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THE THREE PLASE SYSTEM

N-HEXANE - ANILINE - WATER

BY

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#### A THESIS SUBMITTED TO THE FACULTY OF THE DEPARTMENT OF CHEMICAL ENGINEERING OF NEWARK COLLEGE OF ENGINEERING

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#### ABSTRACT OF THESIS

This is a study of the three phase system - n-Hexane - Aniline - Water at  $50^{\circ}$  Centigrade. The data obtained, coupled with data previously established at  $3C^{\circ}$  Centigrade is used to predict a means of recovering aniline from 3-5% aqueous solutions by scrubbing with n-hexane.

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#### EXPERIMENTAL

#### 1. Materials

The n-hexane used was high purity material obtained from Mathieson Company, Inc. It was redistilled through a 24 inch column of 1 inch diameter, packed with 1/8 inch State College Packing. The fraction collected had a boiling point of 155.7°-156.7°F. and a specific gravity of 0.649 at 70°F. This compares with the boiling point of 158°F. and specific gravity of 0.660 at 20°C. found in the literature.<sup>10</sup>. It was stored over sodium hydroxide pellets to assure freedom from moisture.

The aniline was high purity material obtained from Mathieson Company, Inc. It was redistilled from zinc dust and carbon black in a 2h inch column, of 1 inch diameter, packed with 1/8 inch State College Facking. The fraction collected had a boiling point of 183° - 184°C. and a specific gravity of 1.012 at 70°F. This compares with the boiling point of 184.4°C. and a specific gravity of 1.0236 at 20°C. found in the literature.<sup>19</sup>. It was stored over sodium hydroxide to assure freedom from moisture. The color of the aniline was water white.

The laboratory supply of distilled water was used.

#### 2. Determination of Binary and Ternary Solubilities - Volumetric

The three-phase system solubilities were determined by cloud point procedure whose reliability is affirmed by the reproduceability of results in this investigation, and by Greshes, <sup>17.</sup> Seaman, et. al.<sup>20.</sup> and Sidgwick, et. al.<sup>12.</sup>

### TABLE 1

# EXPERIMENTAL DATA

<u>Binary Systems</u> :	(duplicate deter	minations)	
Temperature	ml. Water	rl Ani ine	nl n-llexane
50°	20.0	0.05	0.0
50°	20.0	0.80	0.0
50°	20.0	0.80	0.0
50°	1.350	20.0	0.0
50°	1.325	20.0	0.0
50°	1.350	20.0	0.0
50°	0.0	2.45	20₊0
	0.0	2.40	20₊0
50°	0.0	2.40	20 <b>.</b> 0
50°	0.0	2.40	20 <b>.</b> 0
50°	0.025	0.0	20 <b>.</b> 0
50°	0.025	0.0	20 <b>.</b> 0
50°	20.0	0.0	0,05
50°	20.0	0.0	0,05
50 <b>°</b>	0.0	<b>20.0</b>	4.30
50°	0.0	20.0	4.75

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### TABLE 2

### EXPERIMENTAL DATA

### Ternary Systems: (duplicate determinations)

# A. Water and Aniline; add n-Hexane

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Temperature	ml Water	ml Aniline	al n-Hexane
50°	20.0	0.10	0,30
50°	20.0	0,10	0.25
50°	20.0	0,30	0.25
500	20.0	0.30	0.30
50°	30.0	1.00	0.30
50°	30.0	1.00	0.35
B. n-Hexane ar	nd Amiline; add Wat	tor	
500	0.20	0.10	20.0
50°	0.20	0,10	20.0
50°	0.15	0.50	20.0
500	0.20	0.50	20.0
50°	0.10	1.00	20.0
50°	0,15	1.00	20.0
C. Aniline and	Water; add n-Hexa	ine	
50°	0.50	20.0	3.9
500	0.50	20.0	3.8
50°	0.{0	20.0	3-2
50°	0.00	20.0	3.2
50°	1.00	20.0	3.0
500	1.00	20.0	3.0
D. Aniline and	n-Hexane; add Wa	ter	
50 <b>°</b>	1.20	20.0	1_0
500	1.10	20,0	1.0
50°	0,90	20.0	2.0
50°	0,90	20.0	2,0
50°	0.80	20.0	3.0
509	0.75	20,0	3.0
500	0.60	20.0	1.0
500	0.55	20.0	4.0

# TABLE 2 (continued)

### EXPERIMENTAL DATA

#### Ternary Systems:

E. Aniline and n-Hexane; add Water (gravimetric - single determinations)

Temperaiure	Water	Aniline		n-Hexane	
	ml	nl	weight	nl	weight
50 <b>°</b>	1.10	20.0	20.2345g.	1.0	0.6721g.
50 <b>°</b>	0.35	20.0	20.2391g.	2.0	1.3440g.
50°	0.75	20.0	20 <b>.2386g.</b>	3.0	2.0060g.
50°	0,60	20.0	20.237 g.	4.0	2.6876g.

#### INTRODUCTION

In the manufacture of aniline, the process of separating aniline from water offers considerable difficulty, inconvenience and expense.

The usual method of manufacturing aniline involves the reduction of nitrobenzene with iron filings and hydrochloric acid. \* 1,2, The reduction is carried out in a reaction vessel under reflux. The reaction is continued until the reduction is complete. The mixture is steam distilled; and on condensing the vapors an emulsion is obtained which comprises wet aniline and ani ine in water. This method, still used by many manufacturers, gives rise to large quantities of aniline water and requires large expenditures and losses in processing. The aniline is removed from the separator and sont to the rectifier for purification and removal of water. The amiline water (4,960 lbs, water containing 3-5% aniline is obtained per 860 lbs. of aniline<sup>1</sup>.) is treated in varying ways to recover the aniline.<sup>3,4</sup>. These include, (a) distillation of the aniline which, however, requires large expenditures in steam; (b) extraction with nitrobenzene which is used in the next reduction, but this necessitates a large number of tanks and is in general a cumbersome method; and (c) return of aniline water to the boilor generating steam for use in steam distillation. This last operation, though quite simple, has not found wide application.

A solvent extraction system hight be developed which would

\* References to the literature are listed on page 28.

effectively and inexpensively recover the aniline from the aniline water. The present investigation was undertaken to obtain additional data on an aniline - n-hexane - water system preliminary to prediction and design of a counterflow liquid-phase seperation process for the extraction of aniline water ( and from water saturated aniline).

Drucker<sup>5</sup>. determined some liquid-phase equilibrium for the aniline n-hexane - water system but his interests lay in determining the change in critical solubility temperature and so covered only a small, inadequate fraction of the particular system. Rinary solubilities have been recorded for the systems water-aniline<sup>6,7,8,9,10,11,12</sup>; anilinen-hexane<sup>5,13,14</sup> and n-hexane-water.<sup>15,16</sup>

The following investigation was made to extend the work by Greshes<sup>17</sup>. who studied the system aniline - n-hexane - water over a wide concentration range at  $36^{\circ}$ C. Although extreme care had to be exercised in making binary determinations, his results showed good agreement with data found in the literature. The tie lines obtained by Greshes and in this study were also in good agreement. The extraction ratio found by Greshes for the system at  $36^{\circ}$ C. was equal to 2:1 and is exactly the same as that found in this study of the system at  $50^{\circ}$ C. The binary data comparison is shown in Table 11 on page 26.

Four bottles containing the pure components of the system were placed in a constant temperature bath for a few hours prior to running the cloud point determinations and brought to operating temperature. The bath temperature was maintained within 0.5° of 50°C. by a mercury column thermostat, relay and electric heaters. When running binary mixtures, the primary component was accurately pipetted into a glass-stoppered flask and inversed in the bath until bath temperature had been reached. The secondary component was then titrated slowly from a 10 ml micro-burette and the flask was shaken after each incremental a dition and replaced in the bath until operatin temperature was again reached. At the first sign of clouding, the titration as stopped and the sample shaken and irrersed for 30 minutes to make certain the system was at equilibrium. This was continued until a permanent cloud was obtained. The ternary systems were run in a similar manner except that the two primary compoments were added in a single phase region, th the flask together and the ternary component was titrated, as described, from the microburette.

All runs were in duplicate except for four tests on the aniline and n-hexane plus water system which were measured gravimetrically as checks on the volumetric determinations of solubility in the aniline phase.

The experimental data thus obtained is listed in Mables 1 and 2. In the binary mixtures the primary component has the larger volume (20 - 30 ml). The secondary, titrited, component is in all cases

the lesser amount. The sub-heading of the ternary systems indicate the two primary and ternary components. "Aniline and water; add n-hexane" for example, means the aniline and water are the two primary components and the n-hexane is the titrated, ternary, component. 3. Determination of Three-Phase System Solubilities - Gravimetric As a check on the reliability of the method and on that phase of the procedure wherein volumetric measure was used to determine percentage concentrations, h additional samples were run using weight measurements. Specific volumes of aniline and n-hexane were inroduced into tared bottles from a burette and the weight of each component was recorded. Water was then added until the cloud point was reached and the weight of the water recorded. These cloud point determinations compared very favorably with those previously determined by volumetric measurements.

The data which resulted is recorded in Table 2.

#### 4. Determination of Conjugate and Tie lanes.

The tie lines and three-phase conjugate lines were obtained by charging known mixtures of the three components to graduated cylinders, agitating during the course of 12 - 14 hours and then allowing the phases to separate, all in the constant temperature bath. Samples of the individual phases were pipetted, weighed, accurately diluted with methanol and analyzed for aniline by spectrophotometer in the ultraviolet range. Since the aniline concentration locates a point on a phase boundary curve, this figure is used to pick off the remaining percentages of water and hexane from the equilibrium curves represented by Figures h, 5 and 6. Thus, the entire composition becomes available. The sum of the aniline content of the phases agreed with the quantity of aniline charged.

The aniline analysis was performed on a Beckman Model DU Juartz

spectrophotometer at a wave length of 290 mu.<sup>21.</sup> The proper wave length was determined by plotting the percent transmission of a sample containing 0.0020g aniline per 100 :1. of methanol against the wavelengths in the ultraviolet range (Figure 2). The wavelength selecter for the calibration (290mu) was that wave length which fell just to the right of the minimum at 265 mu. The spectrophotometer was calibrated at 290 mu between 0.001g./100 ml and 0.003g./100ml.

The experimental data are summarized in Tables 3, 4 and 5 and in Figures 1, 2 and 3. Table 3 describes the calibration of the Beckman spectrophotometer for the aniline analysis. Tables 4 and 5 describe the determination of the three-phase conjugate lines and tie lines respectively. Figures 1 and 3 represent part (a) of Table 3 plotted on semi-log and rectangular coordinate paper. Figure 2 represents part (b) of Table 3.

A sample calculation of the data contained in Tables 3 and 4 follows:

Basis: Data for aniline of sample no. 1, Table 4.
1. Original volume of aniline introduced 10.0 ml.
2. Final volu e of aniline at equilibrium 10.0 ml.
3. Aliquot of aniline layer taken for analysis 5.0 ml.
4.2810 ml.

5. Dilutions of 5 :1. aliquot:

a. 5 ml aliquot diluted to 100 ml. with methanol.

b. 5 ml of mixture a diluted to 100 ml with methanol.

c. 5 ml of mixture b diluted to 100 vil with methanol.

d. 5 ml of mixture c diluted to 100 ml with methanol.

6. Spetrophotometer reading of sample 5d. 70.0% transmission.

#### TABLE 3

#### EXPERIMENTAL DATA

Beckman Spectrophotometer Calibration

A. Calibration at 290 mu (Figure 1 and Figure 3).

Concentration g/100 ml.	§ Transmission
0.00100	52.5
0.00150	3: .5
0.00200	28.0
0.00225	23.0
0,00250	19.0
0,00300	16.0

B. Determination of Wavelength (concentration = 0.00200 g/100ml) (Figure 2)

Wavelength	Z Transmission
215	8.5
218	6.5
220	5.1
225	2.5
2:00	1.0
21,0	1.0
243	2.0
21.7	5.2
249	€ <b>.</b> 0
250	10.5
25	27.0
260	37.5
265	36.5
270	31.0
275	26.2
500	23.5
215	24.0
290	20.0
300	50.0
310	(2.0
330	9°•5





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### TABLE 4

#### EXPERIMENTAL DATA

#### Three Mase Idne Data

### 1. Original Volumes of Material Introduced.

Sample N	o. ml Water	ml Aniline	al. n-Hexane
1.	10,0	10.0	10.0
2.	10.0	10.0	20.0
3.	10.0	0.01	30.0
4.	20.0	10.01	10.0
5.	10.0	10.0	20.0
6.	20.0	10.0	10.0
2. Fina	l Volumes at Equilibri	um	
1.	10,0	10.0	10.0
2.	10.0	10.0	20.0
3.	10.0	9,0	31.0
4.	20.0	9.0	11.0
5.	10,0	9.0	21.0
$\epsilon_{*}$	20,5	9.5	10*0

### 3. Weights of 5 ml. Aliquots at Equilibrium Used for Analysis

of Amiline

1.	5.2025	4.3810	3.2400
2.	5.1066	4.9635	3.21,96
3.	5.0081	4.9891	3.2580
4.	5.1360	4.9606	3.2404
5.	5.0943	4.9314	3.2401
6.	5.1013	5.0374	3.25.1

4. Dilutions of Each Sample in 3 above

Sample		Total Dilution
(1)	Hexane	1/0000
(1)	Aniline	1/160,000
(1)	Mater	1/000
(2)	Hexane	1/2000
(2)	Aniline	1/160,000
(2)	Water	1/2000

### TABLE 4 (Continued)

### EXPERIMENTAL DATA

# 4. Dilutions of Each Sample in 3 above

Sample	Total Dilution
<ul><li>(3) Hexane</li><li>(3) Aniline</li><li>(3) Water</li></ul>	1/8000 1/160,000 1/8000
(14) Nexune (14) Aniline (14) Mater	1/8000 1/160,000 1/3000
(5) Hexane (5) Aniline (5) Water	1/3000 1/160,000 1/3000
<ul><li>(6) Hexane</li><li>(6) Aniline</li><li>(6) Water</li></ul>	1/:000 1/160,000 1/?000

### 5. Spectrophotometer Reading of Last Diluted Sample Above

Sample No.	5 Transmission Hexane Layer	Ani ine Layer	ZTransmission Mater Layer
1.	72.0	70.0	72.0
2.	62.0	70.5	72.0
3.	55.0	70.5	34.0
****	73.0	69.5	73.0
5.	52.5	70.5	75.0
6.	72.5	69.0	73.5

### TARLE 5

#### EXPERIMENTAL DATA

#### Tie Lines

1. Original Volumes of Material Introduced.

Samp	ole No.	ml. Water	ml. Aniline	al. n-liexane
	1. 2.	20 <b>.0</b> 15 <b>.</b> 0	0.50 2.00	20.0 30.0
2.	Final Volumes	at Equilibria	lm	
	1.	20.25 16.00	ब्राह्म नाम् व्याप्त नाम्	20 <b>.</b> 25 31.00
3.	Weight of 5 ml	Aliquots at	Equilibrium used for	Analysis of Aniline
	1. 2.	5.0254 5.1042	and the system	3.2491 3.2405
4.	Dilutions of 1	ach Sample ir	1 3 Above	

01	BOON SUMPLE IN 2 ROOVE	
	Sample	Total Dilution
1.	<b>n-Hexane</b> Water	3/2000 3/2000
2. 2.	n-Hexane Water	3/20,000 3/20,000

### 5. Spectrophotometor Reading of Last Diluted Sample Above

Sample	7 Transmission Hexane Layer	<u> % Transmission</u> <u>Mater Layer</u>
1.	29 <b>.0</b>	46.0
2.	57 <b>.</b> 0	73.5

#### RESULTS

#### 1. Three-Phase System Solubilities

The results of the three-phase solubilities of the n-hexane aniline - water system at  $50^{\circ}$ C. are summarized in Tables 6, 7 and 0 and in Figures 4, 5, 6 and 7. The data of Tables 6, 7 and 3 are represented in Figures 4, 5 and 6 respectively, and these represent the water, n-hexane and aniline phases respectively. All three plots are on the same scale. Figure 7 contains a composite of all three systems on a small scale.

A sample calculation of the data contained in these tables follows:

water

Basis: Data for percent water, and ine and n-hexane in the water phase of sample no. 2, Table 6.

1.	Volume of n-hexane (from Table 1)	0.3 ml.
2.	Specific gravity of n-hexane (from Table 2)	0.649g/ml.
3.	Weight of n-hexane $(0.3 \times 0.649)$	0.19g.
4.	Volume of amiline (from Table 1)	0,1 ml.
5.	Specific gravity of aniline (from Table 2)	1.012g/ml.
6.	Weight of amiline (0.1 x 1.012)	0.106.
7.	Volume of water (from Table 1)	20.0 ml.
ĉ.	Specific gravity of water (from Table 2)	1.00g/ml.
9.	Weight of water (20.0 x 1.00)	20.00E.
10.	Total weight of sample:	
	n-hexane aniline	0,19

- 12. Weight percent aniline (0.10/20.29) 0.5%
- 13. Weight percent water (20.0/20.29) 98.6%

### TANE 6

WEIGHT PERCENTROED OF THE VARIOUS COMPONENTS AT EQUILIBRIUM

(duplicate determinations)

Water Phase - Weight 3

Water	Aniline	<u>n-llexane</u>
96.1	3•9	0.0
26.1	3•9	0.0
98.6	0.5	0.9
98.6	0.5	0.9
97 <b>.7</b>	1.5	0_8
97 <b>.</b> 7	1.5	0_5
96.1	3 <b>.2</b>	0.7
96.1	3 <b>.</b> 2	0.7
99.0 99.0	0.0 0.0	0.2



### TABLE 7

### MEIGHT PERCENTAGES OF THE VERIOUS COMPONENTS AN EGUILIBEIUM

(duplicate determinations)

Hexano Mase - Weight 5

Mater	Aniline	n-llexane
0.5	0.0	99 <b>.5</b>
0.0	0.0	99 <b>.</b> 5
1.5	0.0	97 <b>.7</b>
1.5	0.0	97 <b>.</b> 7
1.1	3.8	95 <b>.1</b>
1.1	<b>3.</b>	95 <b>.</b> 1
0.7	7.2	92 <b>.1</b>
0.7	7.2	92 <b>.1</b>
0.0	<b>16.</b> 0 16 <b>.</b> 0	04.0 84.0





### TABLE S

#### MEIGHT PERCENTAGES OF THE VARIOUS COMPOLEMES AT EQUILIBRIUM

(duplicate determinations)

### And Line Phase - Weight %

Mater	Aniline	n-llexane
6.3	93 <b>.</b> 7	0 <b>.0</b>
6.3	93 <b>.</b> 7	0 <b>.</b> 0
2*2	87 <b>.</b> 2	10.6
2•2	37 <b>.</b> 2	10.6
3•5	87.6	€ <b>.9</b>
3•5	87.6	3 <b>.9</b>
4.3	37 <b>.3</b>	5.4
4.3	87 <b>.</b> 3	8.4
	91.7 91.7	4.2 4.2
3.7	90 <b>.</b> 2	6.1
3.7	90 <b>.</b> 2	6.1
3.2 3.2	58.4	6.4 8.4
2*3 2*3	8 <b>6.5</b> 96.5	11.2
0.0	86 <b>.6</b>	13.4
0.0	26 <b>.6</b>	13.4

### The 4 samples determined gravimetrically follow:

(single	determinations)	
4.0	92.1	3.2
3.6	90 <b>.</b> 6	5.8
3.5	37.7	· • j
2.5	36.1	11,4





#### 2. Three-Phase Conjugate and Tie Lines

Tables 9 and b) show the aniline concentration and composition of the various phases at equilibrium of the tie lines and conjugate lines. The conjugate and the lines are represented in Figures  $l_i$ , 5, 6 and 7.

The results of Table 10 are obtained by picking off the composition of each phase from the trilinear phase diagrams (Figures 4, 5 and 6) knowing the percent aniline (Column 6, Table 9).

A sample calculation of the results obtained in Table 9 follows:

Basis: Data for n-hexane phase of sample no. 1 of conjugate line, Table 9.

- 1. Original volume of n-hexane introduced 10.0ml. (From Table 4)
- 2. Final volume of n-hexane at equi ibrium 10.0ml. (From Table 4)
- 3. Aliquot of n-hexane layer taken for analysis 5.0ml. (From Table 4)
- 4. Weight of 5 ml aliquot (From Table 4) 3.2400g.
- 5. Dilution of 5 ml aliquot (From Table 4)

a. 5 ml aliquot diluted to 100 ml with methanol.

- b. 5 ml of solution a diluted to 100 ml with methanol.
- c. 5 ml of solution b diluted to 100 ml with methanol.
- 6.. Spectrophotometer reading of diluted solution 5c (From Table 4) 72.0%
- Concentration of aniline in diluted solution <u>5c</u>
   as determined from Figure 1.
   0.0005g/100ml.

3. Concentration of aniline in diluted solution <u>5b</u> (0.0005 x 100/5)
9. Concentration of aniline in diluted solution <u>5a</u> (0.010 x 100/5)
10. Weight of aniline in the 5 ml aliquot (same as total aniline in solution <u>5a</u>).
11. Weight of aniline in the total 10 ml of the n-hexane phase. (0.20 x 2)
12. Percent of aniline in the n-hexane phase

### TABLE 9

# CILCULITED DATA

### THREE CO JUGATE MASE LINE

### Determination of Aniline Concentration

Sample no.	Component	Concentration from Calibration Curve (Figure 1)	Anount in 5 ml of Phase	Total in Phase	<u>3 Composition</u> in Phase
1.	n-hexane	0.00050	0.20	0.40	6.2
	aniline	0.00055	4.40	8.80	90.0
	water	0.00050	0.20	0.40	3.8
2.	n-hexane	0.00075	0.30	1.20	9•2
	ani ine	0.00054	4.32	8.64	87•0
	water	0.00050	0.20	0.40	3•8
3.	n-hexane	0.00092	0.37	2+29	11.3
	aniline	0.00054	4.32	7+78	86.7
	water	0.00025	0.10	0+20	2.0
4.	n-hexans	0 <b>.0004</b> 8	0.19	0.42	5.9
	anilins	0 <b>.00056</b>	4.48	8.06	90.4
	vater	0 <b>.0004</b> 8	0.19	0.76	3.7
5.	n-hexane	0.00080	0.32	1.34	9.9
	aniline	0.00054	1.32	7.73	06.8
	water	0.00043	0.17	0.34	3.3
6.	n-hexane	0.00049	0.19	0.38	6.0
	ani line	0.00057	4.56	8.65	90.4
	water	0.00046	0.18	0.76	3.6
		TIE LINES			
1.	n-haxane	0,00195	0.065	0 <b>.26</b>	2.0
	water	0,00120	0.040	0.162	0.8
2.	n-hexane	0,00088	0.290	1.0	9.0
	water	0,000146	0.150	0.57	3.5

### TABLE 10

#### CALCULATED DATA

### TIREE CONJUGATE PHASE LINE

### Phase Composition At Equilibrium

Anilin Phase - Weight %

Aniline	Hater	n-Hexane
90.0 27.0 56.7 90.4 36.8 90.4	3.6 2.8 2.5 3.6 2.6 3.6	6.4 10.2 10.5 6.0 10.6 6.0
Water Phase - Weight 🖇		
3.8 3.8 2.0 3.7 3.3 3.3 3.6	96.0 96.0 97.1 96.0 96.1 96.0	0.2 0.2 0.9 0.3 0.6 0.4
n-Hexane - Weight %		
6.2 9.2 11.3 5.9 9.9 6.0	0.9 0.6 0.4 0.9 0.5 0.9	92.9 90.2 88.3 93.2 89.6 93.1
	TIR LINES	
Water Phase - weight \$		
0.8 3.5	98.4 96.1	0.8 0.4
n-nexane mase - weight %		
2 <b>.</b> 0 9 <b>.</b> 0	1.3 0.6	96.7 90.4

#### 3. Conclusions

#### a. Accuracy of measurements

The same difficulties were encountered in making cloud point detorminations as those experienced by Greshes.<sup>17.</sup> The cloud points differed in each phase and only in the aniline phase, upon the addition of n-hexane, did a true cloud point appear. All other cloud point detorminations were recorded as the first droplet of the introduced material which floated or settled to the bottom, as the case might be. Although this required a careful and tedious technique, accurate cloud points were obtained which could be duplicated.

The binary data compare favorably with the equivalent data found in the literature.  $11, 1^2, 1_4$ . This is shown by Table 11.

The three phase conjugate lines compare favorably with one another. The tie-lines agree well with the expected results.<sup>17, 22.</sup>

#### b. Distribution data and curve

These data are represented by Figure 3 which is a graphic representation of the tic lines and three phase line data of Table 10. From the slope of the line and the distribution of aniline between n-hexane and water, the relative volume ratio of water to n-hexane for completely scrubbing a 3% ani line in water solution is found to be 1 in 2 at 50°C. plus or minus  $0.5^{\circ}$ C. Significantly, this is the same extraction ratio as that determined by Greshes, <sup>17</sup> for this system at  $36^{\circ}$ C. as shown by Figure 8.

TABLI	5 11
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BINARY	DATA	CIBIP.	RESON
and they will be about the set		~~~~	and the second

	<u>50°(</u>		<u>36°C.</u>			
	Weight <u>%</u>	Weight <u>%</u>	Meight 5	Weight %		
	Aniline	Water	Aniline	Water		
Potosnak	3.9 93.7	96 <b>.1</b> 6 <b>.</b> 3	కిండిగ <b>ు అ</b> దిత	NAME SALES AND A		
Oreshes <sup>17</sup> .	مىلىكە ئىلىمەتكەنىيەتلە مەسىيە ئۆتكەن (1944	400 mar 400	3.5 94.4	96.5 5.6		
Cambell <sup>11.</sup>	4.1	95.9	same was seen	the set		
Sidgwick <sup>12</sup>	4.1	95•9	3•9	96.1		
	93.6	6•4	94•3	5.7		
	Weight 5	We ight 5	Weight %	Weight %		
	Amiline	n-Nexane	Aniline	n-Nexane		
Potosnal:	16.0	84.0	ىلەركى بالەركى بىلىرىنى بىلىرى	-4-4523-4849		
	88.6	11.4	بىلىرىنى بىل	-4-45		
Greahes <sup>17</sup> .	1999 and 1999	adly talk-star	11.0 90.0	09.0 19.0		
Keyes <sup>11</sup> .	18.0	82.0	11.0	89.0		
	36.0	14.0	88.0	12.0		

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#### c. Application

Using the accumulated data we can now define a method for extracting the aniline from a 3-5% water solution. The information in Table 10 is plotted in Figure 9 on an expanded scale. Using this plot, a graphical solution can be used to determine the merber of equilibrium stages required. The graphical solution is given by Figure 10.

**Basis**:

$$X_0 = feed = 0.04$$
  
 $Y_n = final raffinate = 0.003$   
 $Y_n = final raffinate = 0.003$   
 $Y_1 = final extract = 0.06$ 

Solvent to feed ratio is 2:1; therefore, 2 pounds of n-hexane are required to extract 1 pound of aniline-water. This determines the line  $X_nJ_XY_1$ , since  $X_nJ_X : J_XY_1 :: 2:1$ . Hence,  $X_nJ_X = 6.3$ ,  $J_XY_1 =$ 3.15 and thus,  $Y_1$  is found to be 0.06. The intersection of the lines through  $X_nY_n$  plus 1, and XoY1 determines the point.

	Mass Fraction Aniline in Artract	Mass Fraction Amiline in Maffinate		
	Y.	X		
1.	0.06	0.0lé		
2.	0.025	0.0034		
3.	0.015	0.0077		

The extraction would be carried out in countercurrent fushion similar to that in Figure 11. The final extract could be chilled to around  $0^{\circ}$ C, where aniline and hexane would separate completely. The n-hexane removed would be recycled as shown. The extract temperature required to effect this separation remains to be determined from a study of this system at or near  $0^{\circ}$ C.



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FIGURE 11



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#### BIBLIOGR\_FIN

- 1. Immus, U. S. Patent 1603251, October 10, 1926.
- Leigann, "Aniline and Its Derivatives", New York: John Miley & Son (1368).
- 3. Groggins, "Aniline and Its Derivatives", New York: D. VanNostrand & Co., pp. 17, 26, 36-57, (1942).
- 4. Groggins, "Unit Processes in Organic Chordsbry", New York: McGraw-Hill & Co., pp. 9 -105, (1:30).
- 5. Drucker, Recueil des Travaux Chimique des Pays-Bad", <u>42</u>, p. 552, (1923).
- 6. International Gritical Tables, 3, p. 397.
- 7. Applebey and Davis, "Journal of the Chemical Society", London: 127, p. 1836, (1925).
- 6. Alexjew, "Annalen der Hysik und Chemie", 20, p. 305, (1.36).
- Smith and Dremel, "Industrial and Engineering Chemistry", <u>37</u>, p. 601-2, (1945).
- IHLI and Macy, "Journal of the American Chemical Society", <u>16</u>, p. 1132, (1924).
- 11. Campbell, "Journal of the American Chemical Society", <u>67</u>, p. 981, (1945).
- 12. Sidguick, Pickford and Wilsdon, "Journal of the Chemical Society", London, 22, p. 1122, (1911).
- 13. International Critical Tables, 3, p. 327.
- 14. Keys and Hildebrand, "Journal of the American Chemical Society", 32, p. 2127, (1912).
- 15. Chemical Lubber Handbook, Edition 31, pp. 376-7.
- 16. Scidell, "Solubilities of Organic Compounds", New York: D. Van Nostrand - Co., Volume 2.
- 17. Greshes, "The Three Phase System N-Mexane-Anilino-Water", Newark College of Engineering, (June 1951).

- 10. Scheflan and Jacobs, "Handbook of Solvents", New York: D. Van Nostrand Co., Inc., p. 431, (1953).
- 19. Faith, Keyes and Clark, "Industrial Chemicals", New York: John Miley & Sons, Inc., (1950).
- Seaman, Hugonet & Norton, "Industrial & Engineering Chemistry, Analytical Edition", <u>15</u>, p. 322, (1943).
- 21. American Fetroleum Institute Re earch Project Wi, Mational Bureau of Standards.
- 22. Sherwood, "Absorption and Extraction", New York: Mc-Graw-Hill & Co., pp. 241-244, (1937).

Additional References Used:

- 1. Friedl and Orahin, "Ultraviolet Spectra of Organic Compounds", New York: John Wiley & Sons, Inc., (1951).
- 2. Brown, et al, "Unit Operations", New York: John Wiley : Sons Inc., (1950).
- 3. Tyler, "Chemical Engineering Lonomics", New York: McGraw-Hill Co, Inc., (1931).
- 4. Alders, "Liquid-Liquid Extraction".
- 5. Badger and McCabe, "Elements of Chemical Engineering", New York: McCraw-Hill Co., Inc., (1936).