE(\psi, \beta) \frac{a}{R_0} + O\left(\frac{a}{R_0}\right)^3 \quad (3.1)$$

where

$$E(\psi, \beta) = \frac{3}{2\pi} l(\psi, \beta) \quad (3.2)$$

and  $\psi$  is the angle between the line connecting the sphere centers and the horizontal, and  $\beta$  equals  $b/R_0$ .

If we consider the system shown in Figure 2, the two spheres are located in the same vertical plane, separated by a distance  $z_1$ , and displaced from the cylindrical axis by a given distance as they settle through a quiescent fluid in a direction parallel to the cylindrical axis. In this case, the frictional force in the radial direction  $\vec{F}_x^{23S1}$  due to the wall-sphere interaction effect is given by

$$\vec{F}_x^{23S1} = 16\pi\mu aUE(\eta, \beta) \frac{a}{R_0} + O\left(\frac{a}{R_0}\right)^3 \quad (3.3)$$

where

$$E(\eta, \beta) = \frac{3}{2\pi} l(\eta, \beta) \quad (3.4)$$

and  $\eta = z_1/R_0$ , and  $\beta = b/R_0$

Note that the functions  $l(\psi, \beta)$  and  $l(\eta, \beta)$ , as well as  $E(\psi, \beta)$  and  $E(\eta, \beta)$ , are comparable and differ only in the manner in which the first parameter is expressed. The first parameter is necessary to fully define the location of the spheres.



A detailed expression for  $l(\psi, \beta)$  or  $l(\eta, \beta)$  was derived based upon Greenstein's<sup>(4)</sup> expression for the  $\vec{V}^{22C}$  velocity field.  $l(\psi, \beta)$  or  $l(\eta, \beta)$  was found to be a complicated function of  $(\psi, \beta)$  or  $(\eta, \beta)$  involving modified Bessel functions of the first and second kind and requiring numerical evaluation. A high speed computer was employed to accomplish this numerical evaluation and the program is shown in Appendix 1.

Values of  $E(\psi, \beta)$  and  $l(\psi, \beta)$  vs.  $\beta$  are tabulated in Table 1 for values of  $\psi$  equal to  $30^\circ$ ,  $45^\circ$ , and  $60^\circ$ . Similarly, values of  $E(\eta, \beta)$  and  $l(\eta, \beta)$  vs.  $\beta$  are tabulated in Table 2 for values on  $\eta$  ranging from 0.00001 to 20.

Based on previous work by Greenstein<sup>(4)</sup>, it can be shown that, if the spheres are translating parallel to the cylinder axis only:

$$\vec{F}_x^{11S1} = \vec{F}_x^{13S1} = \vec{0} \quad (3.5)$$

$\vec{F}_x^{22S1}$  is also equal to  $\vec{0}$  for the system shown in Figure 2. However, for the system shown in Figure 1, it can be shown that:

$$\vec{F}_x^{22S1} = \vec{16\pi\mu a} \left( -\frac{3aU}{8b} \cos^2\psi \sin\psi \right) \quad (3.6)$$

This expression becomes for values of  $\psi = 30^\circ$ ,  $45^\circ$  and  $60^\circ$ :

$$\begin{array}{l} \psi \\ 30^\circ \quad \vec{F}_x^{22S1} = \vec{16\pi\mu a} \left( -0.140625 \frac{aU}{b} \right) \\ 45^\circ \quad \vec{F}_x^{22S1} = \vec{16\pi\mu a} \left( -0.132582 \frac{aU}{b} \right) \\ 60^\circ \quad \vec{F}_x^{22S1} = \vec{16\pi\mu a} \left( -0.0811898 \frac{aU}{b} \right) \end{array} \quad (3.7)$$

The total sidewise force exerted by the fluid on the reference sphere for the system described by Figure 1 can be computed as the sum of  $\vec{F}_x^{22S1}$  and  $\vec{F}_x^{23S1}$ :

$$\begin{aligned} \vec{F}_x &= \vec{F}_x^{22S1} + \vec{F}_x^{23S1} \\ &= \vec{16\pi\mu a} \left( -\frac{3}{8} \frac{aU}{b} \cos^2\psi \sin\psi + UE(\psi, \beta) \frac{a}{R_0} \right) + O\left(\frac{a}{R_0}\right)^3 \end{aligned} \quad (3.8)$$

Values of  $E(\psi, \beta)$  can be obtained from Table 1.

The total sidewise force exerted by the fluid on the reference sphere for the system shown in Figure 2 is  $\vec{F}_x^{23S1}$  (given by equation (3.3) ). Values of  $E(\eta, \beta)$  can be obtained from Table 2.

These sidewise forces cause radial migration when the spheres are freely suspended in the fluid. To prevent the spheres from moving sidewise, a force,  $-\vec{F}_x$ , equal in magnitude but opposite in direction to  $\vec{F}_x$  would have to be exerted on the spheres. Forces resulting from successive reflections have been neglected, since they are of the same order of magnitude as the error term (on the order of  $(\frac{a}{R_0})^3$  ).

4. RESULTS FOR THE SIDEWISE FORCE EXERTED ON ONE OF  
TWO SLOWLY ROTATING SPHERES INSIDE A CIRCULAR  
CYLINDER

Now let us again consider the system in Figure 1, but this time with the spheres only rotating. Two equally sized spheres situated at an angle  $\psi$  between the line of centers and the horizontal rotate but do not translate in a quiescent fluid. The frictional force in the radial direction  $\vec{F}_{x,r}^{23S_1}$  due to the wall-sphere interaction effect is given by

$$\vec{F}_{x,r}^{23S_1} = -18\pi\mu a^2\Omega_2\left(\frac{a}{R_0}\right)^2 N(\psi, \beta) + O\left(\frac{a}{R_0}\right)^4 \quad (4.1)$$

where

$$N(\psi, \beta) = \frac{3}{2\pi} n(\psi, \beta) \quad (4.2)$$

and  $\psi$  is the angle between the line connecting the sphere centers and the horizontal, and  $\beta$  equals  $b/R_0$ .

If we consider the system shown in Figure 2, the two spheres are located in the same vertical plane, separated by a given distance  $z_1$  and displaced from the cylindrical axis by a given distance as they rotate in the y-direction (but do not translate) in a quiescent fluid. The frictional force in the radial direction  $\vec{F}_{x,r}^{23S_1}$  due to the wall-sphere interaction effect can be expressed as

$$\vec{F}_{x,r}^{23S_1} = -18\pi\mu a^2\Omega_2\left(\frac{a}{R_0}\right)^2 N(\eta, \beta) + O\left(\frac{a}{R_0}\right)^4 \quad (4.3)$$

where

$$N(\eta, \beta) = \frac{3}{2\pi} n(\eta, \beta) \quad (4.4)$$

and  $\eta = z_1/R_0$ , and  $\beta = b/R_0$ .

The functions  $n(\psi, \beta)$  and  $n(\eta, \beta)$ , and similarly  $N(\psi, \beta)$  and  $N(\eta, \beta)$ , are directly comparable and differ only in the form of the first parameter necessary to define the location of the spheres.

A detailed expression for  $n(\psi, \beta)$  or  $n(\eta, \beta)$  was developed based upon Greenstein's<sup>(4)</sup> expression for the  $\vec{v}^{22C}$  velocity field.

As in the translation problem,  $n(\psi, \beta)$  or  $n(\eta, \beta)$  was determined to be a complicated function of  $(\psi, \beta)$  or  $(\eta, \beta)$  involving modified Bessel functions of the first and second kind. This function was evaluated on a high speed computer using numerical techniques and the program used is shown in Appendix 2.

Values of  $N(\psi, \beta)$  and  $n(\psi, \beta)$  vs.  $\beta$  are tabulated in Table 3 at values of  $\psi$  equal to  $30^\circ$ ,  $45^\circ$  and  $60^\circ$ . Values of  $N(\eta, \beta)$  and  $n(\eta, \beta)$  vs.  $\beta$  are tabulated in Table 4 for values of  $\eta$  ranging from 0.00001 to 20.

Based on previous work by Greenstein<sup>(4)</sup>, it can be shown that, if the spheres are rotating only:

$$\vec{F}_{x,11S_1} = \vec{F}_{x,13S_1} = \vec{0} \quad (4.5)$$

An expression for the values of  $\vec{F}_{x,r}^{22S_1}$  can also be derived from Greenstein's work. For the geometric system described in Figure 1, this expression is:

$$\vec{F}_{x,r}^{22S_1} = \vec{i} 16\pi\mu a \left( \frac{a^3 \Omega_2}{4b^2} \cos^2 \psi \sin \psi \right) \quad (4.6)$$

which, if evaluated at values of  $\psi = 30^\circ$ ,  $45^\circ$  and  $60^\circ$ , becomes:

$$\begin{aligned} \frac{\psi}{30^\circ} \quad \vec{F}_{x,r}^{22S_1} &= \vec{i} 16\pi\mu a \left( 0.09375 \frac{a^3 \Omega_2}{b^2} \right) \\ 45^\circ \quad \vec{F}_{x,r}^{22S_1} &= \vec{i} 16\pi\mu a \left( 0.0883883 \frac{a^3 \Omega_2}{b^2} \right) \\ 60^\circ \quad \vec{F}_{x,r}^{22S_1} &= \vec{i} 16\pi\mu a \left( 0.0541265 \frac{a^3 \Omega_2}{b^2} \right) \end{aligned} \quad (4.7)$$

A similar expression for the system shown in Figure 2 is:

$$\vec{F}_{x,r}^{22S_1} = \vec{i} 16\pi\mu a \left( \frac{a^3 \Omega_2}{z_1^2} \right) \quad (4.8)$$

indicating that this component of the sidewise force increases as the spheres are moved closer together.

The total sidewise force on a reference sphere for either of the geometries discussed is the sum of  $\vec{F}_{x,r}^{22S_1}$  and  $\vec{F}_{x,r}^{23S_1}$ .

Forces resulting from successive reflections have been neglected, since they are of the same order of magnitude as the error term (on the order of  $(\frac{a}{R_0})^4$ ).

## 5. QUALITATIVE DISCUSSION OF RESULTS WHEN SPHERES ARE TRANSLATING AND ROTATING

Let us examine in a qualitative manner the total sidewise force on one sphere when the spheres are translating and rotating. By comparing equation (3.1) with equation (4.1) and equation (3.3) with equation (4.3), it is clear that the value of  $\vec{F}_{x,r}^{23S_1}$  due to rotation is much smaller than the value of  $\vec{F}_x^{23S_1}$  due to translation. This is true because the value of  $a/R_0$  is quite small. As a matter of fact,  $\vec{F}_{x,r}^{23S_1}$  due to rotation is of the order of magnitude  $(\frac{a}{R_0})^2$ , whereas the order of magnitude of  $\vec{F}_x^{23S_1}$  due to translation is  $(\frac{a}{R_0})$ . Hence, when the spheres are translating and rotating, the value of  $\vec{F}_{x,r}^{23S_1}$  due to rotation can be neglected in computing the total sidewise force.

The  $\vec{F}_{x,r}^{22S_1}$  component of the sidewise force due to rotation however, cannot be neglected in computing the total sidewise force on the reference sphere when the spheres are translating and rotating. In particular, for the system shown in Figure 2, the value of  $\vec{F}_x^{22S_1}$  due to translation is zero, whereas the value of  $\vec{F}_{x,r}^{22S_1}$  due to rotation must be computed from equation (4.8). It should be noted, however, that the value of  $\vec{F}_{x,r}^{22S_1}$  computed from equation (4.8) is of the order of  $(\frac{a}{z_1})^2$  which is still an order of magnitude less than the value of  $\vec{F}_x^{23S_1}$  due to translation. For the system described by Figure 1, the value of  $\vec{F}_x^{22S_1}$  due to translation is of the order of  $(\frac{a}{b})$  whereas the value of  $\vec{F}_{x,r}^{22S_1}$  due to rotation is of the order of  $(\frac{a}{b})^2$ . Again, the sidewise component due to rotation is of a lower order of magnitude.

In summary, it can be shown that when two equally sized spheres situated at an angle  $\psi$  between the line of centers and the horizontal translate and rotate through a quiescent fluid, the sidewise force on the reference sphere is influenced much more strongly by the translation of the spheres than by the rotation of the spheres. This conclusion is based on a qualitative inspection of the orders of magnitude of the sidewise components of the frictional forces.

## 6. COMPARISON OF THEORY WITH OTHER THEORETICAL AND EXPERIMENTAL RESULTS

The problem of the motion of two spheres in an infinite medium was first investigated by Smoluchowski<sup>(1)(5)</sup>. In his work, Smoluchowski used the method of reflections but did not consider wall effects. In addition, the spheres were considered to be only translating. Based on expressions derived for the component of force tending to diminish the resistance in the direction of motion along the line connecting the centers of the two spheres, Smoluchowski developed the relationship

$$\sin \epsilon = \frac{3}{4} \frac{a}{r} \left(1 - \frac{3}{2} \frac{a}{r}\right) \cos \psi \sin \mu \quad (6.1)$$

for the angle  $\epsilon$  through which the spheres would be deflected from the vertical towards the line of centers. In other words, the spheres would exhibit motion in a radial direction as well as in a vertical direction.

By not considering wall effects, Smoluchowski only considered those components of the frictional force referred to in this paper as  $\vec{F}^{11S_1}$  and  $\vec{F}^{22S_1}$ . As shown in Figure 3, the other components of the frictional force on Sphere-1 result from wall-sphere interactions, which Smoluchowski did not consider. Equation (6.1) can be derived from Greenstein's<sup>(4)</sup> equation for the  $\vec{V}^{21S_2}$  velocity field by making a number of approximations. This derivation is shown in Appendix 3.

It should be noted that Smoluchowski would predict radial migration only for the system shown in Figure 1. For



the geometry in Figure 2, Smoluchowski's  $\epsilon$  would be zero. This is totally consistent with the derivation presented in Section 3 of this paper which states that  $\vec{F}_x^{11S_1} = \vec{0}$  in both cases and that  $\vec{F}_x^{22S_1}$  exists for the system shown in Figure 1 but is equal to  $\vec{0}$  for the system in Figure 2.

From the results presented in this paper, the total sidewise force ( $\vec{F}_x$ ) on the reference sphere can be calculated. This could be coupled with the appropriate value for the total vertical force ( $\vec{F}_z$ ) on the sphere based on Greenstein's(4) expressions to obtain an angle of deflection,  $\epsilon$ , which would include the effect of wall-sphere interactions. This would therefore extend Smoluchowski's work and result in more theoretically correct values of  $\epsilon$ .

Eveson, Hall and Ward(6) carried out a series of experiments to study the motion of two spheres settling through a quiescent fluid bounded by a circular cylinder. When the spheres were positioned as in Figure 1, it was found that the paths of the spheres were deflected from the vertical by a small angle. The experimental values for these angles were stated to be in agreement with Smoluchowski's relationship (equation (6.1)), although numerical values were not published.

Since the values of  $\epsilon$  tend to be quite small, the difference between equation (6.1) and the method proposed in this paper to obtain  $\epsilon$  may have been beyond the accuracy of Eveson, Hall and Ward's experiments. This would explain the statement that experimental values are in agreement with Smoluchowski's relationship. Nevertheless, the importance of Eveson, Hall and Ward's experiments was to demonstrate that

radial migration does occur when two spheres settle through a quiescent fluid bounded by a circular cylinder, as discussed in this paper.

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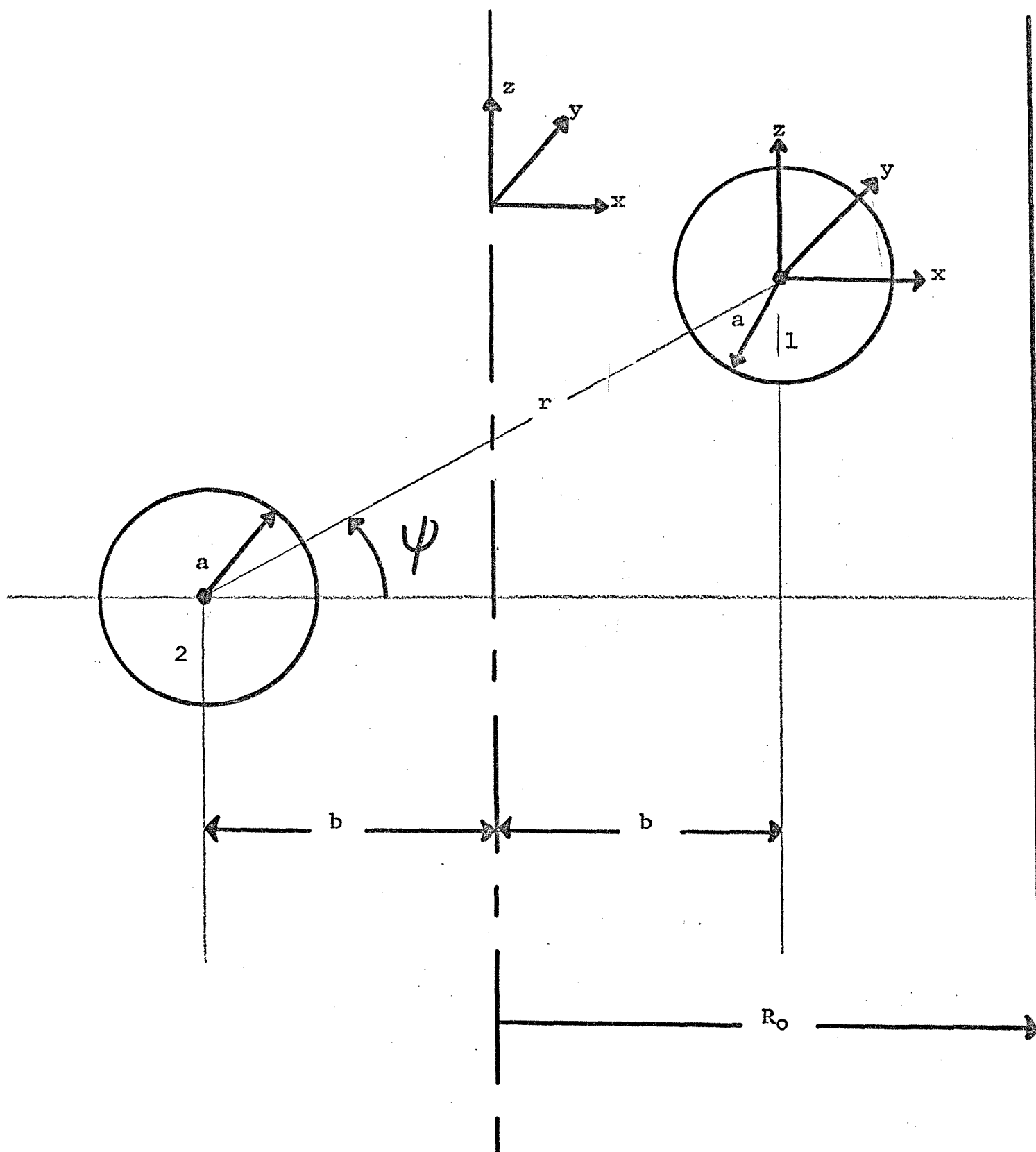


Figure 1 - Two spheres situated at an angle  $\psi$  between the line of centers and the horizontal

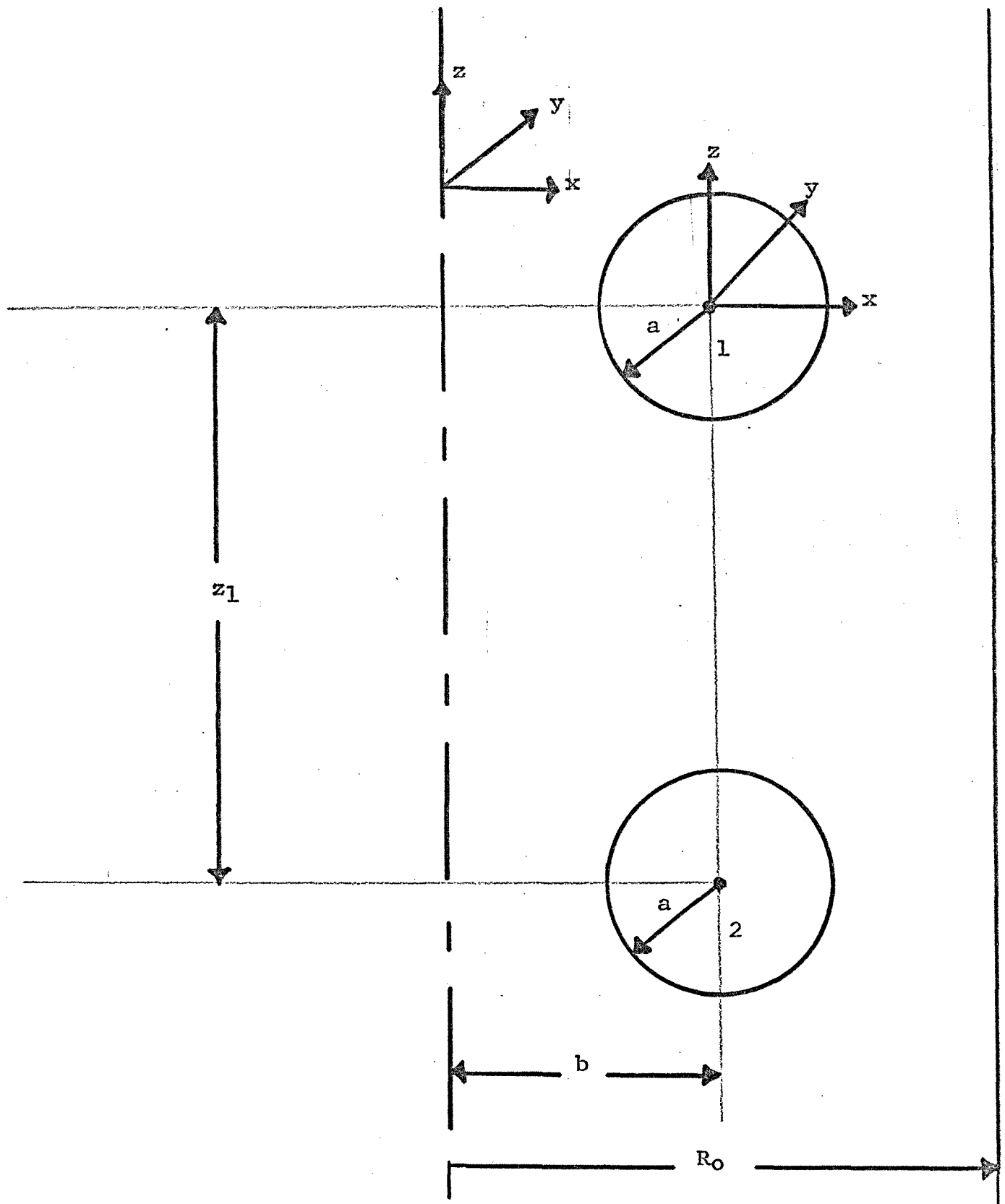


Figure 2 - Two spheres in same vertical plane and displaced from the axis of a circular cylinder by a given distance

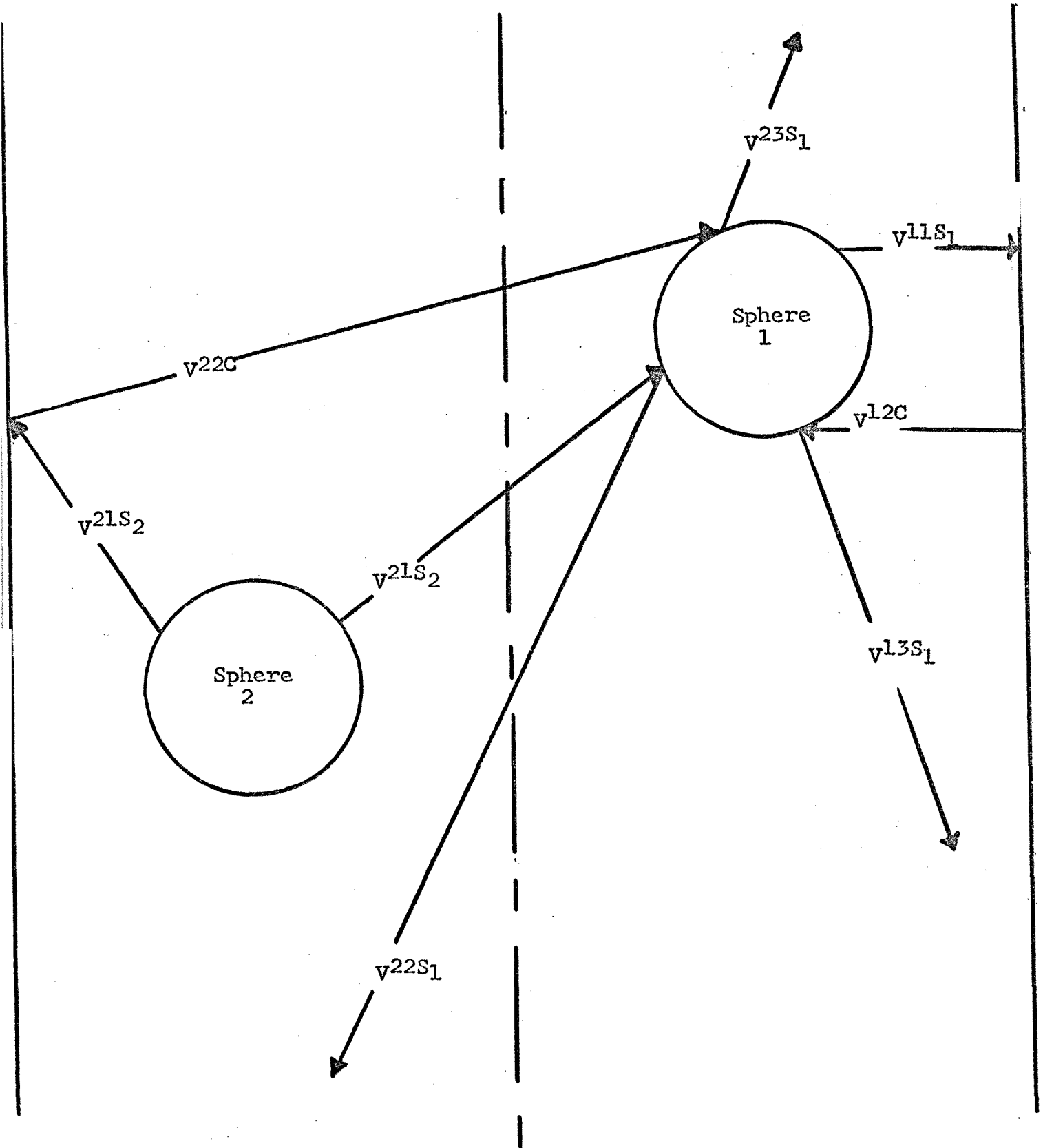


Figure 3 - Schematic representation of velocity fields

TABLE 1

 $I(\psi, \beta)$  AND  $E(\psi, \beta)$  VS.  $\beta$  FOR VARIOUS VALUES OF  $\psi$ 

<u><math>\beta</math></u>	<u><math>I(\psi=30^\circ, \beta)</math></u>	<u><math>E(\psi=30^\circ, \beta)</math></u>	<u><math>I(\psi=45^\circ, \beta)</math></u>	<u><math>E(\psi=45^\circ, \beta)</math></u>
0.05	-0.00229853	-0.00109747	-0.00397989	-0.00190026
0.10	-0.00928425	-0.00443290	-0.0160484	-0.00766256
0.15	-0.0211509	-0.0100988	-0.0363889	-0.0173744
0.20	-0.0381173	-0.0181997	-0.0649391	-0.0310061
0.25	-0.0602832	-0.0287831	-0.100969	-0.0482091
0.30	-0.0873666	-0.0417145	-0.142730	-0.0681484
0.35	-0.1186239	-0.0566387	-0.187597	-0.0895707
0.40	-0.153010	-0.0730568	-0.232452	-0.110988
0.45	-0.189158	-0.0903162	-0.273979	-0.130815
0.50	-0.224951	-0.107406	-0.309214	-0.147639
0.55	-0.258674	-0.123508	-0.336020	-0.160438
0.60	-0.288304	-0.137655	-0.353282	-0.168680
0.65	-0.312224	-0.149076	-0.360951	-0.172342
0.70	-0.329146	-0.157155	-0.360018	-0.171896
0.75	-0.338382	-0.161566	-0.352182	-0.168154
0.80	-0.339953	-0.162316	-0.339547	-0.162122
0.85	-0.334593	-0.159756	-0.369575	-0.176459

<u><math>\beta</math></u>	<u><math>I(\psi=60^\circ, \beta)</math></u>	<u><math>E(\psi=60^\circ, \beta)</math></u>
0.05	-0.00688600	-0.00328782
0.10	-0.0275898	-0.0131731
0.15	-0.0614273	-0.0293294
0.20	-0.105708	-0.0504716
0.25	-0.155181	-0.0740933
0.30	-0.203116	-0.0969805
0.35	-0.243321	-0.116177
0.40	-0.271718	-0.129736
0.45	-0.287007	-0.137035
0.50	-0.290352	-0.138633
0.55	-0.284464	-0.135822
0.60	-0.272576	-0.130146
0.65	-0.257639	-0.123013
0.70	-0.241873	-0.115486
0.75	-0.226672	-0.108228
0.80	-0.212713	-0.101563
0.85	-0.200199	-0.0955879

TABLE 2

1( $\eta, \beta$ ) AND E( $\eta, \beta$ ) VS.  $\beta$  FOR VARIOUS VALUES OF  $\eta$ 

<u><math>\beta</math></u>	<u><math>10^3 \times</math> <math>1(\eta=0.0001, \beta)</math></u>	<u><math>10^3 \times</math> <math>E(\eta=0.0001, \beta)</math></u>	<u><math>1(\eta=0.01, \beta)</math></u>	<u><math>E(\eta=0.01, \beta)</math></u>
0.01			-0.000396754	-0.000189436
0.1	-0.00401767	-0.00191830	-0.00401491	-0.00191698
0.2	-0.00834350	-0.00398373	-0.00833766	-0.00398094
0.3	-0.0133963	-0.00639626	-0.0133866	-0.00639164
0.4	-0.0198913	-0.00949738	-0.0198761	-0.00949015
0.5	-0.0292634	-0.0139723	-0.0292391	-0.0139607
0.6	-0.0449186	-0.0214470	-0.0448753	-0.0214264
0.7	-0.0766169	-0.0365819	-0.0765204	-0.0365358
0.8	-0.162935	-0.0777957	-0.162591	-0.0776315
0.85	-0.278494	-0.132971	-0.277579	-0.132534

<u><math>\beta</math></u>	<u><math>1(\eta=0.05, \beta)</math></u>	<u><math>E(\eta=0.05, \beta)</math></u>	<u><math>1(\eta=0.1, \beta)</math></u>	<u><math>E(\eta=0.1, \beta)</math></u>
0.01	-0.00197782	-0.000944339	-0.00391872	-0.00187105
0.1	-0.0200127	-0.00955535	-0.0396417	-0.0189275
0.2	-0.0415487	-0.0198380	-0.0822317	-0.0392628
0.3	-0.0666740	-0.0318345	-0.131745	-0.0629034
0.4	-0.0989042	-0.0472253	-0.194869	-0.0930429
0.5	-0.145253	-0.0693532	-0.284721	-0.135944
0.6	-0.222218	-0.106101	-0.431302	-0.205932
0.7	-0.376244	-0.179643	-0.714598	-0.341196
0.8	-0.783428	-0.374059	-1.40060	-0.668740
0.85	-1.30630	-0.623715	-2.15616	-1.02949

<u><math>\beta</math></u>	<u><math>1(\eta=0.2, \beta)</math></u>	<u><math>E(\eta=0.2, \beta)</math></u>	<u><math>1(\eta=0.4, \beta)</math></u>	<u><math>E(\eta=0.4, \beta)</math></u>
0.01	-0.00754993	-0.00360483	-0.0130292	-0.00622098
0.1	-0.0762977	-0.0364295	-0.131169	-0.0626287
0.2	-0.157749	-0.0753195	-0.267873	-0.127900
0.3	-0.251124	-0.119903	-0.416489	-0.198859
0.4	-0.367302	-0.175374	-0.584808	-0.279225
0.5	-0.526337	-0.251307	-0.781093	-0.372944
0.6	-0.767524	-0.366466	-1.00452	-0.479625
0.7	-1.17378	-0.560441	-1.20476	-0.575233
0.8	-1.86931	-0.892533	-1.14872	-0.548474
0.85	-2.25217	-1.07533	-0.876416	-0.418458



TABLE 2  
(cont.)

$\beta$	$I(\eta=0.6, \beta)$	$E(\eta=0.6, \beta)$	$I(\eta=0.8, \beta)$	$E(\eta=0.8, \beta)$
0.01	-0.0153857	-0.00734613	-0.0148619	-0.00709601
0.1	-0.154035	-0.0735461	-0.147828	-0.0705827
0.2	-0.308977	-0.147526	-0.290474	-0.138691
0.3	-0.464524	-0.221794	-0.420571	-0.200808
0.4	-0.616680	-0.294443	-0.525693	-0.251000
0.5	-0.751776	-0.358946	-0.584588	-0.279120
0.6	-0.832850	-0.397657	-0.565223	-0.269874
0.7	-0.780844	-0.372826	-0.436937	-0.208622
0.8	-0.502578	-0.239963	-0.219556	-0.104831
0.85	-0.297600	-0.142093	-0.114174	-0.0545139

$\beta$	$I(\eta=1.0, \beta)$	$E(\eta=1.0, \beta)$	$I(\eta=1.2, \beta)$	$E(\eta=1.2, \beta)$
0.01	-0.0125061	-0.00597122	-0.00947619	-0.00452454
0.1	-0.123574	-0.0590022	-0.0930529	-0.0444295
0.2	-0.237817	-0.113549	-0.175655	-0.0838689
0.3	-0.331828	-0.158436	-0.237019	-0.113168
0.4	-0.391901	-0.187119	-0.266462	-0.127226
0.5	-0.401882	-0.191884	-0.255590	-0.122035
0.6	-0.348185	-0.166246	-0.203542	-0.0971848
0.7	-0.234392	-0.111914	-0.124259	-0.0593294
0.8	-0.101027	-0.0482367	-0.0484453	-0.0231309
0.85	-0.0488484	-0.0233234	-0.0374640	-0.0178877

$\beta$	$I(\eta=1.4, \beta)$	$E(\eta=1.4, \beta)$	$I(\eta=1.6, \beta)$	$E(\eta=1.6, \beta)$
0.01	-0.00659991	-0.00315122	-0.00428087	-0.00204396
0.1	-0.0644487	-0.0307720	-0.0416026	-0.0198638
0.2	-0.119604	-0.0571067	-0.0760840	-0.0363274
0.3	-0.156798	-0.0748654	-0.0973271	-0.0464702
0.4	-0.169142	-0.0807594	-0.101455	-0.0484413
0.5	-0.153770	-0.0734195	-0.0883161	-0.0421678
0.6	-0.114801	-0.0548135	-0.0626521	-0.0299142
0.7	-0.0652537	-0.0311563	-0.0336713	-0.0160768
0.8	-0.0236983	-0.0113151	-0.0115458	-0.00551271
0.85	-0.0216344	-0.0103297	-0.00502704	-0.00240023

TABLE 2  
(cont.)

$\beta$	$1(\eta=2.0, \beta)$	$E(\eta=2.0, \beta)$	$1(\eta=2.5, \beta)$	$E(\eta=2.5, \beta)$
0.01	-0.00149058	-0.000711700	-0.000265598	-0.000126814
0.1	-0.0143710	-0.00686162	-0.00253374	-0.00120977
0.2	-0.0256571	-0.0122503	-0.00437855	-0.00209060
0.3	-0.0315330	-0.0150559	-0.00508548	-0.00242814
0.4	-0.0310896	-0.0148442	-0.00460517	-0.00219881
0.5	-0.0252129	-0.0120383	-0.00329796	-0.00157466
0.6	-0.0164206	-0.00784026	-0.00177841	-0.000849129
0.7	-0.00797553	-0.00380804	-0.000620513	-0.000296273
0.8	-0.00241961	-0.00115531	-0.0000800211	-0.0000382073

$\beta$	$10^3x$ $1(\eta=3.0, \beta)$	$10^3x$ $E(\eta=3.0, \beta)$	$10^3x$ $1(\eta=3.5, \beta)$	$10^3x$ $E(\eta=3.5, \beta)$
0.01	-0.00769027	-0.00367183	-0.0168686	-0.00805417
0.1	-0.0645746	-0.0308321	-0.164753	-0.0786638
0.2	-0.0631400	-0.0301471	-0.305920	-0.146066
0.3	-0.0295674	-0.0141174	-0.400714	-0.191327
0.4	-0.180887	-0.0863674	-0.431750	-0.206146
0.5	-0.313453	-0.149663	-0.393039	-0.187662
0.6	-0.352302	-0.168212	-0.296252	-0.141450
0.7	-0.273958	-0.130806	-0.173153	-0.0826745
0.8	-0.132197	-0.0631196	-0.0666206	-0.0318090

$\beta$	$10^3x$ $1(\eta=4.0, \beta)$	$10^3x$ $E(\eta=4.0, \beta)$	$10^6x$ $1(\eta=8.0, \beta)$	$10^6x$ $E(\eta=8.0, \beta)$
0.01	-0.00848402	-0.00405082	-0.000486454	-0.000232265
0.1	-0.0820588	-0.0391802	-0.00118708	-0.000566790
0.2	-0.147932	-0.0706325	-0.000945605	-0.000451493
0.3	-0.185286	-0.0884676	-0.00617888	-0.00295020
0.4	-0.188229	-0.0898728	-0.000446258	-0.000213073
0.5	-0.159769	-0.0762842	-0.00162187	-0.000774384
0.6	-0.112096	-0.0535220	-0.00355178	-0.00169585
0.7	-0.0604338	-0.0288550	-0.00434382	-0.00207402
0.8	-0.0216215	-0.0103235	-0.0206333	-0.00985169

$\beta$	$10^6x$ $1(\eta=20, \beta)$	$10^6x$ $E(\eta=20, \beta)$
0.01	-0.0000990008	-0.0000472694
0.1	-0.000923821	-0.000441092
0.2	-0.00146969	-0.000701723
0.3	-0.00362426	-0.00173046
0.4	-0.00348456	-0.00166375
0.5	-0.00690809	-0.00329837
0.6	-0.00641325	-0.00306210
0.7	-0.0115289	-0.00550462
0.8	-0.00121437	-0.000579818

TABLE 3

 $n(\psi, \beta)$  AND  $N(\psi, \beta)$  VS.  $\beta$  FOR VARIOUS VALUES OF  $\eta$ 

<u><math>\beta</math></u>	<u><math>n(\psi=30^\circ, \beta)</math></u>	<u><math>N(\psi=30^\circ, \beta)</math></u>	<u><math>n(\psi=45^\circ, \beta)</math></u>	<u><math>N(\psi=45^\circ, \beta)</math></u>	<u><math>n(\psi=60^\circ, \beta)</math></u>	<u><math>N(\psi=60^\circ, \beta)</math></u>
0.05	0.202471	0.0966727	0.348894	0.166584	0.595091	0.284135
0.10	0.408763	0.195170	0.693459	0.331102	1.12953	0.539308
0.15	0.622293	0.297123	1.02791	0.490792	1.55069	0.740399
0.20	0.845613	0.403750	1.34385	0.641641	1.82234	0.870102
0.25	1.08034	0.515825	1.63037	0.778445	1.93221	0.922561
0.30	1.32699	0.633591	1.87459	0.895049	1.89340	0.904032
0.35	1.58413	0.756365	2.06234	0.984693	1.73975	0.830670
0.40	1.84802	0.882365	2.18116	1.04143	1.51550	0.723601
0.45	2.11408	1.00940	2.22273	1.06127	1.26412	0.603572
0.50	2.37177	1.11324	2.18438	1.04297	1.01997	0.486998
0.55	2.60902	1.24572	2.07126	0.988952	0.804948	0.384334
0.60	2.80744	1.34045	1.89557	0.905066	0.629114	0.300380
0.65	2.94702	1.40710	1.67505	0.799776	0.493532	0.235644
0.70	3.00770	1.43607	1.42992	0.682737	0.393672	0.187965
0.75	2.97364	1.41981	1.17982	0.563323	0.322461	0.153964
0.80	2.83966	1.35584	0.941555	0.449559	0.272430	0.130076
0.85	2.61165	1.24697	0.727704	0.347453	0.236986	0.113153

TABLE 4

$n(\eta, \beta)$  AND  $N(\eta, \beta)$  VS.  $\beta$  FOR VARIOUS VALUES OF  $\eta$

<u><math>\beta</math></u>	$10^3 \times$ <u><math>n(\eta=0.0001, \beta)</math></u>	$10^3 \times$ <u><math>N(\eta=0.0001, \beta)</math></u>	<u><math>n(\eta=0.01, \beta)</math></u>	<u><math>N(\eta=0.01, \beta)</math></u>
0.1	-0.0380197	-0.0181531	-0.0379953	-0.0181414
0.2	-0.0482421	-0.0230339	-0.0482104	-0.0230188
0.3	-0.0697369	-0.0332969	-0.0696893	-0.0332742
0.4	-0.113109	-0.0540056	-0.113027	-0.0539666
0.5	-0.207279	-0.0989686	-0.207116	-0.0988907
0.6	-0.446028	-0.212963	-0.445624	-0.212699
0.7	-1.23239	-0.588422	-1.23096	-0.587740
0.8	-5.38621	-2.57173	-5.37607	-2.56688
0.85	-15.7216	-7.50649	-15.6763	-7.48486

<u><math>\beta</math></u>	<u><math>n(\eta=0.05, \beta)</math></u>	<u><math>N(\eta=0.05, \beta)</math></u>	<u><math>n(\eta=0.1, \beta)</math></u>	<u><math>N(\eta=0.1, \beta)</math></u>
0.1	-0.189603	-0.0905286	-0.376882	-0.179948
0.2	-0.240489	-0.114825	-0.477484	-0.227982
0.3	-0.347420	-0.165881	-0.688482	-0.328726
0.4	-0.562942	-0.268785	-1.11232	-0.531093
0.5	-1.02997	-0.491775	-2.02544	-0.967077
0.6	-2.20982	-1.05511	-4.30795	-2.05689
0.7	-6.06717	-2.89686	-11.6098	-5.54323
0.8	-26.0465	-12.4363	-47.4312	-22.6467
0.85	-74.1781	-35.4174	-126.007	-60.1640

<u><math>\beta</math></u>	<u><math>n(\eta=0.2, \beta)</math></u>	<u><math>N(\eta=0.2, \beta)</math></u>	<u><math>n(\eta=0.4, \beta)</math></u>	<u><math>N(\eta=0.4, \beta)</math></u>
0.1	-0.735556	-0.351202	-1.33664	-0.638200
0.2	-0.927698	-0.442943	-1.65732	-0.791313
0.3	-1.32768	-0.633921	-2.30645	-1.10125
0.4	-2.12057	-1.01250	-3.53213	-1.68647
0.5	-3.79065	-1.80990	-5.91249	-2.82300
0.6	-7.79962	-3.72404	-10.8854	-5.19737
0.7	-19.6231	-9.36934	-22.2343	-10.6161
0.8	-67.1287	-32.0516	-49.3058	-23.5418
0.85	-145.065	-69.2633	-72.5444	-34.6374

TABLE 4  
(cont.)

$\beta$	$n(\eta=0.6, \beta)$	$N(\eta=0.6, \beta)$	$n(\eta=0.8, \beta)$	$N(\eta=0.8, \beta)$	$n(\eta=1.0, \beta)$	$N(\eta=1.0, \beta)$
0.1	-1.72009	-0.821282	-1.87375	-0.894649	-1.84040	-0.878724
0.2	-2.07976	-0.993013	-2.19939	-1.05013	-2.09488	-1.00023
0.3	-2.77897	-1.32686	-2.80357	-1.33860	-2.54516	-1.21522
0.4	-4.01145	-1.91532	-3.78998	-1.80958	-3.22609	-1.54034
0.5	-6.15745	-2.93996	-5.31759	-2.53896	-4.16849	-1.99031
0.6	-9.92209	-4.73745	-7.57105	-3.61491	-5.35452	-2.55660
0.7	-16.4018	-7.83127	-10.5831	-5.05305	-6.61903	-3.16035
0.8	-26.1424	-12.4821	-13.6925	-6.53769	-7.51153	-3.58649
0.85	-31.1948	-14.8944	-14.6842	-7.01120	-7.59212	-3.62497

$\beta$	$n(\eta=1.2, \beta)$	$N(\eta=1.2, \beta)$	$n(\eta=1.4, \beta)$	$N(\eta=1.4, \beta)$	$n(\eta=1.6, \beta)$	$N(\eta=1.6, \beta)$
0.1	-1.68612	-0.805064	-1.47360	-0.703590	-1.24898	-0.596346
0.2	-1.86398	-0.889985	-1.58706	-0.757767	-1.31568	-0.628190
0.3	-2.16468	-1.03356	-1.77082	-0.845506	-1.41926	-0.677645
0.4	-2.58768	-1.23552	-2.01222	-0.960766	-1.54631	-0.738306
0.5	-3.11486	-1.48724	-2.28406	-1.09056	-1.67440	-0.799467
0.6	-3.68642	-1.76014	-2.53589	-1.21080	-1.77065	-0.845424
0.7	-4.16918	-1.99064	-2.68917	-1.28398	-1.79377	-0.856460
0.8	-4.34316	-2.07370	-2.64677	-1.26374	-1.70306	-0.813153
0.85	-4.23562	-2.02236	-2.52540	-1.20579	-1.60689	-0.767233

$\beta$	$n(\eta=2.0, \beta)$	$N(\eta=2.0, \beta)$
0.1	-0.859034	-0.410158
0.2	-0.876634	-0.418562
0.3	-0.901297	-0.430338
0.4	-0.926101	-0.442181
0.5	-0.941909	-0.449728
0.6	-0.938415	-0.448060
0.7	-0.906276	-0.432715
0.8	-0.840154	-0.401144
0.85	-0.794591	-0.379389

TABLE 4  
(cont.)

<u><math>\beta</math></u>	<u><math>n(\eta=2.5, \beta)</math></u>	<u><math>N(\eta=2.5, \beta)</math></u>	<u><math>n(\eta=3.0, \beta)</math></u>	<u><math>N(\eta=3.0, \beta)</math></u>
0.1	-0.539317	-0.257505	-0.360533	-0.172142
0.2	-0.539883	-0.257775	-0.359113	-0.171464
0.3	-0.539550	-0.257616	-0.356560	-0.170245
0.4	-0.536645	-0.256229	-0.352671	-0.168388
0.5	-0.529326	-0.252734	-0.347304	-0.165825
0.6	-0.516047	-0.246394	-0.340477	-0.162566
0.7	-0.496125	-0.236882	-0.332475	-0.158745
0.8	-0.470220	-0.224513	-0.323896	-0.154649
0.85	-0.455688	-0.217575	-0.319655	-0.152624

<u><math>\beta</math></u>	<u><math>n(\eta=3.5, \beta)</math></u>	<u><math>N(\eta=3.5, \beta)</math></u>	<u><math>n(\eta=4.0, \beta)</math></u>	<u><math>N(\eta=4.0, \beta)</math></u>
0.1	-0.259014	-0.123670	-0.196586	-0.0939108
0.2	-0.258116	-0.123241	-0.196255	-0.0937047
0.3	-0.256634	-0.122534	-0.195558	-0.0933720
0.4	-0.254609	-0.121567	-0.194633	-0.0929305
0.5	-0.252117	-0.120377	-0.193530	-0.0924035
0.6	-0.249285	-0.119025	-0.192309	-0.0918208
0.7	-0.246296	-0.117598	-0.191041	-0.0912154
0.8	-0.243380	-0.116206	-0.189795	-0.0906206
0.85	-0.242030	-0.115561	-0.189200	-0.0903361

<u><math>\beta</math></u>	<u><math>n(\eta=8.0, \beta)</math></u>	<u><math>N(\eta=8.0, \beta)</math></u>	<u><math>n(\eta=20, \beta)</math></u>	<u><math>N(\eta=20, \beta)</math></u>
0.1	-0.0491615	-0.0234729	-0.00785602	-0.00375097
0.2	-0.0491443	-0.0234647	-0.00785557	-0.00375076
0.3	-0.0491157	-0.0234510	-0.00785485	-0.00375041
0.4	-0.0490758	-0.0234320	-0.00785381	-0.00374992
0.5	-0.0490251	-0.0234077	-0.00785250	-0.00374929
0.6	-0.0489633	-0.0233782	-0.00785089	-0.00374852
0.7	-0.0488908	-0.0233436	-0.00784897	-0.00374761
0.8	-0.0488083	-0.0233042	-0.00784676	-0.00374655
0.85	-0.0487623	-0.0232823	-0.00784571	-0.00374605

C	MAIN PROGRAM	TG 0002
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
	READ (5,1111) MAXJ, MAXN, JUNCT, PMAX, DELPO, TESTI,	TG 0003
	1TESTS	TG 0004
1111	FORMAT(I2, 3X,I2, 2X, I1, 9X, 4F10.8)	TG 0005
	READ (5,33) NN	TG 0006
33	FORMAT(I5)	TG 0007
	DO 2222 I=1,NN	TG 0008
	READ (5,200) XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ	TG 0009
200	FORMAT(6F10.9)	TG 0010
2222	V=CVBL(XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ, MAXJ, PMAX,	TG 0011
	DELPO, MAXN, TESTI, TESTS, JUNCT)	TG 0012
1024	STOP	TG 0013
	END	TG 0014
C	PROGRAM COMPUTES FBESI	TG 0015
	FUNCTION FBESI(N,X)	TG 0016
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
	PSUM = 1.0	TG 0017
	TEMP1 = 1.0	TG 0018
	TEMP2 = 1.0	TG 0019
	TEMP3 = 1.0	TG 0020
	K = 0	TG 0021
1	K=K+1	TG 0022
	TEMP1 = TEMP1 + ((0.5 * X)**2)	TG 0023
	PK=K	TG 0024
	TEMP2 = TEMP2 * PK	TG 0025
	AK = N + K	TG 0026
	TEMP3 = TEMP3 * AK	TG 0027
	TERM = TEMP1 / (TEMP2 * TEMP3)	TG 0028
	RATIO = TERM/PSUM	TG 0029
	DIF = RATIO - .1D-09	DP 0030
	PSUM = PSUM + TERM	TG 0031
	IF (DIF) 2,2,1	TG 0032
2	FBESI = PSUM	TG 0033
	RETURN	TG 0034
	END	TG 0035
C	PROGRAM COMPUTES FBESK	TG 0036
	FUNCTION FBESK(N,X)	TG 0037
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
	PSUM=1.0	TG 0038
	TEMP1=1.0	TG 0039
	TEMP2 = 1.0	TG 0040
	TEMP3 = 1.0	TG 0041
	TEMP4=1.0	TG 0042
	K=0	TG 0043
1	K= K + 1	TG 0044
	TEMP1 = TEMP1*((0.5*X)**2)	TG 0045
	PK=K	TG 0046
	TEMP2 = TEMP2 * PK	TG 0047
	BK=N-K	TG 0048
	TEMP3 = TEMP3 * BK	TG 0049
	TEMP4 = -TEMP4	TG 0050
	TERM = (TEMP4 * TEMP1)/(TEMP2*TEMP3)	TG 0051
	RATIO = DABS (TERM)/PSUM	DP 0052
	DIF = RATIO - .1D-09	DP 0053
	PSUM=PSUM + TERM	TG 0054
	IF (K-N+1) 2,3,3	TG 0055
2	IF (DIF) 3,3,1	TG 0056
3	FBESK= 0.5 * PSUM	TG 0057

APPENDIX 1  
 COMPUTER PROGRAM USED TO EVALUATE  
 $I(\psi, \beta)$  AND  $E(\psi, \beta)$   
 OR  
 $I(\eta, \beta)$  AND  $E(\eta, \beta)$

```

      END
C     CVEL FUNCTION SUBPROGRAM
      FUNCTION CVEL (XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ, MAXJ,
1P MAX, DELPO, MAXN, TESTI, TESTS, JUNCT)
      IMPLICIT REAL*8(A-H,O-Z)
C     NON-EXECUTABLE STATEMENTS
      DIMENSION CINT(200), ACINT(200)
11  FORMAT ( 48H1          SPHERE GENERATING CYLINDER VELOCITY FIELD/
156H0          XSUBI          YSUBI          ZS
20H1/1H ,13X, E15.8, 4X, E15.8, 4X, E15.8// 46H0 POSITION AT WHICH
3F15LD STRENGTH IS MEASURED/ 56H0          XSUBJ          YSU
48J          ZSUBJ/1H , 13X, E15.8, 4X, E15.8, 4X, E15.8// 59H0
5          SPHERE AND FIELD POSITIONS IN CYLINDRICAL COORDINATES/ 55H0
6          RSUBI          RSUBJ          PHI/1H , 13X, E15.
78, 4X, E15.8, 4X, E15.8//35H0 COEFFICIENTS OF FILON INTEGRATION/55
8H0          ALPHA          BETA          GAMMA/1H ,13X,
9E15.8,4X, E15.8, 4X, E15.8)
12  FORMAT(140/27H0 BESSEL FUNCTIONS FOR N=12/ 4H0Q1=E15.8, 2X,
1  8H IN(Q1)=E15.8, 2X, 9H IN1(Q1)=E15.8,2X, 8H KN(Q1)=E15.8/
2          4H0Q2=E15.8,2X, 8H IN(Q2)=E15.8,2X,9H IN1(Q2)=
3  E15.8/ 4H0Q3=E15.8, 2X, 8H IN(Q3)=E15.8, 9H IN1(Q3)=E15.8)
13  FORMAT( 45H0          NUMERICAL EVALUATION OF INTEGRAL FOR N= 12,
1  16H BY FILON METHOD/1H0)
15  FORMAT( 48H0          INTEGRAND=G(P)*COSF(P*Z)          P=A(DELPI)B=E15.8,
11H(,F15.8,1H),E15.8//1 8H          7E16.8))
16  FORMAT(110/740CESUM=E15.8,8H COSUM=E15.8, 7H CINTG=E15.8,
18H TINTG=E15.8/ 12H0          TOPINT=E15.8, 7H RECTA=E15.8, 10H          RATIO
2I=E15.8)
17  FORMAT(140/22H0          TOTAL INTEGRAL (N=12, 2H)=E15.8, 19H SUM OF INT
1EGRALS=E15.8,          9H RATIOS=E15.8)
18  FORMAT(47H0          INTEGRAND=H SUBN(P)*COSF(P*Z)          P=A(DELPI)B=E15.8,
11H(,F15.8,1H),E15.8//1 8H          7E16.8))
19  FORMAT(110/10H0          CESUM=E15.8, 8H COSUM=E15.8, 9H          CINTG=E15.8,
1  9H          TINTG=E15.8/ 12H0          TOPINT=E15.8, 8H          RECTA=E15.8,
2  8H          RATIO=E15.8)
101 FORMAT(30H0CYLINDER VELOCITY FIELD AFTER 13, 14H INTEGRATIONS=
1E15.8)
102 FORMAT(110/28H0          FBRESSEL FUNCTIONS FOR N=12/6H0          Q1=E15.8,2X,
1  9H          FIN(Q1)=E15.8,11H          FIN1(Q1)=E15.8, 9H          FKN(Q1)=E15.8/
2          5H0          Q2=E15.8, 9H          FIN(Q2)=E15.8, 11H          FIN1(Q2)=
3  E15.8/ 4H0Q3=E15.8, 9H          FIN(Q3)=E15.8,10H          FIN1(Q3)=E15.8)
C     THIS SECTION COMPUTES FILON COEFFICIENTS, ALPHA, BETA, GAMMA
      RSUBI = DSORT (XSUBI * XSUBI + YSUBI * YSUBI)
      RSUBJ = DSORT (XSUBJ * XSUBJ + YSUBJ * YSUBJ)
      IF (XSUBI) 1,2,3
2  IF (YSUBI) 4,5,6
5  PHII = 0.
      GO TO 7
6  PHII = 3.14159265/2.
      GO TO 7
4  PHII = -3.14159265/2.
      GO TO 7
1  PHII = DATAN (YSUBI/XSUBI) + 3.14159265
      GO TO 7
3  PHII = DATAN (YSUBI/XSUBI)
7  IF(XSUBJ) 8,9,10
9  IF(YSUBJ) 20, 21, 22
21  PHIJ= 0.
      GO TO 23
22  PHIJ= .14159265/2.

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```

      TG 0058
      TG 0059
      TG 0060
      TG 0062
      TG 0063
      DP DP
      TG 0064
      TG 0065
      TG 0066
      TG 0067
      TG 0068
      TG 0069
      TG 0070
      TG 0071
      TG 0072
      TG 0073
      TG 0074
      TG 0075
      TG 0076
      TG 0077
      TG 0078
      TG 0079
      TG 0080
      TG 0081
      TG 0082
      TG 0083
      TG 0084
      TG 0085
      TG 0086
      TG 0087
      TG 0088
      TG 0089
      TG 0090
      TG 0091
      TG 0092
      TG 0093
      TG 0094
      TG 0095
      TG 0096
      TG 0097
      TG 0098
      TG 0099
      TG 0100
      DP 0101
      DP 0102
      TG 0103
      TG 0104
      TG 0105
      TG 0106
      TG 0107
      TG 0108
      TG 0109
      TG 0110
      DP 0111
      TG 0112
      DP 0113
      TG 0114
      TG 0115
      TG 0116
      TG 0117
      TG 0118

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7 GO TO 23
20 PHIJ = - 3.14159265/2.
GO TO 23
8 PHIJ = DATAN (YSURJ/XSUBJ) + 3.14159265
GO TO 23
10 PHIJ = DATAN (YSURJ/XSUBJ)
23 PHI = PHI - PHIJ
Z = ZSUBI - ZSUBJ
AZ = DABS (Z)
DELP = DELPO/(1.0 + DSIN(AZ *DELP))
THETA = Z * DELP
IF(THETA) 24, 25, 24
25 ALPHA = 0.
BETA = 2./3.
GAMMA = 4./3.
GO TO 26
24 THETA2 = THETA * THETA
THETA3 = THETA * THETA2
STHETA = DSIN(THETA)
CTHETA = DCOS(THETA)
SINCOS = STHETA * CTHETA
ALPHA = (THETA2 + THETA*SINCOS-2.*STHETA*STHETA)/ THETA3
BETA = 2.*(THETA*(1. + CTHETA*CTHETA)-2.*SINCOS)/THETA3
GAMMA = 4.*(STHETA-THETA*CTHETA)/THETA3
26 GO TO (27,28,27),JUNCT
27 WRITE (6,11) XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ,
IRSUBI, RSUBJ, PHI, ALPHA, BETA, GAMMA
THIS SECTION COMPUTES THE INTEGRALS FOR N=0 (1) MAXN
C
28 MAXNP= MAXN +1
MAXJP =MAXJ +1
MAXJP1 = MAXJP-1
TNTG = 0.
DO 31 NP=1, MAXNP
N = NP-1
FN =N
A=0.
TNTG = 0.
IF(N) 29, 29, 30
C
INTEGRAL FOR N=0
29 DO 32 JP=1, MAXJP
J=JP-1
DJ=J
P=A + DJ*DELP
IF(P) 40, 41, 40
41 CINT(JP) = 0.0
FGDFP=0.0
GO TO 32
C
CALL BESSEL FUNCTIONS
40 NPLUS1 = N
Q1 =P
Q2 =P*RSUBI
Q3=PARSUBJ
CALL BESI ( Q1, NPLUS1, BIN, IER)
MPLUS1 = NPLUS1 + 1
CALL BESI ( Q1, MPLUS1, BINI, IERY)
CALL BESK ( Q1, NPLUS1, BKN, IER)
CALL BESK ( Q1, MPLUS1, BKNI, IERY)
IF(Q2) 43, 44, 43
44 RINF1 =1.
RINF1 =0.
GO TO 45

```

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TG 0119
TG 0120
TG 0121
TG 0122
TG 0123
TG 0124
TG 0125
TG 0126
TG 0127
TG 0128
TG 0129
TG 0130
TG 0131
TG 0132
TG 0133
TG 0134
TG 0135
TG 0136
TG 0137
TG 0138
TG 0139
TG 0140
TG 0141
TG 0142
TG 0143
TG 0144
TG 0145
TG 0146
TG 0147
TG 0148
TG 0149
TG 0150
TG 0151
TG 0152
TG 0153
TG 0154
TG 0155
TG 0156
TG 0157
TG 0158
TG 0159
TG 0160
TG 0161
TG 0162
GG 1
GG 1A
TG 0164
TG 0165
TG 0166
TG 0167
TG 0168
TG 0169
TG 0170
TG 0171
TG 0172
TG 0173
TG 0174
TG 0175
TG 0176
TG 0177
TG 0178

```

43 CALL BESI ( Q2, MPLUS1, BINRI, IER)	TG 0179
CALL BESI ( Q2, MPLUS1, BINRI, IER)	TG 0180
45 IF(Q3) 46, 47, 46	TG 0181
47 BINRJ = 1.	TG 0182
BINIRJ = 0.	TG 0183
GO TO 48	TG 0184
46 CALL BESI ( Q3, NPLUS1, BINRJ, IER)	TG 0185
CALL BESI ( Q3, MPLUS1, BINRJ, IER)	TG 0186
48 GO TO (49, 49, 50) ,JUNCT	TG 0187
50 WRITE (6,12) N, Q1, BIN, BIN1, BKN, Q2, BINRI,	TG 0188
IBINRI, Q3, BINRJ, BINIRJ	TG 0189
C COMPUTES INTEGRAND CINT(J)	TG 0190
49 A1 = BINRI/BIN	TG 0191
A3 = BINRI/BIN1	TG 0192
A4 = BINIRJ/BIN1	TG 0193
A6 = A3*A4	TG 0194
A7 = A1 * A4	TG 0195
A9 = BIN/BIN1	TG 0196
A10 = A9*A9	TG 0197
A11 = A10 - 2.* A9/P -1.	TG 0198
A12 = BIN1/BIN	
A13 = BKN*BIN1	
A18 = BINRJ/BIN	
A26 = -A7*A12	
A27 = RSUBI*A6*A12	
A28 = RSUBJ*A18*A1*A9	
A29 = -RSUBJ*RSUBI*A3*A9*A18	
A30=(A26+A27+A28+A29)/A11	GG 2
A31=P*A13*A4	GG 3
A32=-A1*A12	GG 4
A33=A12+A3*RSUBI	GG 5
A34=A31*(A32+A33)	GG 6
A35=P*A1	GG 7
A36=RSUBJ*BKN*BIN*A18	GG 8
A37=-BKN1*BIN1*A4	GG 9
A38=A35*(A36+A37)	GG 10
A39=-2.0/(P*A11)	GG 11
A40=-RSUBI*A3	GG 12
A41=A1+A40	GG 13
A42=A4*A41	GG 14
A43=A39*A42	GG 15
53 GOFP=A30+A34+A38+A43	GG 16
IF (JP-1) 1053,1053,1054	GG 17
1053 FGOFP=GOFP	GG 18
1054 CINT(JP) = GOFP*DSIN(P*Z)	GG 19
32 CONTINUE	TG 0201
CESUM = 0.	TG 0202
COSUM = 0.	TG 0203
DO 33 JP=1,MAXJP,2	TG 0204
33 CESUM = CESUM + CINT (JP)	TG 0205
CESUM = CESUM - ( CINT(1)+ CINT(MAXJP))/2.	TG 0206
DO 34 JP=2,MAXJP1,2	TG 0207
34 COSUM = COSUM + CINT(JP)	TG 0208
IF (THE1A) 54, 55, 54	TG 0209
55 CINTG =DELP*(BETA*CESUM + GAMMA*COSUM)	TG 0210
BJ=MAXJ	TG 0211
B= A + BJ *DELP	TG 0212
GO TO 56	TG 0213
54 A1=MAXJ	TG 0214
B= A + BJ *DELP	TG 0215
SINZA =DSIN(Z*A)	DP 0216

	SINZB = DSIN(Z*B)	DP 0217
	COSZA = DCOS(Z*A)	DP 0218
	COSZB = DCOS(Z*B)	DP 0219
	CINTG = DELP*(-ALPHA*(CINT(MAXJP)*COSZB/SINZB - FGOFP*COSZA)	GG 20
1	+ BETA*CESUM + GAMMA*COSUM)	GG 21
56	TINTG = TINTG + CINTG	TG 0222
	TNNTG = TNNTG + CINTG	TG 0223
	DO 35 JP=1, MAXJP	TG 0224
35	ACINT(JP) = DABS(CINT(JP))	DP 0225
	TOPINT = 0.	TG 0226
	DO 37 JP = 1, MAXJP	TG 0227
	IF (TOPINT - ACINT(JP)) 60, 37, 37	TG 0228
60	TOPINT = ACINT(JP)	TG 0229
37	CONTINUE	TG 0230
	BJ=MAXJ	TG 0231
	RECTA = DELP * BJ*TOPINT*2.	TG 0232
	RATIOI = RECTA /DABS(TNNTG)	DP 0233
	GO TO (61, 62, 61), JUNCT	TG 0234
61	WRITE (6,13)N	TG 0235
	WRITE (6,15) A, DELP, B, (CINT(JP), JP=1, MAXJP)	TG 0236
	WRITE (6,16) CESUM, COSUM, CINTG, TINTG, TOPINT, RECTA,	TG 0237
	RATIOI	TG 0238
62	A=B	TG 0239
	BJ=MAXJ	TG 0240
	B = A + BJ *DELP	TG 0241
	IF (B - PMAX) 63, 63, 64	TG 0242
63	IF(TESTI - RATIOI) 29, 29, 64	TG 0243
64	CYL = TINTG	TG 0244
	CYLPHI = TINTG	TG 0245
	IF(RSUBI *RSUBJ) 31, 65, 31	TG 0246
C	INTEGRAL FOR N=1,2,3,...	TG 0247
30	DO 38 JP=1, MAXJP	TG 0248
	J = JP-1	TG 0249
	DJ=J	TG 0250
	P = A+DJ*DELP	TG 0251
	IF(P) 66, 67, 66	TG 0252
67	CINT(JP) = 0.0	GG 22
	FGOFP=0.0	GG 22A
	GO TO 38	TG 0254
66	IF (N-10) 68, 69, 69	TG 0255
69	IF (P/EN - 0.2) 70, 70, 68	TG 0256
C	CALL BESSEL FUNCTIONS	TG 0257
68	NPLUS1 = N	TG 0258
	Q1 = P	TG 0259
	Q2 = P*RSUBI	TG 0260
	Q3 = P*RSUBJ	TG 0261
	CALL BESI ( Q1, NPLUS1, BIN, IER)	TG 0262
	MPLUS1 = NPLUS1 + 1	TG 0263
	CALL BESI ( Q1, MPLUS1, BIN1, IER)	TG 0264
	CALL BFK ( Q1, NPLUS1, BKN, IER)	TG 0265
	CALL BESI ( Q2, NPLUS1, BINRI, IER)	TG 0266
	CALL BESI ( Q2, MPLUS1, BINRIRI, IER)	TG 0267
	CALL BESI ( Q3, NPLUS1, BINRJ, IER)	TG 0268
	CALL BESI ( Q3, MPLUS1, BINRJR, IER)	TG 0269
	CALL BFK(Q1,MPLUS1,BKN1,IER)	
	GO TO (71, 71, 72), JUNCT	TG 0270
72	WRITE (6,12) N, Q1, BIN, BIN1, BKN, Q2, BINRI,	TG 0271
	13BINIRI, Q3, BINRJ, BINRJR	TG 0272
C	COMPUTES INTEGRAND CINT(J)	TG 0273
71	A1 = P+P	TG 0274
	A2 = A1 *A1	TG 0275

A3 = P*A1	TG 0276
A4 = BINI / BIN	TG 0277
A5 = A4/P	TG 0278
A6 = A4 *A4	TG 0279
A7 = BINRI /BIN	TG 0280
A8 = BINRJ / BIN	TG 0281
A12= BINIRI/BIN	TG 0282
A9 =A12*RSUBI	TG 0283
A10 = BINIRJ/BIN	TG 0284
A11 = A7 * A9	TG 0285
A14 = A10 * A7	TG 0286
A15= A12 * A8	TG 0287
A16 = A4* A14	TG 0288
A17 = A9*A10	TG 0289
A18 = - A3 * A4 * A6	TG 0290
A19 = A5 * A5	TG 0291
A20 = A2 * (A5 - A19 * (2. + 3. * FN))	TG 0292
A22 = A1 * (FN -2.*FN * FN * A5 - 4. * FN * A5)	TG 0293
A23 = A18 + A20	TG 0294
A24 = A23 + A22	TG 0295
A27 = BKN * BIN	TG 0298
A58=RSUBJ*A11	
A59=-A16+A17+A58	
A60=P*A59	GG 23
A61=-A4*A11/RSUBJ	
A62=A15*RSUBI/RSUBJ	
A63=FN*(A61+A14+A62)	GG 24
A64=2.0*FN*FN*A11/(P*RSUBJ)	GG 25
A65=A27*(A60+A63+A64)	GG 26
A66=-P*BKN1*BIN*A14	GG 27
A67=-FN*BKN1*BIN*A11/RSUBJ	GG 28
A68=A66+A67	GG 29
A69=-RSUBI*RSUBJ*A15	GG 30
A70=A58*A4	GG 31
A71=A17*A4	GG 32
A72=-A16*A4	GG 33
A73=A3*A4*(A72+A71+A70+A69)/A24	GG 34
A74=BIN/BINI	GG 35
A75=(-2.0*A16+A61*A4+A62*A4+2.0*A17+A58+A69*A74)	GG 36
A76=FN*A1*A4*A75/A24	GG 37
A77=(-A14+A61+A62+A17*A74)	GG 38
A78=FN*FN*P*A4*A77/A24	GG 39
A79=A17-A4*A14	GG 40
A80=2.0*A1*A4*A79/A24	GG 41
A81=2.0*FN*P*A4*A77/A24	GG 42
HOFP=A65+A68+A73+A76+A78+A80+A81	GG 43
IF(JP-1) 1055,1055,1056	GG 44
1055 HOFP = HOFP	GG 45
1056 CINT(JP) = HOFP*DSIN(P*Z)	GG 46
GO TO 38	TG 0306
C CALL FBESSEL FUNCTIONS	TG 0307
70 Q1 = P	TG 0308
Q2 = P* RSUBI	TG 0309
Q3=P*RSUBJ	TG 0310
FIN = FBESI(N,Q1)	TG 0311
FINRI=FBFSI(N,Q2)	TG 0312
IF(Q2-Q3) 73, 74, 73	TG 0313
74 FINRJ = FINRI	TG 0314
GO TO 75	TG 0315
73 FINRJ = FBESI (N,Q3)	TG 0316
75 FINI = FBESI (N+1,Q1)	TG 0317

FINIRI = FBESI (N+1, Q2)	TG 0318
IF(O2 - Q3) 76,77,76	TG 0319
77 FINIRJ = FINIRI	TG 0320
GO TO 78	TG 0321
76 FINIRJ = FBESI (N+1, Q3)	TG 0322
78 FKN = FBESK (N, Q1)	TG 0323
FKN1 = FBESK(N+1,Q1)	
GO TO (79, 79, 80), JUNCT	TG 0324
80 WRITE (6,102) N, Q1, FIN, FIN1, FKN, Q2, FINRI,	TG 0325
1FINIRI, Q3, FINRJ, FINRJ	TG 0326
C COMPUTES INTEGRAND CINT(J)	TG 0327
79 A1 = RSUBJ**2	TG 0328
A2 = 1./RSUBJ	TG 0329
A3 = RSUBJ**N	TG 0330
A4 = RSUBJ **N	TG 0331
A5 = FINRI /FIN	TG 0332
A6 = FINRJ /FIN	TG 0333
A7 = FINIRI/FIN	TG 0334
A8 = FINIRJ / FIN	TG 0335
A9 = FIN1 / FIN	TG 0336
A10 = A9 *A9	TG 0337
A11 = A5 * A6	TG 0338
A12 = A7 *A8	TG 0339
A13 = A7 * A6	TG 0340
A14 = A8 * A5	TG 0341
A15 = FKN *FIN	TG 0342
A19 = P*P	TG 0346
A20 = A19 * A19	TG 0347
A21 = A19 * A20	TG 0348
A22 = N+1	TG 0349
A23 = A22 * A22	TG 0350
A24 = A22 * A23	TG 0351
A25 = - A21 *A9 * A10/(8.*A24)	TG 0352
A26 = A20*(0.5*A9/A22, - 0.5 *A10/A23 -0.75*FN*A10/A23)	TG 0353
A27 = A19*(- 2.*FN*A9/A22 +(FN*FN*(FIN -FIN1) +FN* FIN)/(A22*FIN))	TG 0354
AA27 = A25 + A26	TG 0355
A28 = AA27 + A27	TG 0356
A29 = A3*A4	TG 0357
A34=-A9*A14	
A35=A1*A12	
A36=A34+A35	
A37=RSUBJ*A29	
A38=P*A19*A37/(4.*A23)	GG 48
A39=A38*A36	
A40=A2*A29	
A41=FN*P*A40/(2.*A22)	GG 49
A42=-A9*A11	
A43=A1*A13	
A44=RSUBJ*RSUBJ*A14	
A45=A41*(A42+A43+A44)	
A46=P*A37	GG 50
A47=A46*A11	GG 51
A48=2.*FN*FN*A40*A11/P	GG 52
A49=A15/FN	
A50=A49*(A39+A45+A47+A48)	
A51=-2.*FKN1*FIN*(A46*A14/(2.*A22)+FN*A40*A11/P)	GG 53
A52=A21*A46*A10*A36/(16.*A24*A22*A28)	
A53=1./A9	
A54=FN*P*A20*A40*A10/(8.*A24*A28)	GG 54
A55=A43+A42	
A56=RSUBJ*RSUBJ*A53*A35	

A57=A55-2.*A44+2.*A56	GG	55
A58=A54*A57	GG	56
A59=P*A20*A37*A9/(4.*A23*A28)	GG	57
A60=A35/A22	GG	58
A61=A34/A22	GG	59
A62=A59*(A60+A61-A55)	GG	60
A63=FN+FN*P*A19*A40*A9/(4.*A23*A28)	GG	61
A64=-A44+A55+A56	GG	62
A65=A63*A64	GG	63
A66=FN*P*A19*A40*A9/(2.*A22*A28)	GG	64
A67=A56/A22	GG	65
A68=A55/A22	GG	66
A69=A44/A22	GG	67
A70=RSUBJ*RSUBJ*A11	GG	68
A71=A1*RSUBJ*RSUBJ	GG	69
A72=A71*A13*A53	GG	71A
A73=A66*(A67+A68-A69+A70-A72)	GG	72
HOFP=A50+A51+A52+A58+A62+A65+A73	GG	73
IF(JP-1) 1057,1057,1058	GG	74
1057 HOFP=HOFP	TG	0364
1058 CINT(JP) = HOFP*DSIN(P*Z)	TG	0365
38 CONTINUE	TG	0366
CESUM = 0.	TG	0367
COSUM = 0.	TG	0368
DO 39 JP=1, MAXJP,2	TG	0369
39 CESUM = CESUM + CINT(JP)	TG	0370
CESUM = CESUM -(CINT(1) + CINT(MAXJP))/2.	TG	0371
DO 81 JP =2, MAXJP1, 2	TG	0372
81 COSUM = COSUM + CINT(JP)	TG	0373
IF (THETA) 82, 83, 82	TG	0374
83 CINTG = DELP *(BETA*CESUM + GAMMA * COSUM)	TG	0375
BJ=MAXJ	TG	0376
B = A + BJ *DELP	TG	0377
GO TO 84	TG	0378
82 BJ=MAXJ	TG	0379
B = A + BJ *DELP	DP	0380
SINZA =USIN(Z*A)	DP	0381
SINZB =DSIN(Z*B)	DP	0382
COSZA =DCOS(Z*A)	GG	75
COSZB =DCOS(Z*B)	GG	76
CINTG = DELP*(-ALPHA*(CINT(MAXJP)*COSZB/SINZB - HOFP*COSZA)	TG	0385
1 + BETA*CESUM + GAMMA*COSUM)	TG	0386
84 TINTG = TINTG + CINTG	TG	0387
TNNTG = TNNTG + CINTG	DP	0388
DO 85 JP = 1, MAXJP	TG	0389
85 ACINT(JP) = DABS(CINT(JP))	TG	0390
TOPINT = 0.	TG	0391
DO 86 JP=1,MAXJP	TG	0392
IF(TOPINT-ACINT(JP))87,86,86	TG	0393
87 TOPINT = ACINT (JP)	TG	0394
86 CONTINUE	TG	0395
RJ=MAXJ	DP	0396
RECTA=DELP*BJ	TG	0397
*TOPINT*(1.+2. * RSUBI*RSURJ)	TG	0398
RATIOI = RECTA /DABS(TNNTG)	TG	0399
GO TO (88,89,88), JUNCT	TG	0400
88 WRITE (6,13) N	TG	0401
WRITE (6,18) A, DELP, B, (CINT(JP), JP=1,MAXJP)	TG	0402
WRITE (6,19) CESUM, COSUM, CINTG, TINTG, TOPINT,	TG	0403
1RECTA, RATIOI		
89 A=B		
RJ=MAXJ		

	R= A + BJ *DELTA	TG 0404
	IF(R-PMAX)90,90,91	TG 0405
90	IF(TESTI-RATIOI)30,30,91	TG 0406
91	CYLL = CYL	TG 0407
	CYL = CYL + 2.*TINTG	TG 0408
	CYLPHI = CYLPHI + 2.0*DCOS(FN*PHI)*TINTG	DP 0409
	RATIOS = 2.0*(1.0+4.0*RSUBI*RSUBJ)*DABS(TINTG/CYLL)	DP 0410
	GO TO (92,93, 92),JUNCT	TG 0411
92	WRITE (6,17) N, TINTG, CYL, RATIOS	TG 0412
93	IF(TESTS-RATIOS)31,65,65	TG 0413
31	CONTINUE	TG 0414
C	COMPUTES CVFL	TG 0415
65	CVFL = .3./(2.*3.14159265)* CYLPHI	GG 77
	PROD = (1.-RSUBI)*CVFL	GG 78
	PRODD = (1.-RSUBI)*CYLPHI	TG 0418
	WRITE (6,11) XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ,	TG 0419
	1RSUBI, RSUBJ, PHI, ALPHA, BETA, GAMMA	GG 79
	WRITE (6,1234) PROD, PRODD	GG 80
1234	FORMAT (6H0PROD=E15.8,3X,7H PRODD=E15.8)	TG 0422
	WRITE (6,555) TNNTG,TINTG,CYLPHI,CYLL,CYL,N,	GG 81
	1RATIOS,R,RATIOI,CVEL,PROD,RSUBI	TG 0424
555	FORMAT(1H0/7HOTNNTG=E15.8,3X, 7H TINTG=E15.8,3X, 8H.CYLPHI=E15.8	TG 0425
	1/ 6H0CYLL=E15.8,3X, 5H CYL=E15.8,3X, 3H N=I2/ 8HORATIOS=E15.8,	TG 0426
	23X, 3H R=E15.8, 3X, 8H RATIOI=E15.8/ 6H0CVEL=E15.8,5X,	GG 82
	36H PROD=E15.8,3X,7H RSUBI=E15.8)	TG 0428
	WRITE (6,685) MAXJ,MAXN,JUNCT,DELP,TESTI,TESTS,PMAX	TG 0429
685	FORMAT(1H0/6H0MAXJ=I2,3X, 6H MAXN=I2,3X, 7H JUNCT=I1/ 6H0DELP=E15.	TG 0430
	18,3X, 7H TESTI=E15.8,3X, 7H TESTS=E15.8,3X, 6H PMAX=E15.8)	TG 0431
	GO TO (94,95, 94), JUNCT	TG 0432
94	WRITE (6,101) N, CVFL	TG 0433
95	RETURN	TG 0434
C	THIS PROGRAM COMPUTES EOFBETA	TG 0435
	END	TG 0436
C	.....	TG 0437
C	SUBROUTINE BESK	TG 0438
C	COMPUTE THE K BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER	TG 0439
C	USAGE	TG 0440
C	CALL BESK(X,N,BK,IER)	TG 0441
C	DESCRIPTION OF PARAMETERS	TG 0442
C	X -THE ARGUMENT OF THE K BESSEL FUNCTION DESIRED	TG 0443
C	N -THE ORDER OF THE K BESSEL FUNCTION DESIRED	TG 0444
C	BK -THE RESULTANT K BESSEL FUNCTION	TG 0445
C	IER-RESULTANT ERROR CODE WHERE	TG 0446
C	IER=0 NO ERROR	TG 0447
C	IER=1 N IS NEGATIVE	TG 0448
C	IER=2 X IS ZERO OR NEGATIVE	TG 0449
C	REMARKS	TG 0450
C	N MUST BE GREATER THAN OR EQUAL TO ZERO	TG 0451
C	X SHOULD BE LESS THAN 60 TO AVOID EXCEEDING THE RANGE OF	TG 0452
C	THE MACHINE	TG 0453
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	TG 0454
C	NONE	TG 0455
C	METHOD	TG 0456
C		TG 0457
C		TG 0458
C		TG 0459
C		TG 0460
C		TG 0461
C		TG 0462





	A=.57721566 +DLOG(B)	DP 0523
	C=B+A	TG 0524
	IF(N-1)37,43,37	TG 0525
C		TG 0526
C	COMPUTE K0 USING SERIES EXPANSION	TG 0527
C		TG 0528
	37 GO=-A	TG 0529
	X2J=1.	TG 0530
	FACT=1.	TG 0531
	HJ=.0	TG 0532
	DO 40 J=1,6	TG 0533
	RJ=1./FLOAT(J)	TG 0534
	X2J=X2J*C	TG 0535
	FACT=FACT*RJ*RJ	TG 0536
	HJ=HJ+RJ	TG 0537
	40 GO=GO+X2J*FACT*(HJ-A)	TG 0538
	IF(N)43,42,43	TG 0539
	42 BK=GO	TG 0540
	RETURN	TG 0541
C		TG 0542
C	COMPUTE K1 USING SERIES EXPANSION	TG 0543
C		TG 0544
	43 X2J=B	TG 0545
	FACT=1.	TG 0546
	HJ=1.	TG 0547
	G1=1./X+X2J*(.5+A-HJ)	TG 0548
	DO 50 J=2,8	TG 0549
	X2J=X2J*C	TG 0550
	RJ=1./FLOAT(J)	TG 0551
	FACT=FACT*RJ*RJ	TG 0552
	HJ=HJ+RJ	TG 0553
	50 G1=G1+X2J*FACT*(.5+(A-HJ)*FLOAT(J))	TG 0554
	IF(N-1)31,52,31	TG 0555
	52 BK=G1	TG 0556
	RETURN	TG 0557
	END	TG 0558
C		TG 0559
C	.....	TG 0560
C		TG 0561
C	SUBROUTINE BESI	TG 0562
C		TG 0563
C	PURPOSE	TG 0564
C	COMPUTE THE I BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER	TG 0565
C		TG 0566
C	USAGE	TG 0567
C	CALL BESI(X,N,BI,IER)	TG 0568
C		TG 0569
C	DESCRIPTION OF PARAMETERS	TG 0570
C	X -THE ARGUMENT OF THE I BESSEL FUNCTION DESIRED	TG 0571
C	N -THE ORDER OF THE I BESSEL FUNCTION DESIRED	TG 0572
C	BI -THE RESULTANT I BESSEL FUNCTION	TG 0573
C	IER-RESULTANT ERROR CODE WHERE	TG 0574
C	IER=0 NO ERROR	TG 0575
C	IER=1 N IS NEGATIVE	TG 0576
C	IER=2 X IS NEGATIVE	TG 0577
C		TG 0578
C	REMARKS	TG 0579
C	N MUST BE GREATER THAN OR EQUAL TO ZERO	TG 0580
C	X SHOULD BE LESS THAN 60 TO AVOID EXCEEDING THE RANGE OF	TG 0581
C	THE MACHINE	TG 0582
C		TG 0583

C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	TG 0584
C	NONE	TG 0585
C		TG 0586
C	METHOD	TG 0587
C	COMPUTES ZERO ORDER AND FIRST ORDER BESSEL FUNCTIONS USING	TG 0588
C	SERIES APPROXIMATIONS AND THEN COMPUTES N-TH ORDER FUNCTION	TG 0589
C	USING RECURRENCE RELATION.	TG 0590
C		TG 0591
C	.....	TG 0592
C		TG 0593
	SUBROUTINE BESI(X,N,BI,IER)	TG 0594
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
C		TG 0595
C	CHECK FOR ERRORS IN N AND X AND EXIT IF ANY ARE PRESENT	TG 0596
C		TG 0597
	IER=0	TG 0598
	BI=1.0	TG 0599
	IF(N)150,15,10	TG 0600
	10 IF(X)160,20,20	TG 0601
	15 IF(X)160,17,20	TG 0602
	17 RETURN	TG 0603
C		TG 0604
C	DEFINE TOLERANCE	TG 0605
C		TG 0606
	20 TOL=1.D-6	DP 0607
C		TG 0608
C	IF ARGUMENT GT 12 AND GT N, USE ASYMPTOTIC FORM	TG 0609
C		TG 0610
	IF(X-12.)40,40,30	TG 0611
	30 IF(X-FLOAT(N))40,40,110	TG 0612
C		TG 0613
C	COMPUTE FIRST TERM OF SERIES AND SET INITIAL VALUE OF THE SUM	TG 0614
C		TG 0615
	40 XX=X/2.	TG 0616
	FACTN=1.	TG 0617
	IF(N-1)70,70,50	TG 0618
	50 DO 60 I=2,N	TG 0619
	FI=I	TG 0620
	60 FACTN=FACTN*FI	TG 0621
	70 TERM=(XX**N)/FACTN	TG 0622
	BI=TERM	TG 0623
	XX=XX*XX	TG 0624
C		TG 0625
C	COMPUTE UP TO 30 TERMS, STOPPING WHEN ABS(TERM) LE ABS(SUM OF TERM	TG 0626
C	TIMES TOLERANCE	TG 0627
C		TG 0628
	DO 90 K=1,30	TG 0629
	IF(DABS(TERM)-DABS(BI*TOL))100,100,80	DP 0630
	80 FK=K*(N+K)	TG 0631
	TERM=TERM*(XX/FK)	TG 0632
	90 BI=BI+TERM	TG 0633
C		TG 0634
C	RETURN BI AS ANSWER	TG 0635
C		TG 0636
	100 RETURN	TG 0637
C		TG 0638
C	X GT 12 AND X GT N, SO USE ASYMPTOTIC APPROXIMATION	TG 0639
C		TG 0640
	110 FN=4*N*N	TG 0641
	XX=1./(8.*X)	TG 0642
	TERM=1.	TG 0643

```
BI=1.  
DO 130 K=1,30  
IF(DABS(TERM)-DABS(TOL*BI))140,140,120  
120 FK=(2*K-1)**2  
TERM=TERM**XX*(FK-FN)/FLOAT(K)  
130 BI=BI+TERM  
140 PI=3.141592653  
BI=BI*DEXP(X)/DSQRT(2.0*PI*X)  
GO TO 100  
150 IER=1  
GO TO 100  
160 IER=2  
GO TO 100  
END
```

```
TG 0644  
TG 0645  
DP 0646  
TG 0647  
TG 0648  
TG 0649  
TG 0650  
DP 0651  
TG 0652  
TG 0653  
TG 0654  
TG 0655  
TG 0656  
TG 0657
```

C	MAIN PROGRAM	TG 0002
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
	READ (5,1111) MAXJ, MAXN, JUNCT, PMAX, DELPO, TESTI,	TG 0003
	ITESTS	TG 0004
1111	FORMAT(I2, 3X, I2, 2X, I1, 9X, 4F10.8)	TG 0005
	READ (5,33) NN	TG 0006
33	FORMAT(I5)	TG 0007
	DO 2222 I=1,NN	TG 0008
	READ (5,200) XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ	TG 0009
200	FORMAT(6F10.9)	TG 0010
2222	V=CVEL(XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ, MAXJ, PMAX,	TG 0011
	DELPO, MAXN, TESTI, TESTS, JUNCT)	TG 0012
1028	STOP	TG 0013
	END	TG 0014
C	PROGRAM COMPUTES FBESI	TG 0015
	FUNCTION FBESI(N,X)	TG 0016
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
	PSUM = 1.0	TG 0017
	TEMP1 = 1.0	TG 0018
	TEMP2 = 1.0	TG 0019
	TEMP3 = 1.0	TG 0020
	K = 0	TG 0021
1	K=K+1	TG 0022
	TEMP1 = TEMP1 * ((0.5 * X)**2)	TG 0023
	PK=K	TG 0024
	TEMP2 = TEMP2 * PK	TG 0025
	AK = N + K	TG 0026
	TEMP3 = TEMP3 * AK	TG 0027
	TERM = TEMP1 / (TEMP2 * TEMP3)	TG 0028
	RATIO = TERM/PSUM	TG 0029
	DIF = RATIO - .1D-09	DP 0030
	PSUM = PSUM + TERM	TG 0031
	IF (DIF) 2,2,1	TG 0032
2	FBESI = PSUM	TG 0033
	RETURN	TG 0034
	END	TG 0035
C	PROGRAM COMPUTES FBESK	TG 0036
	FUNCTION FBESK(N,X)	TG 0037
	IMPLICIT REAL*8(A-H,O-Z)	DP DP
	PSUM=1.0	TG 0038
	TEMP1=1.0	TG 0039
	TEMP2 = 1.0	TG 0040
	TEMP3 = 1.0	TG 0041
	TEMP4=1.0	TG 0042
	K=0	TG 0043
1	K= K + 1	TG 0044
	TEMP1 = TEMP1*((0.5*X)**2)	TG 0045
	PK=K	TG 0046
	TEMP2 = TEMP2 * PK	TG 0047
	BK=N-K	TG 0048
	TEMP3 = TEMP3 * BK	TG 0049
	TEMP4 = -TEMP4	TG 0050
	TERM = (TEMP4 * TEMP1)/(TEMP2*TEMP3)	TG 0051
	RATIO = DABS (TERM)/PSUM	DP 0052
	DIF = RATIO - .1D-09	DP 0053
	PSUM=PSUM+ TERM	TG 0054
	IF (K-N+1) 2,3,3	TG 0055
2	IF (DIF) 3,3,1	TG 0056
3	FBESK= 0.5 * PSUM	TG 0057

APPENDIX 2  
COMPUTER PROGRAM USED TO EVALUATE  
M( $\psi, \beta$ ) AND M( $\psi, \beta$ )  
OR  
M( $\eta, \beta$ ) AND M( $\eta, \beta$ )

```

RETURN
END
C   CVEL FUNCTION SUBPROGRAM
    FUNCTION CVEL (XSURI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ, MAXJ,
    1PMAX, DELPO, MAXN, TESTI, TESTS, JUNCT)
    IMPLICIT REAL*(A-H,O-Z)
C   NON-EXECUTABLE STATEMENTS
    DIMENSION CINT(200), ACINT(200)
    11 FORMAT ( 4PHI      SPHERE GENERATING CYLINDER VELOCITY FIELD/
    1A6H0          XSURI          YSUBI          ZS
    2URI/1H ,13X, E15.8, 4X, E15.8, 4X, E15.8// 46H0 POSITION AT WHICH
    3FIELD STRENGTH IS MEASURED/ 56H0          XSUBJ          YSU
    4BJ          ZSUBJ/1H , 13X, E15.8, 4X, E15.8, 4X, E15.8// 59H0
    5 SPHERE AND FIELD POSITIONS IN CYLINDRICAL COORDINATES/ 55H0
    6          PSURI          RSURJ          PHI/1H , 13X, E15.
    78, 4X, E15.8, 4X, E15.8//35H0 COEFFICIENTS OF FILON INTEGRATION/55
    8H0          ALPHA          BETA          GAMMA/1H ,13X,
    9E15.8,4X, E15.8, 4X, E15.8)
    12 FORMAT(1H0/27H0 FBESSEL FUNCTIONS FOR N=12/ 4H0Q1=E15.8, 2X,
    1 8H IN(Q1)=E15.8, 2X, 9H IN1(Q1)=E15.8,2X, 8H KN(Q1)=E15.8/
    2          4H0Q2=E15.8,2X, 8H IN(Q2)=E15.8,2X,9H IN1(Q2)=
    3 E15.8/ 4H0Q3=E15.8, 2X, 8H IN(Q3)=E15.8, 9H IN1(Q3)=E15.8)
    13 FORMAT( 45H0 NUMERICAL EVALUATION OF INTEGRAL FOR N= 12,
    1 16H BY FILON METHOD/1H0)
    15 FORMAT( 48H0 INTEGRAND=G(P)*COSF(P*Z)          P=A(DELPI)B=E15.8,
    11H(,E15.8,1H),E15.8//(( 8H          7E16.8))
    16 FORMAT(1H0/7H0CESUM=E15.8,8H COSUM=E15.8, 7H CINTG=E15.8,
    1PH TINTG=E15.8/ 12H0 TOPINT=E15.8, 7H RECTA=E15.8, 10H RATIO
    2I=E15.8)
    17 FORMAT(1H0/22H0 TOTAL INTEGRAL (N=12, 2H)=E15.8, 19H SUM OF INT
    1EGRALS=E15.8,          9H RATIOS=E15.8)
    18 FORMAT(47H0 INTEGRAND=HSUBN(P)*COSF(P*Z)          P=A(DELPI)B=E15.8,
    11H(,E15.8,1H),E15.8//(( 8H          7E16.8))
    19 FORMAT(1H0/10H0 CESUM=E15.8, 8H COSUM=E15.8, 9H CINTG=E15.8,
    1 9H TINTG=E15.8/ 12H0 TOPINT=E15.8, 8H RECTA=E15.8,
    2 8H RATIOI=E15.8)
    101 FORMAT(30H0CYLINDER VELOCITY FIELD AFTER 13, 14H INTEGRATIONS=
    1E15.8)
    102 FORMAT(1H0/28H0 FBESSEL FUNCTIONS FOR N=12/6H0 Q1=E15.8,2X,
    1 9H FIN(Q1)=E15.8,11H FIN1(Q1)=E15.8, 9H FKN(Q1)=E15.8/
    2          5H0 Q2=E15.8, 9H FIN(Q2)=E15.8, 11H FIN1(Q2)=
    3 E15.8 /4H0Q3=E15.8, 9H FIN(Q3)=E15.8,10H FIN1(Q3)=E15.8)
C   THIS SECTION COMPUTES FILON COEFFICIENTS, ALPHA, BETA, GAMMA
    RSURI = DSORT (XSUBI * XSUBI + YSUBI * YSUBI)
    RSURJ = DSORT (XSUBJ * XSUBJ + YSUBJ * YSUBJ)
    IF (XSURI) 1,2,3
    2 IF(YSUBI) 4,5,6
    5 PHII = 0.
    GO TO 7
    6 PHII = 3.14159265/2.
    GO TO 7
    4 PHII =-3.14159265/2.
    GO TO 7
    1 PHII = DATAN (YSUBI/XSUBI) + 3.14159265
    GO TO 7
    3 PHII = DATAN (YSUBI/XSUBI)
    7 IF(XSUBJ) 8,9,10
    9 IF(YSUBJ) 20, 21, 22
    21 PHIJ= 0.
    GO TO 23
    22 PHIJ= 3.14159265/2.

```

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TG 0058
TG 0059
TG 0060
TG 0062
TG 0063
DP DP
TG 0064
TG 0065
TG 0066
TG 0067
TG 0068
TG 0069
TG 0070
TG 0071
TG 0072
TG 0073
TG 0074
TG 0075
TG 0076
TG 0077
TG 0078
TG 0079
TG 0080
TG 0081
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TG 0098
TG 0099
TG 0100
DP 0101
DP 0102
TG 0103
TG 0104
TG 0105
TG 0106
TG 0107
TG 0108
TG 0109
TG 0110
DP 0111
TG 0112
DP 0113
TG 0114
TG 0115
TG 0116
TG 0117
TG 0118

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	GO TO 23	TG 0119
20	PHIJ = - 3.14159265/2.	TG 0120
	GO TO 23	TG 0121
8	PHIJ = DATAN (YSUBJ/XSUBJ) + 3.14159265	DP 0122
	GO TO 23	TG 0123
10	PHIJ = DATAN (YSUBJ/XSUBJ)	DP 0124
23	PHI = PHII - PHIJ	TG 0125
	Z = ZSUBI - ZSUBJ	TG 0126
	AZ = DARS (Z)	DP 0127
	DELPO = DELPO/(1.0 + DSIN(AZ *DELPO))	DP 0128
	THETA = Z * DELP	TG 0129
	IF(THETA) 24, 25, 24	TG 0130
25	ALPHA = 0.	TG 0131
	BETA = 2./3.	TG 0132
	GAMMA = 4./3.	TG 0133
	GO TO 26	TG 0134
24	THETA2 = THETA * THETA	TG 0135
	THETA3 = THETA * THETA2	TG 0136
	STHETA = DSIN(THETA)	DP 0137
	CTHETA = DCOS(THETA)	DP 0138
	SINCOS = STHETA * CTHETA	TG 0139
	ALPHA =(THETA2 + THETA*SINCOS-2.*STHETA*STHETA)/ THETA3	TG 0140
	BETA =2.*(THETA*(1.+ CTHETA*CTHETA)-2.*SINCOS)/THETA3	TG 0141
	GAMMA = 4.*(STHETA-THETA* CTHETA)/THETA3	TG 0142
26	GO TO (27,28,27),JUNCT	TG 0143
27	WRITE (6,11) XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ,	TG 0144
	IRSUBI, RSUBJ, PHI, ALPHA, BETA, GAMMA	TG 0145
C	THIS SECTION COMPUTES THE INTEGRALS FOR N=0 (1) MAXN	TG 0146
28	MAXNP= MAXN +1	TG 0147
	MAXJP =MAXJ +1	TG 0148
	MAXJPI = MAXJP-1	TG 0149
	TNNTG = 0.	TG 0150
	DO 31 NP=1, MAXNP	TG 0151
	N = NP-1	TG 0152
	FN =N	TG 0153
	A=0.	TG 0154
	TINTG = 0.	TG 0155
	IF(N) 29, 29, 30	TG 0156
C	INTEGRAL FOR N=0	TG 0157
29	DO 32 JP=1, MAXJP	TG 0158
	J=JP-1	TG 0159
	DJ=J	TG 0160
	P=A + DJ*DELP	TG 0161
	IF(P) 40, 41, 40	TG 0162
41	CINT(JP)=0.0	GG 1R
	EQJFP=0.0	GG 1A
	GO TO 32	TG 0164
C	CALL Bessel FUNCTIONS,	TG 0165
40	NPLUS1 = N	TG 0166
	Q1 =P	TG 0167
	Q2 =P*RSUBI	TG 0168
	Q3=P*RSUBJ	TG 0169
	CALL RESI ( Q1, NPLUS1, BIN, IER)	TG 0170
	MPLUS1 = NPLUS1 + 1	TG 0171
	CALL RESI ( Q1, MPLUS1, BIN1, IER)	TG 0172
	CALL RESK ( Q1, NPLUS1, BKN, IER)	TG 0173
	CALL RESK ( Q1, MPLUS1, BKN1, IER)	TG 0174
	IF(Q2) 43, 44, 43	TG 0175
44	BINRI = 1.	TG 0176
	BIN1RI =0.	TG 0177
	GO TO 45	TG 0178

43	CALL BESI ( Q2, MPLUS1, BINRI, IER)	TG 0179
	CALL BESI ( Q2, MPLUS1, BINRI, IER)	TG 0180
45	IF (Q3) 46, 47, 46	TG 0181
47	BINRJ = 1.	TG 0182
	BINRJ = 0.	TG 0183
	GO TO 48	TG 0184
46	CALL BESI ( Q3, NPLUS1, BINRJ, IER)	TG 0185
	CALL BESI ( Q3, MPLUS1, BINRJ, IER)	TG 0186
48	GO TO (49, 49, 50) ,JUNCT	TG 0187
50	WRITE (6,12) N, Q1, BIN, BIN1, BKN, Q2, BINRI,	TG 0188
	IBINRI, Q3, BINRJ, BINRJ	TG 0189
C	COMPUTES INTEGRAND CINT(J)	TG 0190
49	A1=BINRI/BIN	GG 2R
	A2=BINRJ/BIN	GG 3R
	A3=BINRI/BIN1	GG 4R
	A4=BINRJ/BIN1	GG 5R
	A6=A3*A4	GG 6R
	A8=A2*A3	GG 7R
	A9=BIN/BIN1	GG 8R
	A10=A9*A9	GG 9R
	A11=A10-2.0*A9/P-1.0	GG 10R
	A12=BIN1/BIN	GG 11R
	A13=BKN*BIN1	GG 12R
	A26=-A6*A12	GG 13R
	A27=RSUMJ*A8*A9	GG 14R
	A28=(A26+A27)/A11	GG 15R
	A29=-P*A13*A12*A6	GG 16R
	A30=-2.0/(P*A11)	GG 17R
	A31=A30*A6	GG 18R
53	GOFP=A28+A29+A31	GG 19R
	IF (JP-1) 1053,1053,1054	GG 17
1053	FGFP=GOFP	GG 18
1054	CINT(JP) = GOFP*DSIN(P*Z)	GG 19
32	CONTINUE	TG 0201
	CESUM = 0.	TG 0202
	COSUM = 0.	TG 0203
	DO 33 JP=1,MAXJP,2	TG 0204
33	CESUM = CESUM + CINT (JP)	TG 0205
	COSUM = COSUM - ( CINT(1)+ CINT(MAXJP))/2.	TG 0206
	DO 34 JP=2,MAXJP1,2	TG 0207
34	COSUM = COSUM + CINT(JP)	TG 0208
	IF (THE TA) 54, 55, 54	TG 0209
55	CINTG = DELP*(BETA*CESUM + GAMMA*COSUM)	TG 0210
	BJ=MAXJ	TG 0211
	B= A + BJ *DELP	TG 0212
	GO TO 56	TG 0213
54	BJ=MAXJ	TG 0214
	B= A + BJ *DELP	TG 0215
	SINZA =DSIN(Z*A)	DP 0216
	SINZB =DSIN(Z*B)	DP 0217
	COSZA =DCOS(Z*A)	DP 0218
	COSZB =DCOS(Z*B)	DP 0219
	CINTG = DELP*(-ALPHA*(CINT(MAXJP)*COSZB/SINZB - FGFP*COSZA)	GG 20
1	+ BETA*CESUM + GAMMA*COSUM)	GG 21
56	TINTG = TINTG + CINTG	TG 0222
	TNNTG = TNNTG + CINTG	TG 0223
	DO 35 JP=1, MAXJP	TG 0224
35	ACINT(JP) = DABS(CINT(JP))	DP 0225
	TOPINT = 0.	TG 0226
	DO 37 JP = 1, MAXJP	TG 0227
	IF (TOPINT -ACINT(JP)) 60, 37, 37	TG 0228

60	TOPINT = ACINT(JP)	TG	0229
37	CONTINUE	TG	0230
	BJ=MAXJ	TG	0231
	RECTA= DELP * BJ*TOPINT*2.	TG	0232
	RATIOI = RECTA /DABS(TNNTG)	DP	0233
	GO TO (61, 62, 61), JUNCT	TG	0234
61	WRITE (6,13)N	TG	0235
	WRITE (6,15) A, DELP, B, (CINT(JP), JP=1, MAXJP)	TG	0236
	WRITE (6,16) CESUM, COSUM, CINTG, TINTG, TOPINT, RECTA,	TG	0237
	RATIOI	TG	0238
62	A=B	TG	0239
	BJ=MAXJ	TG	0240
	B= A + BJ *DELP	TG	0241
	IF (B- PMAX) 63, 63, 64	TG	0242
63	IF( TESTI - RATIOI) 29, 29, 64	TG	0243
64	CYL = TINTG	TG	0244
	CYLPHI = TINTG	TG	0245
	IF(RSUBI * RSUBJ) 31, 65, 31	TG	0246
C	INTEGRAL FOR N=1,2,3,...	TG	0247
30	DO 38 JP=1, MAXJP	TG	0248
	J= JP-1	TG	0249
	DJ=J	TG	0250
	P= A+DJ*DELP	TG	0251
	IF(P) 66, 67, 66	TG	0252
67	CINT(JP)=0.0	GG	20R
	FHOFP=0.0	GG	22A
	GO TO 38	TG	0254
66	IF (N-10) 68, 69, 69	TG	0255
69	IF(P/FN-0.2) 68,68,68	GG	93R
C	CALL BESSEL FUNCTIONS	TG	0257
68	NPLUS1 = N	TG	0258
	Q1 = P	TG	0259
	Q2 = P*RSUPI	TG	0260
	Q3 = P*RSURJ	TG	0261
	CALL BESI ( Q1, NPLUS1, BIN, IER)	TG	0262
	MPLUS1 = NPLUS1 + 1	TG	0263
	CALL BESI ( Q1, MPLUS1, BIN1, IER)	TG	0264
	CALL BESK ( Q1, NPLUS1, BKN, IER)	TG	0265
	CALL BESI ( Q2, NPLUS1, BINRI, IER)	TG	0266
	CALL BESI ( Q2, MPLUS1, BINR1, IER)	TG	0267
	CALL BESI ( Q3, NPLUS1, BINRJ, IER)	TG	0268
	CALL BESI ( Q3, MPLUS1, BINRJ, IER)	TG	0269
	CALL BESK(Q1,MPLUS1,BKN1,IER)		
	GO TO (71, 71, 72), JUNCT	TG	0270
72	WRITE (6,12) N, Q1, BIN, BIN1, BKN, Q2, BINRI,	TG	0271
	BINR1, Q3, BINRJ, BINRJ	TG	0272
C	COMPUTES INTEGRAND CINT(J)	TG	0273
71	A1=P*P	GG	21R
	A2=A1*A1	GG	22R
	A3=P*A1	GG	23R
	A4=BIN1/BIN	GG	24R
	A5=A4/P	GG	25R
	A6=A4*A4	GG	26R
	A7=BINRI/BIN	GG	27R
	A8=BINRJ/BIN	GG	28R
	A9=BINR1/BIN	GG	29R
	A10=A9*RSUPI	GG	30R
	A11=BINRJ/BIN	GG	31R
	A12=A7*A8	GG	32R
	A13=A11*A7	GG	33R
	A14=A9*A8	GG	34R



A15=A4*FM	GG	35R
A16=A4*A13	GG	36R
A17=A10*A11	GG	37R
A18=-A3*A4*A6	GG	38R
A19=A5*A5	GG	39R
A20=A2*(A5-A19*(2.+3.*FN))	GG	40R
A22=A1*(FN-2.*FN*FN*A5-4.*FN*A5)	GG	41R
A23=A19+A20	GG	42R
A24=A23+A22	GG	43R
A27=BKN*BIN	GG	44R
A30=A14/A15	GG	45R
A31=-FN*FN*A30/RSUBJ	GG	46R
A32=A12/A15	GG	47R
A33=-2.0*FN*FN*FN/(P*RSUBI*RSUBJ)	GG	48R
A34=A32*A33	GG	49R
A35=A9*A11	GG	50R
A36=-P*A35	GG	51R
A37=-FN*A14/RSUBJ	GG	52R
A38=-2.0*FN*A13/RSUBI	GG	53R
A39=A33/FN	GG	54R
A40=A39*A12	GG	55R
A41=A27*(A31+A34+A36+A37+A38+A40)	GG	56R
A42=BKNI*BIN	GG	57R
A43=FN*P*A30/RSUBJ	GG	58R
A44=2.0*FN*FN*A32/(RSUBI*RSUBJ)	GG	59R
A45=A42*(A43+A44)	GG	60R
A46=A3*A4/A24	GG	61R
A47=-A4*A35	GG	62R
A48=RSUBJ*A14	GG	63R
A49=A46*(A47+A48)	GG	64R
A50=FN*A1*A4/A24	GG	65R
A51=A4*A14	GG	66R
A52=-A51/RSUBJ	GG	67R
A53=-2.0*A16/RSUBI	GG	68R
A54=-2.0*RSUBJ*A12/RSUBI	GG	69R
A55=A50*(A52+A53-A35+A54)	GG	70R
A56=FN*FN*P*A4/A24	GG	71R
A57=-2.0*A4*A12	GG	72R
A58=A57/(RSUBI*RSUBJ)	GG	73R
A59=-2.0*A13/RSUBI	GG	74R
A60=A56*(A58+A59)	GG	75R
A61=2.0*A1*A4/A24	GG	76R
A62=-A61*A35	GG	77R
A63=2.0*FN*P*A4/A24	GG	78R
A64=-A14/RSUBJ	GG	79R
A65=A63*(A64+A59)	GG	80R
A66=2.0*FN*FN/A24	GG	81R
A67=A66*(-A64+A58)	GG	82R
A68=2.0*FN*FN*FN/A24	GG	83R
A69=-A30/RSUBJ	GG	84R
A70=2.0*A12/P	GG	85R
A71=A70/(RSUBI*RSUBJ)	GG	86R
A72=A68*(A69+A71)	GG	87R
A73=2.0*FN*FN*FN*FN/A24	GG	88R
A74=-2.0*A32/P	GG	89R
A75=A74/(RSUBI*RSUBJ)	GG	90R
A76=A73*A75	GG	91R
HOFP=A41+A45+A49+A55+A60+A62+A65+A67+A72+A76	GG	92R
IF(JP-1) 1055,1055,1056	GG	44
1055 HOFP = HOFP	GG	45
1056 CINT(JP) = HOFP*DSIN(P*Z)	GG	46

A47=A46*A11	GG	50
A48=2.*FN*FN*A40*A11/P	GG	51
A49=A15/FN	GG	52
A50=A49*(A19+A45+A67+A48)		
A51=-2.*FKU1*FIN*(A46*A14*(2.*A22)+FN*A40*A11/P)	GG	53
A52=1.01*A46*A18*A36*(16.*A24*A22*A28)		
A53=1./A9		
A54=FN*P*20*A40*A10/(8.*A24*A28)	GG	54
A55=A43/A42		
A56=SUBJ*RSUBJ*A53*A35		
A57=A55-2.*A44+2.*A56		
A58=A54*A57		
A59=P*20*A37*A9/(4.*A23*A28)	GG	55
A60=A35/A22	GG	56
A61=A34/A22	GG	57
A62=A59*(A60+A61-A55)	GG	58
A63=FN*FN*P*A19*A49*A9/(4.*A23*A28)	GG	59
A64=-A63+A55+A56	GG	60
A65=A63*A64	GG	61
A66=FN*P*A19*A49*A9/(2.*A22*A28)	GG	62
A67=A50/A22	GG	63
A68=A55/A22	GG	64
A69=A47/A22	GG	65
A70=SUBJ*RSUBJ*A11	GG	66
A71=A1*RSUBJ*RSUBJ	GG	67
A72=A71*A13*A53	GG	68
A73=A70*(A71+A72-A73+A72)	GG	69
HDFP=A50+A51+A52+A58+A62+A65+A73	GG	71A
FF(JP-1) 1057,1057,1058	GG	72
1058 FHJFF=HDFP	GG	73
1058 CINT(JP) = HDFP*OSIN(P*Z)	GG	74

38 CONTINUE	TG	0364
CESUM = 0.	TG	0365
COSUM = 0.	TG	0366
DO 39 JP=1, MAXJP,2	TG	0367
39 CESUM = CESUM + CINT(JP)	TG	0368
CESUM = CESUM - (CINT(1) + CINT(MAXJP))/2.	TG	0369
DO 81 JP =2, MAXJP1, 2	TG	0370
81 COSUM = COSUM + CINT(JP)	TG	0371
IF (THETA) 82, 83, 82	TG	0372
83 CINTG = DELP *(BETA*CESUM + GAMMA * COSUM)	TG	0373
BJ=MAXJ	TG	0374
B = A + BJ *DELP	TG	0375
GO TO 84	TG	0376
82 BJ=MAXJ	TG	0377
B = A + BJ *DELP	TG	0378
SINZA =DSIN(Z*A)	DP	0379
SINZB =DSIN(Z*B)	DP	0380
COSZA =DCOS(Z*A)	DP	0381
COSZB =DCOS(Z*B)	DP	0382
CINTG = DELP*(-ALPHA*(CINT(MAXJP)*COSZB/SINZB - FHDFP*COSZA)	GG	75
+ BETA*CESUM + GAMMA*COSUM)	GG	76
1		
84 TINTG = TINTG + CINTG	TG	0385
TNNIG = TNNIG + CINTG	TG	0386
DO 85 JP = 1, MAXJP	TG	0387
85 ACINT(JP) = DABS(CINT(JP))	DP	0388
TOPINT = 0.	TG	0389
DO 85 JP=1,MAXJP	TG	0390
IF (TOPINT-ACINT(JP))87,86,86	TG	0391

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R7 TOPINT = ACINT (JP)
R6 CONTINUE
  BJ=MAXJ
  RECTA=DELP*BJ *TOPINT*(1.+2. * RSUBI*RSURJ)
  RATIOI = RECTA /DABS(TNNTG)
  GO TO (88,89,88), JUNCT
R8 WRITE (6,13) N
  WRITE (6,18) A, DELP, B, (CINT(JP), JP=1,MAXJP)
  WRITE (6,19) CESUM, COSUM, CINTG, TINTG, TOPINT,
  IRECTA, RATIOI
R9 A=R
  BJ=MAXJ
  B= A + BJ *DELP
  IF(B-PMAX)90,90,91
R90 IF(TESTI-RATIOI)30,30,91
R91 CYLL = CYL
  CYL = CYL +2.*TINTG
  CYLPHI = CYLPHI + 2.0*DCOS(FN*PHI)*TINTG
  RATIOS = 2.0*(1.0+4.0*RSUBI*RSURJ)*DABS(TINTG/CYLL)
  GO TO (92,93, 92),JUNCT
R92 WRITE (6,17) N, TINTG, CYL, RATIOS
R93 IF(TESTS-RATIOS)31,65,65
R31 CONTINUE
C COMPUTES CVEL
R65 CVEL = 3./(2.*3.14159265)* CYLPHI
  PRODD = (1.-RSUBI)*CVEL
  PRODD = (1.-RSUBI)*CYLPHI
  WRITE (6,11) XSUBI, YSUBI, ZSUBI, XSUBJ, YSUBJ, ZSUBJ,
  IRSUBI, RSURJ, PHI, ALPHA, BETA, GAMMA
  WRITE (6,1234) PRODD, PRODD
R1234 FORMAT (6H0PRODD=E15.8,3X,7H PRODD=E15.8)
  WRITE (6,555) TNNTG,TINTG,CYLPHI,CYLL,CYL,N,
  IRATIOS,R,RATIOI,CVEL,PRODD,RSUBI
R555 FORMAT(140/7HOTNNTG=E15.8,3X, 7H TINTG=E15.8,3X, 8H CYLPHI=E15.8
  1/ 6HOCYLL=E15.8,3X, 5H CYL=E15.8,3X, 3H N=12/ 8HORATIOS=E15.8,
  23X, 3H B=E15.8, 3X, 8H RATIOI=E15.8/ 6HOCVEL=E15.8,5X,
  36H PRODD=E15.8,3X,7H RSUBI=E15.8)
  WRITE (6,685) MAXJ,MAXN,JUNCT,DELP,TESTI,TESTS,PMAX
R685 FORMAT(140/6HOMAXJ=12,3X, 6H MAXN=12,3X, 7H JUNCT=11/ 6HODELP=E15.
  18,3X, 7H TESTI=E15.8,3X, 7H TESTS=E15.8,3X, 6H PMAX=E15.8)
  GO TO (94,95, 94), JUNCT
R94 WRITE (6,101) N, CVEL
R95 RETURN
C THIS PROGRAM COMPUTES EOFBETA
  END
C
C .....
C
C SUBROUTINE BESK
C
C COMPUTE THE K BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER
C
C USAGE
C CALL BESK(X,N,BK,IER)
C
C DESCRIPTION OF PARAMETERS
C X -THE ARGUMENT OF THE K BESSEL FUNCTION DESIRED
C N -THE ORDER OF THE K BESSEL FUNCTION DESIRED
C BK -THE RESULTANT K BESSEL FUNCTION
C IER-RESULTANT ERPR CODE WHERE
C IER=0 NO ERROR

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TG 0392
TG 0393
TG 0394
TG 0395
DP 0396
TG 0397
TG 0398
TG 0399
TG 0400
TG 0401
TG 0402
TG 0403
TG 0404
TG 0405
TG 0406
TG 0407
TG 0408
DP 0409
DP 0410
TG 0411
TG 0412
TG 0413
TG 0414
TG 0415
GG 77
GG 78
TG 0418
TG 0419
GG 79
GG 80
TG 0422
GG 81
TG 0424
TG 0425
TG 0426
GG 82
TG 0428
TG 0429
TG 0430
TG 0431
TG 0432
TG 0433
TG 0434
TG 0435
TG 0436
TG 0437
TG 0438
TG 0439
TG 0440
TG 0441
TG 0442
TG 0443
TG 0444
TG 0445
TG 0446
TG 0447
TG 0448
TG 0449
TG 0450

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C          IER=1  N IS NEGATIVE          TG 0451
C          IER=2  X IS ZERO OR NEGATIVE  TG 0452
C
C          REMARKS                        TG 0453
C          N MUST BE GREATER THAN OR EQUAL TO ZERO      TG 0454
C          X SHOULD BE LESS THAN 60 TO AVOID EXCEEDING THE RANGE OF
C          THE MACHINE                               TG 0455
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  TG 0456
C          NONE                                       TG 0457
C
C          METHOD                                     TG 0458
C          COMPUTES ZERO ORDER AND FIRST ORDER BESSEL FUNCTIONS USING
C          SERIES APPROXIMATIONS AND THEN COMPUTES N TH ORDER FUNCTION
C          USING RECURRENCE RELATION.                TG 0459
C          RECURRENCE RELATION AND POLYNOMIAL APPROXIMATION TECHNIQUE
C          AS DESCRIBED BY A.J.M.HITCHCOCK, @POLYNOMIAL APPROXIMATIONS
C          TO BESSEL FUNCTIONS OF ORDER ZERO AND ONE AND TO RELATED
C          FUNCTIONS@, M.T.A.C., V.11,1957,PP.86-88, AND G.N. WATSON,
C          @A TREATISE ON THE THEORY OF BESSEL FUNCTIONS@, CAMBRIDGE
C          UNIVERSITY PRESS, 1958, P. 62              TG 0460
C
C          .....                                TG 0461
C
C          SUBROUTINE BESK(X,N,BK,IER)                TG 0462
C          IMPLICIT REAL*8(A-H,O-Z)                   TG 0463
C          DIMENSION T(12)                            TG 0464
C          BK=.0                                       TG 0465
C          IF(N)10,11,11                               TG 0466
10  IER=1                                             TG 0467
C          RETURN                                     TG 0468
11  IF(X)12,12,20                                    TG 0469
12  IER=2                                             TG 0470
C          RETURN                                     TG 0471
20  IER=0                                             TG 0472
C          IF(X-1.)36,36,25                           TG 0473
25  A=DEXP(-X)                                        TG 0474
C          B=1./X                                      TG 0475
C          C=OSQRT(B)                                  TG 0476
C          T(1)=B                                       TG 0477
C          DO 26 L=2,12                                 TG 0478
26  T(L)=T(L-1)*B                                    TG 0479
C          IF(N-1)27,29,27                             TG 0480
C
C          COMPUTE K0 USING POLYNOMIAL APPROXIMATION  TG 0481
C
C          27 G0=A*(1.25331414-.15666418*T(1)+.088111278*T(2)-.091390954*T(3)
C          2+.13445962*T(4)-.22998503*T(5)+.37924097*T(6)-.52472773*T(7)
C          3+.55753684*T(8)-.42626329*T(9)+.21845181*T(10)-.066809767*T(11)
C          4+.009189383*T(12))*C                       TG 0482
C          IF(N)20,28,29                               TG 0483
28  BK=G0                                             TG 0484
C          RETURN                                     TG 0485
C
C          COMPUTE K1 USING POLYNOMIAL APPROXIMATION  TG 0486
C
C          29 G1=A*(1.2533141+.46999270*T(1)-.14685830*T(2)+.12804266*T(3)
C          2-.17364315*T(4)+.28476181*T(5)-.45943421*T(6)+.62833907*T(7)
C          3-.66322954*T(8)+.50502386*T(9)-.25313038*T(10)+.078800012*T(11)
C          4-.010824177*T(12))*C                       TG 0487
C          IF(N-1)20,30,31                             TG 0488

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30	BK=G1	TG 0511
	RETURN	TG 0512
C		TG 0513
C	FROM K0,K1 COMPUTE KN USING RECURRENCE RELATION	TG 0514
C		TG 0515
31	DO 35 J=2,N	TG 0516
	GJ=2.*(FLOAT(J)-1.)*G1/X+G0	TG 0517
	G0=G1	TG 0518
35	G1=GJ	TG 0519
	BK=GJ	TG 0520
	RETURN	TG 0521
36	B=X/2.	TG 0522
	A=.57721566 +DLOG(B)	DP 0523
	C=B**B	TG 0524
	IF(N-1)37,43,37	TG 0525
C		TG 0526
C	COMPUTE K0 USING SERIES EXPANSION	TG 0527
C		TG 0528
37	G0=-A	TG 0529
	X2J=1.	TG 0530
	FACT=1.	TG 0531
	HJ=.0	TG 0532
	DO 40 J=1,6	TG 0533
	RJ=1./FLOAT(J)	TG 0534
	X2J=X2J*C	TG 0535
	FACT=FACT*RJ*RJ	TG 0536
	HJ=HJ+RJ	TG 0537
40	G0=G0+X2J*FACT*(HJ-A)	TG 0538
	IF(N)43,42,43	TG 0539
42	BK=G0	TG 0540
	RETURN	TG 0541
C		TG 0542
C	COMPUTE K1 USING SERIES EXPANSION	TG 0543
C		TG 0544
43	X2J=3	TG 0545
	FACT=1.	TG 0546
	HJ=1.	TG 0547
	G1=1./X+X2J*(.5+A-HJ)	TG 0548
	DO 50 J=2,8	TG 0549
	X2J=X2J*C	TG 0550
	RJ=1./FLOAT(J)	TG 0551
	FACT=FACT*RJ*RJ	TG 0552
	HJ=HJ+RJ	TG 0553
50	G1=G1+X2J*FACT*(.5+(A-HJ)*FLOAT(J))	TG 0554
	IF(N-1)31,52,31	TG 0555
52	BK=G1	TG 0556
	RETURN	TG 0557
	END	TG 0558
C		TG 0559
C	.....	TG 0560
C		TG 0561
C	SUBROUTINE BESI	TG 0562
C		TG 0563
C	PURPOSE	TG 0564
C	COMPUTE THE I BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER	TG 0565
C		TG 0566
C	USAGE	TG 0567
C	CALL BESI(X,N,BI,IER)	TG 0568
C		TG 0569
C	DESCRIPTION OF PARAMETERS	TG 0570
C	X -THE ARGUMENT OF THE I BESSEL FUNCTION DESIRED	TG 0571

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C      N -THE ORDER OF THE I BESSEL FUNCTION DESIRED          TG 0572
C      RI -THE RESULTANT I BESSEL FUNCTION                   TG 0573
C      IER-RESULTANT ERROR CODE WHERE                        TG 0574
C      IER=0 NO ERROR                                       TG 0575
C      IER=1 N IS NEGATIVE                                  TG 0576
C      IER=2 X IS NEGATIVE                                  TG 0577
C                                                           TG 0578
C      REMARKS                                               TG 0579
C      N MUST BE GREATER THAN OR EQUAL TO ZERO              TG 0580
C      X SHOULD BE LESS THAN 60 TO AVOID EXCEEDING THE RANGE OF
C      THE MACHINE                                           TG 0581
C                                                           TG 0582
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED          TG 0583
C      NONE                                                  TG 0584
C                                                           TG 0585
C      METHOD                                                 TG 0586
C      COMPUTES ZERO ORDER AND FIRST ORDER BESSEL FUNCTIONS USING
C      SERIES APPROXIMATIONS AND THEN COMPUTES N-TH ORDER FUNCTION
C      USING RECURRENCE RELATION.                            TG 0587
C                                                           TG 0588
C                                                           TG 0589
C                                                           TG 0590
C                                                           TG 0591
C      .....                                               TG 0592
C      SUBROUTINE BESI(X,N,RI,IER)                            TG 0593
C      IMPLICIT REAL*8(A-H,O-Z)                               TG 0594
C                                                           DP   DP
C      CHECK FOR ERRORS IN N AND X AND EXIT IF ANY ARE PRESENT
C                                                           TG 0595
C                                                           TG 0596
C                                                           TG 0597
C      IER=0                                                  TG 0598
C      RI=1.0                                                 TG 0599
C      IF(N)150,15,10                                         TG 0600
C 10 IF(X)160,20,20                                           TG 0601
C 15 IF(X)160,17,20                                           TG 0602
C 17 RETURN                                                  TG 0603
C                                                           TG 0604
C      DEFINE TOLERANCE                                       TG 0605
C                                                           TG 0606
C 20 TOL=1.0D-6                                              DP 0607
C                                                           TG 0608
C      IF ARGUMENT GT 12 AND GT N, USE ASYMPTOTIC FORM      TG 0609
C                                                           TG 0610
C      IF(X-12.)40,40,30                                       TG 0611
C 30 IF(X-FLOAT(N))40,40,110                                   TG 0612
C                                                           TG 0613
C      COMPUTE FIRST TERM OF SERIES AND SET INITIAL VALUE OF THE SUM
C                                                           TG 0614
C                                                           TG 0615
C 40 XX=X/2.                                                 TG 0616
C      FACTN=1.                                               TG 0617
C      IF(N-1)70,70,50                                         TG 0618
C 50 DO 60 I=2,N                                             TG 0619
C      FI=I                                                    TG 0620
C 60 FACTN=FACTN*FI                                           TG 0621
C 70 TERM=(XX**N)/FACTN                                        TG 0622
C      RI=TERM                                                 TG 0623
C      XX=XX*XX                                               TG 0624
C                                                           TG 0625
C      COMPUTE UP TO 30 TERMS, STOPPING WHEN ABS(TERM) LE ABS(SUM OF TERM
C      TIMES TOLERANCE                                       TG 0626
C                                                           TG 0627
C                                                           TG 0628
C      DO 90 K=1,30                                           TG 0629
C      IF(DABS(TERM)-DABS(BI*TOL))100,100,80                 DP 0630
C 80 FK=K*(N+K)                                              TG 0631

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      TERM=TERM*(XX/FK)
90  BI=BI+TERM
C
C      RETURN BI AS ANSWER
C
100 RETURN
C
C      X GT 12 AND X GT N, SO USE ASYMPTOTIC APPROXIMATION
C
110 FN=4*N*N
      XX=1./(8.*X)
      TERM=1.
      BI=1.
      DO 130 K=1,30
      IF(DABS(TERM)-DABS(TOL*BI))140,140,120
120  FK=(2*K-1)**2
      TERM=TERM*XX*(FK-FN)/FLOAT(K)
130  BI=BI+TERM
140  PI=3.141592653
      BI=BI*DEXP(X)/DSQRT(2.0*PI*X)
      GO TO 100
150  IER=1
      GO TO 100
160  IER=2
      GO TO 100
      END

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TG 0632
TG 0633
TG 0634
TG 0635
TG 0636
TG 0637
TG 0638
TG 0639
TG 0640
TG 0641
TG 0642
TG 0643
TG 0644
TG 0645
DP 0646
TG 0647
TG 0648
TG 0649
TG 0650
DP 0651
TG 0652
TG 0653
TG 0654
TG 0655
TG 0656
TG 0657

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DERIVATION OF EQUATION (6.1) FROM GREENSTEIN'S  
EXPRESSION FOR  $\vec{v}^{2LS_2}$  VELOCITY FIELD

Greenstein<sup>(4)</sup> provides the following expression for the  $\vec{v}^{2LS_2}$  velocity field if only translation is considered:

$$\vec{v}^{2LS_2} = \vec{i} \left( \frac{1}{2} A r^{-1} \sin \psi \cos \psi \right) + \vec{k} \left( A r^{-1} \sin^2 \psi + \frac{A}{2} r^{-1} \cos^2 \psi \right) \quad (\text{A.3.1})$$

where

$$A = \frac{3}{2} aU \quad (\text{A.3.2})$$

Therefore:

$$\vec{F}_x^{2S_1} = 6\pi\mu a (\vec{v}_x^{2LS_2}) = 6\pi\mu a \left( \frac{3U}{4} \frac{a}{r} \sin \psi \cos \psi \right) \quad (\text{A.3.3})$$

and

$$\vec{F}_z^{2S_1} = 6\pi\mu a (\vec{v}_z^{2LS_2}) = 6\pi\mu a \left( \frac{3U}{2} \frac{a}{r} \sin^2 \psi + \frac{3U}{4} \frac{a}{r} \cos^2 \psi \right) \quad (\text{A.3.4})$$

Also, from Stokes law:

$$F_z^{1S_1} = 6\pi\mu aU \quad (\text{A.3.5})$$

Computing  $\epsilon$ , the angle of deflection:

$$\tan \epsilon = \frac{\vec{F}_x^{II}}{\vec{F}_z^{II}} = \frac{6\pi\mu aU \left( \frac{3}{4} \frac{a}{r} \sin \psi \cos \psi \right)}{6\pi\mu aU \left( 1 + \frac{3}{2} \frac{a}{r} \sin^2 \psi + \frac{3}{4} \frac{a}{r} \cos^2 \psi \right)} \quad (\text{A.3.6})$$

The denominator of equation (A.3.6) can be simplified to:

$$1 + \frac{3}{2} \frac{a}{r} (\sin^2 \psi + \cos^2 \psi) - \frac{3}{4} \frac{a}{r} \cos^2 \psi = 1 + \frac{3}{2} \frac{a}{r} - \frac{3}{4} \frac{a}{r} \cos^2 \psi \quad (\text{A.3.7})$$

Hence,

$$\tan \epsilon = \frac{\frac{3}{4} \frac{a}{r} \sin \psi \cos \psi}{1 + \frac{3}{2} \frac{a}{r} - \frac{3}{4} \frac{a}{r} \cos^2 \psi} \quad (\text{A.3.8})$$

Dividing the denominator into the numerator, we obtain:

$$\tan \epsilon = \frac{3}{4} \frac{a}{r} \sin \psi \cos \psi - \frac{9}{8} \frac{a^2}{r^2} \sin \psi \cos \psi + \frac{9}{16} \frac{a^2}{r^2} \sin \psi \cos^3 \psi + \dots \quad (\text{A.3.9})$$

Neglecting the third term on the right hand side of equation

(A.3.9) and subsequent higher order terms, we obtain:

$$\tan \epsilon \approx \frac{3}{4} \frac{a}{r} \left( 1 - \frac{3}{2} \frac{a}{r} \right) \sin \psi \cos \psi \quad (\text{A.3.10})$$

Furthermore, since  $\epsilon$  is small,  $\tan \epsilon$  is approximately equal to  $\sin \epsilon$ . Therefore,

$$\sin \epsilon \approx \frac{3}{4} \frac{a}{r} \left( 1 - \frac{3}{2} \frac{a}{r} \right) \sin \psi \cos \psi \quad (\text{A.3.11})$$

which is the equation (6.1), given by Smoluchowski.